

Unit - II

Introduction to Ac distribution system :-

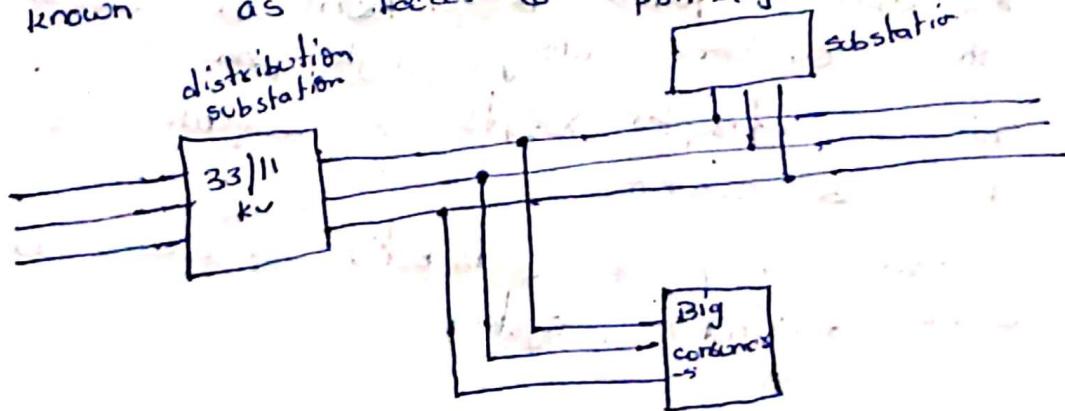
- Nowadays electrical energy is generated, transmitted and distributed in the form of alternating current.
- One important reason for widespread use of alternating current in preference to direct current is the fact that alternating voltage can be conveniently changed in magnitude by means of transformer.
- Transformer has made it possible to transmit AC power at high voltage and utilize it at a safe potential.
- High

The Ac Distribution system is classified into

- primary distribution system
- secondary distribution system

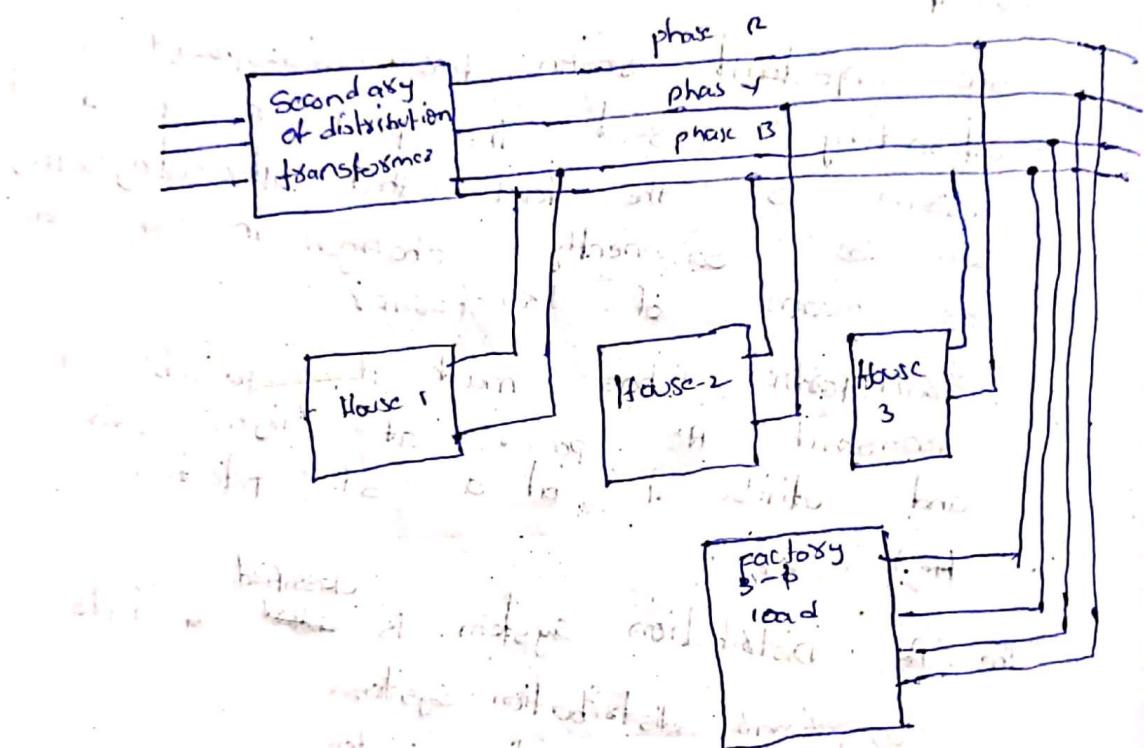
Primary distribution systems:-

The part of the electric utility system which is in between the distribution substation and distribution transformer is called primary distribution system and is made up of circuits known as factors (or) primary factors



