PhsHW11

November 22, 2024



For $V_0(x,t)$:

$$V_0(x,t) = Re(e^{j\omega t}[V_f^+e^{-j\beta x} + V_f^-e^{+j\beta x}])$$

where -L \times 0

$$V_1(x,t) = Re(e^{j\omega t}[V_t^+e^{-j\beta x}])$$

where x 0

$$I_{0}(x,t) = Re(e^{j\omega t}[\frac{V_{f}^{+}}{Z_{0}}e^{-j\beta x} - \frac{V_{f}^{-}}{Z_{0}}e^{+j\beta x}])$$

$$I_1(x,t)=Re(e^{j\omega t}[\frac{V_t^+}{Z_1}e^{-j\beta x}])$$

At x = -L:

$$V_0(-L,t) = V_{in}(t) = Re(V_s e^{j\omega t})$$

$$Re(e^{j\omega t}[V_f^+e^{j\beta L}+V_f^-e^{-j\beta L}])=Re(V_se^{j\omega t})$$

Boundary conditions:

At x = -L:

$$V_f^+ e^{j\beta L} + V_f^- e^{-j\beta L} = V_s$$

At x = 0 (voltage continuity):

$$V_f^+ + V_f^- = V_t^+$$

At x = 0 (current continuity):

$$\frac{V_f^+}{Z_0} - \frac{V_f^-}{Z_0} = \frac{V_t^+}{Z_1}$$

With reflection coefficient:

$$\rho=\frac{Z_1-Z_0}{Z_1+Z_0}$$

$$V_f^+(e^{j\beta L} + \rho e^{-j\beta L}) = V_s$$

Therefore:

$$V_f^+ = \frac{V_s}{e^{j\beta L} + \rho e^{-j\beta L}}$$

Since $V_f^- = \rho V_f^+$:

$$V_f^- = \frac{\rho V_s}{e^{j\beta L} + \rho e^{-j\beta L}}$$

And from voltage continuity at x = 0:

$$V_t^+ = V_f^+ + V_f^- = V_f^+ (1+\rho)$$

Therefore:

$$V_t^+ = \frac{V_s(1+\rho)}{e^{j\beta L} + \rho e^{-j\beta L}}$$

[2]: # Question 1.2

We know:

$$V_f^+ = \frac{V_s}{e^{j\beta_0 L} + \rho e^{-j\beta_0 L}}$$

$$V_f^- = \frac{\rho V_s}{e^{j\beta_0 L} + \rho e^{-j\beta_0 L}}$$

where = 1/2

Substituting these in:

$$\begin{split} V_0(x,0) &= Re[V_s(\frac{e^{-j\beta_0x}}{e^{j\beta_0L} + \frac{1}{2}e^{-j\beta_0L}} + \frac{\frac{1}{2}e^{+j\beta_0x}}{e^{j\beta_0L} + \frac{1}{2}e^{-j\beta_0L}})] \\ &= Re[V_s(\frac{e^{-j\beta_0x} + \frac{1}{2}e^{+j\beta_0x}}{e^{j\beta_0L} + \frac{1}{2}e^{-j\beta_0L}})] \end{split}$$

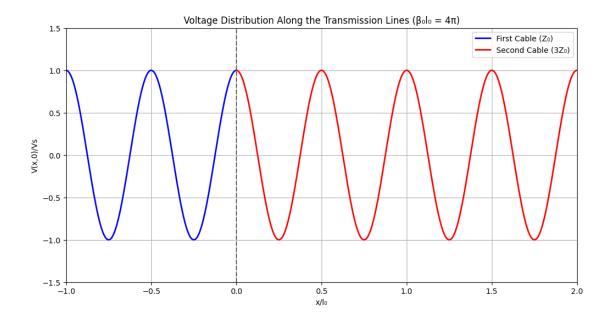
Similarly for second cable (x 0):

$$\begin{split} V_1(x,0) &= Re[V_t^+ e^{-j\beta_0 x}] \\ &= Re[V_s \frac{\frac{3}{2} e^{-j\beta_0 x}}{e^{j\beta_0 L} + \frac{1}{2} e^{-j\beta_0 L}}] \end{split}$$

