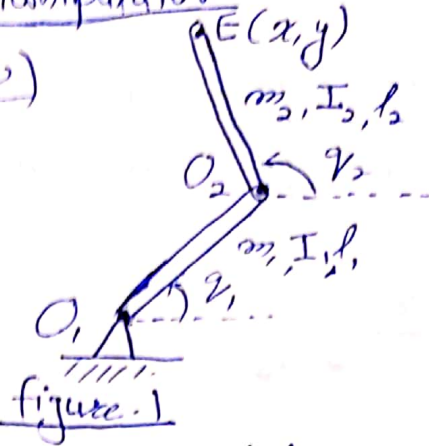


2R Manipulator -  
(E/b/w)



E - end effector

$(x, y)$  - end effector position

$(q_1, q_2)$  - joint angles

Note: absolute angles  
assume origin at  $O_1$ .

Let us assume that motors are connected to both joints  $O_1$  &  $O_2$ . and we have the ability to control either torques  $\tau_1$  and  $\tau_2$  applied at these joints or control the angles  $q_1$  and  $q_2$ .

Task-1 (T1) - Given arbitrary trajectory of end effector (given  $x, y$  as functions of time) make the robot follow this trajectory.

Using figure.1

$$x = l_1 \cos q_1 + l_2 \cos q_2$$

$$y = l_1 \sin q_1 + l_2 \sin q_2$$

or using simplified notations

$$\left. \begin{aligned} x &= l_1 c q_1 + l_2 c q_2 \\ y &= l_1 s q_1 + l_2 s q_2 \end{aligned} \right\} \text{--- (1)}$$

Differentiating (1), we get

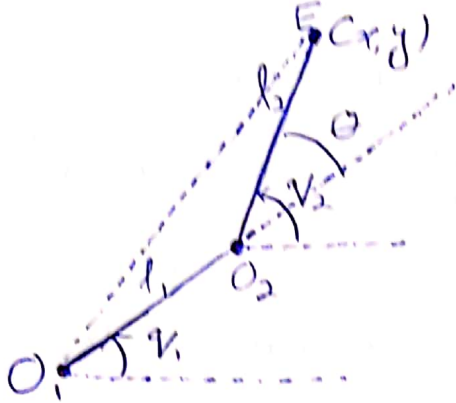
$$\dot{x} = -l_1 s q_1 \cdot \dot{q}_1 - l_2 s q_2 \cdot \dot{q}_2$$

$$\dot{y} = l_1 c q_1 \cdot \dot{q}_1 + l_2 c q_2 \cdot \dot{q}_2$$

$\Rightarrow$  End-effector velocity

$$\begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} -l_1 s q_1 & -l_2 s q_2 \\ l_1 c q_1 & l_2 c q_2 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} \text{--- (2)}$$

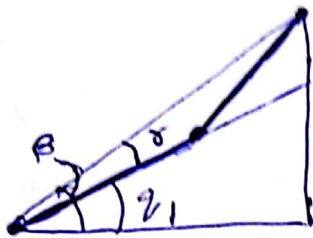
We could also need the reverse relationships. Given  $x, y$ , we need to be able to solve for  $\theta_1$  and  $\theta_2$  using (1).



Cosine rule using  $\triangle O_1 O_2 E$   
+ switching to the acute angle

$$\theta = \cos^{-1} \left( \frac{x^2 + y^2 - l_1^2 - l_2^2}{2 l_1 l_2} \right)$$

