

1 Power System:

A Power system consists of Generation, Transmission and Distribution. An Modern power system is divided into four major parts. They are Generation, Transmission, Sub Transmission and Distribution.

Power System Analysis:

The Evolution of power system is called as Power system Analysis.

Functions of Power System Analysis:

- ① To monitor the voltage at various buses.
- ② Real & Reactive power flow between the buses.
- ③ To Design the circuit breakers.
- ④ To plan future expansion of the existing system.
- ⑤ To Analyse the system under different fault conditions.
- ⑥ To study the ability of the system for small and large disturbances. (Steady state & Transience stability)
- ⑦ To

Components of Power System :

The components of power system includes Generators, Power Transformers, Transmission lines, distribution lines, Loads, & compensation devices like shunt, series, static VAR compensators.

Representation of Power system Components :

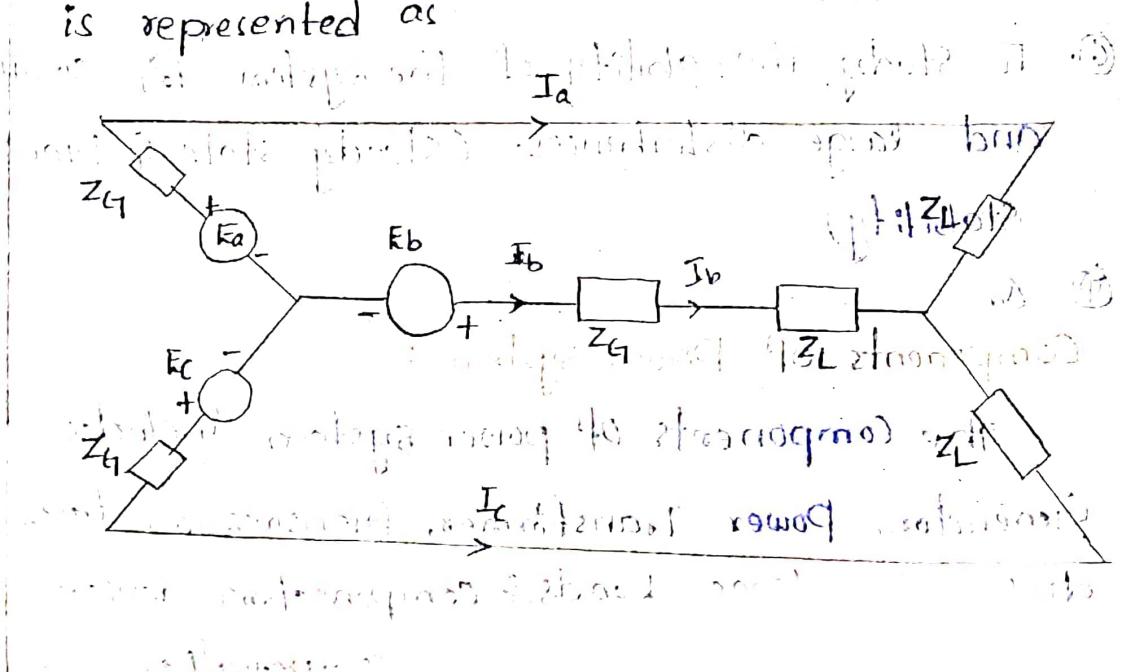
A complete diagram of a power system representing all 3 phases becomes too complicated for a system of practical size. So that much so that, it may no longer convey the information if is intended to convey.

It is much more practical to represent a power system by means of simple ~~single~~ symbols for each component resulting in what is called One Line (or) Single Line Diagram.

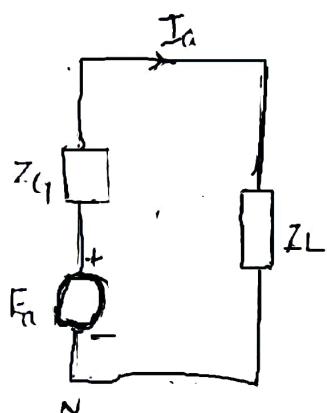
Per Unit System leads to great simplification of 3-d network involving Transformer. An Impedance diagram drawn on a per unit basis doesn't requires Ideal Transformers to be included in it.

An important element of the Power System is the Synchronous machine which is greatly influenced by system during both Steady state and Transient condition.

The synchronous machine model in steady state is represented as



The 1- ϕ equivalent of balanced 3- ϕ work is as shown in figure

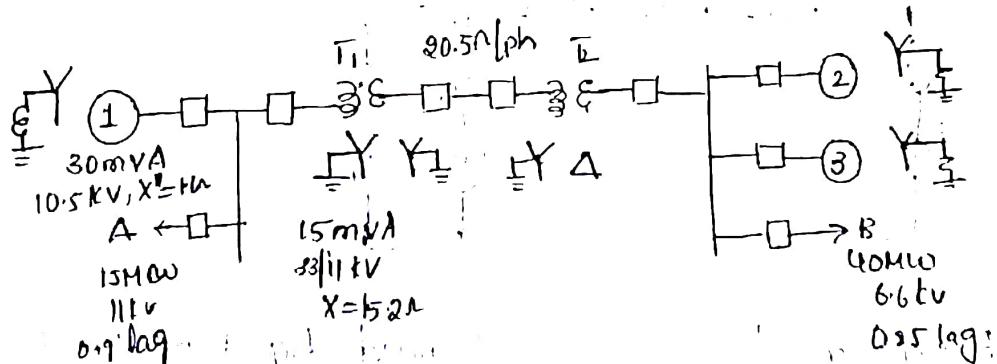


Impedance (or) Reactance Diagram:

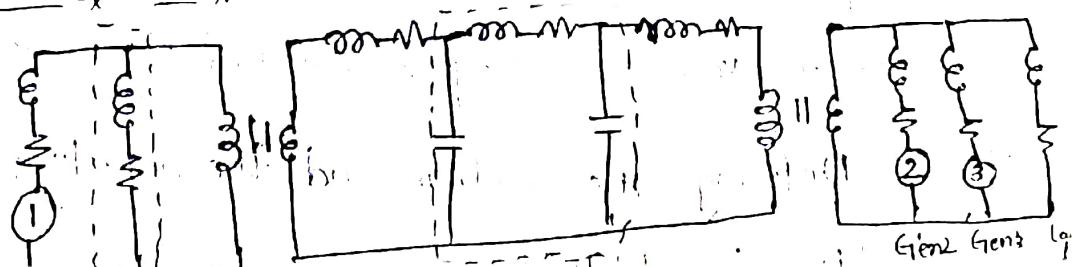
The Circuit Breakers need not be shown in a load flow study but are must for protection. Steadily represented by rectangular blocks.

Generators & Transformer connection Star, Delta or the neutral winding are indicated by the symbol drawn by the sign of the representation of these elements.

Single line diagram of Simple Power system:

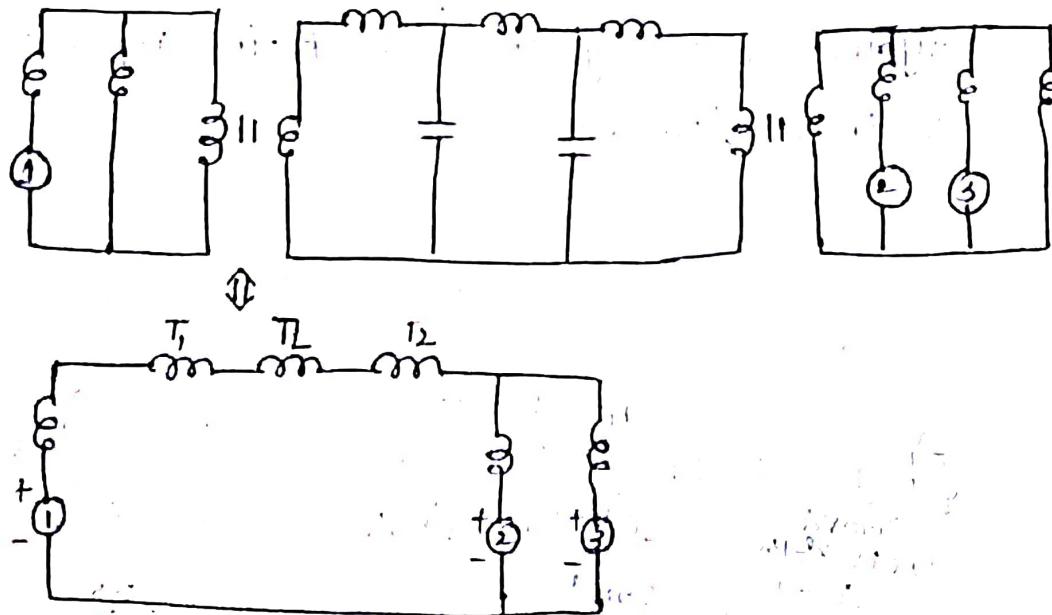


Impedance diagram:



- * Magnetising reactances of the Trans formers have been neglected.
- * Generators are represented as Voltage sources with series resistance and inductive reactance.
- * Transmission line is represented by π model
Loads are assumed to be passive.
- * Not involving rotating machines and are represented by resistance & inductive reactance in series.
- * Neutral grounding impedances don't appear in the diagram.
- * As Balanced conditions are assumed

Reactance Diagram:



Reactance diagram is obtained by removing resistance in Impedance diagram.) intended

* Steps involved in solving a problem Using digital Computer

Step 1: Defining the problem and the objectives of the Analysis are studied.

* Assessment of data available and preparation of the input data in proper format.

* This step also involves methods to synthesise and estimate the missing data.

* Development of suitable mathematical models to represent the power system and various components.

* This step also involves the integrating the models of various components and formulating the mathematical equations to be formed.

* Selection of suitable technique to solve the mathematical equations.

* In most of the Analysis the equations are non linear; and a suitable numerical method has to be chosen which depends on computation time, involves, memory required, and accuracy, reliability of method and convergence characteristics.

* Modern digital computers have very high computation speed and large memory.

* For real time Applications, the computation time is important, because if computation time is less then more time is required.

* Development of flow chart or Algorithm for the solution of the equations.

* The Algorithm should have the operational limitations of the power system.

* The Last step involves the Actual development of computer programme in a high level languages

those are FORTRAN, C++, MATLAB are extensively used for the programming.

* The programme developed should be flexible & reliable and capable of handling diverse data.

Graph Theory:

Graph:

* The Geometrical interconnection of the elements ⁱⁿ ~~of~~ a network.

* Which describes to replace the network components by single line segments irrespective of the characteristics of a components.

* The Line segments are called elements and their terminals are called as nodes.

* A Node of an element are incident if the node is a terminal of the element

* Nodes can be incident to one or more elements.

Sub Graph:

* Sub Graph is any subset of elements of graph.

Path:

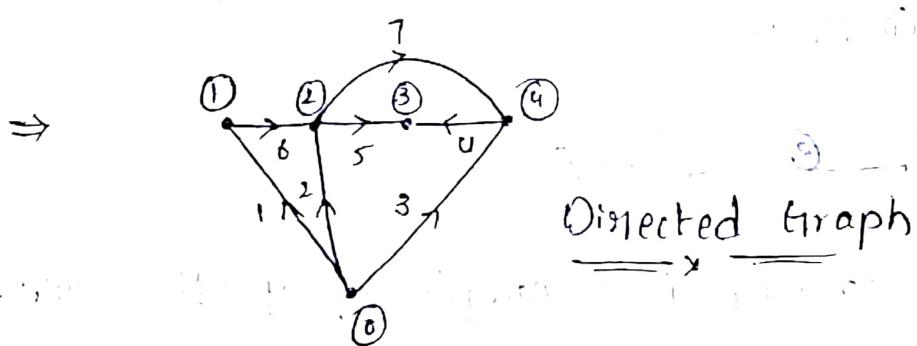
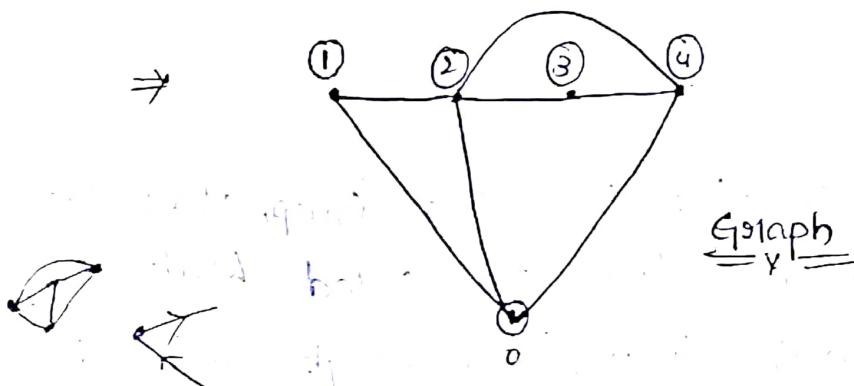
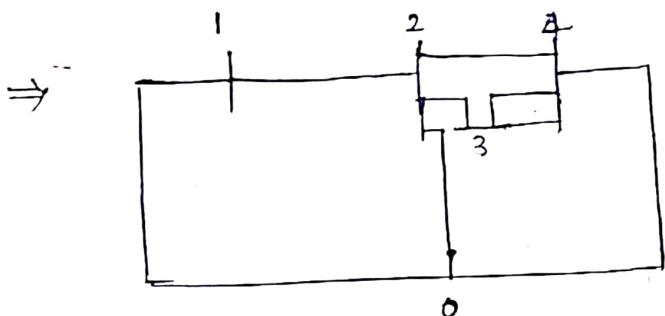
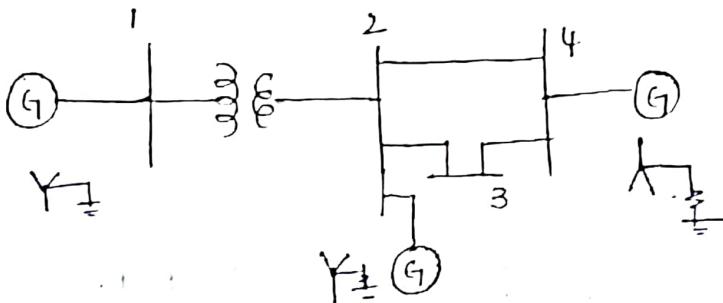
* It is a sub Graph of connected elements with not more than two elements connected to any one node.

Connected Graph:

* A Graph is connected if and only if there is a path between every pair of nodes.

Oriented (or) Directed graph:

* If each element of the connected graph is assign a direction is called Oriented (or) Directed graph.



Tree :

* A connected Sub Graph containing all nodes of the Graph but no loop is called a Tree.

* Elements of ~~Branch~~^{Tree} are called Branches

* No. of branches required $b = n - 1$

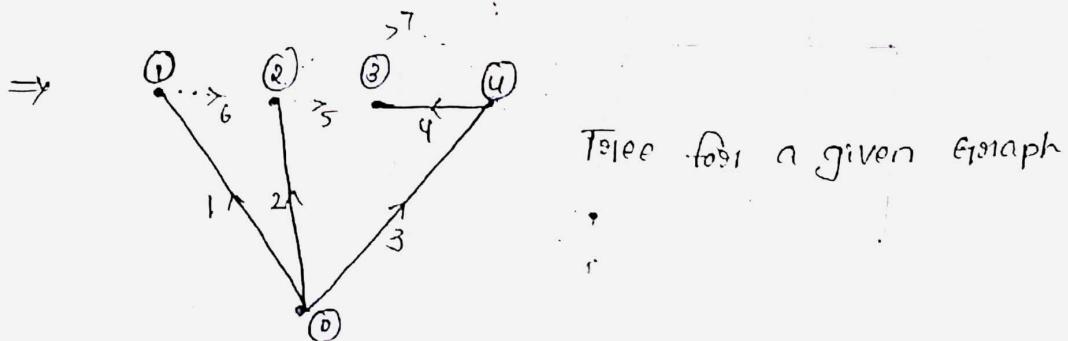
Ex. Find a tree with $n = 6$ nodes and $b = 5$ branches.

Ans. A tree with $n = 6$ nodes and $b = 5$ branches has $n - b = 1$ loop.

Number of possible trees for a graph is

$$\Rightarrow |[A] [A]^T|$$

where A is reduced incidence Matrix.



Co-Tree :

* The Elements of the connected graph that are not included in the tree are called links and form a subgraph not necessarily connected called Co-Tree.



* The Co-Tree is a compliment of the tree.

* The no. of links in a Co-Tree.

$$d = e - b \quad e \rightarrow \text{total no. of elements of graph}$$

$$= e - (n - 1) \quad b \rightarrow \text{no. of branches in a tree}$$

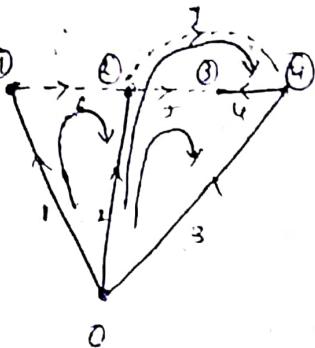
$$= e - n + 1 \quad n \rightarrow \text{total no. of nodes}$$

Loop :

* If a link is added to the Tree the resulting graph contains one closed path called a loop.

* the addition of each subsequent link forms one (or) more additional loops.

- * Loops which contains only one link are independent and are called Basic Loop or Independent Loop.
- * Orientation of the Basic Loop is chosen to be same that of links.



Cut Set:

* A set of elements that if removed divides a connected graph into two connected sub graphs.

* A unique independent group of cutsets may be chosen if each cutset contains only one branch.

* Independent cutset are called as Basic Cutsets
No. of cutsets = No. of Branches.

* Orientation of the Basic cutset is chosen to be same as that of its Branch.

Incidence Matrices:

* Any oriented graph can be described completely in the compact complex Matrix form.

* When it specifies the orientation of the each branch in the graph and the nodes at which this branch is incident. This matrix is called as Incidence Matrix.

Types of Incidence Matrix:

- ① Element Node Incidence Matrix $[A]$ exn
- ② Bus Incidence Matrix $[A]$ exn-1
- ③ Branch path Incidence Matrix $[K]$ ~~b x node~~
- ④ Basic cutset Incidence Matrix $[B]$ exn-1
- ⑤ Augmented cutset Matrix $[\hat{B}]$ exn
- ⑥ Basic Loop Incidence Matrix $[C]$ exl
- ⑦ Augmented Loop Incidence Matrix $[\hat{C}]$ exl

① Element Node Incidence Matrix $[A]$:

* The incidence of elements to nodes in a connected graph is shown by the Element node Incidence Matrix $[A]$.

$$a_{ij} = +1$$

If the i th element is incident to and oriented away from j th node.

$$a_{ij} = -1$$

If the i th element is incident to and oriented towards j th node.

