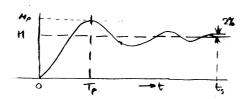
## **LECTURE 8 – PERFORMANCE PARAMETERS**

One often used measure of how well a system responds to driving signals is to look at the response to a unit step input in terms of the shape of the output.

Here are the parameters that will be looked at.



 $T_p$  - the time to the first peak

 $M_{\%}$  - the maximum percentage overshot  $M_{\%} = \frac{100(M_P - M)}{M}$ 

 $t_s$  - the settling time for the output to get within 2% of its final value.

These parameters only apply to a system that is essentially second order (perhaps with smaller higher order effects) and is UNDERDAMPED.

Hence we are looking at

$$\begin{split} y(t) &= \mathcal{L}^{-1}\{\frac{1}{s} \cdot \frac{K}{s^2 + 2\xi\omega_n s + \omega_n^2}\} \\ &= \frac{K}{\omega_n^2} \left[ 1 - \frac{1}{\sqrt{1 - \xi^2}} \cdot e^{-\xi\omega_n t} \cdot sin(\omega_n \sqrt{1 - \xi^2} t + \varphi) \right] \end{split}$$
 With  $\varphi = tan^{-1}(\frac{\sqrt{1 - \xi^2}}{\xi})$ 

ANALYSIS FOR  $T_p$ 

To find  $T_p$  look for  $\dot{y}(t) = 0$ 

First rewrite y(t) as:

$$y(t) = \frac{\kappa}{\omega_n^2} \left[ 1 - e^{-\xi \omega t} \left( \cos \omega_n \sqrt{1 - \xi^2} t + \frac{\xi}{\sqrt{1 - \xi^2}} \sin(\omega_n \sqrt{1 - \xi^2} t) \right) \right]$$

Then differentiate it and equate  $\dot{y}(t)$  with zero making  $t = T_P$ .

$$\sin(\omega_n\sqrt{1-\xi^2}T_p)=0$$

$$\omega_n \sqrt{1-\xi^2} \cdot T_p = n\pi$$
  $n=1,2...$  and reselect  $n=1$  for the first rise.

$$\therefore T_p = \frac{\pi}{\omega_n \sqrt{1 - \xi^2}}$$

ANALYSIS FOR  $M_{\%}$ 

 $\mathit{M}_\mathit{P}$  is obtained by back substitution of  $\mathit{T}_\mathit{p}$  in  $\mathit{y}(t)$ 

$$M_{p} = \frac{K}{\omega_{n}^{2}} \left[ 1 + \frac{1}{\omega_{n}\sqrt{1-\xi^{2}}} \cdot e^{\frac{-\xi\pi}{\sqrt{1-\xi^{2}}}} \cdot sin(\pi - \varphi) \right]$$

But  $\varphi = \sin^{-1}\sqrt{1 - \xi^2}$ 

$$M_p = \frac{K}{\omega_n^2} \left[ 1 + \frac{1}{\omega_n \sqrt{1 - \xi^2}} \cdot e^{\frac{-\xi \pi}{\sqrt{1 - \xi^2}}} \cdot \sin(\sin^{-1}\omega_n \sqrt{1 - \xi^2}) \right]$$

Since  $M = \frac{K}{\omega_n^2}$ 

and 
$$M_{\%} = \frac{M_p - M}{M} \times 100 = \frac{K}{\omega_n^2} \left[ \frac{\frac{-\xi \pi}{\sqrt{1 - \xi^2}}}{\frac{K}{\omega_n^2}} \right] \cdot 100$$

$$\therefore M_{\%} = 100e^{\frac{-\xi\pi}{\sqrt{1-\xi^2}}}$$

ANALYSIS FOR  $t_s$ 

We chose a bandwidth within which the ripple is regarded as insignificant. 2% is often used. This means that the factor in y(t) that multiplies the sin (the amplitude) must be reduced to that value (0.02) at the time of interest.

$$\therefore \frac{1}{\sqrt{1-\xi^2}} e^{-\xi\omega_n t_s} = \chi(\equiv 0.02)$$

Take logs to get  $t_s = \frac{1}{\xi \omega_n} \cdot \ln \left[ \frac{1}{x\sqrt{1-\xi^2}} \right]$ 