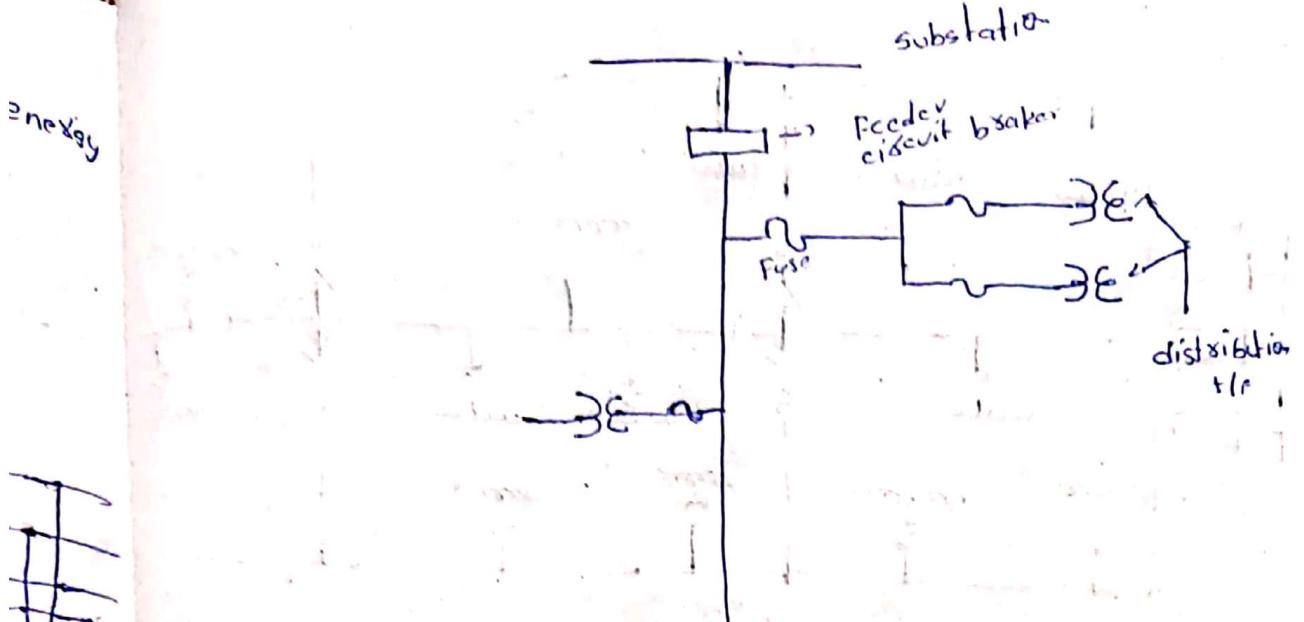
Secondary distribution system

The part of electric utility system which is in between distribution transformer to electric energy delivered to consumer is known as secondary distribution system. This working voltage level is $400/230\text{V}$ 3-ph 4-wire system.



Design considerations of radial type primary feeder

- most of distribution system are designed to be radial distribution system.
- In radial distribution system, only one path is connected between each customer and substation.
- The electric power flows from the substation to the customers along single path.
- This, it interrupted, results in complete loss of power to customers.
- In India 99% of distribution of power is by radial distribution system.



Advantages

- consumes simple in construction, design and operation
- cheaper in cost

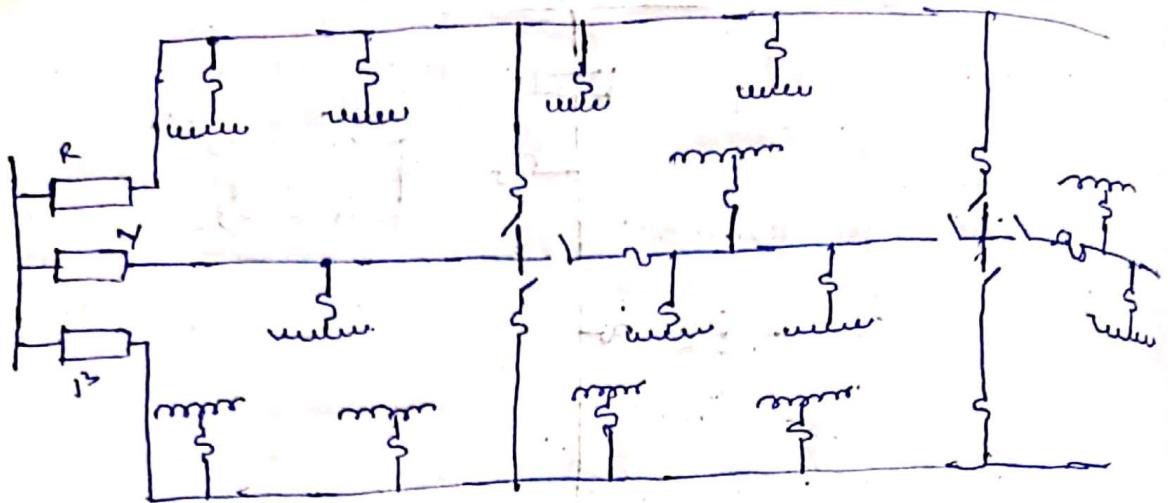
Disadvantages

- consumers at far end of feeder is subjected to voltage fluctuations with respect to variation in load.
- Reliability of service is low.
- If fault occurs at any location on the primary feeder causes power outage to every consumer at feeder.

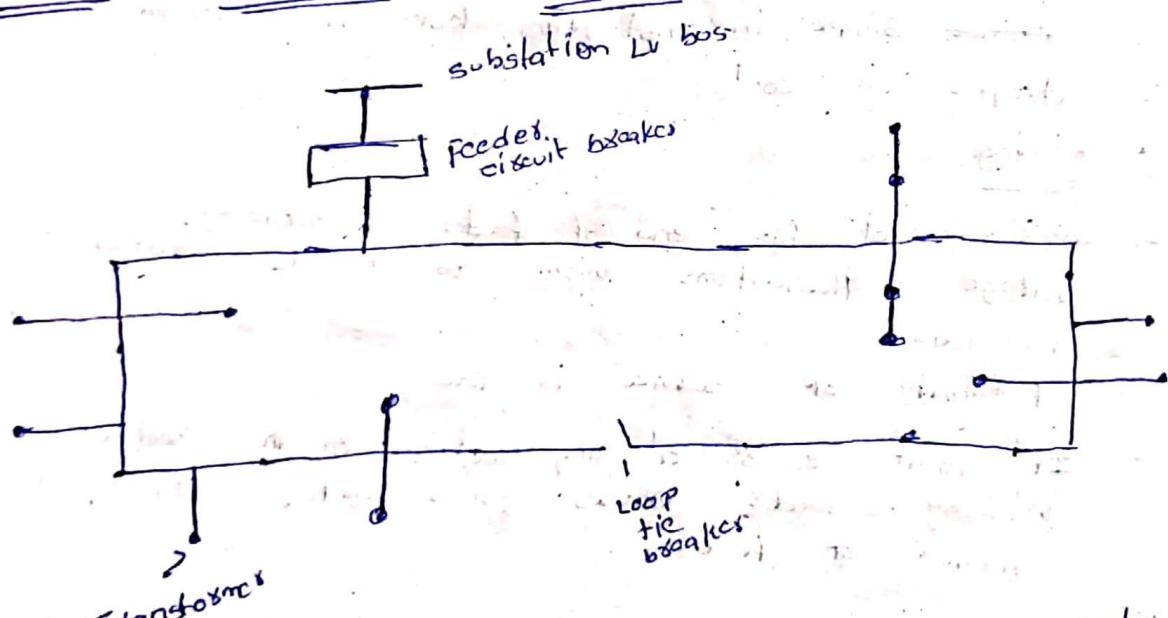
is
or
bc
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power
by

modified Radial type primary feeders with Tie and
secondary Sectionalizing switches

- In order to get rid from the power outage problem for a given radial type primary feeder, if it is modified by employing tie switches and sectionalizing switches.
- Hence modified radial type primary feeders with tie switches and sectionalizing switches provides fast restoration of service to consumers by switching unfailed section feeders to an adjacent feeders.



