C18110078 rakadiya Jaydeep

MEB39- Introduction to Robotics

Assignment @

Task@ show that columns of rotaton materine

-> Let's telke a base reforme XYZ

with origin at o.

-> Pis q vector demoting point p in xyz

P= (P1, P2, P3)

$$= \begin{bmatrix} P_1 \\ P_2 \\ P_3 \end{bmatrix}$$

= Now, for rotation trunsformation, it preserves the length of oxismat between two points.

=) so, we rotate the focusine with rotation matricisa, Ro. New distans vector donoting P FOIDT W. J. +. X14121,

A As disterace between two points will be program $\vec{P}, \vec{T} \vec{P}_i = (\vec{P}_0)^T (\vec{P}_0)$ P,TP = (ROPI) (ROPI) P, (I) P, = PT (ROTRO) PT - (B) 4 from (B), (554) = T4(0012)4 PO RO = I, so every rotestion moutaine satisfies this oclasion and they are orthogonal modèlces.

$$(R'_0)^T(R'_0) = T$$

$$\Rightarrow \det(R'_0)^2 = 1$$

$$\det(R'_0) = \pm 1$$

"handness" of coardmate system so, it has determinant value = 1.

del(Po) = 1

Show that P(sca)) RT = s(R(a)) - - from the properties of partition mulsise sca). b = ax B and P(axb) = PaxPb. Now, to prove R(sigs)PT = s(pa), vets take a vector \vec{p} , so, $(R(s(\vec{a}))R^{T}\vec{p}) = R(\vec{a} \times R^{T}\vec{p})$ = Pax x PRTP = RAXP R(S(97) PT. P = S(RQ). P from abone equication, P(sca)) PT = S(pa)TUSK 6 Work out various cardinate form and workout po using a composition to RRP of homogeneous tourstormation to RRP SCAR

$$R_0 = \begin{bmatrix} 0.001 - 400.0 & 0 \\ -45001 & 0.00.0 & 0 \end{bmatrix}$$

$$P_1^2 = \begin{bmatrix} 12 \\ 0 \\ 0 \end{bmatrix}$$

$$R_{1}^{2} = \begin{cases} \cos \alpha_{2} - \sin \alpha_{2} & 0 \\ + \sin \alpha_{2} & \cos \alpha_{2} & 0 \\ 0 & 0 \end{cases}$$

$$P_2^3 = \begin{bmatrix} 13 \\ 0 \\ 6 \end{bmatrix}$$

$$R_{q}^{3} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$P P_3 = \begin{bmatrix} 0 \\ 0 \\ 24+d \end{bmatrix}$$

$$P_{0} = \int L_{3}(\cos \alpha | \cos \alpha - \sin \alpha | \sin \alpha) + L_{2}\cos \alpha |$$

$$L_{3}(\cos \alpha | \sin \alpha | + \cos \alpha | \sin \alpha) + L_{2}\sin \alpha |$$

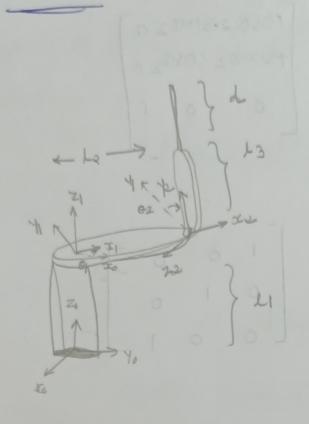
$$L_{1}(\cos \alpha | \sin \alpha | + \cos \alpha | \sin \alpha)) + L_{2}\sin \alpha |$$

$$L_{1}(\cos \alpha | \sin \alpha | + \cos \alpha | \sin \alpha)) + L_{2}\sin \alpha |$$

CALIFORNIA TO TOUR A TOURISM

21 + SIN (Class) (d + 13)

TUSK® Sternford type RRP configuration:

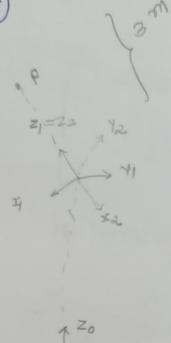


$$R_{1}^{2} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \varphi_{2} - \sin \varphi_{2} \end{bmatrix}$$

$$P0 = \begin{bmatrix} 12(0501 - \cos 025) \pi o_1(d+13) \\ 15|\pi o_1 + \cos 015|\pi o_2(d+13) \\ 1|+ 5|\pi (02)(d+13) \end{bmatrix}$$

$$Pd = \begin{bmatrix} \cos \alpha, -\sin \alpha, \sigma \\ \sin \alpha, \cos \alpha, \sigma \end{bmatrix}$$

$$P_1^2 = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$



Base station

$$P_1^2 = \begin{bmatrix} 0 \\ a \\ 3 \end{bmatrix}$$

$$P_0' = \begin{bmatrix} 0 \\ 0 \\ 10 \end{bmatrix}$$

$$R_0' = (R_0'), (R_0')_2$$

$$(R_0^{\dagger})_1 = \begin{bmatrix} 1 & 0 & 6 \\ 0 & 00300 & -50030 \end{bmatrix}$$

$$(R_0^{\dagger})_2 = \begin{bmatrix} \cos 60 & -\sin 60 & 0 \\ +\sin 60 & \cos 60 & 0 \end{bmatrix}$$