Expand the log to get  $t_S = \frac{1}{\xi \omega_n} \left[ \ln \frac{1}{x} + \frac{1}{2} \ln \frac{1}{(1-\xi^2)} \right]$ 

If we recognise that the parameters of interest are usually associated with low damping where  $\xi \leq 0.3$ , we see that  $\frac{1}{2} \ln \frac{1}{(1-\xi^2)} \rightarrow \text{very small or zero}$ .

$$\therefore t_s \simeq \frac{1}{\xi \omega_n} \ln \left( \frac{1}{x} \right)$$
 and if we make  $x = 0.02$ 

$$\therefore t_S \simeq \frac{3.91}{\xi \omega_n}$$

## **EXAMPLE**

If a system transfer function is  $G(s) = \frac{1}{0.01s^2 + 0.05s + 1}$  and a unit step is applied to the input, find the three performance parameters:  $T_p$ ,  $M_{\%}$  and  $t_s$ .

Rewrite

$$G(s) = \frac{100}{s^2 + 5s + 100}$$

Find the characteristic equation roots from

$$s^2 + 5s + 100 = 0$$
  $\therefore s = -2.5 \pm i\sqrt{93.75}$ 

Therefore the system is UNDERDAMPED and appropriate for analysis.

We can also equate  $2\xi \omega_n = 5$ ,  $\omega_n^2 = 100$  :  $\omega_n = 10$ 

$$\therefore \xi = \frac{5}{2.10} = 0.25$$

$$\therefore T_p = \frac{\pi}{\omega_n \sqrt{1 - \xi^2}} = \frac{3.14}{10\sqrt{1 - 0.25^2}} = 0.324 \text{ seconds}$$

$$\therefore M_{\%} = 100e^{\frac{-\xi\pi}{\sqrt{1-\xi^2}}} = 100e^{\frac{-0.25\cdot\pi}{\sqrt{1-0.25^2}}} = 44.4\%$$

$$t_s = \frac{3.91}{\xi \omega_n} = \frac{3.91}{0.25 \cdot 10} = 1.56$$
 seconds

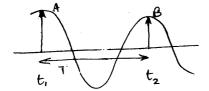
The student should now try this exercise with

$$G(s) = \frac{1/16}{\frac{s^2}{16} + \frac{10}{16}s + 1}$$
 and be careful.

## THE LOGARITHMIC DECREMENT

If we can capture just a few oscillations of the output of a system that has been perturbed in some way, we can still find the damping coefficient.

Consider the waveform:



We recall the transient is of the form:

$$\frac{K}{\omega_n^2\sqrt{1-\xi^2}} \cdot e^{-\xi\omega_n t} \cdot sin(\omega_n\sqrt{1-\xi^2}t)$$

If we assume A & B are measured at the peak of the waveform, then

$$A \propto e^{-\xi \omega_n t_1}$$
 and  $B \propto e^{-\xi \omega_n t_2}$ 

The ratio 
$$\frac{A}{B}=\frac{e^{-\xi\omega_nt_1}}{e^{-\xi\omega_nt_2}}=e^{-\xi\omega_n(t_1-t_2)}\equiv R$$

R can be measured.  $T=(t_2-t_1)$  can be measured.

Take logs to get  $-\xi \omega_n (t_1-t_2) = \ln R$ 

$$\therefore \xi = \frac{1}{\omega_n T} \ln R$$

But T is the period of waveform  $= \frac{2\pi}{\omega_n\sqrt{1-\xi^2}} \equiv T$ 

If we assume  $\xi \ll 1$  , then  $T \simeq \frac{2\pi}{\omega_n}$ 

$$\therefore \xi \simeq \frac{1}{\omega_n} \cdot \frac{\omega_n}{2\pi} \ln R = \frac{1}{2\pi} \cdot \ln R$$

Hence just by measuring R above we can get  $\xi$ .

## **EXAMPLE**

A technician measures A=2.4cm and B=1.9cm on a scope for successive peaks of a waveform output. What is the damping coeficient in the system?

$$R = \frac{2.4}{1.9} = 1.263$$
  $\therefore \xi = \frac{1}{2\pi} \ln 1.263 = \frac{0.233}{6.283} = 0.037$