Design consideration of Loop type primary Feeders



- Loop type primary feeders loops through the feeder and returns to bus bar
- Loop type primary feeders assignment is beneficial to provide service for the loads where high reliability is important, i.e., in areas of hospitals (or) any emergency service centres.
- Less conductor material is required than of the radial distribution system.

Advantages

- more reliable
- less voltage fluctuation.
- less conductor material is required as the post of ring carries less current than in radial distribution system.

Disadvantages

- difficult to design when compared to radial type
- primary feeders

factors affecting primary feeds

The primary feeds voltage level is most important factor affecting the system design, cost, and operation.

some of the design and operation aspects affected by primary feeds voltage level are:

- 1) primary feeds length
- 2) primary feeds loading
- 3) no. of distribution substations
- 4) rating of distribution substations
- 5) number of sub transmission lines
- 6) system maintenance practise
- 7) The extent of tree trimming
- 8) joint use of utility pole.
- 9) Type of pole-line design and construction at pole line.
- 10) appearance



Introduction to Ac distribution systems voltage drop calculations

All the methods used for solution of Dc distribution will apply equally well for solution of Ac distribution.

→ The resistances have to be replaced by impedances the currents in various sections of distributor and voltages at load points are vector sum and not simply arithmetic sums.

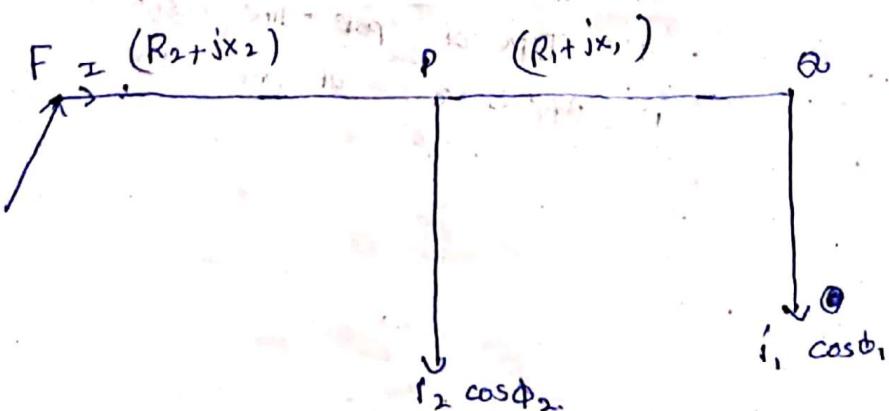
→ Further the loads tapped off from a given distribution will be at different factors.

→ To illustrate it, Ac distribution system can be explained in two different cases:

- 1) power factor setfixed to receiving end voltage
- 2) power factor setfixed to respective load voltage

i) power factor setfixed to receiving end voltage

consider the distributor PQ with concentrate loads of I_1 and I_2 tapped off with power factor of $\cos\phi_1$ and $\cos\phi_2$ at points P and Q respectively as shown in below fig.



$(R_2 + jx_2)$ and $(R_1 + jx_1)$ be the impedances of section FP and PQ.

∴ current in section PQ is = $I_1 (\cos\phi_1 - j\sin\phi_1)$

voltage drop in section PQ is given by.

$$v_{PQ} = V_1 = I_1 (\cos \phi_1 - j \sin \phi_1) (R_1 + j X_1)$$

current in section FP is

$$I = I_1 + I_2$$

$$I = I_1 (\cos \phi_1 - j \sin \phi_1) + I_2 (\cos \phi_2 - j \sin \phi_2)$$

$$I = I (\cos \phi - j \sin \phi)$$

voltage drop in section FP

$$v_{FP} = V_2 = I (\cos \phi - j \sin \phi) (R_2 + j X_2)$$

∴ voltage at point F

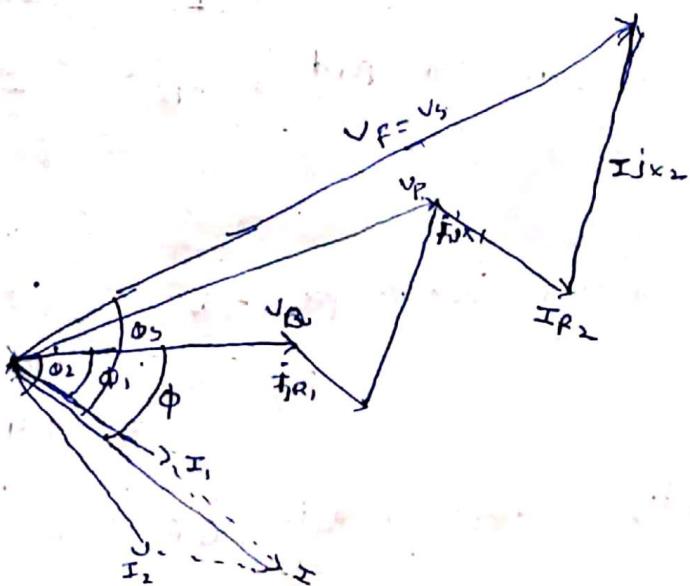
$$V_F = V_R + V_1 + V_2$$

voltage at sending end = $V_F \angle \phi_s$

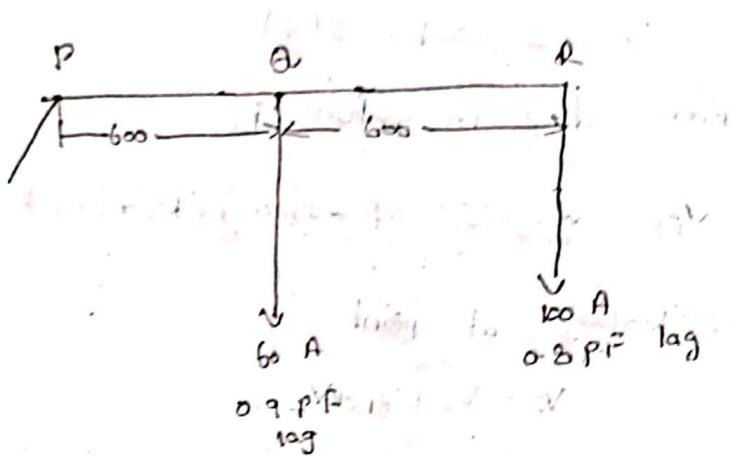
ϕ_s = sending end phase angle

The phasor diagram is shown in below fig.

- In phasor diagram receiving end voltage V_R is taken as reference voltage.
- In this case power factor of loads are lagged behind to V_R , hence currents I_1 and I_2 lags behind V_R by an angle ϕ_1 and ϕ_2 .