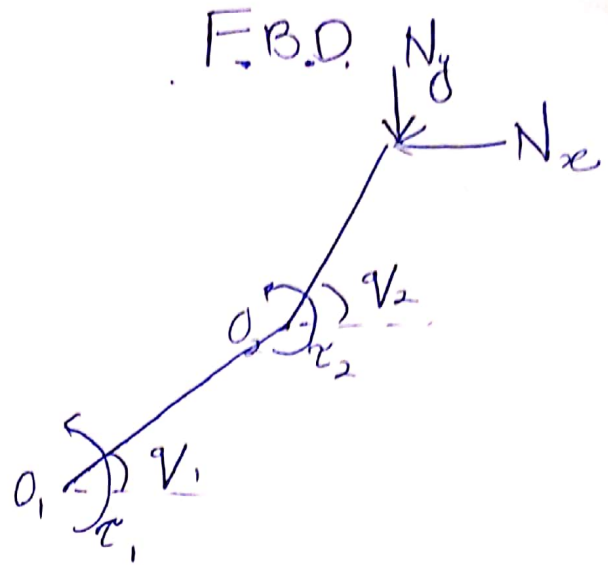
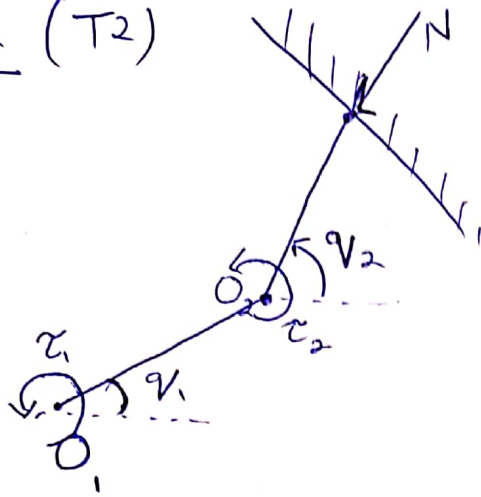
$$\theta_1 = \tan^{-1} \left( \frac{y}{x} \right) - \tan^{-1} \left( \frac{l_2 \sin \theta}{l_1 + l_2 \cos \theta} \right) \quad (3)$$



$$\theta_2 = \theta + \theta_1$$

By rotating motors by  $\theta_1$  and  $\theta_2$  respectively, the manipulator can reach to any point  $(x, y)$  of a given trajectory.

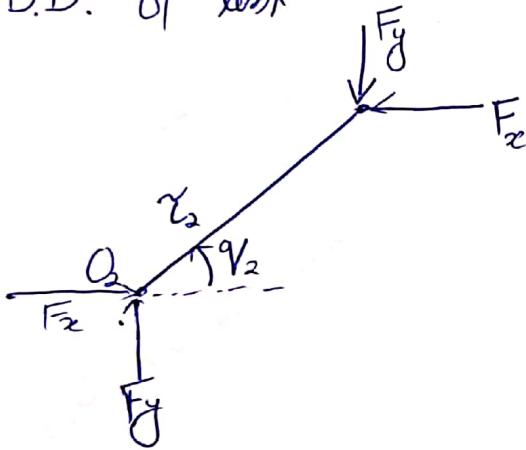
## Task 2 (T2)



Static equilibrium

$$\Rightarrow \sum M_{O_1} = 0 \quad \& \quad \sum M_{O_2} = 0$$

F.B.D. of link 2

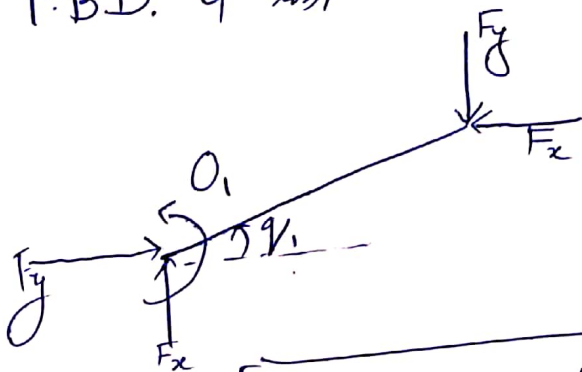


Ignore gravity

$$\sum M_{O_2} = 0$$

$$\Rightarrow F_y l_2 \cos \theta_2 - F_x l_2 \sin \theta_2 = \tau_2$$

F.B.D. of link 1



$$\sum M_{O_1} = 0$$

$$\Rightarrow F_y l_1 \cos \theta_1 - F_x l_1 \sin \theta_1 = \tau_1$$

$$\therefore \begin{cases} F_y l_1 \cos \theta_1 - F_x l_1 \sin \theta_1 = \tau_1 \\ F_y l_2 \cos \theta_2 - F_x l_2 \sin \theta_2 = \tau_2 \end{cases} \quad (4)$$

$\tau_1$  and  $\tau_2$  must be applied by the motors respectively to balance the wall reaction forces.

