

Otto Cycle

This is the last part (which was the first part in prior years)

- Between $1 \rightarrow 2$ we have

$$\Delta u = \cancel{Q} + W_{12}$$

So

see next item

$$W_{12} = C_v \Delta T_{12} = C_v T_2 \left(1 - \frac{1}{r^{\gamma-1}}\right)$$

- Now $1 \rightarrow 2$ is adiabatic

$$T_2 = T_1 \left(\frac{V_1}{V_2}\right)^{\gamma-1}$$

$$\text{So } \Delta T_{12} = T_1 (r^{\gamma-1} - 1)$$

$$\left(\frac{T_2}{T_1}\right) = r^{\gamma-1} \quad \text{so}$$

- Then for $2 \rightarrow 3$

$$C_v \Delta T_{23} = \cancel{Q} + \cancel{W}$$

$$\Delta T_{12} = T_2 \left(1 - \frac{1}{r^{\gamma-1}}\right)$$

$$\Delta T_{23} = \frac{Q_{in}}{C_v}$$

- Then similarly for $3 \rightarrow 4$

$$\Delta u = W$$

$$T_4 = T_3 \left(\frac{V_3}{V_4}\right)^{\gamma-1} = T_3 \frac{1}{r^{\gamma-1}}$$

$$\Delta u = C_v (T_4 - T_3)$$

$$\Delta W = -C_v T_3 \left(1 - \frac{1}{r^{\gamma-1}}\right) = W_{34}$$

So

$$= Q_{in}$$

$$W_{net} = W_{34} + W_{12} = -C_V (T_3 - T_2) \left(1 - \frac{1}{r^{\gamma-1}}\right)$$

Finally

$$\eta = -\frac{W_{net}}{Q_{in}} = + \frac{Q_{in}}{Q_{in}} \left(1 - \frac{1}{r^{\gamma-1}}\right)$$

$$\boxed{\eta = 1 - \frac{1}{r^{\gamma-1}}}$$

b) For 1 mol

$$pV = Nk_B T$$

$$V = \frac{N k_B T}{p} = \frac{RT}{p} = \frac{8.32 \frac{J}{mol \cdot K} \cdot 300 K}{10^5 N/m^2} = 25.2$$

Now the volume of the cylinder is 2.5L
So

$$\frac{2.5 L}{25 L} = \frac{n_{ml}}{1 \text{ mol}} \Rightarrow \boxed{n_{ml} = 0.1}$$

c) We use

1 → 2

$$T_f = T_i \left(\frac{V_i}{V_f} \right)^{\gamma-1}$$

$$P_f = P_i \left(\frac{V_i}{V_f} \right)^{\gamma}$$

$$T_2 = T_1 r^{\gamma-1}$$

$$P_2 = P_1 r^{\gamma}$$

$$V_2 = V_1 / r$$

$$\underline{T_2 = 689 \text{ } ^\circ\text{K}}$$

$$\underline{P_2 = 18.4 \text{ b}}$$

$$\underline{V_2 = 0.3 \text{ L}}$$

$$\Delta U_{12} = W_{1 \rightarrow 2} = C_v (T_f - T_i) = C_v T_i (r^{\gamma-1} - 1)$$

Now $C_v T_i = U_i$, for 1 mol we have

$$C_v^{1\text{mol}} = \frac{5R}{2}$$

$$C_v^{0.1\text{mol}} = 0.1 \times \frac{5R}{2} = 0.832 \frac{\text{J}}{^\circ\text{K}} \times \frac{5}{2} = 2.08 \frac{\text{J}}{^\circ\text{K}}$$

$$\underline{\Delta U_{12} = \Delta W_{12} = 810 \text{ J}, \quad Q = 0}$$

2 → 3

Now

$$\underline{\Delta U_{23} = Q_{in} + \overset{0}{W} = 2,200 \text{ J} \quad W = 0}$$

$$C_v (T_3 - T_2) = Q_{in}$$

$$Q_{in} = 0.1 \text{ mol} \times \frac{22000 \text{ J}}{\text{mol}} = 2,200 \text{ J}$$