A two-wire distributor 1200 m long is loaded as shown in fig. The power factor at the two load points refers to the voltage at P. The impedance at each line is $(0.15 + j0.2) \Omega$. Calculate the sending end voltage, current, and power fact. The voltage at point R is 230 V.



Given:

$$i_1 = 100 \text{ A}$$

$$\cos \phi_1 = 0.8$$

$$i_2 = 60 \text{ A}$$

$$\cos \phi_2 = 0.9$$

$$V_R = 230 \text{ V}$$

$$V_P = 230 + j0$$

$$Z_{per} = Z_{eff} = (0.15 + j0.2) \Omega$$

Load current at point R, $I_R = 100 \angle \cos^{-1} 0.8$

$$= 100 \angle -36.86^\circ$$

$$\boxed{I_R = 80 - j60 \text{ A} = I_{QR}}$$

Load current at point Q, $I_Q = 60 \angle \cos^{-1} 0.9$

$$= 60 \angle 25.84^\circ$$

$$= (54 - j26.16) \text{ A}$$

Current in section PQ, $I_{PQ} = I_Q + I_R$

$$= 80 - j60 + 54 - j26.16$$

$$= 134 - j86.16 = 159.3 \angle -32.7^\circ \text{ A}$$

Voltage drop in section QR, $V_{QR} = I_{QR} Z_{per}$

$$= 100 \angle -36.86^\circ \times (0.15 + j0.2)$$

$$= 95 \angle 16.26^\circ$$

loaded
to two

The
calculate
& factors.

voltage drop in section PQ, $V_{PA} = I_{PA} \times Z_{PQ}$

$$= 159.3 \angle -32.7^\circ \times (0.15 + j0.12)$$
$$V_{PA} = 39.82 \angle 20.39^\circ$$
$$\boxed{V_{PA} = 37.32 \angle +j13.87}$$

$$V_p = V_R + V_{PA} + V_{AP}$$

$$V_p = 230 + 39.82 \angle 20.39^\circ + 25 \angle 156.26^\circ$$

$$\boxed{V_p = 292.1 \angle 4.24^\circ}$$

$$\boxed{V_p = 292.1 \angle 4.24^\circ}$$

sending end current $I_{PA} = 159.3 \angle -32.74^\circ$

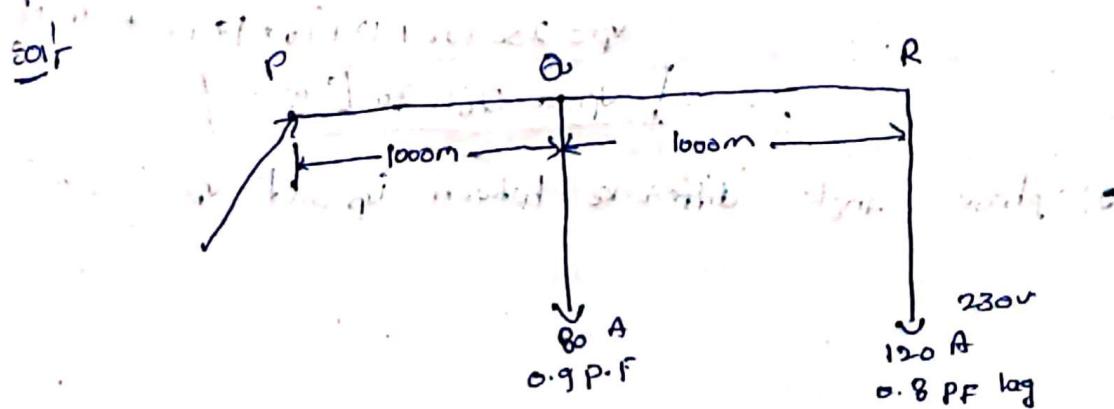
power factor at sending end is $\cos(\phi)$

$$\cos(4.24 - (-32.74))$$

$$\cos(36.84) = 0.8 \text{ lag}$$

A single phase distribution 2 km long supplies a load of 120 A at 0.8 pf lagging, at its far end and a load of 80 A at 0.9 pf lagging at its mid-point. Both power factors are offered to voltage at far end. The impedance per kilometer is $(0.05 + j0.1)\Omega$. If the voltage at far end is maintained at 230 V determine the following

- 1) voltage at sending end
- 2) phase angle between the voltage at both ends.



$$z_{PA} = (0.05 + j0.1)$$

$$z_{QR} = (0.05 + j0.1)$$

$$V_p = 230 + j0 \text{ V}$$

$$V_R = 230 \angle 0^\circ$$

$$\text{current at point R} \quad I_R = 120 (\cos\phi - j\sin\phi)$$

$$I_P = 120 (0.8 - j0.6)$$

$$I_P = (96 - j72) \text{ A}$$

$$\text{current at point } I_Q = 80 (0.9 - j0.436)$$

$$= (72 - j34.8) \text{ A}$$

$$\text{current in section PR} \quad I_{PR} = I_R = (96 - j72) \text{ A}$$

$$\text{current in section PQ} \quad I_{PQ} = I_Q + I_P$$

$$= 72 - j34.8 + 96 - j72$$

$$I_{PQ} = 168 - j106.88 \text{ A}$$

$$\text{voltage drop in section PR} \quad V_{PR} = I_{PR} z_{PR}$$

$$= (96 - j72) (0.05 + j0.1)$$

$$= (12 + j6) \text{ V}$$

$$\text{voltage drop in section PQ} \quad V_{PQ} = I_{PQ} z_{PQ}$$

$$= (168 - j106.88) (0.05 + j0.1)$$

$$= (19.12 + j11.48) \text{ V}$$

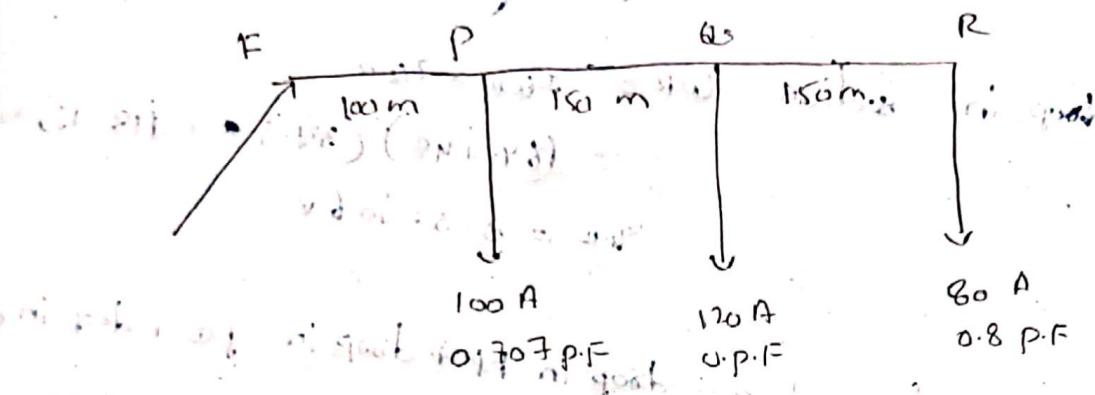
$$\text{sending end voltage } V_p = V_R + V_{PR} + V_{PQ}$$