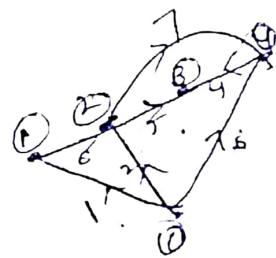
$$a_{ij} = 0$$

If the i th element is not incident to the j th node.

The dimensions of A matrix is $e \times n$, where e is no. of elements and n is no. of nodes.

$$A \Rightarrow$$

e\bus	(1)	(2)	(3)	(4)
1	+1	-1	0	0
2	+1	0	-1	0
3	+1	0	0	0
4	0	0	0	-1
5	0	0	+1	-1
6	0	+1	-1	0
7	0	0	+1	0



exn

Reduced(ex)

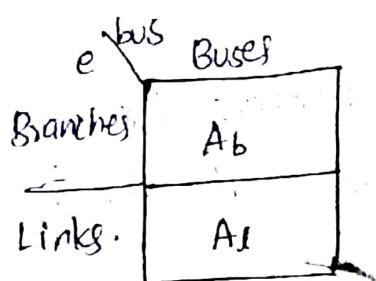
② Bus Incidence Matrices [A] :

- * Any node of a connected graph can be selected as the reference node. The variables of the other nodes referred to as buses can be measured with respect to the unsigned reference.
- * Delete the column corresponding to the reference node is bus incidence matrix (BSI) element Bus Incidence Matrix.

The order is $A = (exn-1)$

$$A \Rightarrow$$

e\bus	(1)	(2)	(3)	(4)
1	-1	0	0	0
2	0	-1	0	0
3	0	0	0	-1
4	0	0	-1	+1
5	0	+1	-1	0
6	+1	-1	0	0
7	0	+1	0	-1



$$A_b = b \times (n-1) = \text{branches} \times \text{Buses}$$

$$A_I = 1 \times (n-1)$$

* Where: A_b is a non singular matrix with rank $(n-1)$

③ Branch Path Incidence Matrix $[k]$:

x x x x x

The incidence of branches to paths in a tree is shown by the branch path incidence matrix, where a path is oriented from a bus to the reference mode.

$$k_{ij}=1$$

If the i th branch is in the path from j th bus to reference and is oriented in the same direction.

$$k_{ij}=-1$$

If the i th branch is in the path from j th bus to reference and is oriented in the opposite direction.

$$k_{ij}=0$$

If the i th branch is not in the path from j th bus to reference.

With node zero as reference, the branch path incidence matrix associated with the tree is given as follows.

Path	0	1	2	3
1	-1	0	0	0
2	0	-1	0	0
3	0	0	-1	0
4	0	0	0	-1

$$K = \text{branches} \times \text{paths}$$

$$K^T = \text{paths} \times \text{branches}$$

$$K^T \cdot A_b = (\text{paths} \times \text{branches}) \times (\text{branches} \times \text{buses})$$

$$= \text{paths} \times \text{buses}$$

$$K^T = U A_b^{-1} = A_b^{-1}$$

square matrix, with

This is a non-singular

rank ($n-1$).

The Branch path incidences to p matrix K and a sub branch Ab relate the branches-to-path and branches-to-buses respectively.

Since there is a one-to-one correspondence between paths and buses.

$$A_b K^T = U \Rightarrow K^T = A_b^{-1}$$

④ Basic cutset Matrix $[B]$

The incidence of elements to basic cutsets of a connected graph is shown by the basic cutset incidence matrix $[B]$.

$$b_{ij} = +1$$

If i th element is incident to and oriented in the same direction as j th basic cutset.

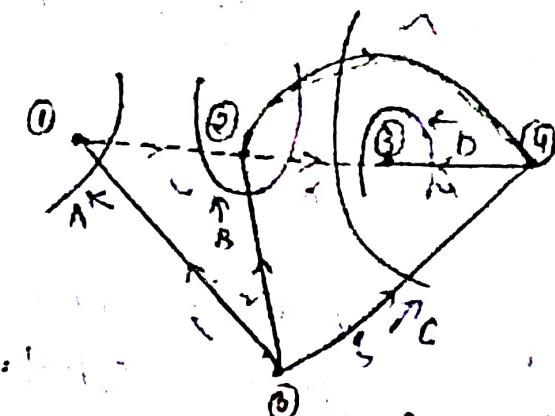
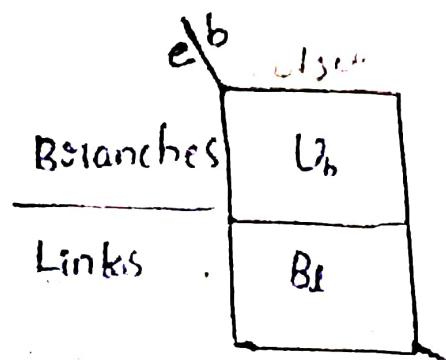
$$b_{ij} = -1$$

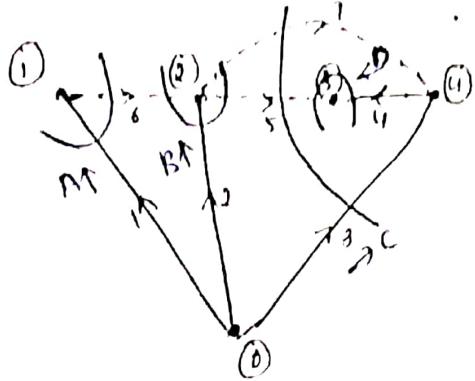
If the i th element is incident to and oriented in the opposite direction to the j th basic cutset.

$$b_{ij} = 0$$

If the i th element is not incident to the j th basic cutset.

	b	A	B	C	D
1	+1	0	0	0	
2	0	+1	0	0	
3	0	0	-1	0	
4	0	0	0	+1	
5	0	-1	+1	+1	
6	-1	+1	0	0	
7	0	-1	+1	0	





* The Identity Matrix B_I will shows one to one correspondence of Branches & Basic cutsets.

* The subMatrix B_I can be obtained from Bus Incidence Matrix A

* Since there is a One to One Correspondence of the branches and cutsets $B_I A_B$ shows the incidence of the links to Buses.

$$B_I A_B = A_I$$

$$B_I = A_I A_B^{-1}$$

We know that $A_B^{-1} = K^T$

$$\boxed{B_I = A_I K^T}$$

⑤ Augmented ^{Cutset}
Matrix = (\hat{B})

	1	2	3	4	5
1	1	0	0	0	0
2	0	1	0	0	0
3	0	0	1	0	0
4	0	0	0	1	0
5	0	0	0	0	1

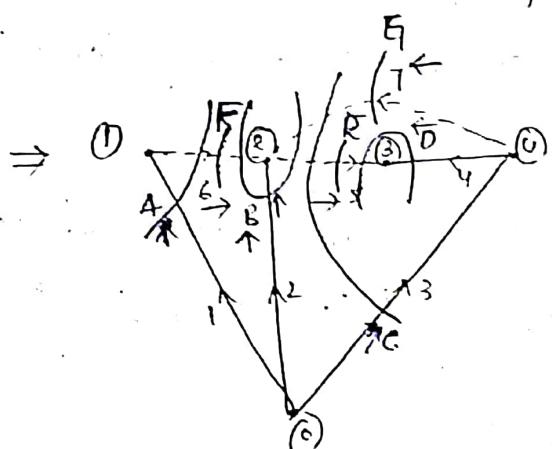
* Fictitious cutset called Tie cutsets

* An Augmented Cutset Incidence Matrix is formed by adjoining to the Basic Cutset Incidence Matrix

corresponding to these Tie cutsets

$$\Rightarrow$$

	Basic cutset			Tie cutset			
	A	B	C	D	E	F	G
Branches	1	1					
	2		1				
	3			1			
	4				1		
Links	5	-1	1	1	1		
	6	-1	1			1	
	7	-1	1				1



* A Tie cutset is oriented in the same direction as the associated links.

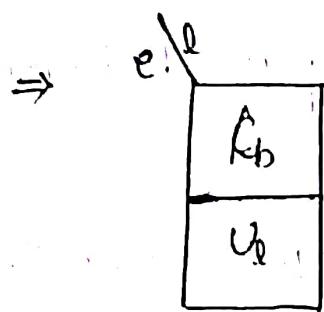
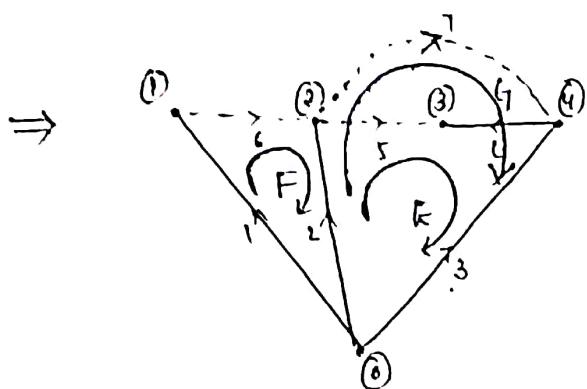
$$\Rightarrow$$

	Basic cutset		Tie cutset
Branches	U_B	0	
Links	B_L	U_L	

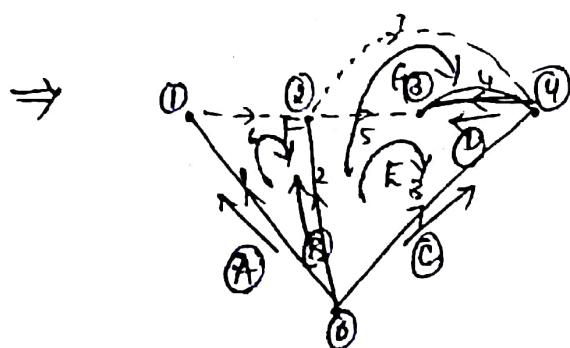
* This is the square matrix of orders (ex e) and e is non singular.

⑥ Basic Loop Incidence Matrix \div (C)

* The Incidence of elements to Basic loops of a connected graph is shown by Basic Loop Incidence Matrix [C].

$$\Rightarrow \begin{array}{c|ccc|c} & E & F & G \\ \hline 1 & & 0 & +1 & 0 \\ 2 & & +1 & -1 & 1 \\ 3 & & -1 & 0 & -1 \\ 4 & & -1 & 0 & 0 \\ 5 & & +1 & 0 & 0 \\ 6 & & 0 & +1 & 0 \\ 7 & & 0 & 0 & +1 \end{array}$$


⑦ Augmented loop Incidence Matrix $\div [C]$



$\Rightarrow A, B, C, D$ are the imaginary loops

⇒

		Open loops				Basic loop		
		A	B	C	D	E	F	G
Branches	1	+1				0	+1	0
	2		+1			+1	-1	+1
	3			+1		-1	0	-1
	4				+1	-1	0	0
	5	0	0	0	0	+1	0	0
	6	0	0	0	0	0	+1	0
	7	0	0	0	0	0	0	+1

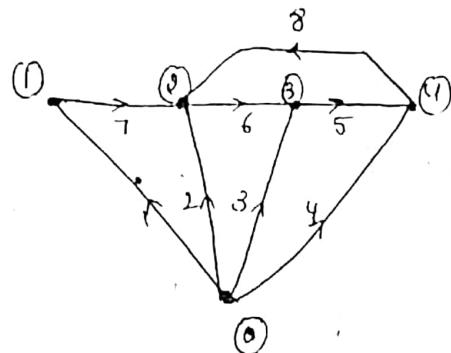
⇒

		Open loops		Basic loops	
		U_b	C_b	U_e	C_e
Links	0				

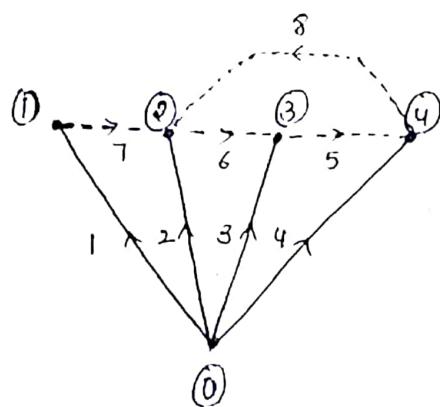
- * An Open loop is defined as a path between adjacent loads connected by a branch.
- * The orientation of an open loop is same as that of the associated branch.

Problems

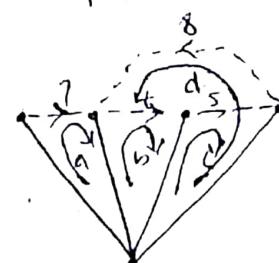
- ① Show the Basic loops and Basic cutsets for the graph shown below. and verify any relation between them.



⇒ Consider the tree having branches 1, 2, 3, 4



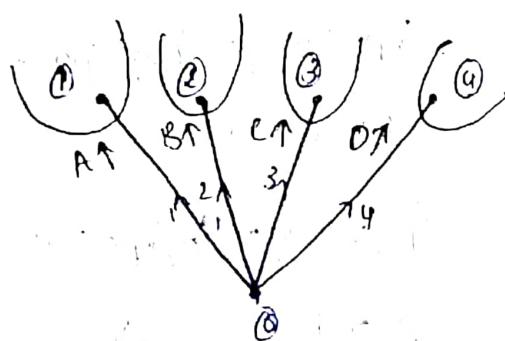
$$\text{Basic loops} = l = 4$$



$$b = n - 1 = 5 - 1 = 4$$

$$l = e - b = 8 - 4 = 4$$

⇒ Basic cutsets = b = 4

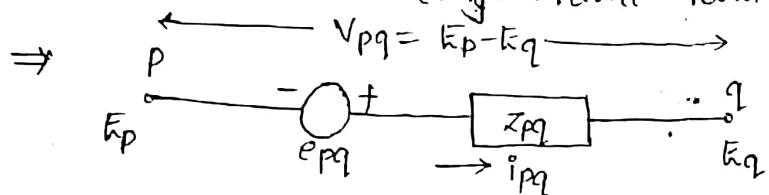


$$\text{Basic cutsets} = \text{branches} = \text{no. of links} = 4$$

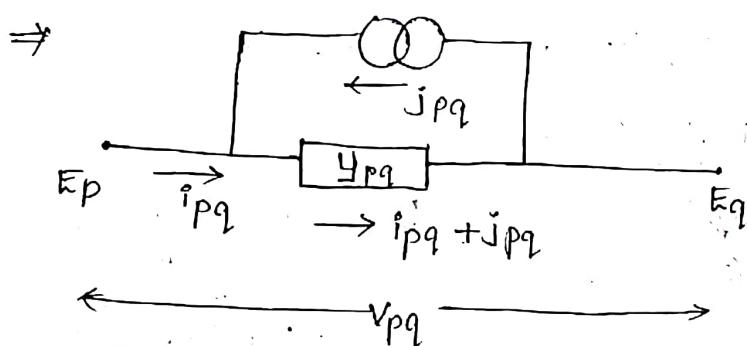
Primitive Network

* A set of unconnected elements is "Primitive Network". (or) A set of uncoupled elements is called "Primitive Network".

* The Network components represented both in impedance form and a admittance form.



\therefore Impedance form



\therefore Admittance form

* In Impedance form $V_{pq} + e_{pq} - i_{pq}Z_{pq} = 0$

$$V_{pq} + e_{pq} = i_{pq} Z_{pq} \quad \text{--- (1)}$$

$$\bar{V} + \bar{e} = [\bar{Z}] \bar{i}$$

* In Admittance form $i_{pq} + j_{pq} - Y_{pq}V_{pq} = 0$

$$i_{pq} + j_{pq} = Y_{pq}V_{pq} \quad \text{--- (2)}$$

$$\bar{i} + \bar{j} = [Y] \bar{V}$$

* Where V_{pq} is voltage across the elements Pq
 e_{pq} is source voltage in series with element Pq

Pq

i_{pq} is current through element PQ

j_{pq} is source & current in parallel with element PQ

Z_{pq} is self Impedance

Y_{pq} is self Admittance.

* The performance equation of primitive network can be derived from eq(1) & (2) by expressing the variables and as vectors and parameters as matrices.

* In Impedance form

$$\bar{V} + \bar{E} = [Z] \bar{I} \quad \text{--- (1)}$$

* In Admittance form

$$\bar{I} + \bar{J} = [Y] \bar{V} \quad \text{--- (2)}$$

* These network equations can be formed in the reference of i) Bus frame of reference.

ii) Loop frame of reference.

iii) Branch frame of reference.

* In the above equations the diagonal elements of the matrices $[Z]$ & $[Y]$ is self impedance i.e., $Z_{ppq,pq}$ & Self Admittance i.e., $y_{ppq,pq}$.

* The half-diagonal elements are Z_{pqrs} (or) y_{pqrs} .

* Matrix of Admittance $[Y]$ can be obtained by inverting the matrix of Impedance $[Z]$.

$$[Y] = [Z]^{-1}$$

* $[Z], [Y]$ are diagonal matrices if no mutual coupling between the elements.

\Rightarrow from eq ①

$$V_{pq} + E_{pq} = i_{pq} Z_{pq}$$

$$Y_{pq} V_{pq} + Y_{pq} E_{pq} = i_{pq}$$

Sub i_{pq} in eq ②

$$i_{pq} + j_{pq} = Y_{pq} V_{pq}$$

$$Y_{pq} V_{pq} + Y_{pq} E_{pq} + j_{pq} = Y_{pq} V_{pq}$$

$$\boxed{j_{pq} = -Y_{pq} E_{pq}}$$

* The parallel source current in Admittance form is related to the ^{series} source voltage in impedance form by using equation $j_{pq} = -Y_{pq} e_{pq}$

Bus

Formation of Network by Bus frame of Reference

$$* \bar{E}_{BUS} = \bar{Z}_{BUS} \cdot \bar{I}_{BUS}$$

$$* \bar{Y}_{BUS} = \bar{Y}_{BUS} \bar{E}_{BUS}$$

where \bar{E}_{BUS} is vector of Bus voltages measured with respect to the reference voltages.

\bar{I}_{BUS} is vector of impressed Bus currents

\bar{Z}_{BUS} is Bus Impedance Matrix whose elements are open circuit driving point & transfer impedances.