TUSK (1) Munipulator Jacobian for SCARA: RRP -) Petrence fociones is term ces tesk (6). > Jegcobign can be calculated as, J = []] = [3] if porsonatte it revolute 10int = \-\\ -\d3(05(\-\l35\m(01+\a2)\-\las\ma) 13 COS(01+02) + L2 COSQ)

$$J_{2} = \begin{bmatrix} z_{1} \times (\gamma - 0_{1}) \\ z_{2} \end{bmatrix}$$

$$= \begin{bmatrix} -13 + 65 \cdot (01 + 62) \\ 13 \cos(01 + 62) \end{bmatrix}$$

$$= \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$J = \begin{cases} -l_{3}sm(0)+c_{2}-l_{3}smo_{1} & -l_{3}slm(0)+co_{2} \\ l_{3}co_{3}(0)+co_{2}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & & & & & & & & \\ l_{3}co_{3}(0)+co_{2}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & & & & & & \\ l_{3}co_{3}(0)+co_{2}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & & & & & \\ l_{3}co_{3}(0)+co_{2}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & & & & \\ l_{3}co_{3}(0)+co_{2}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & & & \\ l_{3}co_{3}(0)+co_{2}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & & & \\ l_{3}co_{3}(0)+co_{2}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & & & \\ l_{3}co_{3}(0)+co_{2}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & & & \\ l_{3}co_{3}(0)+co_{2}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}) & 0 \\ & & & \\ l_{3}co_{3}(0)+co_{3}+l_{2}smo_{1} & l_{3}co_{3}(co_{1}+co_{2}+co_{3}+c$$

$$R_0' = \begin{bmatrix} \cos \alpha_1 & -\sin \alpha_1 & 0 \\ \sin \alpha_1 & \cos \alpha_1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$P_1^2 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$R_1^2 = \begin{bmatrix} \cos \alpha - \sin \alpha \alpha & 0 \\ \sin \alpha \alpha & \cos \alpha \alpha & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$R_{a}^{B} = \begin{bmatrix} \cos \alpha & -\sin \alpha & 0 \\ \sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{bmatrix} \qquad P_{3}^{\dagger} = \begin{bmatrix} 13 \\ 0 \\ 0 \end{bmatrix}$$

$$O_{2} = Po' + Ro' P_{1}^{2}$$

$$= \begin{bmatrix} \cos Q | \mathcal{L} | \\ \cos Q \end{pmatrix}$$

where,

$$JI = \begin{bmatrix} ZIX(P-0I) \\ ZI \end{bmatrix}$$

$$J_3 = \int z_3 \times (P-03)^2$$

Meets a Rob are costhogoral.

Det's asserme that restendon matrix to imm be contition as,

$$Po' = \begin{bmatrix} z_1 & z_2 & z_3 \end{bmatrix}$$

where, fi sepssont whole column ri(3x1).

A NOCO; for dry sotution mutals,

$$(Ro')^{\dagger}(Ro') = I$$

$$\begin{bmatrix} \frac{2}{3} \end{bmatrix} \begin{bmatrix} \frac{2}{3} \\ \frac{2}{3} \end{bmatrix} \begin{bmatrix} \frac{2}{3$$

of From whome equation it is dear theet,

?: ?: = 0. so, colymns of solution (
$$i \neq i$$
) matter are orthogonal.

TISKED Types of gearboxes.

> Hondory gent box: Handory gent box is andely 48ed in various robotics applications. Planetery four box allows to reduce the roteston speed and moveage the torque out put m motors. Phreterry gear box corsists of sur gedo, planet gedo and olog gedo. son gear is attached in the middle of planet grass and olog gras. This systems sines poss various possibillities to attach motor at any pear depending upon various geals. a) (voloidal gear pore: (vloidal gearbox B not oudely rused in motor applications. But sometimes it can be used to reduce speed

SIGNIFICOINTY, It provides high outlo fee speed

and low backlash. -) bernel good box: Bernel gear box charges the orespect does relative to motor core rotestor axis. Benel geors motor con be used to minimize the design so but votime where we have Space constactionts.