$$V_p = 230 + j0 + 12 + j6 + 19.12 + j11.48$$

$$V_p = 261.70 \angle 3.83^\circ \text{ V}$$

2) phase angle difference between V_p and $V_R = 3.83^\circ$

3) Determine the total voltage drop of a single phase distribution as shown in below fig.
The impedance is $(0.25 + j0.125)$ Ω per kilometer



Sol:

Impedance of Section FP $Z_{FP} = (0.25 + j0.125) \times \frac{100}{1000}$
 $= (25 + j12.5) \times 10^{-3} \Omega$

Impedance of section PQ $Z_{PQ} = (0.25 + j0.125) \times \frac{150}{1000}$
 $= (37.5 + j18.75) \times 10^{-3} \Omega$

Impedance of section QR $Z_{QR} = (0.25 + j0.125) \times \frac{150}{1000}$
 $= (37.5 + j18.75) \times 10^{-3} \Omega$

current in section QR $I_{QR} = I_R = 80 (0.8 - j0.6)$
 $I_{QR} = I_R = (64 - j48) A$

current in section PQ $I_{PQ} = I_R + I_Q$
 $= 80(0.8 - j0.6) + 120(1 + j0)$
 $I_{PQ} = 184 - j48 A$

current in section FP $I_{FP} = I_P + I_Q + I_R$
 $= 100(0.707 - j0.707) + 120(1 + j0)$
 $+ 80(0.8 - j0.6)$
 $I_{FP} = (254.7 - j118.7) A$

drop in section IP $V_{FP} = I_{FP} \times Z_{FP}$
 $= (254.7 - j118.7) \times (25 + j12.5) \times 10^{-3}$
 $= (7.85 + j0.126) V$

$$\text{drop in section } PA = \frac{V_{PA}}{Z_{PA}} = I_{PA} R^2 / Z_{PA}$$

$$= (184 - j48)(37.5 + j18.75) \times 10^{-3}$$

$$V_{PA} = (7.8 + j1.65)V$$

$$\text{drop in section } QR = I_{QR} R^2 / Z_{QR}$$

$$= (64 - j48)(37.5 + j18.75) \times 10^{-3}$$

$$V_{QR} = 3.3 - j0.6V$$

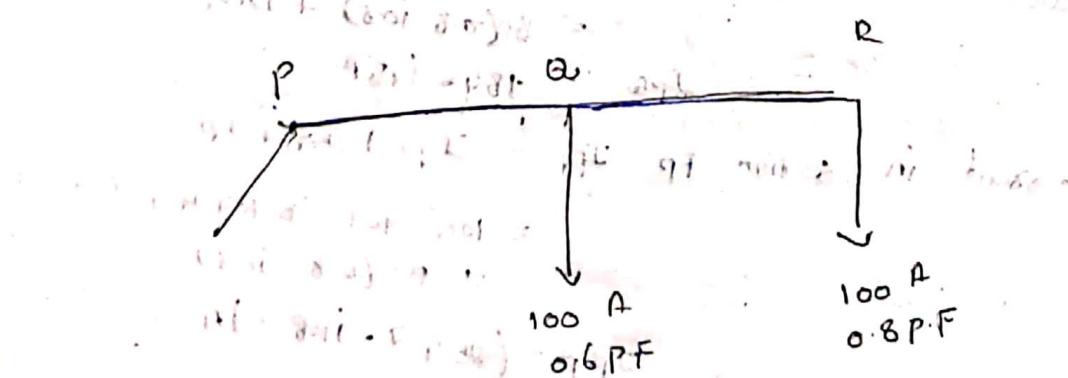
Total Voltage drop = drop in FP + drop in PA + drop in QR

$$= (7.85 + j0.126) + (7.8 + j1.65) + (3.3 - j0)$$

$$= 18.99 + j3.82V$$

$$\boxed{\text{Total drop} = 18.99V}$$

A single phase distributor PQR fed at point P shown in fig. The power factors are lagging with respect to the voltage at far end. The impedance to supply end and also to far end is $(0.1 + j0.15)\Omega$. If the section PA and QR is $(0.1 + j0.15)\Omega$, calculate the voltage at far end is $230V$, calculate the voltage at supply end and also to far end.



$$Z_{PA} = 0.1 + j0.15 \quad \text{and} \quad 4\pi \cdot 10^{-7} \quad \text{units of per km}$$

$$Z_{QR} = 0.1 + j0.15 \quad \text{per km}$$

75) $\times_{10^{-3}}$

current in section QP is $I_{QP} = I_P = 100(\cos 8 - j \sin 6)$

75) $\times_{10^{-3}}$

in QR

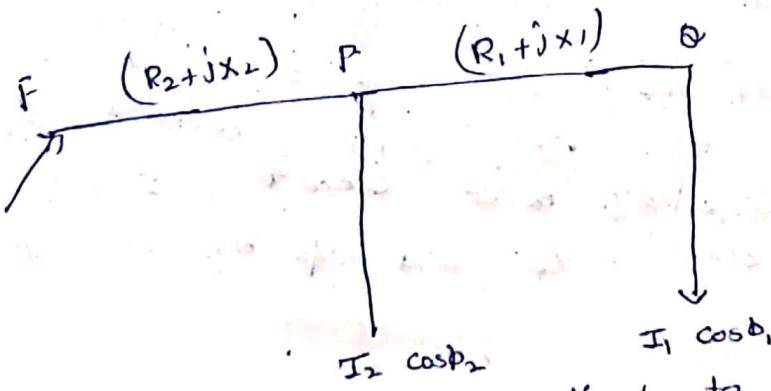
3.3 - j0.1

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feed

o/a
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power factor effected to respective load voltage.

consider a distributor FE with concentrated loads of I_1 and I_2 tapped off with power factors of $\cos \phi_1$ and $\cos \phi_2$ at points Q and P respectively as shown in below fig.



