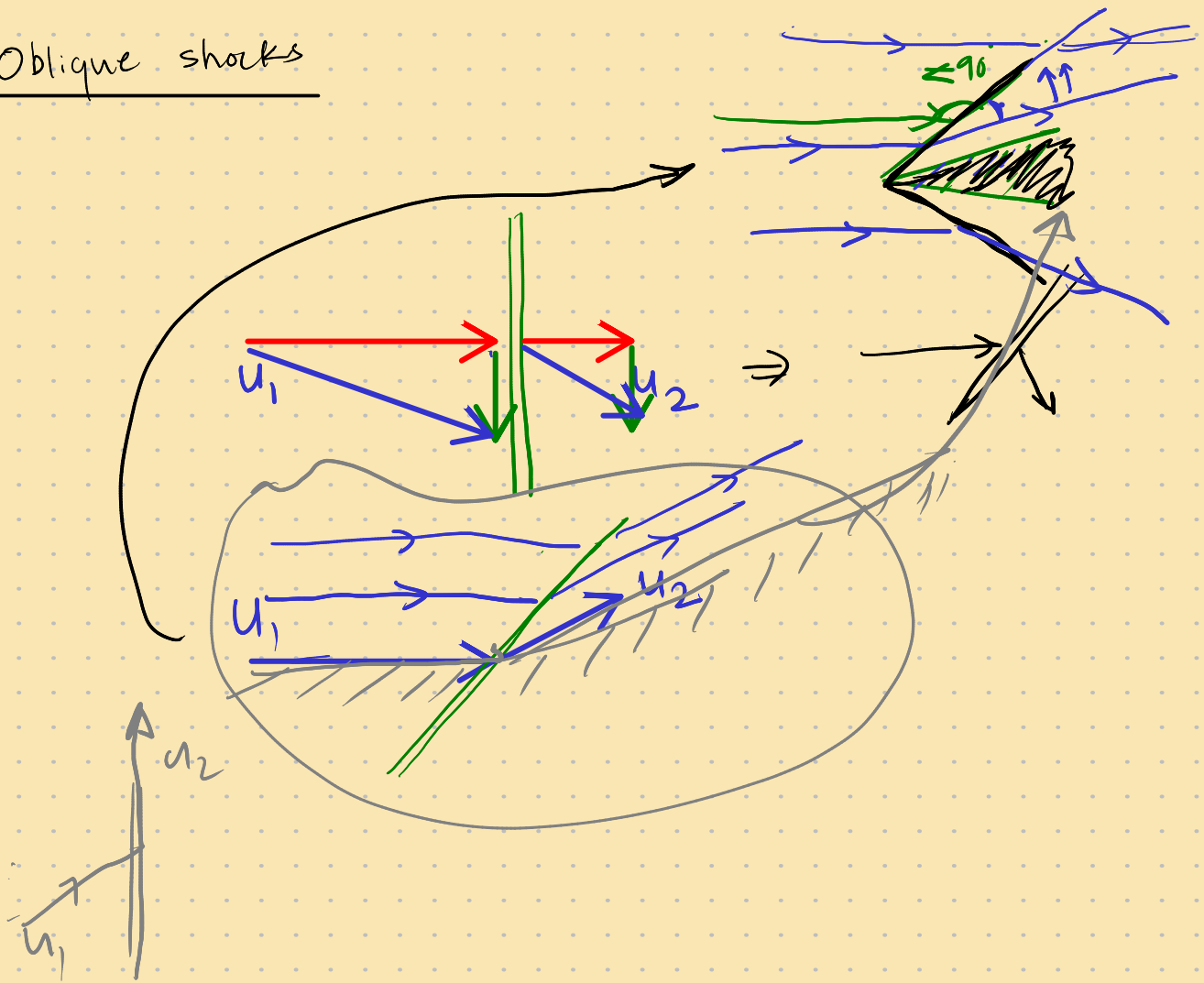
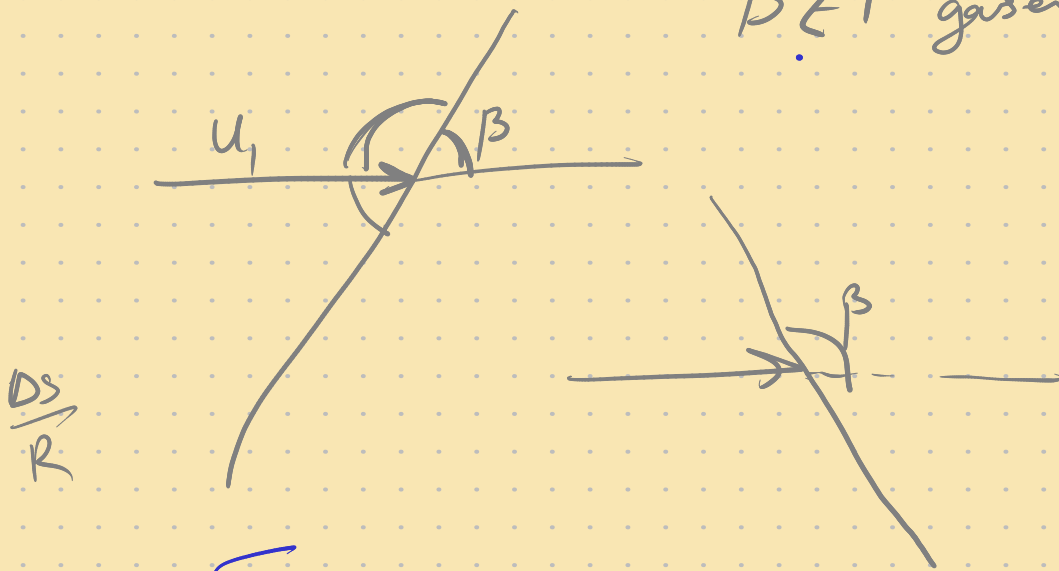