\bar{Y}_{BUS} is Bus Admittance Matrix whose elements are short circuit driving point & transfer Admittances.

* There are $(n-1)$ no. of nodal equations
where n = no. of nodes.

Branch frame of Reference :-

* 'b' independent branch equations

$$\bar{E}_{BR} = Z_{BR} \bar{I}_{BR}$$

$$\bar{P}_{BR} = Y_{BR} \bar{E}_{BR}$$

* where

E_{BR} = vector of voltages across branches

I_{BR} = Vector of currents through branches

Z_{BR} = Branch Impedance Matrix

Y_{BR} = Branch Admittance Matrix

Loop frame of Reference :-

* 'l' independent Loop equations

$$\bar{E}_{loop} = Z_{loop} \bar{I}_{loop}$$

$$\bar{P}_{loop} = Y_{loop} \bar{E}_{loop}$$

* where

E_{loop} = Vector of Voltages of basic loops

I_{loop} = Vector of Basic Loop current

Z_{loop} = Loop Impedance Matrix

Y_{loop} = Loop Admittance matrix

Bus Admittance & Bus Impedance Matrix

* The Bus Admittance Matrix $[Y_{kj}]$ can be obtained by using Bus Impedance Matrix $[A]$.

* The performance equation of primitive network

$$\bar{I} + \bar{j} = [Y] \bar{V} \quad \text{---(1)}$$

* Premultiply by A^t .

$$A^t \bar{I} + A^t \bar{j} = A^t [Y] \bar{V} \quad \text{---(1)}$$

* Since the Matrix A shows the incidence of elements to Buses.

* Where A^t is a vector in which each element is Algebraic sum of the current through the network element terminating at Bus.

* With KCL The Algebraic sum of the currents at the node is zero.

$$\therefore A^t \bar{I} = 0 \quad \text{---(2)}$$

* Similarly $A^t \bar{j}$ gives the Algebraic sum of the source currents at each bus and equals the vector impressed bus currents.

$$\bar{I}_{\text{BUS}} = A^t \cdot \bar{j} \quad \text{---(3)}$$

* Now $I_{\text{BUS}} = A^t [Y] \bar{V} \quad \text{---(4)}$ By substituting eq(2) & eq(3) in eq(1).

* Power into the network is

$(I_{\text{BUS}}^*)^T E_{\text{BUS}}$ and the sum of the power in the primitive network is

$$(j^*)^T \bar{V}$$

* The power in the primitive and interconnected network must be equal i.e., the transformation of variable must be power invariant.

* Hence

$$(Y_{BUS}^*)^T E_{BUS} = (j^*)^T \bar{V} \quad \text{--- (5)}$$

* From Eq (3)

$$(E_{BUS}^*)^T = (j^*)^T A^*$$

$$\text{where } A^* = A$$

* Now From Eq (5)

$$(j^*)^T A E_{BUS} = (j^*)^T \bar{V} \quad \forall j$$

$$\bar{V} = A E_{BUS} \quad \text{--- (6)}$$

* Substitute in eq (4)

$$I_{BUS} = A^T [y] A E_{BUS}$$

$$I_{BUS} = Y_{BUS} E_{BUS}$$

$$[\text{where } Y_{BUS} = A^T [y] A]$$

* Bus Incidence Matrix is a singular matrix

$A^T [y] A$ is a singular transfer matrix is Y_{BUS}

$$\therefore Z_{BUS} = Y_{BUS}^{-1} = [A^T [y] A]^{-1}$$

$$\boxed{\begin{aligned} Y_{BUS} &= A^T [y] A \\ \therefore Z_{BUS} &= [A^T [y] A]^{-1} \end{aligned}}$$

Branch Admittance & Branch Impedance Matrix

* The Branch Admittance Matrix Y_{BR} can be obtained by Basic Cutset Incidence Matrix.

* The Performance equation is

$$i + j = [y] \bar{v}$$

* Pre multiply with the above B^t

$$B^t i + B^t j = B^t [y] \bar{v} \quad \text{--- (1)}$$

* By using KCL $B^t i = 0$ since $B^t i$ is the Algebraic Sum entering into the Sub network.

$$\mathfrak{I}_{BR} = B^t j \quad \text{--- (2)}$$

* Substitute in above equation.

$$\mathfrak{I}_{BR} = B^t [y] \bar{v} \quad \text{--- (3)}$$

* The power into the network ~~is~~ = sum of power in

$$(I_{BR}^*)^t E_{BR} = (j^*)^t \bar{v}$$

primitive
nlw

$$(j^*)^t B^* E_{BR} = (j^*)^t \bar{v}$$

$(B^* = B)$

$$\bar{v} = B E_{BR}$$

$$\mathfrak{I}_{BR} = B^t [y] B E_{BR}$$

* let $Y_{BR} = B^t [y] B$

$$\mathfrak{I}_{BR} = Y_{BR} E_{BR}$$

$$* Z_{BR} = Y_{BR}^{-1} = [B^t [y] B]^{-1}$$

$$\boxed{\begin{aligned} Y_{BR} &= B^t [y] B \\ \therefore Z_{BR} &= [B^t [y] B]^{-1} \end{aligned}}$$

Loop Admittance \times loop Impedance \times Matrix \dagger

* The $[Z_{loop}]$ & $[Y_{loop}]$ can be obtained by

Basic Loop Incidence Matrix.

$$\bar{V} + \bar{e} = [Z] \bar{i} \quad \text{--- (1)}$$

* Pre multiply with c^t

$$c^t \bar{V} + c^t \bar{e} = c^t [Z] \bar{i} \quad \text{--- (2)}$$

* By using KVL $c^t \bar{V} = 0$ since $c^t \bar{V}$ is the algebraic sum of voltages in the loop.

$$c^t \bar{e} = E_{loop} \quad \text{--- (3)}$$

* Substitute in eq (2)

$$E_{loop} = c^t [Z] \bar{i} \quad \text{--- (4)}$$

* The power in the network is equal to sum of powers in the loop network

$$(I_{loop}^*)^T E_{loop} = (I^*)^T \bar{e}$$

$$(I_{loop}^*)^T c^t \bar{e} = (I^*)^T \bar{e} \quad \text{from (3)}$$

$$(I^*)^T = (I_{loop}^*)^T c^t$$

$$\bar{i} = c^* I_{loop}$$

$$i = c I_{loop} \quad (\because c^* = c)$$

$$E_{loop} = c^t [Z] c I_{loop} \quad \text{Substitute in eq (4)}$$

$$Z_{loop} = c^t [Z] c$$

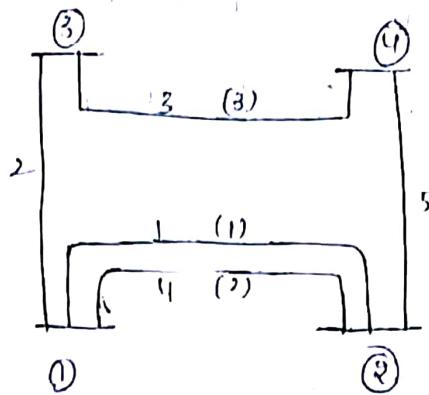
$$E_{loop} = Z_{loop} I_{loop}$$

$$Y_{loop} = Z_{loop}^{-1} = (c^t [Z] c)^{-1}$$

$$\boxed{Z_{loop} = c^t [Z] c}$$
$$\boxed{Y_{loop} = [c^t [Z] c]^{-1}}$$

	Loop	Bus	Branch
Current	$\vec{I} = C \vec{V}_{loop}$	$\vec{V}_{bus} = A^T \vec{J}$	$\vec{I}_{BR} = B^T \vec{J}$
Voltage	$\vec{V}_{loop} = C^T \vec{I}$	$\vec{V} = A \vec{E}_{bus}$	$\vec{V} = B \vec{E}_{BR}$

① Form the Incidence Matrices $[\hat{A}]$, $[A]$, $[B]$, $[\hat{B}]$, $[C]$, $[E]$ for the network shown in figure.



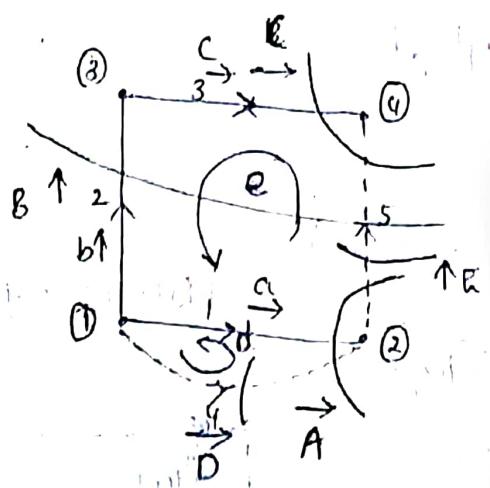
(n) Nodes = 6

(e) Elements = 5

(b) Branches = $b = (n-1) = 6-1 = 5$

(l) Links = $e-b = 5-3 = 2$

Tree: Assign directions



\Rightarrow Element node incidence matrix $[\hat{A}]$:

e \ n	(1)	(2)	(3)	(4)
1	+1	-1	0	0
2	-1	0	-1	0
3	0	0	+1	-1
4	+1	-1	0	0
5	0	+1	0	-1

$[\hat{A}] \Rightarrow$

\Rightarrow Bus Incidence Matrix $[A]$:

\Rightarrow node 1 is reference

e \ buses	(1)	(2)	(3)
1	-1	0	0
2	0	-1	0
3	0	+1	-1
4	-1	0	0
5	+1	0	1

\Rightarrow Branch path Incidence matrix $[\mathbf{R}]$:

\Rightarrow node 1 is reference

b \ Path	(2)	(3)	(4)
1	-1	0	0
2	0	-1	-1
3	0	0	-1

\Rightarrow Basic cutset matrix $[B]$:

basic no. of cutsets = no. of branches = 3

e \ col	A	B	C
1	1	0	0
2	0	1	0
3	0	0	1
4	1	0	0
5	-1	+1	+1

$[B] \Rightarrow$

⇒ Augmented Cutset Incidence matrix, $[{\hat{B}}]$

$e \backslash r$	A	B	C	D	E	
1	1					
2		1				
3			1			
4	+1	0	0	1	0	
5	-1	+1	+1	0	+1	

$\Rightarrow [{\hat{B}}]$

⇒ Basic Loop Incidence Matrix, $[c]$

$e \backslash \text{loop}$	a	b	c	d	e	
1	-1	+1				
2	0	-1				
3	0	-1				
4	+1	0				
5	0	-1				

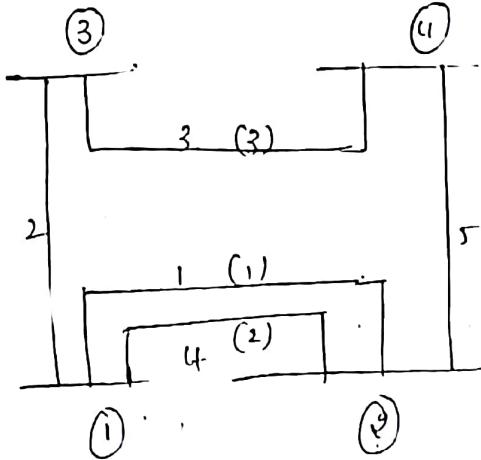
$\Rightarrow [c]$

⇒ Augment Loop Incidence matrix $[{\hat{c}}]$

$e \backslash \text{loops}$	a	b	c	d	e	
1	1	0	-1	-1	+1	
2	0	1	0	0	-1	
3	0		1	0	-1	
4	0	0	0	+1	+1	
5	0	0	0	0	0	

$\Rightarrow [{\hat{c}}]$

⑥ Form the Y_{bus} matrix $Y_{BUS}, Y_{BII}, Z_{loop}$ by
singular Transformation



Element	Bus code (P-Q)	Impedance Z_{pqpq}
1	1-2 (1)	0.6
2	1-3	0.5
3	2-4	0.5
4	1-2 (2)	0.4
5	2-4 (1)	0.2

$[Z] \Rightarrow$

e	1	2	3	4	5
1	0.6				
2		0.5			
3			0.5		
4				0.4	
5					0.2

$$[Y] = [Z]^{-1} = \begin{bmatrix} 1/0.6 & 0 & 0 & 0 & 0 \\ 0 & 1/0.5 & 0 & 0 & 0 \\ 0 & 0 & 1/0.5 & 0 & 0 \\ 0 & 0 & 0 & 1/0.4 & 0 \\ 0 & 0 & 0 & 0 & 1/0.2 \end{bmatrix}$$

$$[Y] = \begin{bmatrix} 1 & 2 & 3 & 4 & 5 \\ 2 & 0 & 0 & 0 & 0 \\ 3 & 0 & 2 & 0 & 0 \\ 4 & 0 & 0 & 2.5 & 0 \\ 5 & 0 & 0 & 0 & 5 \end{bmatrix}$$

$$\Rightarrow Y_{Bus} = A^T [Y] A$$

$$= \begin{bmatrix} -1 & 0 & 0 & -1 & +1 \\ 0 & -1 & -1 & 0 & 0 \\ 0 & 0 & -1 & 0 & -1 \end{bmatrix}_{3 \times 5} \times \begin{bmatrix} 1.67 & 0 & 0 & 0 & 0 \\ 0 & 2 & 0 & 0 & 0 \\ 0 & 0 & 2 & 0 & 0 \\ 0 & 0 & 0 & 2.5 & 0 \\ 0 & 0 & 0 & 0 & 5 \end{bmatrix}_{5 \times 5} \times \begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & +1 & -1 \\ -1 & 0 & 0 \\ -1 & 0 & -1 \end{bmatrix}_{5 \times 3}$$

$$Y_{Bus} = \begin{bmatrix} -1.67 & 0 & 0 & -2.5 & 5 \\ 0 & -2 & 2 & 0 & 0 \\ 0 & 0 & -2 & 0 & -5 \end{bmatrix}_{3 \times 5} \begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & +1 & -1 \\ -1 & 0 & 0 \\ -1 & 0 & -1 \end{bmatrix}_{5 \times 3}$$

$$Y_{Bus} = \begin{bmatrix} -1.67 & 0 & -5 \\ 0 & 4 & -2 \\ -5 & -2 & 7 \end{bmatrix}_{3 \times 3} \begin{bmatrix} 1.67 \\ 2.5 \\ 5 \end{bmatrix}_{3 \times 1}$$

$$\Rightarrow Y_{B,1} = B^T [Y] B$$

$$= \begin{bmatrix} 1 & 0 & 0 & 1 & -1 \\ 0 & 1 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 & 1 \end{bmatrix}_{3 \times 5} \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 2 & 0 & 0 \\ 0 & 0 & 0 & 2.5 & 0 \\ 0 & 0 & 0 & 0 & 5 \end{bmatrix}_{5 \times 5} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \\ -1 & 1 & 1 \end{bmatrix}_{5 \times 3}$$

$$= \begin{bmatrix} 1.67 & 0 & 0 & 2.5 & -5 \\ 0 & 2 & 0 & 0 & 5 \\ 0 & 0 & 2 & 0 & 5 \end{bmatrix}_{3 \times 5} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \\ -1 & 1 & 1 \end{bmatrix}_{5 \times 3}$$

$$Y_{RN} = \begin{bmatrix} 9.11 & -5 & -5 \\ -5 & 7 & 5 \\ -5 & 5 & 7 \end{bmatrix}_{3 \times 3}$$

$$\Rightarrow Z_{loop} = C^{-1} [Z] C^{-1}$$

$$= \begin{bmatrix} 1 & 0 & 0 & | & 0 \\ 1 & -1 & 1 & | & 1 \\ 1 & 1 & 1 & | & 1 \end{bmatrix}_{3 \times 5} \begin{bmatrix} 0.6 & 0 & 0 & 0 & 0 \\ 0 & 0.5 & 0 & 0 & 0 \\ 0 & 0 & 0.5 & 0 & 0 \\ 0 & 0 & 0 & 0.4 & 0 \\ 0 & 0 & 0 & 0 & 0.2 \end{bmatrix}_{5 \times 5} \begin{bmatrix} -1 & 1 \\ 0 & -1 \\ 0 & -1 \\ 1 & 0 \\ 0 & 1 \end{bmatrix}_{3 \times 2}$$

$$= \begin{bmatrix} -0.6 & 0 & 0 & 0.4 & 0 \\ 0.6 & -0.5 & -0.5 & 0.4 & 0.2 \end{bmatrix}_{2 \times 5} \begin{bmatrix} -1 & 1 \\ 0 & -1 \\ 0 & -1 \\ 1 & 0 \\ 0 & 1 \end{bmatrix}_{5 \times 2} \begin{bmatrix} 0.6 & 0.3 \\ 0.5 & 0.1 \\ 0.4 & 0.2 \end{bmatrix}_{3 \times 2}$$

$$= \begin{bmatrix} 1 & -0.6 \\ -0.6 & 1.8 \end{bmatrix}_{2 \times 2}$$

$$Z_{loop} = \begin{bmatrix} 1 & -0.6 \\ -0.6 & 1.8 \end{bmatrix}_{2 \times 2}$$

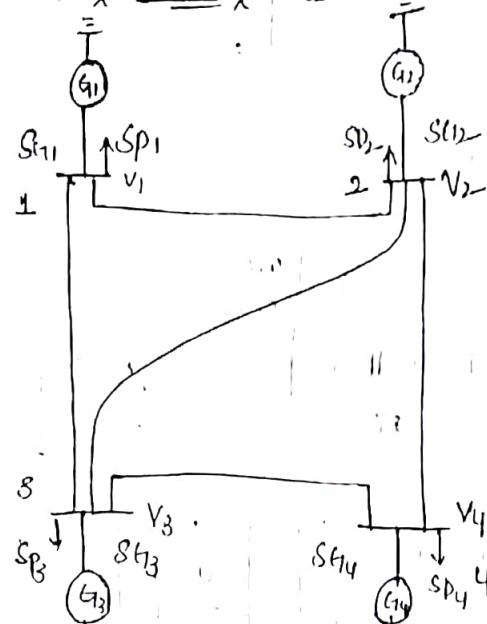
$$\Rightarrow Y_{loop} = [Z_{loop}]^{-1}$$

$$= \begin{bmatrix} 1 & -0.6 \\ -0.6 & 1.8 \end{bmatrix}^{-1}$$

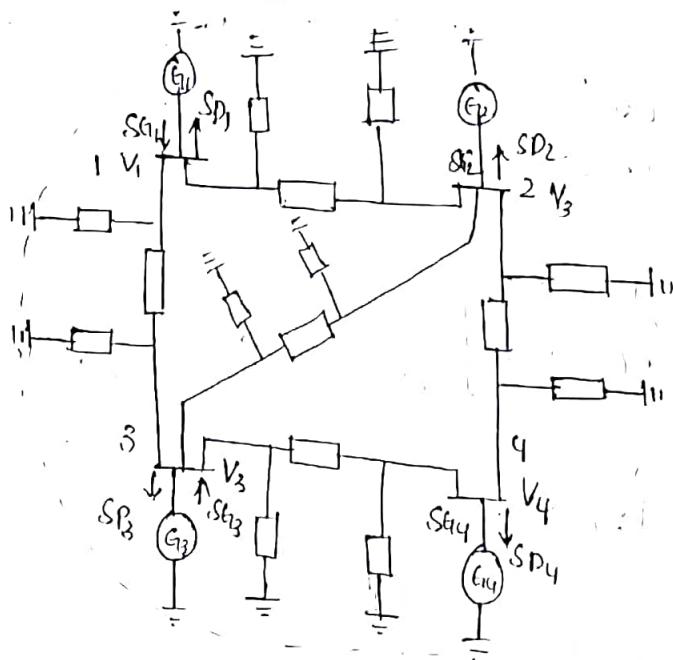
$$= \frac{1}{1.8 - 0.36} \begin{bmatrix} 1.8 & 0.6 \\ 0.6 & 1 \end{bmatrix}$$

$$\begin{array}{c} 2.6 \\ 1.2 \\ 1.0 \\ \hline 1.9 \\ 0.36 \\ 1.44 \end{array} Y_{loop} = \begin{bmatrix} 1.95 & 0.416 \\ 0.416 & 0.69 \end{bmatrix}_{2 \times 2}$$