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Since _0L = 4 : e^{j\beta_0L}=e^{-j\beta_0L}=1 Therefore: V_0(x,0)=Re[V_s(\frac{2}{3})(e^{-j\beta_0x}+\frac{1}{2}e^{+j\beta_0x})] V_1(x,0)=Re[V_se^{-j\beta_0x}] For -L _x _0: V_0(x,0)=V_s\cos(\beta_0x) For x _0:
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[3]: import numpy as np
    import matplotlib.pyplot as plt
    # Parameters
    Vs = 1.0
    beta0_10 = 4*np.pi # l = 4
    # For first cable (-L \ x \ 0)
    x1_10 = np.linspace(-1, 0, 500) # x/l from -1 to 0
    V1 = Vs * np.cos(beta0_10 * x1_10) # cos(4 x/l)
    # For second cable (0 x)
    x2_{10} = np.linspace(0, 2, 500) # x/l from 0 to 2
    V2 = Vs * np.cos(beta0_10 * x2_10) # cos(4 x/l)
    # Plotting
    plt.figure(figsize=(12, 6))
    plt.plot(x1_10, V1, 'blue', label='First Cable (Z)', linewidth=2)
    plt.plot(x2_10, V2, 'red', label='Second Cable (3Z)', linewidth=2)
    plt.axvline(x=0, color='black', linestyle='--', alpha=0.5) # marking x=0
    plt.grid(True)
    plt.xlabel('x/1')
    plt.ylabel('V(x,0)/Vs')
    plt.title('Voltage Distribution Along the Transmission Lines ( 1 = 4)')
    plt.legend()
    plt.ylim(-1.5, 1.5)
    plt.xlim(-1, 2)
    plt.show()
```

 $V_1(x,0) = V_{\varepsilon} \cos(\beta_0 x)$



[4]: # Question 1.3

Recall,

$$V_0(x) = V_f^+ e^{-j\beta_0 x} + V_f^- e^{+j\beta_0 x}$$

and
$$V_f^+ = \frac{2}{3}V_s \ V_f^- = \frac{1}{3}V_s$$

So:

$$\begin{split} V_0(x) &= \frac{2}{3} V_s e^{-j\beta_0 x} + \frac{1}{3} V_s e^{+j\beta_0 x} \\ &= V_s [\frac{2}{3} (\cos(\beta_0 x) - j \sin(\beta_0 x)) + \frac{1}{3} (\cos(\beta_0 x) + j \sin(\beta_0 x))] \\ &= V_s [\cos(\beta_0 x) - j \frac{1}{3} \sin(\beta_0 x)] \end{split}$$

For polar form $|V_0(x)|e^{j\phi}$:

$$\begin{split} |V_0(x)| &= V_s \sqrt{\cos^2(\beta_0 x) + \tfrac{1}{9} \sin^2(\beta_0 x)} \\ \phi &= -\tan^{-1}(\tfrac{\frac{1}{3} \sin(\beta_0 x)}{\cos(\beta_0 x)}) \end{split}$$

[5]: ## Question 2.1

- 1) KCL at V node (first capacitor):
- Current entering: I
- Current leaving: I

 \bullet Current through capacitor: C dV /dt

$$C\frac{dV_1}{dt} = I_1 - I_2$$

In state variables (C=1):

$$\dot{x_3} = x_1 - x_2$$

2) KVL around first L loop:

$$L\frac{dI_1}{dt} = V_0 - V_1$$

In state variables (L=1):

$$\dot{x_1} = \cos(t) - x_3$$

3) KVL around second L loop: Since V = I R and R=1:

$$L\frac{dI_2}{dt} = V_1 - I_2$$

In state variables (L=1):

$$\dot{x_2} = x_3 - x_2$$

This gives us:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 0 & -1 \\ 0 & -1 & 1 \\ 1 & -1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} \cos(t)$$

[6]: ## Question 2.2

Given:

$$\dot{X} = AX + BU$$

where:

$$A = \begin{bmatrix} 0 & 0 & -1 \\ 0 & -1 & 1 \\ 1 & -1 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}, \quad U = \begin{bmatrix} \cos(t) \\ 0 \\ 0 \end{bmatrix}$$

0.0.1 (1) Steady-State Assumptions

Since $U(t) = \begin{bmatrix} \cos(t) \\ 0 \\ 0 \end{bmatrix}$, we write it in complex exponential form using Euler's formula:

$$U(t) = \operatorname{Re}\left(\begin{bmatrix} e^{j\omega t} \\ 0 \\ 0 \end{bmatrix}\right)$$

where $\omega = 1$.

Assume the steady-state solution is:

$$X(t) = \operatorname{Re}\left(\begin{bmatrix} X_1 \\ X_2 \\ X_3 \end{bmatrix} e^{j\omega t}\right)$$

where $\begin{bmatrix} X_1 \\ X_2 \\ X_3 \end{bmatrix}$ are the phasors for the steady-state solution.

0.0.2 (2) Frequency-Domain Representation

From the derivation, we have:

$$(j\omega I-A)\begin{bmatrix}X_1\\X_2\\X_3\end{bmatrix}=B\begin{bmatrix}1\\0\\0\end{bmatrix}$$

Substituting $\omega = 1$, we get:

$$(jI - A) \begin{bmatrix} X_1 \\ X_2 \\ X_3 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$$