# Oblique shocks



BZT gasen



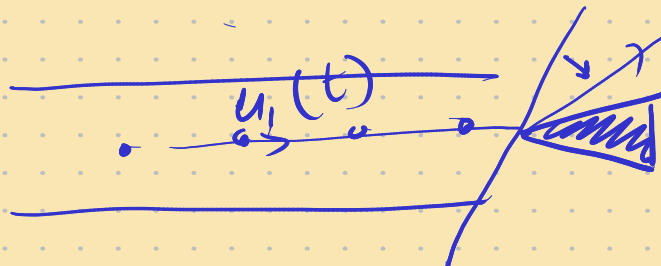
$$M_2 = \sqrt{\frac{2}{\gamma(\gamma-1)}}$$

$t \rightarrow t_{\text{test}}$

$$u_2 \uparrow \Rightarrow T_2 \uparrow$$

$$\frac{u_2}{\sqrt{T_2}}$$

$P_0(t)$

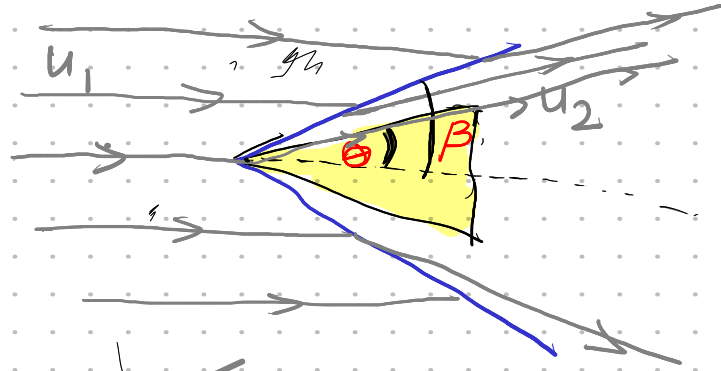


## Oblique Shock -

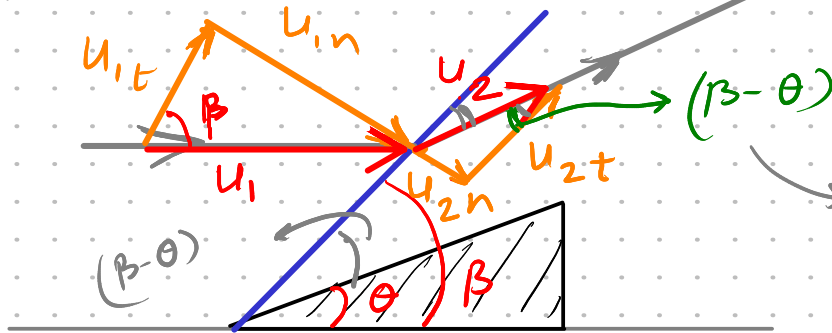
→ 2D -

→  $\theta$  - Half angle of wedge

$\beta$  - Half angle of shock



$$\beta = f(\theta, M_1, \gamma, P_1, \dots)$$



$$\tan(\beta - \theta) = \frac{U_{2n}}{U_{2t}}$$

$$\theta = \beta - \tan^{-1}\left(\frac{U_{2n}}{U_{2t}}\right)$$

$$U_{1n} = U_1 \sin \beta, \quad U_{1t} = U_1 \cos \beta$$

$$U_{2n} = U_2 \sin(\beta - \theta), \quad U_{2t} = U_2 \cos(\beta - \theta)$$

Clearly, there is no change in the tangential velocity.

$$\Rightarrow U_{1t} = U_{2t}$$

The normal component of the velocity encounters a normal shock. Hence normal shock relations apply.

So, the algo is this.

Given  $M_1$  &  $\beta$ ,

$$M_{1n} = M_1 \sin \beta$$

$$M_{2n} = M_2 \sin(\beta - \theta)$$

$$M_{1t} = M_1 \cos \beta$$

$$M_{2t} = M_2 \cos(\beta - \theta)$$

the inverse function.

$$\text{i.e. } \theta = g(\beta) = f^{-1}(\beta)$$