→ If the power factors are effected to respective load point voltage, the current I_2 lags behind voltage V_2 by an angle ϕ_2 , whereas current I_1 lags behind voltage V_1 by an angle ϕ_1 . V_1 and V_2 are the voltage drops in section PQ and FP respectively.

Let $(R_2 + jx_2)$ and $(R_1 + jx_1)$ be impedances of FP and PQ.

→ current in section PQ is $= I_1 (\cos\phi_1 - j\sin\phi_1)$.
Voltage drop in section PQ is given by

$$V_1 = I_1 (\cos\phi_1 - j\sin\phi_1) (R_1 + jx_1)$$

voltage at point P is

$V_P = \text{voltage at point Q} + \text{voltage drop in section PQ}$

$$V_P = V_Q + V_1$$

$$V_P = V_P \underline{\Delta}$$

$$I_2 = I_2 \underline{|-\phi_2|}$$

$$I_2 = I_2 \underline{|-(\phi_2 - \alpha)|}$$

$$I_{FP} = I_2 + I_1 = I_2 (\cos(\phi_2 - \alpha) + j\sin(\phi_2 - \alpha)) + I_1 (\cos\phi_1 - j\sin\phi_1)$$

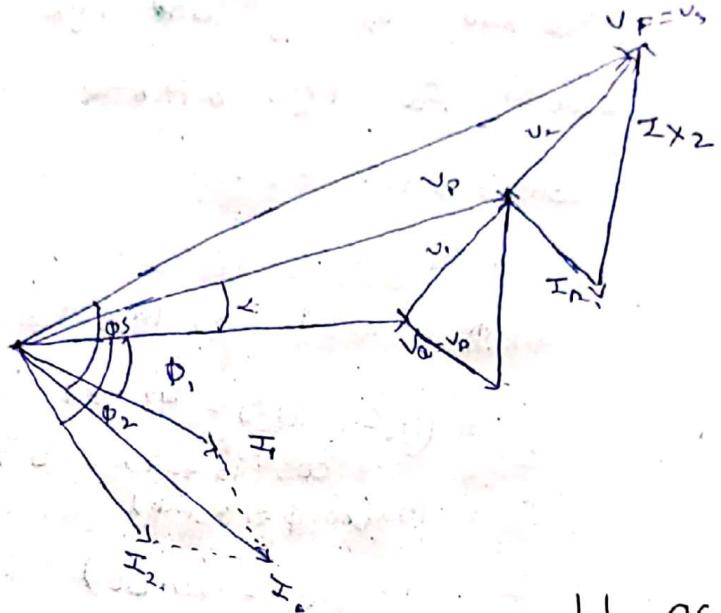
voltage drop in section FP, $V_2 = I_{FP} (R_2 + jx_2)$

voltage at point F, $V_F = V_P + V_2$

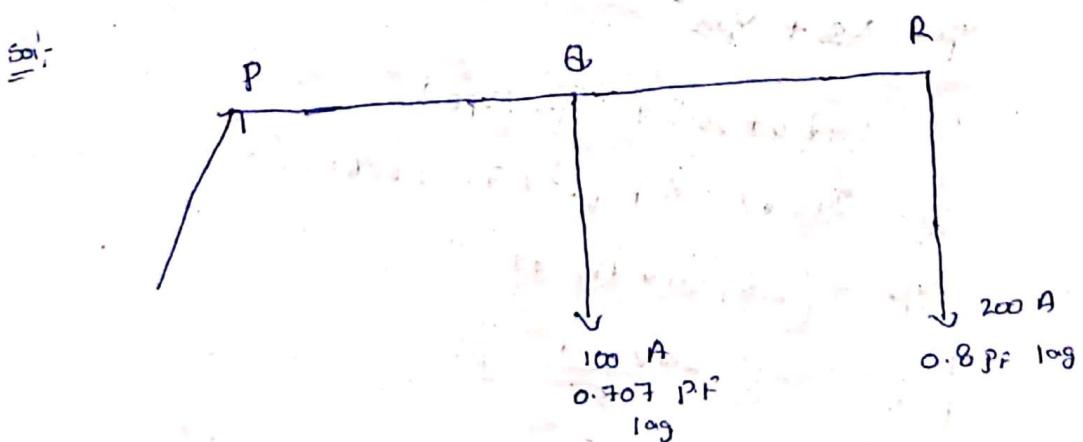
→ The phasor diagram of AC distribution is shown in Fig.

→ In phasor diagram, respective load voltage V_F and V_A axis taken as reference vectors.

→ In this case power factors $\cos\phi_1$ and $\cos\phi_2$ of the loads are referred to V_P and V_A respectively, hence currents I_1 and I_2 lags behind V_A and V_P by an angle ϕ_1 and ϕ_2 .



A single phase two wire AC feed is loaded as shown in fig. The power factors are lagging and are referred to voltage at the respective load points. The impedance of section PQ and QR are $(0.03 + j0.05)$ and $(0.05 + j0.08)$ Ω , respectively. Determine voltage magnitude and phase angle at the supply end, if voltage at the far end is 230 V.