$$\underline{T_3 = T_2 + \frac{Q_{in}}{C_v} = 1747 \text{ } ^\circ\text{K}}$$

$$P_3 = \frac{Nk_B T}{V}$$

$$\frac{P_3}{P_2} = \frac{T_3}{T_2}$$

$$\underline{P_3} = P_2 \frac{T_3}{T_2} = \underline{46,5 \text{ b}}$$

$$\underline{V_3 = 0,3 \text{ L}}$$

3 → 4

$$\Delta U = \cancel{Q} + W$$

$$\Delta U = C_v (T_f - T_i)$$

$$= -C_v T_i \left(1 - \frac{1}{r^{\gamma-1}}\right)$$

$$\underline{W_{34} = \Delta U = -2052 \text{ J}}$$

4 → 1

$$\Delta U = Q + \cancel{W}$$

$$C_v (T_1 - T_4) = Q$$

$$\underline{\Delta U = Q = -958 \text{ J}}$$

$$W = 0$$

Adiabatic

$$T_f V_f^{\gamma-1} = T_i V_i^{\gamma-1}$$

$$T_4 = T_3 \frac{1}{r^{\gamma-1}}$$

$$\underline{T_4 = 760^\circ \text{ K}}$$

$$\underline{\frac{P_4}{P_1} = \frac{T_4}{T_1} = 6,33 \text{ b}}$$

$$\underline{V_4 = 2,5 \text{ L}}$$

As a quick check we note

$$W_{\text{net}} = W_{12} + W_{34} = -1242.5$$

$$Q_{\text{in}} = 2200.5$$

So

$$\eta = \frac{|W_{\text{net}}|}{Q} = 0.56$$

which should be compared
with $1 - \frac{1}{r^{\gamma-1}} = 1 - \frac{1}{8^{\gamma-1}} \approx 0.56$

Manipulating Taylor Series

$$a) \quad \frac{1}{1+x} = 1 - x + x^2 - x^3 + \dots$$

This follows from the geometric series
 $1/(1-u) = 1 + u + u^2 + \dots$ with $u = -x$

Integrating

$$\int_0^x \frac{dx'}{1+x'} = \log(1+x) = x - \frac{x^2}{2} + \frac{x^3}{3} - \frac{x^4}{4} + \dots$$

b)

c) For x large we have $e^{-x} \ll 1$

$$\frac{1}{e^x - 1} = \frac{e^{-x}}{1 - e^{-x}}$$

call $u = e^{-x} \ll 1$

$$\frac{1}{e^x - 1} = \frac{u}{(1-u)} = u (1 + u + u^2 + \dots)$$

$$\boxed{\frac{1}{e^x - 1} = e^{-x} (1 + e^{-x} + e^{-2x} + O(e^{-3x}))}$$

$$d) \frac{1}{e^x - 1}$$

we expand $e^x = 1 + x + \frac{x^2}{2} + \frac{x^3}{6}$

$$\frac{1}{e^x - 1} \approx \frac{1}{x + x^2/2 + x^3/6} = \frac{1}{x} \frac{1}{(1 + x/2 + x^2/6 + O(x^3))}$$

calling, $u = x/2 + x^2/6$, we have

$$\frac{1}{e^x - 1} \approx \frac{1}{x} \left(\frac{1}{1+u} + O(x^3) \right)$$

$$\approx \frac{1}{x} (1 - u + u^2 + O(x^3))$$

$$\approx \frac{1}{x} \left(1 - \left(\frac{x}{2} + \frac{x^2}{6} \right) + \left(\frac{x^2}{4} \right) + O(x^3) \right)$$

$$\frac{1}{e^x - 1} \approx \frac{1}{x} \left(1 - \frac{x}{2} + \frac{x^2}{12} \right) + O(x^2)$$

$$e) \frac{1}{e^{-x} + 1} \approx 1 - e^{-x} + e^{-2x} \quad \text{set } u = e^{-x}$$

$$f) \log(1 - e^{-x}) \approx \log(1 - (1 - x + \frac{x^2}{2} - \frac{x^3}{6}))$$

$$\approx \log x (1 - \frac{x}{2} + \frac{x^2}{6}) = \log x + \log(1 - \frac{x}{2} + \frac{x^2}{6})$$

So

$$\log(1 - e^{-x}) = \log(x) + \log\left(1 - \overbrace{\frac{x}{2} + \frac{x^2}{6}}^{\text{call it } u}\right) + O(x^3)$$

Setting $u = -\frac{x}{2} + \frac{x^2}{6}$ we have

$$\log(1 + u) = u - \frac{u^2}{2} + O(u^3) \quad \text{with } x \text{ of order } u$$

So

$$\log(1 - e^{-x}) \approx \log(x) + \left(-\frac{x}{2} + \frac{x^2}{6}\right) - \frac{1}{2}\left(-\frac{x}{2}\right)^2 + O(x^3)$$

$$\log(1 - e^{-x}) \approx \log x - \frac{x}{2} + \frac{x^2}{24} + O(x^3)$$

Energy of SHO

a) We have

$$Z = \frac{1}{1 - e^{-\beta \hbar \omega_0}}$$

Then

$$\langle E \rangle = - \frac{\partial}{\partial \beta} \log Z = + \frac{\partial}{\partial \beta} \log (1 - e^{-\beta \hbar \omega_0})$$

$$= \frac{1}{1 - e^{-\beta \hbar \omega_0}} e^{-\beta \hbar \omega_0} \hbar \omega_0$$

$$\boxed{\langle E \rangle = \frac{\hbar \omega_0}{e^{\beta \hbar \omega_0} - 1}}$$

b) Then

$$\frac{\langle E \rangle}{\hbar \omega_0} = \frac{1}{e^{\hbar \omega_0 / k_B T} - 1} = \langle n \rangle$$