So we know,

$$u_{1t} = u_{2t}$$

$$\therefore u_1 \cos \beta = u_2 \cos(\beta - \theta)$$

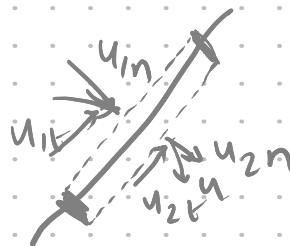
$$\therefore \frac{u_1}{u_2} = \frac{\cos(\beta - \theta)}{\cos(\beta)}$$

$$\frac{u_{1n} / \sin \beta}{u_{2n} / \sin(\beta - \theta)} = 1$$

$$\therefore \frac{u_{1n}}{u_{2n}} = \frac{\cos(\beta - \theta)}{\cos(\beta)} \cdot \frac{\sin(\beta)}{\sin(\beta - \theta)} = \frac{\tan \beta}{\tan(\beta - \theta)} \quad \text{--- (A)}$$

From mass conservation,

$$\rho_1 u_{1n} = \rho_2 u_{2n} \quad \text{--- (B)}$$



From (A) & (B).

$$\frac{\rho_2}{\rho_1} = \frac{\tan(\beta - \theta)}{\tan(\beta)} \quad \text{--- (C)}$$

$$\text{Now, } \frac{\rho_2}{\rho_1} = f_3(M_1 \sin \beta) = \frac{(r-1) M_1^2 \sin^2 \beta}{(r-1) M_1^2 \sin^2 \beta + 2} \quad \text{--- (D)}$$

$$\frac{u_{1n}}{a_1} = \frac{u_1 \sin \beta}{a_1} = \underline{M_1 \sin \beta}$$

Using ③ & ④ it can be shown that

$$\tan \theta = 2 \cot \beta \left[ \frac{M_1^2 \sin^2 \beta - 1}{2 + M_1^2 [\gamma + \cos 2\beta]} \right]$$

This gives us  $\theta = g(\beta) = f^{-1}(\beta)$

Now we can either use a plot or use a computer

Q: What is the minimum achievable value of  $\beta$ ?