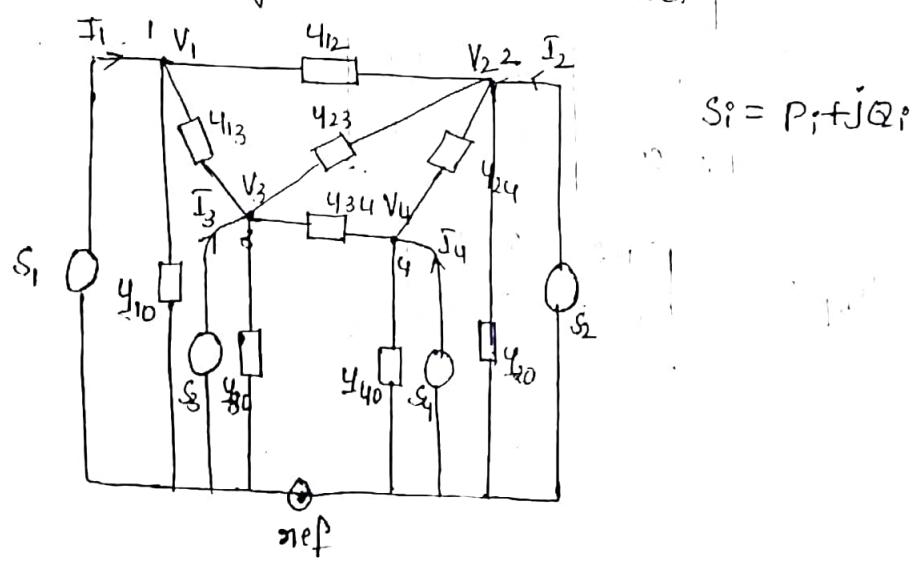
Direct Inspection Method :-



⇒ Equivalent Circuit :- [with reference & grounds]



⇒ Combining all the references



$$S_i = P_i + jQ_i$$

At i th bus the net complex power is injected into the bus is given by

$$\begin{aligned} S_i &= \sum_j I_j^* G_{ij} \\ &= (P_{i\text{in}} - P_{D,i}) + j(P_{i\text{in}} - Q_{D,i}) \end{aligned}$$

Applying KCL at nodes 1, 2, 3 & 4

$$\underline{\underline{x}} = \text{Node 1: } I_1 = V_1 Y_{10} + (V_1 - V_2) Y_{12} + (V_1 - V_3) Y_{13}$$

$$I_1 = V_1 (Y_{10} + Y_{12} + Y_{13}) + V_2 (-Y_{12}) - V_3 (-Y_{13})$$

$$\underline{\underline{x}} = \text{Node 2: } I_2 = V_2 Y_{20} + (V_2 - V_1) Y_{12} + (V_2 - V_3) Y_{23} + (V_2 - V_4) Y_{24}$$

$$I_2 = V_2 (Y_{20} + Y_{12} + Y_{23} + Y_{24}) - V_1 Y_{12} - V_3 Y_{23} - V_4 Y_{24}$$

$$\underline{\underline{x}} = \text{Node 3: } I_3 = V_3 Y_{30} + (V_3 - V_1) Y_{13} + (V_3 - V_2) Y_{23} + (V_3 - V_4) Y_{34}$$

$$I_3 = -V_1 Y_{13} + V_3 (Y_{30} + Y_{13} + Y_{23} + Y_{34}) - V_2 Y_{23} - V_4 Y_{34}$$

$$\underline{\underline{x}} = \text{Node 4: } I_4 = V_4 Y_{40} + (V_4 - V_2) Y_{24} + (V_4 - V_3) Y_{34}$$

$$I_4 = -V_2 Y_{24} - V_3 Y_{34} + V_4 (Y_{40} + Y_{24} + Y_{34})$$

Write these equations in Matrix form.

$$\begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ I_4 \end{bmatrix} = \begin{bmatrix} Y_{10} + Y_{12} + Y_{13} & -Y_{12} & -Y_{13} & 0 \\ -Y_{12} & Y_{20} + Y_{12} + Y_{23} + Y_{34} & -Y_{23} & -Y_{24} \\ -Y_{13} & -Y_{23} & Y_{30} + Y_{13} + Y_{23} + Y_{34} & -Y_{34} \\ 0 & -Y_{24} & -Y_{34} & Y_{40} + Y_{24} + Y_{34} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \end{bmatrix}$$

It can write as follows.

$$\begin{bmatrix} \mathfrak{Y}_1 \\ \mathfrak{Y}_2 \\ \mathfrak{Y}_3 \\ \mathfrak{Y}_4 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} & Y_{13} & Y_{14} \\ Y_{21} & Y_{22} & Y_{23} & Y_{24} \\ Y_{31} & Y_{32} & Y_{33} & Y_{34} \\ Y_{41} & Y_{42} & Y_{43} & Y_{44} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \end{bmatrix}$$

$$\Rightarrow \therefore Y_{11} = Y_{10} + Y_{12} + Y_{13} ; Y_{22} = Y_{20} + Y_{12} + Y_{23} + Y_{24}$$

$$Y_{12} = Y_{21} = -Y_{12} \quad Y_{33} = Y_{30} + Y_{13} + Y_{23} + Y_{34}$$

$$Y_{23} = Y_{32} = -Y_{23}$$

$$Y_{44} = Y_{40} + Y_{24} + Y_{34}$$

$$Y_{31} = Y_{13} = -Y_{13}$$

$$Y_{14} = Y_{41} = -Y_{14} = 0$$

$$Y_{24} = Y_{42} = -Y_{24}$$

$$Y_{34} = Y_{43} = -Y_{34}$$

\Rightarrow Where Y_{ii} = Self Admittance

Y_{ik} = Mutual Admittance

$$\Rightarrow \mathfrak{Y}_i = \sum_{k=1}^n Y_{ik} V_k \quad i = 1, 2, 3, \dots, n$$

$$\Rightarrow \mathfrak{Y}_{\text{BUS}} = Y_{\text{BUS}} V_{\text{BUS}}$$

* Where Y_{BUS} is $n \times n$ matrix where n is no. of buses.

$m = n+1$ i.e., no. of nodes

* Y_{BUS} is the symmetrical matrix so only $\frac{n(n+1)}{2}$ terms are to be stored in Y_{BUS} system

* As $i \neq k$ are not connected. Y_{BUS} of large networks are very sparse. \rightarrow matrix containing more non-zero elements.

zeros] i.e., It has a large no. of zero elements.

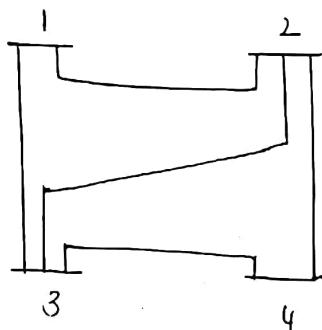
* The sparsity may be as high as 90% which reduced numerical calculation and less memory required. $V_{BUS} = Z_{BUS} I_{BUS}$

* While Y_{BUS} is a sparse matrix, Z_{BUS} is a full Matrix i.e., zero elements in the Y_{BUS} Matrix becomes non zeros in Z_{BUS} Matrix.

* Y_{BUS} is used in load flow problems and Z_{BUS} is used in short circuit study.

26/12/2016
Problem
=x=

① The fig. shows Single Line Diagram of Simple four bus system. Find Y_{BUS} by direct inspection method.



Line	R_{PU}	X_{PU}	Z_{PU}	$Y_{PU} = \frac{1}{Z_{PU}}$
1-2	0.05	0.15	$\rightarrow 0.05 + j0.15 - Z_{12}$	$\rightarrow 1-2 - j6.67 = Y_{12}$
1-3	0.10	0.30	$\rightarrow 0.10 + j0.30 - Z_{13}$	$\rightarrow 1-3 - j3 = Y_{13}$
2-3	0.15	0.45	$\rightarrow 0.15 + j0.45 - Z_{23}$	$\rightarrow 0.667 - j2 - Y_{23}$
2-4	0.10	0.30	$\rightarrow 0.10 + j0.30 - Z_{24}$	$\rightarrow 1-3 - Y_{24}$
3-4	0.05	0.15	$\rightarrow 0.05 + j0.15 - Z_{34}$	$\rightarrow 2-j6 - Y_{34}$

Sol $[Y_{BUS}]$ order is [no. of Buses x no. of Buses]

$$[Y_{BUS}]_{4 \times 4} = \begin{bmatrix} Y_{11} & Y_{12} & Y_{13} & Y_{14} \\ Y_{21} & Y_{22} & Y_{23} & Y_{24} \\ Y_{31} & Y_{32} & Y_{33} & Y_{34} \\ Y_{41} & Y_{42} & Y_{43} & Y_{44} \end{bmatrix}_{4 \times 4}$$

$$y_{11} = y_{12} + y_{13}$$

$$= 2-j6 + 1-j3$$

$$= 3-j9$$

$$y_{12} = (2-j6) = -2+j6 = y_{21}$$

$$y_{13} = (1-j3) = -1+j3 = y_{31}$$

$$y_{14} = y_{41} = 0$$

$$y_{22} = y_{21} + y_{23} + y_{24}$$

$$= +2+j6 + 0.667-j2 + 1-j3$$

$$= \cancel{-0.667+j1} = 3.667-j11$$

$$y_{23} = y_{32} = -(y_{23}) = -(0.667-j2) = -0.667+j2$$

$$y_{24} = y_{42} = -(y_{24}) = -(1-j3) = -1+j3$$

$$y_{32} = -0.667+j2$$

$$y_{33} = y_{31} + y_{32} + y_{34}$$

$$= 1-j3 + 0.667-j2 + 2-j6$$

$$= 3.667-j11$$

$$y_{34} = - (0-j1) = 0+j6$$

$$y_{41} = 0$$

$$y_{42} = -1+j3$$

$$y_{43} = 0+j1$$

$$y_{44} = y_{42} + y_{43}$$

$$= \cancel{0+j3} + \cancel{0+j1}$$

$$= 3+j9$$

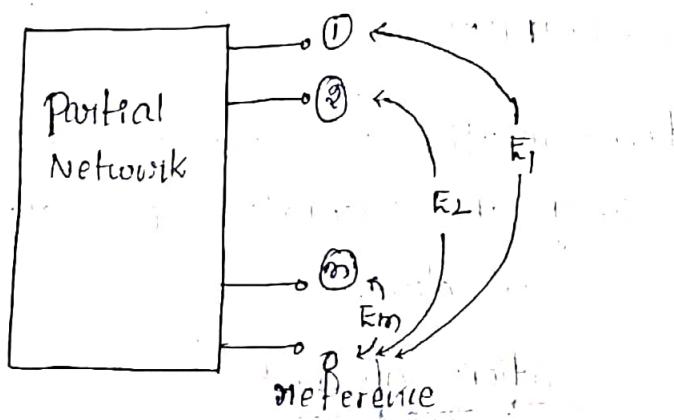
$$Y_{BUS} = \begin{bmatrix} 3-j9 & -2+j6 & -1+j3 & 0 \\ -2+j6 & 3.667-j11 & -0.667+j2 & -1+j3 \\ -1+j3 & -0.667+j2 & 3.667-j11 & -2+j6 \\ 0 & -1+j3 & -2+j6 & 3-j9 \end{bmatrix}$$

4×4

The procedure for obtaining y or z matrix

- * The procedure for obtaining y (or) z in any frame of reference requires involving inversions and multiplication which is laborious and time consuming processes.
- * For large systems involving more number of nodes if the mutual coupling exist between the elements direct inspection method is not applicable so it is not applicable to built \bar{Z}_{bus} by using an algorithm where symmetrically consider element by element for addition and build the complete network directly from element parameters and such an algorithm can be very convenient to various manipulation that may be needed when system is in operation such as addition of lines, removal of lines and change in parameters.

Algorithm for Bus Impedance Matrix



- * Assume the partial network having 'n' buses and reference node '0'.

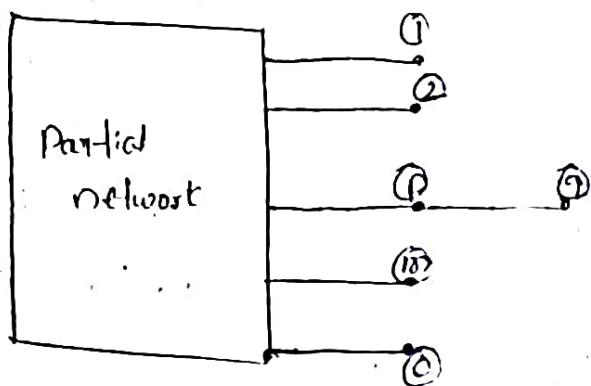
$$* \bar{E}_{bus} = Z_{bus} \times \bar{I}_{bus}$$

$\bar{E}_{\text{bus}} = m \times 1$ vector of bus voltages measured with respect to all nodes with reference

$\bar{I}_{\text{bus}} = m \times 1$ vector of impressed bus currents

* When an element PQ is added to the partial network it may be a branch (or) link.

Case 1: \Rightarrow Addition of branch



* If PQ is a branch a new bus B_{PQ} is added to the partial network & the resultant Z_{bus} is of order $(m+1) \times (m+1)$.

* The new voltage & current vectors of dimensions

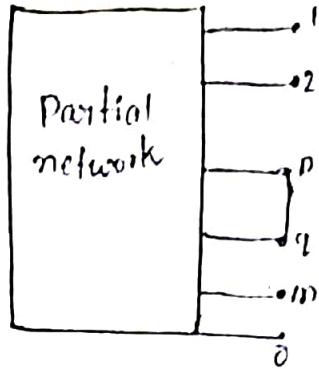
$$\bar{E}_{\text{bus}} = (m+1) \times 1$$

$$\bar{I}_{\text{bus}} = (m+1) \times 1$$

* To determine the new bus impedance matrix requires only the calculation of elements required in new row and column.

Case 2: \Rightarrow Addition of link

* If PQ is a link no new bus is added to the partial network. The dimensions are unchanged.



* All the elements of the Bus Impedance Matrix must be recalculated to include the effect of the added link.

Case 1: Addition of Branch

* The performance equation is given as

$$\bar{E}_{BUS} = Z_{BUS} \bar{I}_{BUS}$$

$$\Rightarrow \begin{bmatrix} E_1 \\ E_2 \\ E_3 \\ \vdots \\ E_p \\ \vdots \\ E_m \\ E_q \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} & \cdots & Z_{1p} & \cdots & Z_{1m} & Z_{1q} \\ Z_{21} & Z_{22} & \cdots & Z_{2p} & \cdots & Z_{2m} & Z_{2q} \\ \vdots & \vdots & \ddots & \vdots & \ddots & \vdots & \vdots \\ Z_{p1} & Z_{p2} & \cdots & Z_{pp} & \cdots & Z_{pm} & Z_{pq} \\ \vdots & \vdots & & \vdots & & \vdots & \vdots \\ Z_{m1} & Z_{m2} & \cdots & Z_{mp} & \cdots & Z_{mm} & Z_{mq} \\ Z_{q1} & Z_{q2} & \cdots & Z_{qp} & \cdots & Z_{qm} & Z_{qq} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ \vdots \\ I_p \\ \vdots \\ I_m \\ I_q \end{bmatrix} \quad \text{---(1)}$$

* The network consists of bilateral passive elements

$$\text{Hence } Z_{qi} = Z_{iq} \quad i=1,2,3 \dots m$$

* And, refers to the buses not including new bus 'q'.

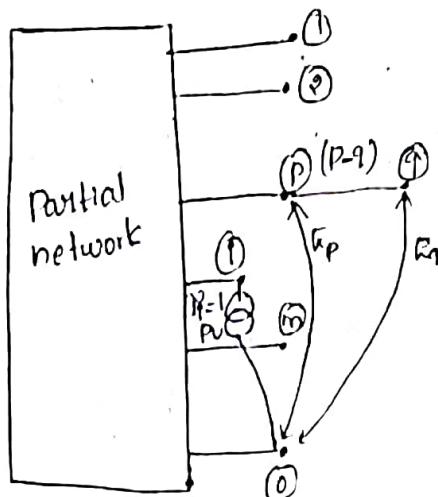
* The Added branch pq is assumed to be mutually coupled with one or more elements of partial network.

* The elements Z_{qi} can be determined by

Injecting a current at i th bus and calculating
the voltage at q th bus with respect to the

$$Z_{qi} = \frac{V_q}{I_i}$$

reference node as shown in the figure.