$$Z_{PQ} = 0.03 + j0.05$$

$$Z_{QR} = 0.05 + j0.08$$

voltage at Q $V_Q = V_p + \text{drop in section } QR$

$$V_Q = 230 + I_R \times Z_{QR}$$

$$V_Q = 230 + jR(\cos\phi_x - j\sin\phi_x)$$

$$V_Q = 230 + 200(0.8 - j0.6) (0.05 + j0.08)$$

$$V_Q = 247.6 + j6.8$$

$$V_Q = 247.69 \angle 11.573^\circ$$

V_Q leads V_R by an angle 11.573°

current I_Q lags difference vector by $(\phi_1 - \alpha)$

$$\cos\phi_1 = 0.707$$

$$\phi_1 = 45^\circ$$

The current I_Q lags difference vector by $(\phi_1 - \alpha)$

$$= (45 - 1.573) = 43.427$$

$$\cos(43.427) = 0.72$$

$$\sin(43.427) = 0.63$$

$$I_Q = 100(\cos\phi - j\sin\alpha)$$

$$I_Q = 100(0.72 - j0.68)$$

$$I_R = 200(0.8 - j0.6)$$

$$I_{PA} = I_Q + I_R$$

$$I_{PA} = 100(0.72 - j0.68) + 200(0.8 - j0.6)$$

$$I_{PA} = 100(0.72 - j0.68) + 200(0.8 - j0.6)$$

$$I_{PA} = (232.7 - j188.67)$$

$$V_P = V_Q + V_{PA}$$

$$V_P = 247.6 + j6.8 + I_{PA} (2\pi f)$$

$$V_P = 247.6 + j6.8 + (232.7 - j188.67)(0.03 + j0.05)$$

$$V_P = (264.01 + j12.77) V$$

$$V_P = 264.32 \angle 2.77^\circ$$

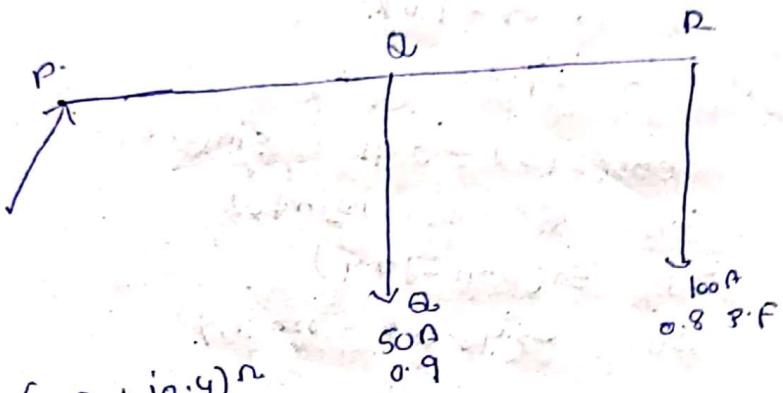
phase angle b/w V_R and $V_P = 2.77^\circ$

A 1-phi distributed has loop resistance of 0.3Ω and a reactance of 0.4Ω . The load end at the distributed has a load current of $100A$ and a power factor 0.8 lag at $220V$. The midpoint Q of distributed has bad current of $50A$ at power factor 0.9 lag with voltage difference, voltage and sending end voltage and power factors.

Sol:

$(\Phi, -\alpha)$

$$= 0.68$$



$$Z_{PP} = (0.3 + j0.4)\Omega$$

$$Z_{PQ} = Z_{PR}/2 = \frac{0.3 + j0.4}{2} = (0.15 + j0.2)\Omega$$

$$Z_{QR} = Z_{PR}/2 = \frac{0.3 + j0.4}{2} = (0.15 + j0.2)\Omega$$

voltage at load end R is $V_R = 220 \angle 0^\circ$

load current at point R $I_R = 100(0.8 - j0.6)$

$$I_R = 80 - j60$$

current in section QP $I_{QP} = I_{QR} = I_R = 80 - j60$

voltage drop in section QP is given by.

$$V_{QP} = I_{QP} * Z_{QP}$$

$$V_{QP} = (80 - j60) * (0.15 + j0.2)$$

$$V_{QP} = 24 + j7V$$

voltage drop at point Q $V_Q = V_P + V_{QP}$

$$V_Q = 220 + (24 + j7)$$

$$V_Q = 244 + j7 = 244 \angle 11.64^\circ$$

$$\alpha = 1.64^\circ$$

current I_Q lags difference vector by $(\phi_1 - \alpha)$

$$\cos \phi_1 = 0.9$$

$$\phi_1 = 25.84$$

current I_Q lags difference vector by $(\phi_1 - \alpha)$

$$= (25.84 - 1.64)$$

$$= 24.2$$

$$\cos(24.2) = 0.91 \quad \sin(24.2) = 0.4$$

$$I_Q = 100(\cos \phi_1 - j \sin \phi_1)$$

$$I_Q = 50(0.91 - j0.4)$$

$$I_Q = 45.5 - j20.49$$

$$\text{#} I_{PQ} = I_Q + I_R$$

$$I_{PQ} = (45 - j20.49) + (80 - j60)$$

$$I_{PQ} = (125.6 - j80.49) A$$

voltage drop in sec PQ

$$V_{PQ} = I_{PQ} \times Z_{PQ}$$

$$V_{PQ} = (125.6 - j80.49) \times (0.15 + j0.2)$$

$$V_{PQ} = (34.93 + j13.30) V$$

$$V_P = V_Q + V_{PQ}$$

$$V_P = (244 + j7) + (34.93 + j13.30)$$

$$\boxed{V_P = 279.66 \angle 4.1^\circ}$$

phase angle below V_P and $V_R = 4.11^\circ$

sending end current = $I_{PQ} = 125.6 - j80.49$

$$= I_{PQ} = 149.18 \angle -32.65^\circ A$$

sending end power factor = power factor at current + power factor at voltage

$$\text{sending end power factor} = 4.11 + 32.65 \\ = 36.86$$

$$\cos(36.86) = 0.801 \text{ lag}$$

design

consideration of secondary distribution system

→ secondary distribution system receives power from secondary side of distribution system transformed at low voltage through a supply power to various loads service lines.

→ secondary distribution system are generally radial type except for some specific areas such as hospitals, business centers and military installations.

→ secondary side of distribution transformer supplies power through service conductor to service meter and also incl uding:-

A separate service system for each customer with separate distribution transformer and secondary connection.

The radial system with a common secondary main which is supplied by one distribution transformer and feeding a group of customers.

objectives of distribution

system protection

- primary objectives of distribution system protection
- 1) minimize fault duration
 - 2) minimize the number of customers affected by fault

secondary objectives:-

- Eliminate safety hazards as early as possible
- minimize service failure to the smallest branch of distribution system.
- protect the consumer's apparatus

- protected the distribution system from unnecessary service interruption and disturbances.
- disconnected the faulted branches, transformers (or) other components.

Types of common faults in distribution system

- over head distribution system are subjected to two types of faults and they are temporary (a) Transient and permanent fault.
- depending on the nature of system involved, most of faults are temporary in nature.
- Temporary faults occur when phase conductor of the system gets in contact electrically with other phase conductors (b) to the ground momentarily due to trees, birds (c) other animals, high winds, lightning flashovers etc..

- The duration of this fault is to be minimized by using
- The duration of this fault is to be minimized by using high speed (or) instantaneous tripping
- Automatic reclosing of a relay prevents unnecessary fuse breaking.
- permanent faults are those that require repair by a repair crew in term of following.
- replacing the broken down conductors, blown fuses (d) any other damaged apparatus.
- removing tree limbs from lines
- manually reclosing a circuit breaker to restore the service.

Generally the types of faults in distribution system are:-

- 1) Single line to ground fault (SLG)
 - 2) Line to ~~ground~~ line fault (LL)
 - 3) Double line to ground fault (LLG)
 - 4) Three phase fault (LLL)
- procedure for fault calculation:

The possible fault types that might occur in a distribution system are:-

- 1) single line to ground fault (SLG)
- 2) line to line fault (LL)
- 3) double line to ground fault (LLG)
- 4) three phase fault (LLL)

The first, second and third type of faults can take place on two phase feeders and fourth type of fault can take place only on three phase feeders.