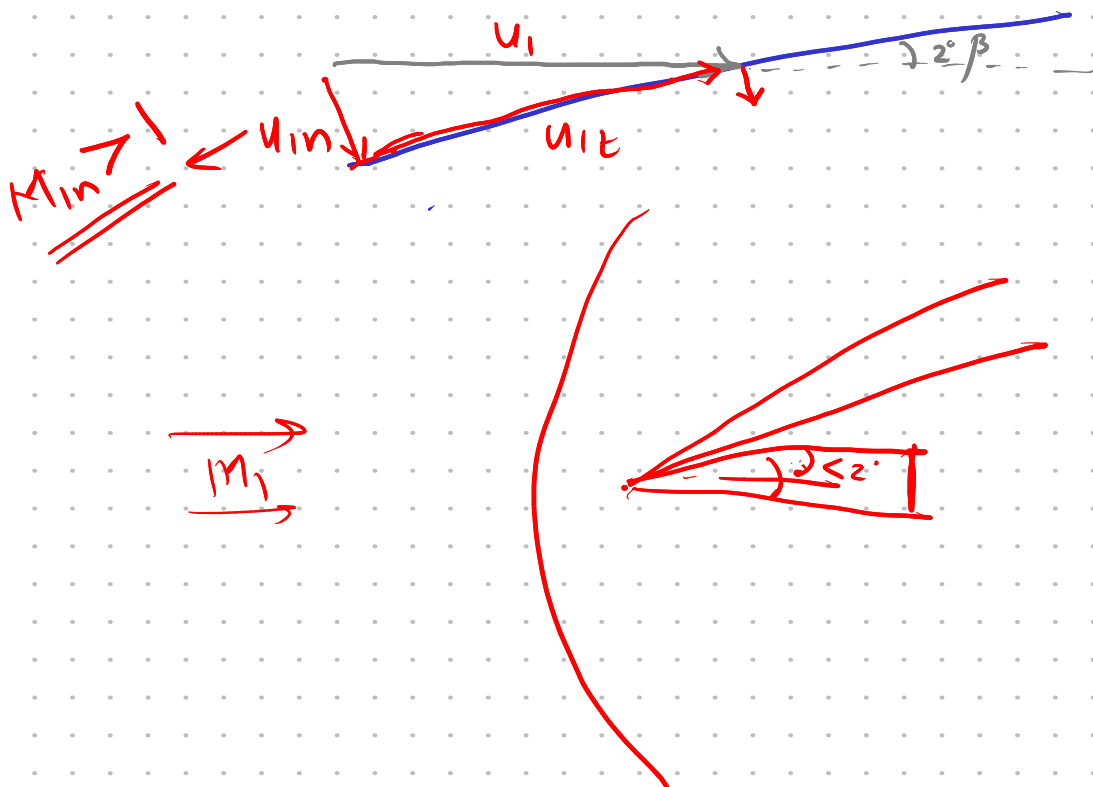
$$\rightarrow \frac{p_2}{p_1} = 1 + \frac{2\gamma}{\gamma+1} (M_1^2 \sin^2 \beta - 1)$$