* Since all other bus currents as zero

$$\begin{aligned} \Rightarrow E_1 &= Z_{1i} I_i \\ E_2 &= Z_{2i} I_i \\ E_3 &= Z_{3i} I_i \\ &\vdots \\ E_p &= Z_{pi} I_i \\ E_m &= Z_{mi} I_i \\ &\vdots \\ E_q &= Z_{qi} I_i \end{aligned} \quad \left. \right\} \text{---(2)}$$

* Z_{qi} can be obtained directly by calculating I_q
by letting the current at i th bus as
IPU in above equations,

$$I_i = IPU$$

* The Bus Voltages associated with added element
and the voltage across the element is related as

* However, Δ_{pq} is not equal to zero. Since the added branch is mutually coupled to one or more elements of partial network.

$$\Delta_{pq} = E_p - E_\sigma \quad \text{---(6)}$$

where

E_p & E_σ are voltages at the buses in partial network.

Now from equations (4) & (5)

$$I_{pq} = Y_{pq} V_{pq} + V_{pq} + Y_{pq} E_\sigma V_{\sigma\sigma} = 0.$$

$$\Delta_{pq} = -\frac{Y_{pq} E_\sigma V_{\sigma\sigma}}{Y_{pq} Y_{pq}}$$

$$\text{from eq(6)} \quad V_{\sigma\sigma} = E_p - E_\sigma$$

Substituting eq (6) in it

$$\Delta_{pq} = -\frac{Y_{pq} E_\sigma (E_p - E_\sigma)}{Y_{pq} Y_{pq}}$$

Substituting this in eq(3)

from eq(3)

$$E_q = E_p - V_{pq}$$

$$= \frac{E_p + Y_{pq} E_\sigma (E_p - E_\sigma)}{Y_{pq} Y_{pq}}$$

$$E_q = E_p + \frac{Y_{pq} E_\sigma (E_p - E_\sigma)}{Y_{pq} Y_{pq}}$$

* Substitute β , k_q, k_p , ϵ & ϵ_{ext} from Eq(4) with $\beta_p = 1$

$$\Rightarrow Z_{qi} = Z_{pi} + \frac{y_{pq}\epsilon\sigma(Z_{ei} - Z_{qi})}{y_{pq}y_q} \quad p=1,2,3 \dots m \\ i \neq q$$

$$Z_{qi} = Z_{pi} + \frac{y_{pq}\epsilon\sigma(Z_{ei} - Z_{qi})}{y_{pq}y_q} \quad -\textcircled{7}$$

$p=1,2,3 \dots m$ (if mutual inductor
is absent)

$i \neq q$

$y_{pq}\epsilon\sigma = 0$

$\therefore Z_{qi} = Z_{pi} + Z_{pi,p}$

* The Element Z_{qq} can be calculated by injecting current at q th bus and calculating voltage at that bus since all the other bus currents are zero.

$E_1 = Z_{1q} I_q$

$E_2 = Z_{2q} I_q$

$E_p = Z_{pq} I_q$

$E_m = Z_{mp} I_q$

$E_q = Z_{qq} I_q$

* Letting $I_q = 1 \text{ pu}$ in above equations

* Z_{qq} can be obtained directly by calculating E_q .
The voltages at buses p & q are related as

$E_q = E_p - V_{pq} \quad \textcircled{7}$

$\Rightarrow -I_{pq} = -I_q = -1 \text{ pu} \quad \textcircled{8}$

From eq(4) & eq(8)

$i_{pq} = y_{pq}V_{pq} + y_{pq}\epsilon\sigma V_{\text{ext}} = -1$

$V_{pq} = -\left[\frac{-1 + y_{pq}\epsilon\sigma V_{\text{ext}}}{y_{pq}y_q} \right]$

$$\Rightarrow E_p = k_p - V_{pq} \quad \text{--- (3)}$$

* The currents in the elements of the network are expressed in terms of the primitive admittances and the voltages across the element.

$$\Rightarrow \begin{bmatrix} i_{pq} \\ i_{pe} \end{bmatrix} = \begin{bmatrix} y_{mm} & y_{m\sigma} \\ y_{p\sigma p\sigma} & y_{\sigma\sigma} \end{bmatrix} \cdot \begin{bmatrix} V_m \\ V_{\sigma} \end{bmatrix} \quad \text{--- (4)}$$

* Where $p\sigma$ is the fixed element subscript and refers to the added element &

* σ is the variable subscript and refers to all other elements.

* i_{pq} & V_{pq} are current through and voltage across the added elements.

* $i_{\sigma\sigma}$ & $V_{\sigma\sigma}$ are current and voltage vectors of elements of the partial network.

* y_{mpq} self admittance of the added element.

* $y_{pq\sigma}$ ^{vector of} mutual admittances between the added element $p\sigma$ and elements σ of the partial network.

* $y_{p\sigma p\sigma}$ is the transpose of vector $y_{pq\sigma}$

* $y_{\sigma\sigma\sigma}$ is the primitive admittance matrix of partial elements.

* The current in the added branch, $i_{pq}=0$ since open circuit.

$$\Rightarrow i_{pq}=0 \quad \text{--- (5)}$$

$$V_{pq} = - \left[\frac{1 + y_{pq} \rho_\sigma (E_e - E_\sigma)}{y_{pq} \rho_\sigma} \right]$$

* From Eq (1)

$$E_q = E_p - V_{pq}$$

$$E_q = E_p + \frac{1 + y_{pq} \rho_\sigma (E_e - E_\sigma)}{y_{pq} \rho_\sigma}$$

* By substituting E_q, E_p and E_e, E_σ we get

$$\boxed{Z_{qq} = Z_{pq} + \frac{1 + y_{pq} \rho_\sigma (Z_{eq} - Z_{oq})}{y_{pq} \rho_\sigma}}$$

* If there is no mutual coupling between q and other elements of partial network then the elements of $y_{pq\sigma\rho} = 0$

$$\Rightarrow \therefore \frac{1}{y_{pq\sigma\rho}} = Z_{pq\sigma\rho}$$

$$Z_{qi} = Z_{pi} \quad i=1, 2, \dots, m \\ i \neq q$$

$$\boxed{Z_{qq} = Z_{pq} + Z_{pq\sigma\rho}} \quad - \textcircled{10}$$

* If there is no mutual coupling and p is the reference bus.

$$\Rightarrow Z_{pi} = 0 \quad \text{for all the values of } i = 1, 2, \dots, m \\ i \neq 2$$

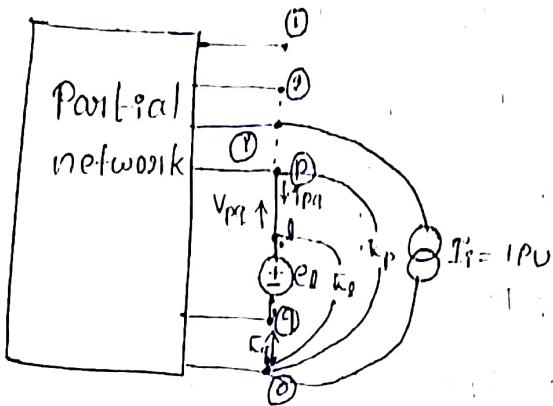
$$\Rightarrow Z_{qi} = 0 \quad i=1, 2, \dots, m \\ i \neq q$$

$$\Rightarrow Z_{pq} = 0$$

$$\Rightarrow Z_{qq} = Z_{pq\sigma\rho}$$

from \textcircled{10}

Case 2: Addition of a link



* If the added element pq is the link then the procedure for recalculating the elements of the bus impedance matrix is to connect e_p in series with the added element.

* A Voltage source e_l as shown in the figure. This creates a fictitious node 'l' which will be eliminated later. The voltage source e_l is selected such that the current through the added link is zero.

* The performance equation for partial network with the added element e_l in series with voltage source.

$$\begin{bmatrix} E_1 \\ E_2 \\ E_3 \\ \vdots \\ E_p \\ \vdots \\ E_m \\ e_l \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} & \cdots & Z_{1p} & \cdots & Z_{1m} & Z_{1l} \\ Z_{21} & Z_{22} & \cdots & Z_{2p} & \cdots & Z_{2m} & Z_{2l} \\ Z_{31} & Z_{32} & \cdots & Z_{3p} & \cdots & Z_{3m} & Z_{3l} \\ \vdots & \vdots & & \vdots & & \vdots & \vdots \\ Z_{p1} & Z_{p2} & \cdots & Z_{pp} & \cdots & Z_{pm} & Z_{pl} \\ \vdots & \vdots & & \vdots & & \vdots & \vdots \\ Z_{m1} & Z_{m2} & \cdots & Z_{mp} & \cdots & Z_{mm} & Z_{ml} \\ Z_{l1} & Z_{l2} & \cdots & Z_{lp} & \cdots & Z_{lm} & Z_{ll} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ I_3 \\ \vdots \\ I_p \\ \vdots \\ I_m \\ I_l \end{bmatrix}$$

* Now from Figure $e_l = E_l - E_q$

* The element z_{li} can be determined by injecting current at i th bus and calculating voltage at $buses l^{th}$ node with respect to bus q :

* Since all other bus current is equal to zero

$$E_k = Z_k I_i \quad k=1,2,3 \dots m$$

$$E_l = Z_l I_i$$

* Letting $I_p = 1 \text{ pu}$, z_{li} can be obtained directly by calculating E_l .

* The series voltage source E_l is

$$E_l = E_p - E_q - V_{pl} \quad [\text{Here } V_{pl} = V_{pq}]$$

* Since $i_{pq} = 0$, the element P_l can be treated as a branch.

$$\therefore i_{pl} = g_{ppl} \bar{V}_{pl} + g_{pel} \bar{V}_{el}$$

$$[i_{pl} = i_{pq} = 0]$$

$$\therefore V_{pl} = \frac{-g_{pel} V_{el}}{g_{ppl}}$$

We can write

$$\because [P_l = P_q]$$

$$g_{pel} = g_{pqel}$$

$$g_{ppl} = g_{pqpl}$$

$$\Rightarrow V_{pl} = \frac{-g_{pqel} V_{el}}{g_{pqpl}}$$

$$\therefore z_{li} = Z_{pi} - Z_{qi} + \frac{g_{pqel} (Z_{ei} - Z_{qi})}{g_{pqpl}}$$

$i=1, 2, 3 \dots m$
 $i \neq l$

* The element z_{pq} can be calculated by injecting the current at p th bus with bus 'q' as reference and calculating the voltage at p th bus with respect to bus 'q'.

* Since All the bus current are zero

$$k_k = z_{k0} \varphi_0$$

$$\varphi_1 = z_{p0} \varphi_0$$

$$\Psi_q^e \text{ Now } i_{p1} = -\varphi_p = -1$$

* The current in terms of primitive admittances and voltage in terms of

$$i_{pl} = g_{ppl} \varphi_{pl} + g_{plq} \varphi_{pq} = -1$$

$$\varphi_{pl} = - \left[\frac{1 + g_{plq} \varphi_{pq}}{g_{ppl}} \right]$$

$$\therefore g_{plq} = g_{pq} \varphi_{pq}$$

$$g_{plpl} = g_{pq} \varphi_{pq}$$

$$\therefore \varphi_{pl} = - \left[\frac{1 + g_{pq} \varphi_{pq}}{g_{plpl}} \right]$$

$$* z_{pl} = z_{pl} + z_{q,p} + \frac{1 + g_{pq} \varphi_{pq} (x_{pl} - z_{pl})}{y_{pq}}$$

* If there is no mutual coupling then the element

$$g_{pq} \varphi_{pq} = 0$$

$$\frac{1}{g_{pq}} = j_{pq}$$

$$* z_{pl} = z_{pi} - z_{qi}, \quad i=1, 2, 3, \dots, m$$

$$z_{pl} = z_{pl} - z_{qi} + j_{pq}$$

* If there is no mutual coupling & no preference

$$Z_{pi} = 0$$

$$Z_{di} = Z_{pi} - Z_{qi}$$

$$Z_{pi} = 0$$

$$Z_{di} = -Z_{qi} + Z_{pi}$$

* Now it remains to calculate the required Bus Impedance matrix to include the effect of Added Link.

* The fictitious node i is eliminated by short-circuiting the source voltage source. L.H.S.

$$E_{BUS} = Z_{BUS} P_{BUS} + Z_{ij} P_i \quad (i)$$

$$\text{Now } P_i = Z_{ij} P_{BUS} + Z_{ii} P_i = 0 \quad (ii)$$

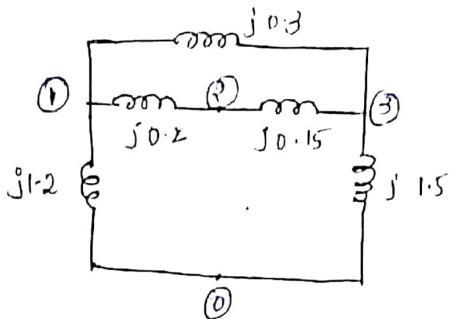
* By solving (i) & (ii)

$$E_{BUS} = \left(Z_{BUS} - \frac{Z_{ii} Z_{ij}}{Z_{ii}} \right) P_{BUS} = V_{pi}$$

$$* Z_{BUS} (\text{modified}) = Z_{BUS} (\text{before modified}) - \frac{Z_{pi} Z_{qi}}{Z_{ii}}$$

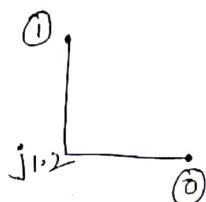
$$* Z_{ij} (\text{new}) = Z_{ij} (\text{old}) - \frac{Z_{pi} Z_{qi}}{Z_{ii}}$$

Problem:
 ① Form the Zbus for the following network.



Step 1:

Step ①:
 [We are adding element in reference & 1st bus]
 * Add Element(1) between 1st node and reference.



$$P=0, Q=1$$

which is a branch & no. mutual coupling.

$$Z_{qi} = Z_{pi} + \frac{Y_{pq}e\sigma(Z_{qi} - Z_{qi})}{Y_{pq}Y_p}$$

As no mutual coupling, $Y_{pq}e\sigma = 0$

$$Z_{qi} = Z_{pi}$$

$$Z_{qi} = Z_{pi} = 0 \quad (\text{As reference is } P)$$

$$Z_{1i} = Z_{0i} = 0$$

$$\Rightarrow i=0$$

$$Z_{10} = Z_{01} = 0$$

$$\Rightarrow q=1$$

$$Z_{11} = Z_{qq} = Z_{pq} + Z_{pq}Y_p \\ = Z_{01} + j1.2$$

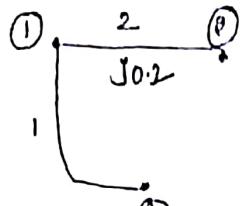
$$= j1.2$$

$$\therefore Z_{BUS} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \\ 1 & j1.2 \end{bmatrix}$$

Step 2: Adding element between 1st & 2nd bus

$$P=1, Q=2$$

Added element is branch



$\delta_{pqrs} = 0$ [The branch has no mutual coupling]

$$Z_{pqrs} = Z_{12} = j0.2$$

$$Z_{\text{BUS}} = \begin{bmatrix} j1.2 & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix}$$

$$\text{We know } Z_{11} = j1.2$$

$$\text{Now } Z_{qi} = Z_{pi}$$

$$Z_{qi} = Z_{pi}$$

$$i=1 \Rightarrow Z_{q1} = Z_{p1}$$

$$Z_{12} = Z_{21} = Z_{11}$$

$$Z_{12} = Z_{21} = Z_{11} = j1.2$$

$$\text{Now } Z_{qq} = Z_{pq} + \frac{1}{\delta_{pqrs}}$$

$$Z_{qq} = Z_{pq} + \frac{1 + \delta_{pqrs} (Z_{p1} - Z_{q1})}{\delta_{pqrs}}$$

$$= Z_{pq} + \frac{1}{\delta_{pqrs}}$$

$$Z_{qq} = Z_{12} + \frac{1}{\delta_{1212}}$$

$$= Z_{12} + Z_{1212}$$

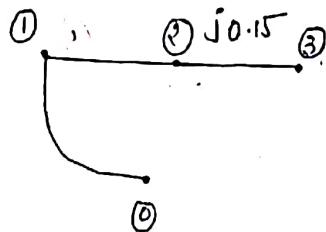
$$= Z_{11} + j0.2$$

$$= j1.2 + j0.2$$

$$= j1.4$$

$$Z_{BUS} = \begin{bmatrix} 1 & & \\ & 2 & \\ & & 3 \end{bmatrix} \begin{bmatrix} j1\cdot1 & j1\cdot2 \\ j1\cdot2 & j1\cdot4 \end{bmatrix}$$

Step 3:



The element is added in between node 1 as
a branch

$$\text{Now } P=2, Q=3$$

1 2 3

$$Z_{BUS} = \begin{bmatrix} 1 & & \\ & 2 & \\ & & 3 \end{bmatrix} \begin{bmatrix} j1\cdot2 & j1\cdot2 & z_{13} \\ j1\cdot2 & j1\cdot4 & z_{23} \\ z_{13} & z_{23} & z_{33} \end{bmatrix}$$

$$\text{Now } Z_{qi} = Z_{pi} \Rightarrow z_{31} = z_{21}$$

$$i=1,2$$

$$i=1 \quad z_{31} = z_{21} = j1\cdot2$$

$$z_{31} = z_{13} = j1\cdot2$$

$$i=2 \quad z_{32} = z_{22} = j1\cdot4$$

$$z_{32} = z_{23} = j1\cdot4$$

$$\text{Now } Z_{qq} = Z_{pp} + \frac{1}{y_{pq} p_q}$$

$$z_{33} = z_{23} + \frac{1}{y_{23} p_3}$$

$$= j1\cdot4 + \bar{y}_{23} p_3$$

$$= j1\cdot4 + j0.15$$

$$= j1\cdot55$$

$$Z_{BUS} = \begin{bmatrix} 1 & & \\ & 2 & \\ & & 3 \end{bmatrix} \begin{bmatrix} j1\cdot2 & j1\cdot2 & j1\cdot2 \\ j1\cdot2 & j1\cdot4 & j1\cdot4 \\ j1\cdot2 & j1\cdot4 & j1\cdot55 \end{bmatrix}$$

Step 4:

$\Rightarrow x =$ Adding element in between reference & 3rd bus

Now $P=0$ & $Q=3$

Added element is link

w.k.t

$$Z_{di} = Z_{pi} - Z_{qi} + \frac{g_{pq}e_0 (Z_{ei} - Z_{qi})}{Y_{pq} Y_{pq}}$$

$$Z_{di} = Z_{pi} - Z_{qi}$$

$$i = 1, 2, 3$$

$$Z_{BUS} =$$

$$Z_{d1} = Z_{D1} - Z_{31}$$

$$= 0 - j1.2$$

$$= -j1.2 = Z_{d1}$$

$$Z_{d2} = Z_{D2} - Z_{32}$$

$$= 0 - j1.4$$

$$= -j1.4 = Z_{d2}$$

$$Z_{d3} = Z_{D3} - Z_{33}$$

$$= 0 - j1.55$$

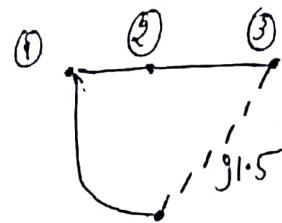
$$= -j1.55 = Z_{d3}$$

$$Z_{dl} = Z_{pl} - Z_{ql} + \frac{1}{Y_{pq} Y_{pq}}$$

$$= Z_{Dl} - Z_{3l} + Z_{D3} Z_{33}$$

$$= 0 + j1.55 + j1.5$$

$$= j3.05$$



~~Step 5~~

$$Z_{BUS} (\text{new}) = Z_{BUS} (\text{old}) - \frac{Z_{Pf} Z_{Qf}}{Z_{Df}}$$

$$\frac{[Z_{Pf}][Z_{Qf}]}{Z_{Df}} = \frac{1}{Z_{Df}} \begin{bmatrix} Z_{11} \\ Z_{22} \\ Z_{33} \\ Z_{12} \\ Z_{21} \\ Z_{13} \\ Z_{31} \end{bmatrix} \begin{bmatrix} Z_{11} & Z_{12} & Z_{13} \\ Z_{21} & Z_{22} & Z_{23} \\ Z_{31} & Z_{32} & Z_{33} \end{bmatrix}$$

$$= \frac{1}{j3.05} \begin{bmatrix} -j1.2 \\ -j1.4 \\ -j1.55 \end{bmatrix} \begin{bmatrix} -j1.2 & -j1.4 & -j1.55 \end{bmatrix}$$

$$= \frac{1}{j3.05} \begin{bmatrix} -5.8025 \end{bmatrix}$$

$$= \frac{1}{j3.05} \begin{bmatrix} -1.44 & -1.68 & -1.86 \\ -1.68 & -1.96 & -2.17 \\ -1.86 & -2.17 & -2.40 \end{bmatrix}$$

$$= \begin{bmatrix} j0.472 & j0.5508 & j0.609 \\ j0.5508 & j0.642 & j0.7114 \\ j0.609 & j0.7114 & j0.786 \end{bmatrix}$$

$$Z_{BUS} (\text{new}) = \begin{bmatrix} j1.2 & j1.2 & j1.4 \\ j1.2 & j1.4 & j1.4 \\ j1.2 & j1.4 & j1.55 \end{bmatrix} - \begin{bmatrix} j0.472 & j0.5508 & j0.609 \\ j0.5508 & j0.642 & j0.7114 \\ j0.609 & j0.7114 & j0.786 \end{bmatrix}$$

$$Z_{BUS} (\text{new}) = \begin{bmatrix} j0.728 & j0.692 & j0.591 \\ j0.692 & j0.758 & j0.59 \\ j0.591 & j0.659 & j0.763 \end{bmatrix}$$

Step 5 ~~+~~ Add Element in between 1 & 3
~~= x =~~

$$Z_{di} = Z_{pi} - Z_{qi} + \frac{g_{pq}(Z_{ei} - Z_{ci})}{Z_{pq} Z_{ci}}$$

$$= Z_{pi} - Z_{qi}$$

for 12,3

$$Z_{11} = Z_{11} - Z_{12}$$

$$= J0.728 - J0.591$$

$$= J0.137 + J0.591$$

$$Z_{12} = Z_{12} - Z_{21}$$

$$= J0.629 - J0.589$$

$$= J0.058 + J0.589$$

$$Z_{13} = Z_{13} - Z_{23}$$

$$= J0.59 - J0.763$$

$$= J0.172 + J0.763$$

$$Z_{11} = Z_{11} - Z_{21} + \frac{1}{Z_{22}}$$

$$= Z_1 - Z_{21} + J0.131$$

$$= J0.127 + J0.172 + J0.03$$

$$= J0.432$$

$$= J0.599$$

$$Z_{\text{bus}}(\text{new}) = \left| \frac{Z_{\text{bus}}(\text{old}) - \frac{Z_{11}Z_{22}}{Z_{21}}} {Z_{21}} \right|$$

$$\frac{Z_{11}Z_{22}}{Z_{21}} = \frac{1}{Z_{21}} \begin{bmatrix} Z_{11} \\ Z_{22} \\ Z_{13} \end{bmatrix} \begin{bmatrix} Z_{11} & Z_{12} & Z_{13} \\ Z_{21} & Z_{22} & Z_{23} \\ Z_{13} & Z_{23} & Z_{33} \end{bmatrix}$$

$$= \frac{1}{J0.599} \begin{bmatrix} J0.127 \\ -J0.03 \\ -J0.172 \end{bmatrix} \begin{bmatrix} J0.127 & J0.03 & -J0.172 \\ -J0.03 & -J0.009 & -J0.0516 \\ -J0.172 & -J0.0516 & -J0.29 \end{bmatrix}$$

$$= \frac{1}{J0.599} \begin{bmatrix} -0.0161 & 0.00381 & 0.218 \\ 0.00381 & -0.0009 & -0.00516 \\ 0.0218 & -0.00516 & -0.029 \end{bmatrix}$$

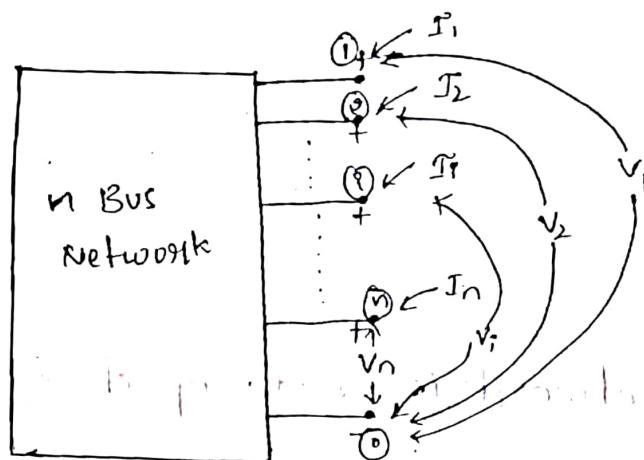
$$= \begin{bmatrix} J0.0263 & -J0.00636 & -J0.0363 \\ -J0.00636 & -J0.0015 & J0.0861 \\ -J0.0363 & J0.00636 & J0.0484 \end{bmatrix}$$

$$Z_{\text{BUS} \text{ (new)}} = Z_{\text{BUS} \text{ (old)}} - \frac{Z_{11} Z_{22}}{Z_{12}}$$

$$= \begin{bmatrix} 50.728 & j0.691 & j0.591 \\ j0.692 & j0.458 & j0.639 \\ j0.59 & j0.659 & j0.735 \end{bmatrix} - \begin{bmatrix} j0.0267 & j0.00631-j0 \\ j0.00636 & -j0 \\ j0 & j0 \end{bmatrix}$$

31/12/2016

Formulation of Z_{BUS} Matrix \div [Type Modification Method]



* Figure shows a general n-bus linear passive network - the general form of the network performance equation. it is also an easy way to determine the Z_{BUS} matrix.

$$V_{\text{BUS}} = Z_{\text{BUS}} I_{\text{BUS}}$$

Where V_{BUS} is $n \times 1$ vector of Bus voltages with respect to reference.

I_{BUS} is $n \times 1$ vector of injected bus currents.

Z_{BUS} is $n \times n$ vector of impedance of bus.

* The known voltage equation in expanded form can be written as follows:

$$\begin{bmatrix} V_1 \\ V_2 \\ \vdots \\ V_l \\ \vdots \\ V_n \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} & \cdots & Z_{1l} & \cdots & Z_{1n} \\ Z_{21} & Z_{22} & \cdots & Z_{2l} & \cdots & Z_{2n} \\ \vdots & \vdots & \ddots & \vdots & \ddots & \vdots \\ Z_{l1} & Z_{l2} & \cdots & Z_{ll} & \cdots & Z_{ln} \\ \vdots & \vdots & \ddots & \vdots & \ddots & \vdots \\ Z_{n1} & Z_{n2} & \cdots & Z_{nl} & \cdots & Z_{nn} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ \vdots \\ I_l \\ \vdots \\ I_n \end{bmatrix}$$

* If a unit current is injected into the i^{th} Bus and all the other Bus currents as zero and the open circuit bus currents at each bus is measured.

$$Z_{1i} = \frac{V_1}{I_1}$$

$$Z_{2i} = \frac{V_2}{I_2}$$

$$Z_{li} = \frac{V_l}{I_l}$$

$$Z_{ni} = \frac{V_n}{I_n}$$

* Since the network is made up of linear passive network

$$Z_{ij}^t = Z_{ji}^t$$

* By Adding impedances one at a time till all the impedances have been included with this a new matrix is produced and the order of the matrix may or may not increase depending upon whether the addition of the impedance creates a new bus or not.

* Assume an n bus partial network and there is no mutual coupling between the components of the net-

* When an impedance Z_b is added to the network, the 4 types of modifications are possible.

Z_b = Branch impedance.

$Z_{\text{bus}}(\text{old}) \longrightarrow Z_{\text{bus}}(\text{new})$

- ① Z_b is added from a new bus to the reference bus i.e., a new branch is added and the dimension of Z_{bus} goes up by 1. This is Type-1 modification.
- ② Z_b is added from a new bus to the old bus and this is Type-2 Modification.
- ③ Z_b is added from an old bus to the reference bus i.e., a new link is added and the dimension of Z_{bus} does not change and this is Type-3 Modification.
- ④ Z_b is added in between two old buses and this is Type-4 Modification.

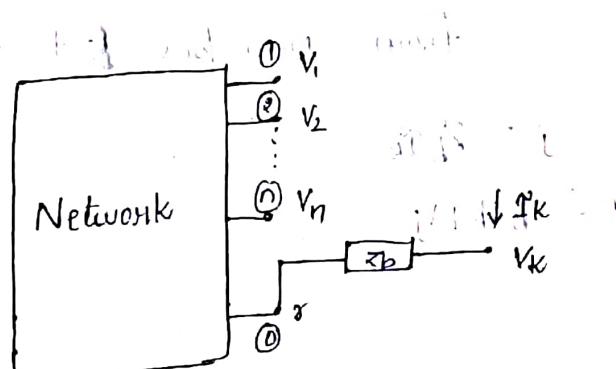
* In the following discussion

i, j are old buses

r is reference bus

k is new bus

* Type-1 Modification:



* For this new branch k

$$V_k = z_b \mathfrak{P}_k$$

$$z_{ki} = z_{ik} = 0 \quad i=1, 2, \dots, n$$

[Since there is no mutual coupling]

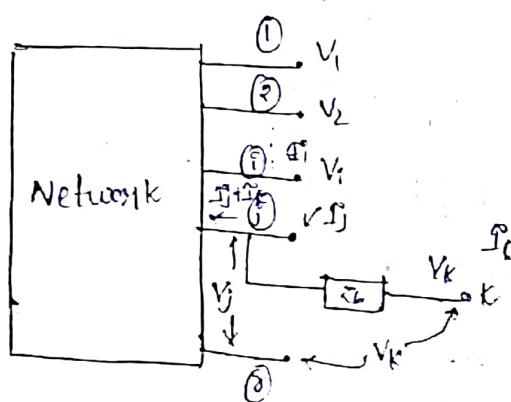
$$z_{kk} = z_b$$

* ∵ The new Bus Impedance matrix is given as

$$\begin{bmatrix} V_1 \\ V_2 \\ \vdots \\ V_n \\ V_k \end{bmatrix}_{(n+1) \times 1} = \begin{bmatrix} z_{11} & \cdots & z_{1n} & | & 0 \\ z_{21} & \cdots & z_{2n} & | & \vdots \\ \vdots & & \vdots & | & \vdots \\ z_{n1} & \cdots & z_{nn} & | & 0 \\ 0 & \cdots & 0 & | & z_{bb} \end{bmatrix}_{(n+1) \times (n+1)} \begin{bmatrix} \mathfrak{P}_1 \\ \mathfrak{P}_2 \\ \vdots \\ \mathfrak{P}_n \\ \mathfrak{P}_k \end{bmatrix}_{(n+1) \times 1}$$

$$Z_{BUS \text{ (new)}} = \begin{bmatrix} [Z_{BUS \text{ (old)}}] & 0 \\ 0 & \dots & 0 & z_{bb} \end{bmatrix} = [z_{bb}]$$

* Type-2 Modification :



* z_b is added from new bus k to the old bus j .

$$V_k - V_j = z_b \mathfrak{P}_k$$

$$V_k = z_b \mathfrak{P}_k + V_j$$

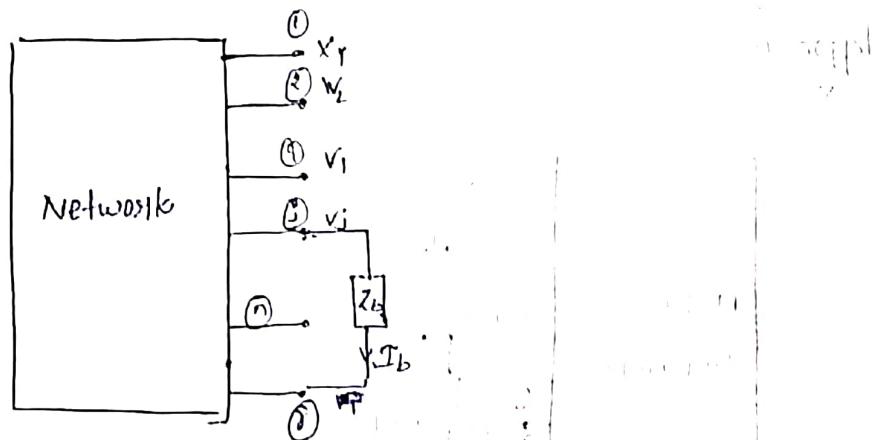
$$= Z_b I_k + z_{j1} I_1 + z_{j2} I_2 + \dots + z_{jj} (I_j + I_k) + \dots + z_{jn} I_n$$

$$V_k = z_{j1} x_1 + \dots + z_{jj} x_j + \dots + z_{jn} x_n + (z_{jj} + z_b) I_k$$

$$\begin{bmatrix} V_1 \\ V_2 \\ \vdots \\ V_n \\ V_k \end{bmatrix} = \begin{bmatrix} z_{11} & \dots & z_{1n} & | & z_{1j} \\ \vdots & & \vdots & & \vdots \\ z_{n1} & \dots & z_{nn} & | & z_{nj} \\ \hline z_{j1} & \dots & z_{jj} & z_{jn} & z_{jj} + z_b \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ \vdots \\ I_n \\ I_k \end{bmatrix}$$

$$Z_{BUS} (\text{new}) = \begin{bmatrix} Z_{BUS} (\text{old}) & \begin{bmatrix} z_{j1} \\ z_{jj} \\ z_{nj} \\ z_{jj} + z_b \end{bmatrix} \\ \hline \begin{bmatrix} z_{j1} & z_{jj} & z_{nj} & z_{jj} + z_b \end{bmatrix} \end{bmatrix}$$

* Type-3 Modification



- * Z_b is connected to old Bus from reference bus.
- * By connecting Bus k to the reference bus (or)

By setting $V_k = 0$

$$\begin{bmatrix} V_1 \\ V_2 \\ \vdots \\ V_n \\ 0 \end{bmatrix} = \begin{bmatrix} z_{11} & \dots & z_{1n} & | & z_{1j} \\ \vdots & & \vdots & & \vdots \\ z_{n1} & \dots & z_{nn} & | & z_{nj} \\ \hline z_{j1} & \dots & z_{jj} & z_{jn} & z_{jj} + z_b \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ \vdots \\ I_n \\ I_k \end{bmatrix}$$

* Eliminate I_k in the set of equations

$$0 = z_{11}I_1 + z_{12}I_2 + \dots + z_{1n}I_n + (z_{jj} + I_b) I_k$$

$$I_k = \frac{1}{z_{jj} + z_b} (z_{11}I_1 + \dots + z_{1n}I_n)$$

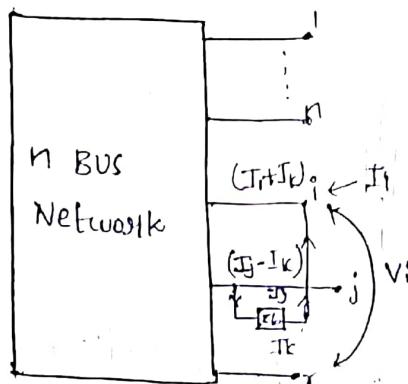
* Now $V_i = z_{ii}I_1 + z_{i2}I_2 + \dots + z_{in}I_n + z_{ij}I_k$

$$V_i = \left[z_{ii} - \frac{1}{z_{jj} + z_b} (z_{ij} \dots z_{1j}) \right] I_1 +$$

$$\left[z_{12} - \frac{1}{z_{jj} + z_b} (z_{ij} \dots z_{1j}) \right] I_2 + \dots$$

* $Z_{bus} (new) = Z_{bus} (old) - \frac{1}{z_{jj} + z_b} \begin{bmatrix} z_{1j} \\ \vdots \\ z_{nj} \end{bmatrix} \begin{bmatrix} z_{11} & \dots & z_{1j} \end{bmatrix}$

Type-4 \div
 \underline{x}



* Z_b is connected in between 2 old buses $i \& j$. The voltage at i th bus is given as

$$V_i = z_{ii}I_1 + z_{i2}I_2 + z_{i3}I_3 + \dots + z_{it}I_t + (z_{ji} - z_{ik})I_b$$

$$+ z_{ij}(I_j - I_k) + \dots + z_{in}I_n$$

The voltage at j th bus is given as.

$$V_j = z_{ji}I_1 + z_{j2}I_2 + \dots + z_{jt}I_t + (z_{ji} + z_{ik})I_b + z_{jj}(I_j - I_k) +$$

$$+ z_{jn}I_n$$

$$V_j = Z_b T_k + V_i$$

* Substituting & rearranging the equations

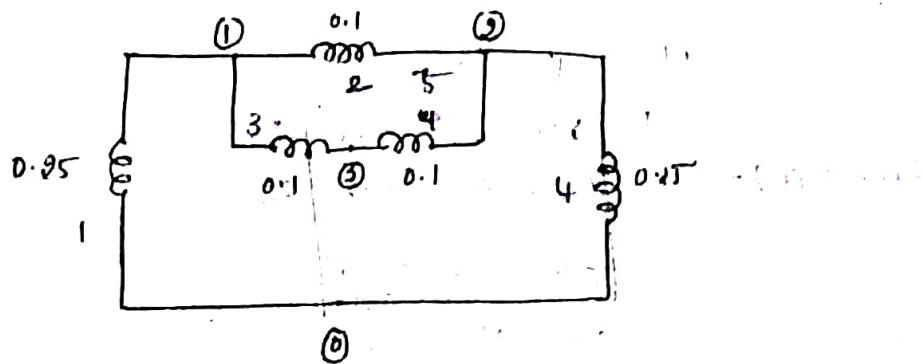
$$\Rightarrow 0 = (Z_{ii} - Z_{jj}) + \dots + (Z_{ii} - Z_{jj}) T_i + (Z_{ij} - Z_{ji}) T_j + \dots + (Z_{in} - Z_{jn}) T_n + (Z_b + Z_{ii} + Z_{jj} - Z_{ii} - Z_{jj}) T_k$$

$$\Rightarrow \begin{bmatrix} V_1 \\ V_2 \\ \vdots \\ V_n \\ 0 \end{bmatrix} = \begin{bmatrix} Z_{BUS} \\ Z_{ii} - Z_{jj} \\ \vdots \\ Z_{ni} - Z_{nj} \\ (Z_{ii} - Z_{jj})(Z_{in} - Z_{jn}) \end{bmatrix} \begin{bmatrix} T_i \\ T_j \\ \vdots \\ T_n \\ T_k \end{bmatrix}$$

$$\Rightarrow Z_{BUS(\text{new})} = Z_{BUS(\text{old})} \frac{1}{Z_b + Z_{ii} + Z_{jj} - 2Z_{ij}} \begin{bmatrix} Z_{ii} + Z_{jj} \\ \vdots \\ Z_{ni} - Z_{nj} \end{bmatrix} \begin{bmatrix} Z_{ii} - Z_{jj} \\ \vdots \\ Z_{in} - Z_{jn} \end{bmatrix}$$

Problem

For the ~~free~~ Bus network shown in figure built ~~free~~ ~~bus~~ by using Type Modification.