0.0.3 (3) Matrix Substitution

$$jI - A = \begin{bmatrix} j & 0 & 1 \\ 0 & j+1 & -1 \\ -1 & 1 & j \end{bmatrix}$$

Solving the linear system of equations:

$$\begin{bmatrix} j & 0 & 1 \\ 0 & j+1 & -1 \\ -1 & 1 & j \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \\ X_3 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$$

0.0.4 (4) Solve the Linear System

- 1. From the first equation: $jX_1 + X_3 = 1$
- 2. From the second equation: $(j+1)X_2 X_3 = 0$
- 3. From the third equation: $-X_1 + X_2 + jX_3 = 0$

Solving this system, we get:

$$X_1 = 1$$

$$X_2 = \frac{1+j}{j+1}$$

$$X_3 = 1-j$$

0.0.5 (5) Convert to Time Domain

The steady-state solution is the real part of $\mathbf{X}e^{j\omega t}$, where:

$$\mathbf{X} = \begin{bmatrix} X_1 \\ X_2 \\ X_3 \end{bmatrix} = \begin{bmatrix} 1 \\ \frac{1+j}{j+1} \\ 1-j \end{bmatrix}$$

$$\mathbf{X}_1(t)$$
:

$$X_1(t) = \operatorname{Re}(X_1 e^{j\omega t}) = \operatorname{Re}(1 \cdot e^{j\omega t}) = \cos(\omega t) = \cos(t)$$

$$\mathbf{X}_2(t)$$
:

$$X_2(t) = \operatorname{Re}\left(\frac{1+j}{j+1}e^{j\omega t}\right)$$

Simplifying the fraction:

$$\frac{1+j}{j+1} = \frac{(1+j)(j-1)}{(j+1)(j-1)} = \frac{2j}{-2} = -j$$

Therefore:

$$X_2(t) = \operatorname{Re}(-je^{j\omega t}) = \operatorname{Re}(-j(\cos(\omega t) + j\sin(\omega t))) = \operatorname{Re}(-\sin(\omega t) - j\cos(\omega t)) = \sin(t)$$

$$\mathbf{X}_3(t)$$
:

$$X_3(t) = \operatorname{Re}((1-j)e^{j\omega t}) = \operatorname{Re}((1-j)(\cos(\omega t) + j\sin(\omega t)))$$

Expanding:

$$X_3(t) = \text{Re}(\cos(\omega t) - j\cos(\omega t) + j\sin(\omega t) + \sin(\omega t)) = \cos(t) + \sin(t)$$

Thus, the steady-state solutions are:

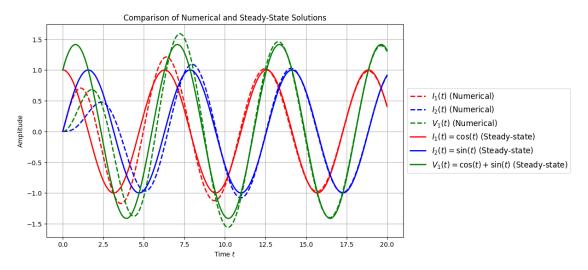
$$\begin{split} I_1(t) &= \mathbf{X}_1(t) = \cos(t) \\ I_2(t) &= \mathbf{X}_2(t) = \sin(t) \\ V_1(t) &= \mathbf{X}_3(t) = \cos(t) + \sin(t) \end{split}$$

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# Input vector
    u = np.array([np.cos(t), 0, 0])
    # Compute the derivatives
    dxdt = A @ np.array([x1, x2, x3]) + u
    return dxdt
# Initial conditions: x1(0), x2(0), x3(0)
initial_conditions = [0, 0, 0]
# Time span for the solution (e.g., from t=0 to t=10)
t_{span} = (0, 20)
# Solve the system using solve_ivp
sol = solve_ivp(system, t_span, initial_conditions, t_eval=np.linspace(0, 20, __
→1000))
# Steady-state solutions
t = np.linspace(0, 20, 1000)
I1 steady = np.cos(t) # I1(t) = cos(t)
I2 steady = np.sin(t) # I2(t) = sin(t)
V1_steady = np.cos(t) + np.sin(t) # V1(t) = cos(t) + sin(t)
# Plot the solutions
plt.figure(figsize=(10, 6))
# Numerical solutions
plt.plot(sol.t, sol.y[0], label=r'$I_1(t)$ (Numerical)', color='r', u
 ⇒linestyle='--', linewidth=2)
plt.plot(sol.t, sol.y[1], label=r'$I_2(t)$ (Numerical)', color='b', __
 ⇔linestyle='--', linewidth=2)
plt.plot(sol.t, sol.y[2], label=r'$V_1(t)$ (Numerical)', color='g', __
 ⇒linestyle='--', linewidth=2)
# Steady-state solutions
plt.plot(t, I1_steady, label=r'$I_1(t) = \cos(t)$ (Steady-state)', color='r', __
 ⇒linewidth=2)
plt.plot(t, I2_steady, label=r'$I_2(t) = \sin(t)$ (Steady-state)', color='b', __
 →linewidth=2)
plt.plot(t, V1\_steady, label=r'$V_1(t) = \cos(t) + \sin(t)$ (Steady-state)', \( \)

color='g', linewidth=2)

plt.title('Comparison of Numerical and Steady-State Solutions')
plt.xlabel('Time $t$')
plt.ylabel('Amplitude')
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plt.legend(loc="center left", bbox_to_anchor=(1, 0.5), fontsize=12)
plt.grid(True)
plt.show()
```



0.1 Comment

The transient state of the system converges to the steady-state solution after some time.