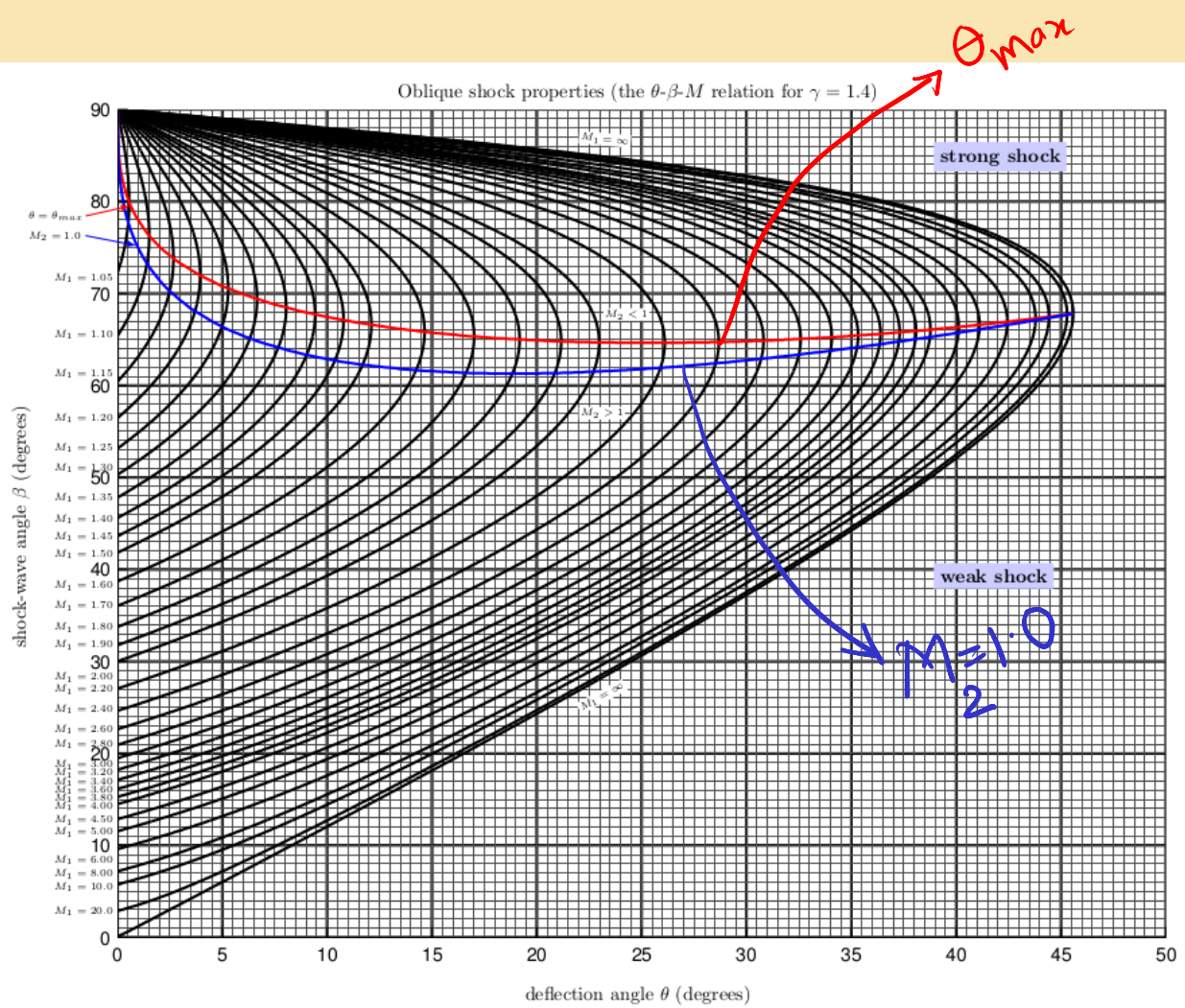
$$\sin^{-1}(1/M_1) \leq \beta < 90$$

$$p_2 > p_1 \Rightarrow M_1^2 \sin^2 \beta > 1$$

$$\sin^2 \beta > 1/M_1^2 \Rightarrow \sin \beta > 1/M_1$$

$$\beta > \sin^{-1}(1/M_1)$$

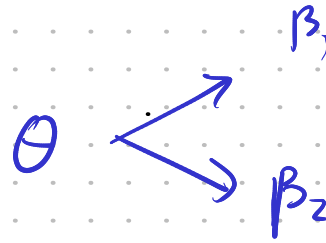




Q:- What is maximum value of  $\beta$ ?

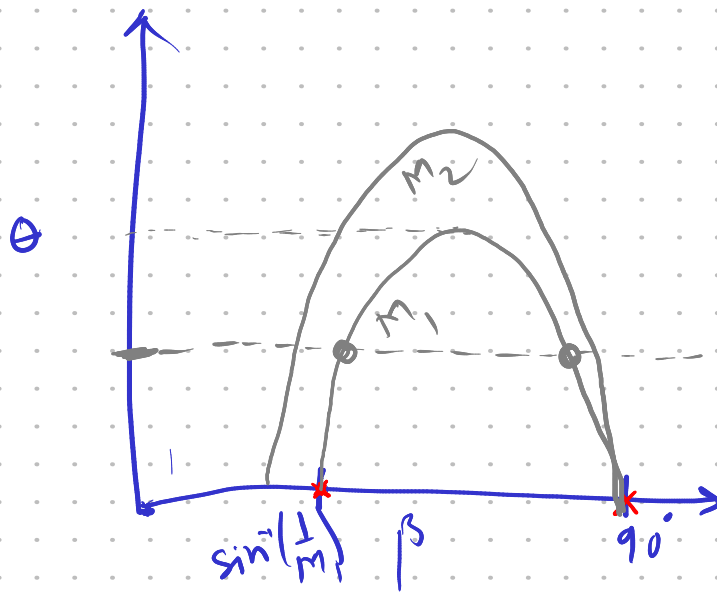
Q:- What is the possible range of  $\theta$ ?