Sol

Step 1: Add Element b/in reference & 1st Bus
Type 1 Modification; Added element is Branch

$$Z_{bb} = 0.25 \Omega$$

$$Z_{BUS} = \begin{bmatrix} 0.25 \end{bmatrix}$$

Step 2:

$$\xrightarrow{x=1} \quad \text{Add element b/w 1st & 2nd Buses}$$

Type-2 Modification:

$$Z_b = 0.1\Omega$$

$$Z_{BUS}(\text{new}) = \begin{bmatrix} Z_{BUS}(\text{old}) & \rightarrow \\ \downarrow & Z_{BUS} + Z_b \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 2 & 1 \\ 1 & 0.25 \rightarrow 0.25 \\ 2 & 0.25 & 0.35 \end{bmatrix}$$

Step 3:

$$\xrightarrow{x=2} \quad \text{Add element b/w 1st & 3rd where } i=1 \& k=3$$

Type-2 Modification

$$Z_b = 0.1\Omega$$

$$Z_{BUS}(\text{new}) = \begin{bmatrix} 1 & 2 & 3 \\ 1 & 0.25 & 0.25 \\ 2 & 0.25 & 0.35 \\ 3 & 0.05 & 0.35 (0.25+0.1) \end{bmatrix} \begin{bmatrix} Z_{11} \\ Z_{12} \\ Z_{21} \end{bmatrix}$$

Where $i=1 \& k=3$

$$Z_{11} = Z_{11} = 0.25$$

$$Z_{12} = Z_{21} = 0.25$$

$$Z_{11} + Z_b = Z_{11} + Z_b = 0.25 + 0.1 = 0.35 \Omega$$

Step 4:

Add Element between $\textcircled{2}$ & $\textcircled{3}$ ref

Type - 3 Modification

$$Z_b = 0.05 \Omega$$

$$Z_{\text{BUS}}^{\text{(new)}} = Z_{\text{BUS}(\text{old})} - \frac{1}{z_{jj} + z_b} \begin{bmatrix} z_{1j} \\ z_{2j} \\ \vdots \\ z_{nj} \end{bmatrix} \begin{bmatrix} z_{j1} & z_{j2} & \cdots & z_{jn} \end{bmatrix}$$

$$= \begin{bmatrix} 0.25 & 0.25 & 0.25 \\ 0.25 & 0.35 & 0.25 \\ 0.25 & 0.25 & 0.35 \end{bmatrix} - \frac{1}{0.35 + 0.25} \begin{bmatrix} z_{12} \\ z_{22} \\ z_{32} \end{bmatrix} \begin{bmatrix} z_{11} & z_{13} \\ z_{21} & z_{23} \end{bmatrix}$$

where $j=2, i=0$

$$= \begin{bmatrix} 0.25 & 0.25 & 0.25 \\ 0.25 & 0.35 & 0.25 \\ 0.25 & 0.25 & 0.35 \end{bmatrix} - \frac{1}{0.6} \begin{bmatrix} 0.25 \\ 0.35 \\ 0.25 \end{bmatrix} \begin{bmatrix} 0.25 & 0.35 & 0.25 \end{bmatrix}$$

$$= \begin{bmatrix} 0.25 & 0.25 & 0.25 \\ 0.25 & 0.35 & 0.25 \\ 0.25 & 0.25 & 0.35 \end{bmatrix} - \frac{1}{0.6} \begin{bmatrix} 0.0625 & 0.0875 & 0.0625 \\ 0.0875 & 0.1225 & 0.0875 \\ 0.0625 & 0.0875 & 0.0625 \end{bmatrix}$$

$$Z_{\text{BUS}} = \begin{bmatrix} 0.1458 & 0.1041 & 0.1458 \\ 0.1041 & 0.1458 & 0.1041 \\ 0.1458 & 0.1041 & 0.2458 \end{bmatrix}$$

Step 5:

Add Element b/w $\textcircled{2}$ & $\textcircled{3}$

Type - 4 Modification

where $i=2, j=3$

$$Z_b = 0.1$$

$$Z_{BUS(111)} = \frac{1}{Z_{11} + Z_{12} + Z_{13} - Z_{11}} \begin{bmatrix} Z_{11} - Z_{12} \\ Z_{11} - Z_{13} \\ Z_{11} - Z_{11} \end{bmatrix} \begin{bmatrix} Z_{11} - Z_{11} & Z_{12} - Z_{12} & Z_{13} - Z_{13} \end{bmatrix}$$

$$\Rightarrow Z_{BUS(111)} = \frac{1}{0.11 + Z_{12} + Z_{13} - Z_{11}} \begin{bmatrix} Z_{12} - Z_{13} \\ Z_{12} - Z_{13} \\ Z_{12} - Z_{13} \end{bmatrix} \begin{bmatrix} Z_{11} - Z_{11} & Z_{12} - Z_{12} & Z_{13} - Z_{13} \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} 0.1041 & 0.1041 & 0.1041 \\ 0.1041 & 0.1458 & 0.1041 \\ 0.1041 & 0.1041 & 0.2458 \end{bmatrix} - \frac{1}{0.11 + 0.1041 + 0.2458 - 2(0.1041)} \begin{bmatrix} 0.1041 - 0.1041 \\ 0.1458 - 0.1041 \\ 0.1041 - 0.2458 \end{bmatrix}$$

$$\begin{bmatrix} 0.1041 - 0.1041 & 0.1458 - 0.1041 & 0.1041 - 0.2458 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} 0.1041 & 0.1041 & 0.1041 \\ 0.1041 & 0.1458 & 0.1041 \\ 0.1041 & 0.1041 & 0.2458 \end{bmatrix} - \frac{1}{0.2834} \begin{bmatrix} -0.0417 \\ 0.0417 \\ -0.1417 \end{bmatrix} \begin{bmatrix} -0.0417 & 0.0417 & -0.1417 \end{bmatrix}$$

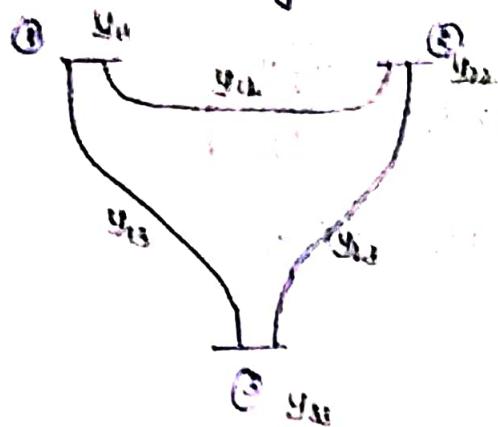
$$\Rightarrow \begin{bmatrix} 0.1041 & 0.1041 & 0.1041 \\ 0.1041 & 0.1458 & 0.1041 \\ 0.1041 & 0.1041 & 0.2458 \end{bmatrix} - \frac{1}{0.2834} \begin{bmatrix} 0.00173 & -0.00173 & 0.0059 \\ -0.00173 & 0.00173 & -0.0059 \\ 0.00390 & -0.00390 & 0.020 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} 0.1396 & 0.1102 & 0.1250 \\ 0.1102 & 0.1396 & 0.1250 \\ 0.1250 & 0.1250 & 0.1750 \end{bmatrix} - \begin{bmatrix} 0.00173 & -0.00173 & 0.0059 \\ -0.00173 & 0.00173 & -0.0059 \\ 0.00390 & -0.00390 & 0.020 \end{bmatrix}$$

$$Z_{BUS} = \begin{bmatrix} 0.1396 & 0.1102 & 0.1250 \\ 0.1102 & 0.1396 & 0.1250 \\ 0.1250 & 0.1250 & 0.1750 \end{bmatrix}$$

~~Elimination
of node~~

Consider a 3 bus system as shown in the figure



The performance equations is

$$\mathfrak{I}_1 = y_{11}V_1 + y_{12}V_2 + y_{13}V_3$$

or

$$\begin{bmatrix} \mathfrak{I}_1 \\ \mathfrak{I}_2 \\ \mathfrak{I}_3 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} & y_{13} \\ y_{21} & y_{22} & y_{23} \\ y_{31} & y_{32} & y_{33} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \end{bmatrix}$$

$$\text{By } \mathfrak{I}_2 = y_{21}V_1 + y_{22}V_2 + y_{23}V_3$$

$$\mathfrak{I}_3 = y_{31}V_1 + y_{32}V_2 + y_{33}V_3$$

$\mathfrak{I}_3 = 0$ if node 3 is eliminated

$$0 = y_{31}V_1 + y_{32}V_2 + y_{33}V_3$$

$$V_3 = \frac{-(y_{31}V_1 + y_{32}V_2)}{y_{33}}$$

Substitute V_3 in equation \mathfrak{I}_1

$$\begin{aligned} \mathfrak{I}_1 &= y_{11}V_1 + y_{12}V_2 + y_{13} \left[\frac{-y_{31}V_1 - y_{32}V_2}{y_{33}} \right] \\ &= V_1 \left[y_{11} - \frac{y_{13}y_{31}}{y_{33}} \right] + V_2 \left[y_{12} - \frac{y_{13}y_{32}}{y_{33}} \right] \end{aligned}$$

Assume $y_{11}' = y_{11} - \frac{y_{13}y_{31}}{y_{33}}$ and $y_{12}' = y_{12} - \frac{y_{13}y_{32}}{y_{33}}$.

$$y_{12} = y_{12}(\text{old}) - \frac{y_{13} y_{32}}{y_{33}}$$

$$y_{21} = y_{21}(\text{old}) - \frac{y_{13} y_{31}}{y_{33}}$$

$$\therefore y_{ij(\text{new})} = y_{ij(\text{old})} - \frac{y_{il} y_{lj}}{y_{ll}}$$

$$\text{by } z_{ij}(\text{new}) = z_{ij}(\text{old}) - \frac{z_{il} z_{lj}}{z_{ll}}$$

Problem

① Eliminate 3rd bus for the given Bus Admittance

Matrix -

$$Y_{BVS} = \begin{bmatrix} -j2.86 & 0 & j2.86 \\ 0 & -j4 & j2 \\ j2.86 & j2 & j8.86 \end{bmatrix}$$

(without mutual coupling)

Sol

$$y_{ij(\text{new})} = y_{ij(\text{old})} - \frac{y_{il} y_{lj}}{y_{ll}}$$

where $l=3$

~~$j^2 = -j4$~~

$$\Rightarrow i=1, j=1$$

$$y_{11}(\text{new}) = y_{11}(\text{old}) - \frac{y_{13} y_{31}}{y_{33}}$$

$$= -j8.86 - \frac{j2.86 \cdot j2.86}{-j2.86}$$

$$= -j1.9$$

$$y_{12}(\text{new}) = y_{12}(\text{old}) - \frac{y_{13} y_{32}}{y_{33}}$$

$$= 0 - \frac{j2.86 \cdot j2}{-j8.86}$$

$$= j0.64$$

$$Y_{21}(\text{new}) = Y_{21} \text{ old} - \frac{Y_{23} Y_{31}}{Y_{33}}$$

$$= 0 - \frac{j2 \cdot j2.86}{-j8.86}$$

$$= j0.64$$

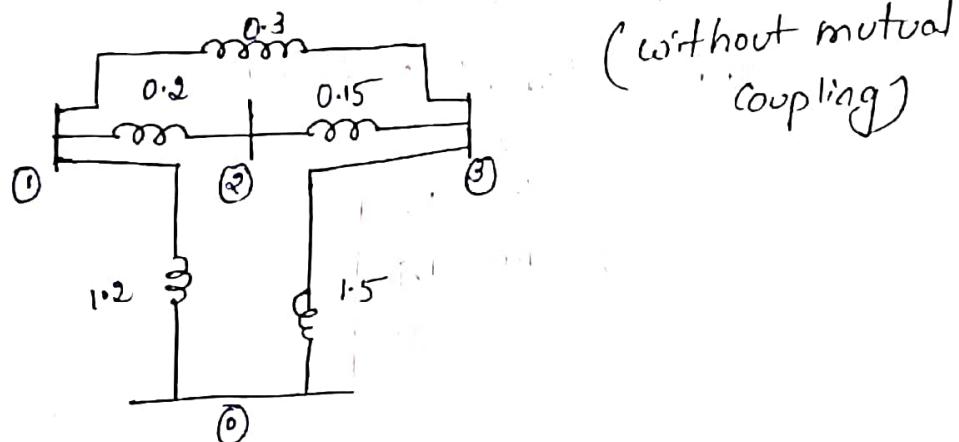
$$Y_{22}(\text{new}) = Y_{22} \text{ old} - \frac{Y_{23} Y_{32}}{Y_{33}}$$

$$= -j6 - \frac{j2 j2}{-j8.86}$$

$$= -j5.54$$

$$Y_{\text{BUS}}(\text{new}) = \begin{bmatrix} -j1.9 & j0.64 \\ j0.64 & -j5.54 \end{bmatrix}$$

② Determine Z_{BUS} for the given network



Step 1:
Adding element b/n def & 1st bus

$$\tau=0, K=1$$

Type-1 Modification
Added element is Branch

$$Z_{\text{BUS}} = 1 \begin{bmatrix} 1.2 \end{bmatrix}_{1 \times 1}$$

Step 2: Adding Element bln ① & ②

Type-2 Modification

old - 1 New K=2

Added element is a branch

$$Z_{BUS} = \begin{matrix} & 1 & 2 \\ 1 & \left[\begin{matrix} 1.2 & \xrightarrow{1.2} \\ \downarrow & \\ 1.2 & 1.4 \end{matrix} \right] \\ 2 & \end{matrix}$$

$$Z_{22} = 1.2 + 0.2 = 1.4$$

Step 3: Adding Element bln ② & ③

Old i=2 New - K-3

Type-2 Modification

Added element is branch

$$Z_{BUS} = \begin{matrix} & 1 & 2 & 3 \\ 1 & \left[\begin{matrix} 1.2 & 1.2 & \xrightarrow{1.2} \\ & 1.4 & 1.4 \end{matrix} \right] \\ 2 & \left[\begin{matrix} 1.2 & 1.4 & 1.4 \\ \downarrow & & \\ 1.2 & 1.4 & 1.55 \end{matrix} \right] \\ 3 & \end{matrix}$$

Z

Step 4: Adding element bln ③ & ref

$$Z_{BUS} = \begin{matrix} & 1 & 2 & 3 & 4 \\ 1 & \left[\begin{matrix} 1.2 & 1.2 & 1.2 & 1.2 \\ & 1.4 & 1.4 & 1.4 \\ & 1.2 & 1.4 & 1.55 & 1.55 \end{matrix} \right] \\ 2 & \\ 3 & \\ 4 & \end{matrix}$$

$\downarrow = 4$

$$Z_{11}(\text{new}) = Z_{11}(\text{old}) - \frac{Z_{14} Z_{41}}{Z_{44}}$$

$$= 1.2 - \frac{1.2 \times 1.2}{3.05}$$

$$= 0.728$$

$$Z_{12}(\text{new}) = Z_{12}(\text{old}) - \frac{Z_{14} Z_{42}}{Z_{44}}$$

$$= 1.2 - \frac{1.2 \times 1.2}{3.05}$$

$$= 0.649 = Z_{21}$$

$$Z_{13}(\text{new}) = Z_{13}(\text{old}) - \frac{Z_{14} Z_{43}}{Z_{44}}$$

$$= 1.2 - \frac{1.2 \times 1.2}{3.05}$$

$$= 0.591 = Z_{31}$$

$$Z_{22}(\text{new}) = Z_{22}(\text{old}) - \frac{Z_{24} Z_{42}}{Z_{44}}$$

$$= 1.4 - \frac{1.4 \times 1.4}{3.05}$$

$$= 0.751$$

$$Z_{23} = Z_{23} - \frac{Z_{24} Z_{43}}{Z_{44}}$$

$$= 1.4 - \frac{1.4 \times 1.51}{3.05}$$

$$= 0.68 = Z_{32}$$

$$Z_{33} = 0.76$$

$$X_{BUS} = \begin{bmatrix} 0.728 & 0.649 & 0.591 \\ 0.649 & 0.591 & 0.68 \\ 0.591 & 0.68 & 0.76 \end{bmatrix}$$