### Task-3 Lagrangian's equations -

$$\text{Lagrangian: } \mathcal{L} = K - V$$

K.E                  P.E

$$\boxed{\frac{d}{dt} \left( \frac{\partial \mathcal{L}}{\partial \dot{q}_i} \right) - \frac{\partial \mathcal{L}}{\partial q_i} = Q_i'} \quad \text{--- (5)}$$

$Q_i'$  are generalized forces derived using principle of virtual work.

$$K = \underbrace{\frac{1}{2} \left( \frac{1}{3} m_1 l_1^2 \right) \dot{q}_1^2}_{\text{pure rotation about } O_1} + \underbrace{\frac{1}{2} m_2 v_{C_2}^2}_{\text{translation of } l_2} + \underbrace{\frac{1}{2} \left( \frac{1}{12} m_2 l_2^2 \right) \dot{q}_2^2}_{\text{rotation of } l_2 \text{ about C.G.}}$$

$$v_{C_2}^2 = (l_1 \dot{q}_1)^2 + \left( \frac{l_2}{2} \dot{q}_2 \right)^2 + 2l_1 \dot{q}_1 \frac{l_2}{2} \dot{q}_2 \cos(q_2 - q_1)$$

Let us bring back gravity

$$V = m_1 g \frac{l_1}{2} \sin q_2 + m_2 g \left( l_1 \sin q_1 + \frac{l_2}{2} \sin q_2 \right)$$

Using the above steps:

$$\frac{1}{3} m_1 l_1^2 \ddot{q}_1 + m_2 l_1^2 \ddot{q}_1 + \frac{m_2 l_1 l_2}{2} \ddot{q}_2 \cos(q_2 - q_1) - m_2 \frac{l_1 l_2}{2} \dot{q}_2 (\dot{q}_2 - \dot{q}_1) \sin(q_2 - q_1) + m_1 g \frac{l_1}{2} \cos q_2 + m_2 g l_1 \cos q_1 = \tau_1$$

$$\frac{1}{3} m_2 l_2^2 \ddot{q}_2 + m_2 \frac{l_2^2}{2} \ddot{q}_2 + \frac{m_2 l_1 l_2}{2} \ddot{q}_1 \cos(q_2 - q_1) - m_2 l_1 l_2 \dot{q}_1 (\dot{q}_2 - \dot{q}_1) \sin(q_2 - q_1) + m_2 g \frac{l_2}{2} \sin q_2 = \tau_2$$



Equation (4) is valid for any end effector  $F_x$  and  $F_y$  (Not just wall reaction)  
 $F_x = kx$   
 $F_y = ky$   
 (Spring forces)

from (1)  $\Rightarrow$

$$F_x = k(l_1 c q_1 + l_2 c q_2)$$

$$F_y = k(l_1 s q_1 + l_2 s q_2)$$

from (4)

$$k(l_1 s q_1 + l_2 s q_2) l_2 c q_2 - k(l_1 c q_1 + l_2 c q_2) l_2 s q_2 = \tau_{2s}$$

$$k(l_1 s q_1 + l_2 s q_2) l_1 c q_1 - k(l_1 c q_1 + l_2 c q_2) l_2 s q_2 = \tau_{1s}$$

If the motor torques are set to be  $\tau_1 + \tau_{1s}$  &  $\tau_2 + \tau_{2s}$  respectively, the manipulator ~~will~~ will behave like a spring.