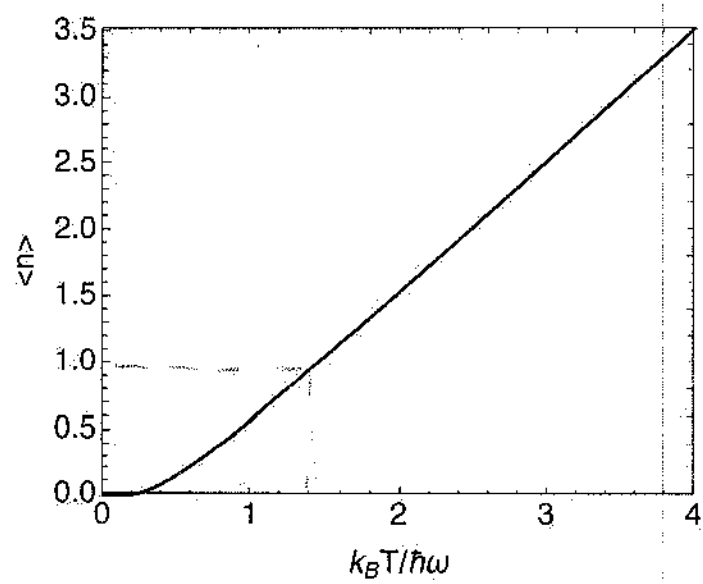
Then



Then from graph

$$\langle n \rangle = 1 \quad \text{when}$$

$$k_B T / \hbar \omega_0 = 1.45$$



or

$$k_B T = 1.45 \hbar \omega_0$$

(c) Then a nice plot of $\langle E \rangle$ is given in the problem statement.

(d) Using the series of problem 1

with $x \equiv \hbar \omega_0 / k_B T$

at low temperature $k_B T \ll \hbar \omega_0$ then $x \gg 1$,
and

$$\frac{1}{e^x - 1} = \frac{e^{-x}}{1 - e^{-x}} \approx e^{-x} (1 + e^{-x} + \dots)$$

And

$$\langle E \rangle = \hbar \omega_0 e^{-\beta \hbar \omega_0} (1 + e^{-\beta \hbar \omega_0} + \dots)$$

At high temperature $x \ll 1$

$$\frac{1}{e^x - 1} \approx \frac{1}{x} - \frac{1}{2}$$

$$\langle E \rangle = \hbar \omega_0 \left(\frac{k_B T}{\hbar \omega_0} - \frac{1}{2} \right) \approx k_B T \left(1 - \frac{\hbar \omega_0}{2 k_B T} \right)$$

e) At high temperature the number of quanta $\langle n \rangle$ is very large. In this regime $\langle n \rangle \gg 1$, quantum mechanics becomes continuous, $\frac{\Delta E}{E} \ll 1$, and it approaches classical mechanics.

This is the Bohr correspondence principle

f) We have

$$i) \quad U = N \left[\frac{5}{2} kT + \frac{\hbar \omega_0}{e^{\beta \hbar \omega_0} - 1} \right]$$

this is $f_0(T)$

Then

$$ii) \quad C_V = \left(\frac{dU}{dT} \right)_V = N \left[\frac{5}{2} k + \frac{-\hbar \omega_0 e^{\beta \hbar \omega_0}}{(e^{\beta \hbar \omega_0} - 1)^2} \hbar \omega_0 \frac{2}{dT} \frac{1}{kT} \right]$$

$$= N \left[\frac{5}{2} k + \frac{(\beta \hbar \omega_0)^2 e^{\beta \hbar \omega_0}}{(e^{\beta \hbar \omega_0} - 1)} k \right]$$

$$C_V = Nk \left[\frac{5}{2} + \frac{(\beta \hbar \omega_0)^2 e^{\beta \hbar \omega_0}}{(e^{\beta \hbar \omega_0} - 1)^2} \right]$$

So

$$C_p = C_v + Nk_B$$

$$C_p = Nk_B \left[\frac{7}{2} + \frac{(\beta \hbar \omega_0)^2}{(e^{\beta \hbar \omega_0} - 1)^2} \right]$$

iii) So we see that the model nicely captures the transition from $C_p = \frac{7}{2} = 3.5$ to $\frac{9}{2} = 4.5$

but misses the transition to $\frac{5}{2}$ at low temperatures