~~Step 5~~

Adding element b/m 1×3 as a link
 $i=1 \ j=3$

now $\boxed{1 \times 4}$

Type 4 Modification

$$Z_{BUC} = \begin{bmatrix} 1 & 2 & 3 & 4 \\ 1 & 0.723 & 0.649 & 0.590 \\ 2 & 0.649 & 0.487 & 0.680 \\ 3 & 0.59 & 0.68 & 0.76 \\ 4 & 0.59 & 0.68 & 0.76 \end{bmatrix}$$

$$Z_{44} = Z_{B} + Z_{11} + Z_{33} - Z_{13}$$

$$\begin{aligned} Z_{11}(\text{new}) &= Z_{11}(\text{old}) - \frac{Z_{14}Z_{41}}{Z_{44}} \\ &= 0.723 - \frac{0.59 \times 0.59}{1.06} \\ &= 0.399 \end{aligned}$$

$$\begin{aligned} Z_{12}(\text{new}) &= 0.649 - \frac{0.59 \times 0.68}{1.06} \\ &= 0.210 = Z_{21} \end{aligned}$$

$$\begin{aligned} Z_{13}(\text{new}) &= 0.59 - \frac{0.59 \times 0.76}{1.06} \\ &= 0.1669 = Z_{31} \end{aligned}$$

$$Z_{22} = 0.649 - \frac{0.68 \times 0.68}{1.06}$$

$$\approx 0.212$$

$$Z_{33} = 0.59 - \frac{0.76 \times 0.76}{1.06}$$

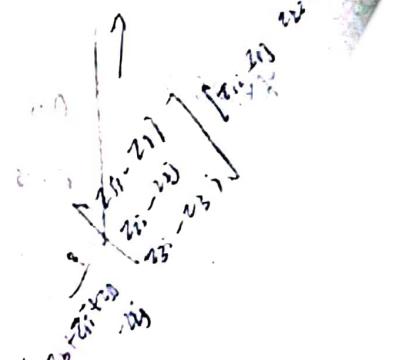
$$\approx 0.1650 = 0.015$$

$$Z_{23} = 0.68 - \frac{0.68 \times 0.76}{1.06}$$

$$\approx 0.192 = Z_{32}$$

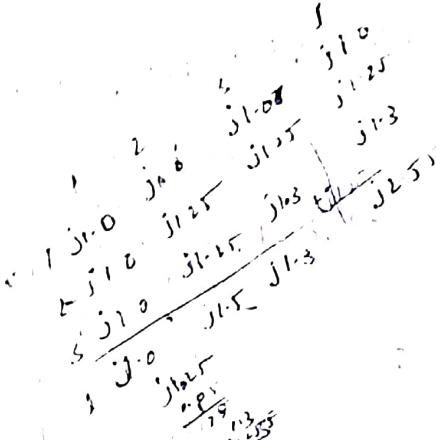
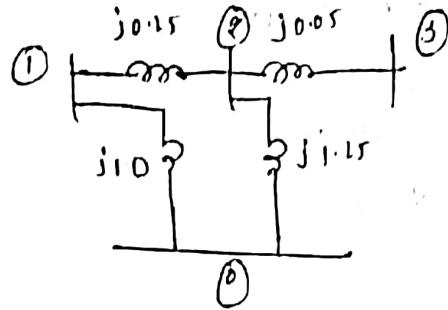
Ans:

$$\begin{bmatrix} 0.697 & 0.658 & 0.629 \\ 0.658 & 0.754 & 0.8178 \\ 0.629 & 0.754 & 0.714 \end{bmatrix}$$

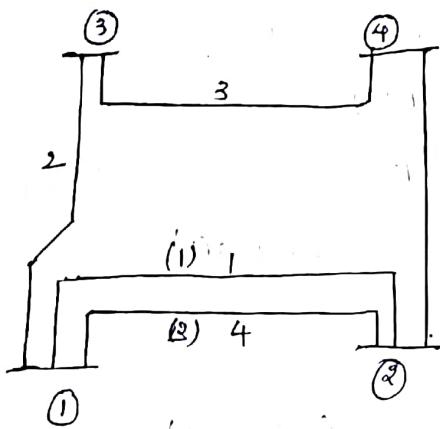


Assignment

Find: Z_{bus}



(3) Form Z_{bus} (with Mutual Coupling)



$$Z_1 = \frac{Z_{11} + Z_{12}}{Z_{11} Z_{22}}$$

Element number	Self		Mutual	
	Bus code p-q	Impedance	Bus code p-s	Impedance
1	1-2(1)	0.6		
4	1-2(2)	0.4	1-2(1)	0.2
2	1-3	0.5	1-2(1)	0.1
3	3-4	0.5		
5	2-4	0.2		

So

Step 1: Element-1 b/n p=1 & q=2

P=1=reference.

$$Z_{\text{bus}}^{\text{(new)}} = \begin{bmatrix} 0 & 0 \\ 0 & 0.6 \end{bmatrix} = 2 \begin{bmatrix} 0.6 \end{bmatrix}$$

Step 2:

Element 4 connected b/w ① & ④

$$P=1 = \text{ref} \quad Q=2 \quad \text{and } i=2$$

Mutually coupled element - 1

$$Z_{eq\sigma} = \begin{matrix} 2 \\ 1 \end{matrix} \begin{bmatrix} 1 & 0 \\ 0.6 & Z_{10} \\ Z_{21} & Z_{22} \end{bmatrix}$$

$$Z_{10} = Z_{21} =$$

$$\Rightarrow Z_{11} = Z_{11} - Z_{10} + \frac{g_{pq,\sigma}(Z_{11} - Z_{21})}{g_{pq\sigma}}$$

$$\Rightarrow Z_{11} = Z_{22} = \frac{Z_{12} - Z_{22}}{0} + \frac{g_{12(2),12(1)}(Z_{12} - Z_{22})}{g_{12(2),12(2)}} \quad (a)$$

$$\Rightarrow Z_{11} = -Z_{21} + \frac{1 + g_{12(2),12(1)}(Z_{12} - Z_{21})}{g_{12(2),12(2)}} \quad (b)$$

$$\text{Here } Z_{12} = Z_{10} = 0$$

Now we have to consider primitive impedance matrix

$$Z_{eq} \Rightarrow \begin{bmatrix} 1-2(1) & 1-2(2) \\ 1-2(2) & 1-2(1) \end{bmatrix} \begin{bmatrix} 0.6 & 0.2 \\ 0.2 & 0.4 \end{bmatrix}$$

$$Y_{eq} = (Z_{eq})^{-1} = \frac{1}{0.24 - 0.08} \begin{bmatrix} 0.4 & -0.2 \\ -0.2 & 0.6 \end{bmatrix}$$

$$= \frac{2.5}{0.16} \begin{bmatrix} 0.4 & -0.2 \\ -0.2 & 0.6 \end{bmatrix}$$

$$= \frac{1}{5} \begin{bmatrix} 0.4 & -0.2 \\ -0.2 & 0.6 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} 1-2(1) & 1-2(2) \\ 1-2(2) & 1-2(1) \end{bmatrix} \begin{bmatrix} 2 & -1 \\ -1 & 3 \end{bmatrix}$$

$$y_{12}(1) y_{12}(2) = -1 = y_{12}(2) y_{11}(1)$$

∴ from (a)

$$Z_{21} = Z_{12} = -0.6 + \frac{(-1)(-0.4)}{3} \\ = -0.4$$

$$Z_{11} = +0.6 + \frac{1 \div (-1) (0.4)}{3} \\ = 0.6$$

$$Z_{BUS} = \begin{bmatrix} 0.6 & -0.4 \\ -0.4 & 0.6 \end{bmatrix}$$

$$Z_{22}(\text{new}) = Z_{22}(\text{old}) - \frac{Z_{21} Z_{12}}{Z_{11}} \\ = 0.6 - \frac{-0.4 \times -0.4}{0.6} \\ = 0.33$$

$$Z_{BUS}(\text{new}) = [0.33]$$

Step 3

Add Element-2 b/w ① & ③

$$P=1 \text{ (ref)}, Q=3 \text{ (new)} \quad i=2 \quad p=1 \sigma=2$$

Mutually coupled element - 1

$$Z_{BUS} = 2 \begin{bmatrix} 0.33 & Z_{23} \\ Z_{32} & Z_{33} \end{bmatrix}$$

$$Z_{23} = Z_{32} = Z_3 - Z_{33} + \frac{y_{13,12}(1) \{ Z_{13} - Z_{23} \} y_{13,12}(2)}{y_{13,12}(1) \{ Z_{13} - Z_{23} \} y_{13,12}(2)}$$

$$Z_{23} = Z_{32} = \frac{\begin{bmatrix} Y_{13,12(1)} & Y_{13,12(2)} \end{bmatrix} \begin{bmatrix} Z_{12} - Z_{22(1)} \\ Z_{12} - Z_{22(2)} \end{bmatrix}}{Y_{13,13}}$$

$$Z_{33} = 1 + \frac{\begin{bmatrix} Y_{13,12(1)} & Y_{13,12(2)} \end{bmatrix} \begin{bmatrix} Z_{12} - Z_{22} \\ Z_{13} - Z_{23} \end{bmatrix}}{Y_{13,13}}$$

Now Primitive Impedance matrix for mutual coupling

$$Z_{PQe\sigma} = \begin{bmatrix} 1-2(1) & 1-2(2) & 1-3 \\ 1-2(2) & 0.6 & 0.2 & 0.1 \\ 1-3 & 0.2 & 0.4 & 0 \end{bmatrix}$$

$$= \frac{\text{Adj}}{|Z_{PQe\sigma}|}$$

$$= |Z_{PQe\sigma}| = 0.6(0.4 \times 0.5 - 0) - 0.2(0.2 \times 0.5 - 0) + 0.1(0 - 0.1 \times 0.4) \\ = 0.096$$

Adj:

$$\text{Co-factor} = \begin{bmatrix} 0.4 & 0 & 0.2 & 0.4 \\ 0 & 0.5 & 0.1 & 0 \\ 0.2 & 0.1 & 0.6 & 0.2 \\ 0.4 & 0 & 0.2 & 0.4 \end{bmatrix}$$

$$\text{Adj} = \begin{bmatrix} 0.2 & -0.1 & -0.04 \\ -0.1 & 0.29 & 0.02 \\ -0.04 & 0.02 & 0.2 \end{bmatrix}$$

$$(Z_{PQe\sigma})^{-1} = Y_{PQe\sigma} = \begin{bmatrix} 1-2(1) & 1-2(2) & 1-3 \\ 2.088 & -1.041 & -0.416 \\ -1.041 & 2.3208 & 0.208 \\ -0.416 & 0.208 & 0.0233 \end{bmatrix}$$

$$Z_{33} = Z_{23} = \frac{[-0.4117 \quad 0.2083]}{2.013} \begin{bmatrix} -0.33 \\ -0.55 \end{bmatrix}$$

$$= \frac{\begin{bmatrix} 0.13751 & -0.068 \\ 0.13751 & -0.068 \end{bmatrix}}{2.013}$$

$$= \frac{0.0687}{2.013}$$

$$Z_{23} = \frac{1 + [-0.4117 \quad 0.2083] \begin{bmatrix} -0.33 \\ -0.55 \end{bmatrix}}{2.013}$$

$$= \frac{1 + 0.0687}{2.013}$$

$$= 0.513$$

$$= 0.4833$$

$$Z_{BUS} (\text{new}) = \begin{bmatrix} 0.033 & 0.033 \\ 0.033 & 0.4833 \end{bmatrix}$$

Step 4 :-

Add. elements b/m ③ & ④

$$P=3 \quad q=4 \quad \begin{matrix} 1-2-3-4 \\ 1-2-3-4 \end{matrix}$$

$$Z_{BUS} (\text{new}) = \begin{matrix} 2 & \begin{bmatrix} 0.033 & 0.033 \rightarrow 0.033 \\ 0.033 & 0.4833 \rightarrow 0.4821 \end{bmatrix} \\ 3 & \begin{bmatrix} 0.033 & 0.4833 \rightarrow 0.4821 \\ 0.4833 & 0.9833 \end{bmatrix} \\ 4 & \end{matrix}$$

Step 5:

Add Element 5 b/n P=2, Q=4

$$l=4 \quad \text{new}$$

Added element is line

$$\begin{array}{cccc} & 2 & 3 & 4 \\ 2 & & & \\ 3 & & & \\ 4 & & & \end{array}$$

$$Z_{BUS}(\text{new}) = \begin{matrix} 2 & \left[\begin{array}{cccc} 0.033 & 0.033 & 0.033 & 0.033 \\ 0.033 & 0.4833 & 0.4833 & 0.4833 \\ 0.033 & 0.4833 & 0.9833 & 0.9833 \\ 0.033 & 0.4833 & 0.9833 & 1.45 \end{array} \right] & 0.33 - 0.033 = 0.3 \\ 3 & \rightarrow -0.45 \\ 4 & \rightarrow -0.95 \\ l & \rightarrow 1.45 \end{matrix}$$

if l=9

$$Z_{2l}(\text{new}) = \begin{matrix} 2 & \left[\begin{array}{c} 0.033 \\ 0.33 - \frac{0.033 \times 0.033}{1.45} \end{array} \right] & 1 \\ 3 & & \\ 4 & & \\ l & & \end{matrix}$$

$$= 0.3290 \quad \text{new}$$

$$Z_{23}(\text{new}) = \begin{matrix} 2 & \left[\begin{array}{c} 0.033 - \frac{0.033 \times 0.4833}{1.45} \end{array} \right] & 1 \\ 3 & & \\ 4 & & \\ l & & \end{matrix}$$

$$= 0.3025 \quad 2 \quad 3 \quad 4 \quad l$$

$$Z_{BUS}(\text{new}) = \begin{matrix} 2 & \left[\begin{array}{cccc} 0.033 & 0.033 & 0.033 & 0.3 \\ 0.033 & 0.4833 & 0.4833 & -0.45 \\ 0.033 & 0.4833 & 0.9833 & -0.95 \\ 0.3 & -0.45 & -0.95 & 1.45 \end{array} \right] & 1 \\ 3 & & \\ 4 & & \\ l & & \end{matrix}$$

$$Z_{22}(\text{new})^2 = 0.33 - \frac{0.3 \times 0.3}{1.45}$$

$$= 0.067$$

$$Z_{23}(\text{new}) = 0.033 - \frac{0.3 \times -0.45}{1.45}$$

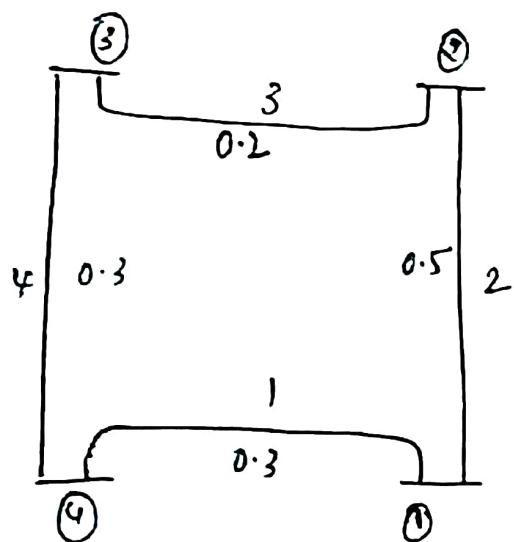
$$= 0.4833 = Z_{32}$$

$$Z_{24} = 0.033 - \frac{0.3 \times -0.95}{1.45}$$

$$= 0.526 = Z_{42} \quad \text{and} \quad Z_{242}$$

$$\bar{Z}_{\text{BUS}}(\text{new}) = \begin{bmatrix} 0.271 & 0.126 & & \\ 0.126 & 0.3434 & 0.1385 & \\ & 0.1385 & 0.3609 & \end{bmatrix}$$

Form Z_{BUS}



Elimination of Node & [Matrix Algebra]

$$* \quad \mathfrak{I} = \mathfrak{V} V \quad [\mathfrak{I}_{BUS} = \mathfrak{V}_{BUS} \quad \mathfrak{V}_{BUS}]$$

$$\begin{bmatrix} \mathfrak{I}_A \\ \mathfrak{I}_X \end{bmatrix} = \begin{bmatrix} K & \omega \\ L^T & M \end{bmatrix} \begin{bmatrix} \mathfrak{V}_A \\ \mathfrak{V}_X \end{bmatrix}$$

⇒ where \mathfrak{V}_A & \mathfrak{V}_X are sub matrix of voltage & currents of the nodes to be eliminated.

$$\mathfrak{I}_X = \omega^T \mathfrak{V}_A + M \mathfrak{V}_X = 0$$

$$\mathfrak{V}_X = M^{-1} \omega^T \mathfrak{V}_A$$

$$\mathfrak{I}_A = \mathfrak{V}_A (K - \omega M^{-1} \omega^T)$$

$$\therefore \mathfrak{I}_{BUS} = K - \omega M^{-1} \omega^T$$

$$\mathfrak{I}_{BUS} = \begin{bmatrix} K & \omega \\ \hline y_{11} & y_{12} & y_{13} \\ y_{21} & y_{22} & y_{23} \\ \hline y_{31} & y_{32} & y_{33} \end{bmatrix}$$

$\omega^T \quad M$

$$\therefore \mathfrak{I}_{BUS} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} - \begin{bmatrix} y_{13} \\ y_{23} \end{bmatrix} \frac{1}{y_{33}} \begin{bmatrix} y_{31} & y_{32} \end{bmatrix}$$

$$= \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} - \frac{1}{y_{33}} \begin{bmatrix} y_{13} \\ y_{23} \end{bmatrix} \begin{bmatrix} y_{31} & y_{32} \end{bmatrix}$$

$$y_{ij}(\text{new}) = y_{ij}(\text{old}) - \frac{y_{in} y_{nj}}{y_{mm}} \quad i=j=1, 2, \dots, (n-1)$$