- However even on these feeders usually only one fault takes place due to multi-grounded construction.
- The relative numbers of occurrence of different types of faults depend upon the various factors like feeder configuration, height of ground wires, voltage levels, grounding methods, relative insulation, level of ground and between phases, speed of fault clearing, atmospheric conditions etc..
- The relative numbers of occurrence of different types of faults in a distribution system are mentioned as follows

- single line to ground fault (SLG) = 7 A
- line to line fault (LL) = 15 A
- double line to ground fault (LLG) = 10 A
- Three phase fault = 5 A

→ The actual fault current is usually less than the rated three phase value.

- However, LG fault often produces a greater fault current than that of three phase fault especially when generators are neutral grounded.
- In general the maximum and minimum values of fault currents are both calculated for a given distribution system.

The maximum fault current is determined based on following assumption:

- All generators are connected.
- Fault is a dead short circuit
- Load is maximum.

The minimum fault current is determined based on following assumptions:

- minimum number of generators connected
- fault is not a dead short circuit
- load is minimum.

The calculated maximum fault current values are used to determine the setting capacity of protected devices.

The calculated minimum fault current values are used in co-ordinating the operations of protective devices.

- To determine fault currents, one has to determine the positive, negative and zero sequence impedance of system at Hu side of distribution substation + transformer.
- These impedances are usually readily available from transmission fault studies.
- ∵ for any given fault on radial feeder, one can simplify add Thevenin's impedance to the appropriate impedance as the fault is moved away from substation along the feeder.

principle of operation or fuse!

- It is an over current protective device with circuit opening ability when directly heated and gets destroyed due to flow of over current through it in the event of an overloaded (or) short circuit condition.
- Hence the purpose of the fuse is to isolate the failure line from system.
- fuse is made up of material having low melting point, high conductivity and least deterioration due to oxidation.
e.g. silver, copper etc.
- It is kept in series with the circuit to protect.
- under normal operating conditions i.e; short circuit condition (or) over load condition, the fuse is at a temperature below its melting point since it carries the normal current without overheating.
- under abnormal operating conditions i.e; short circuit condition (or) over load condition, the current flow through the fuse increases beyond its rated value such that the temperature rises and fuse gets melted.

resulting in the disconnecting of circuit to be protected by it.

→ Time required to blow out the fuse depends upon the magnitude of excessive current i.e., greater the current then the smaller is the time taken to blow out the fuse.

Advantages

- cheapest form of protection
- require no maintenance
- Breaks heavy short circuit current without noise (or) smoke
- minimum time of operation can be made much shorter than that of circuit breaker

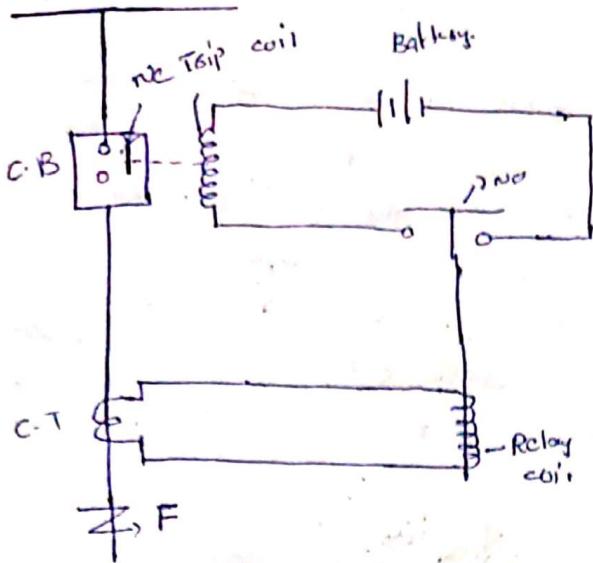
Disadvantages

considerable time is required in removing
(or) replacing the fuse after operation.

Principle of operation of circuit breakers

Circuit breaker is an automatic interrupting device which is capable of breaking and making of a circuit under all conditions i.e., faults (or) normal operating conditions.

- Circuit breaker isolates the circuit under fault condition with the help of relay.
- A relay has two basic contacts named as NO (normally open) and NC (normally closed) contact.
- With the help of these contacts we can operate the relay.



under normal condition the N.C coil is closed and no coil is opened; and current through current transformer is constant so the relay coil doesn't magnetize.

when fault occurs on distribution line the current through the current transformer increases and relay coil gets magnetized and attracts the N.O contact downwards. so due to this closed circuit N.C contact. so the circuit breaker operates and isolate the faulty section.

→ A circuit breaker essentially consists of fixed contact and moving contact called as electrodes.

→ Under normal operating condition, the contacts remains closed; under fault condition these two contacts get open and breaks the circuit.

→ whenever fault occurs on any part of distribution system, the trip coil of circuit breaker gets energized and moving coil is pulled away from fixed contact by some mechanism resulting in opening of circuit.

→ When contact of circuit breaker is separated under fault conditions, an arc is struck between contacts.

→ The production of arc not only delays

The current interruption process but it also generate enormous amount of heat which may cause damage to system (or) circuit breaker itself.

- Hence primary task of a circuit breaker is to extinguish the arc that is developed due to separation of its contacts in an arc extinguishing medium such as air case of air blast circuit breaker, vacuum in case of vacuum circuit breaker, oil in case of oil circuit breaker and SF₆ gas in case of SF₆ circuit breaker.

Objectives of co-ordination

- minimize the extent of faults in order to reduce the number of customers affected.
- minimize the service interruptions due to temporary faults.
- minimize the duration of service outages to identify the location of fault.

General co-ordination procedure

- Gather the required and aforementioned data.
- select the initial location for protective device on the given distribution circuit.
- determine the maximum and minimum fault current values at each of selected locations and at the end of feeds mains, branches and laterals.
- pickout the necessary protective device located at the distribution substation in order to protect the substation transformer properly from any fault that might occur in distribution circuit.
- co-ordinate the protective devices from the substation outward (i.e., from the end of the distribution circuit back to substation).

- Re-consider and change if necessary the initial locations of protective devices
- Re-examine the chosen protective device for current carrying capacity, interlocking capacity and minimum pick up rating.
- Draw a composite Tcc curve showing the co-ordination of all protective devices employed with the curves drawn from common base voltage.
- Draw a circuit diagram which shows the configuration, the maximum and minimum values of fault currents and the ratings of protective devices employed and so on.