$$\tan(\theta) = \frac{2 \cot \beta (M_1^2 \sin^2 \beta - 1)}{2 + M_1^2 (\gamma + \cos 2\beta)}$$



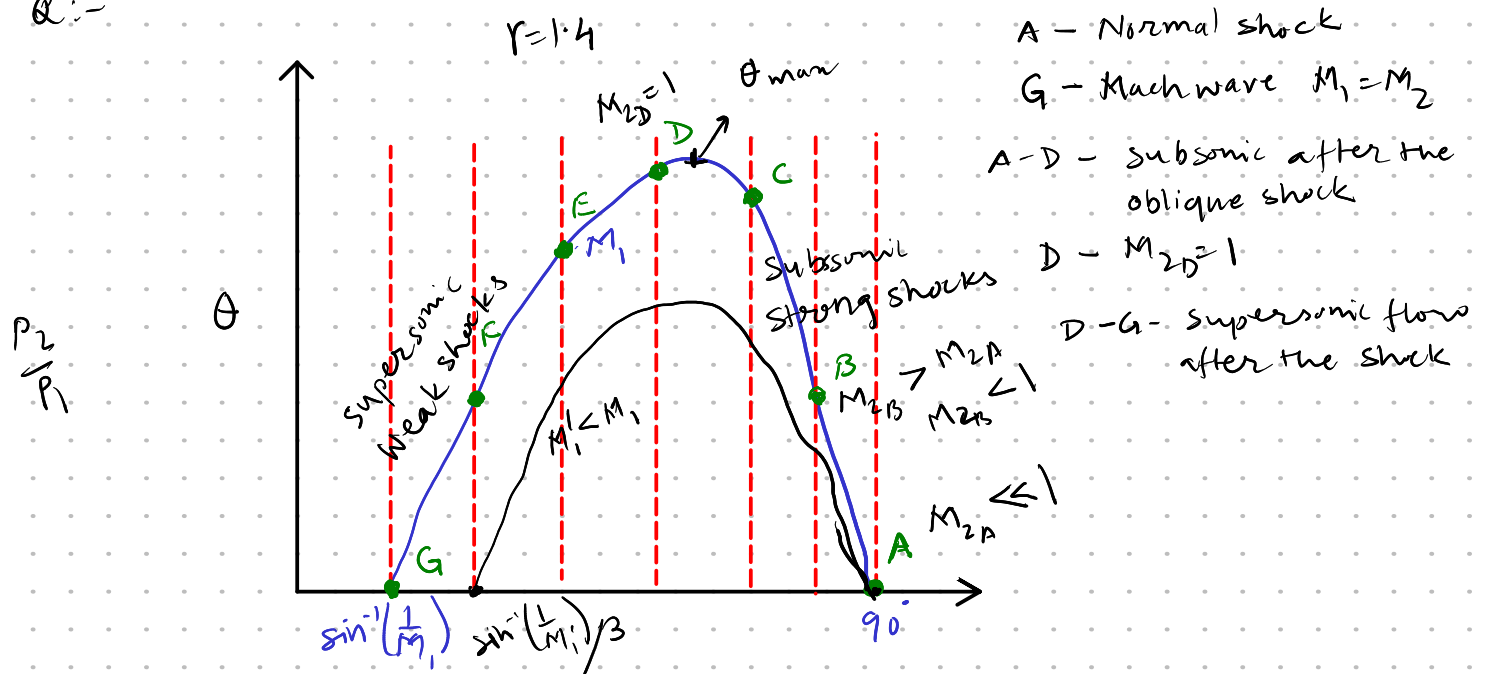
Fix  $\gamma$  - gas

$M_1$  - Upstream Mach num.



$M_1, \gamma$   
 $M_2, \gamma$   
 $M_2 > M_1$

Q:-

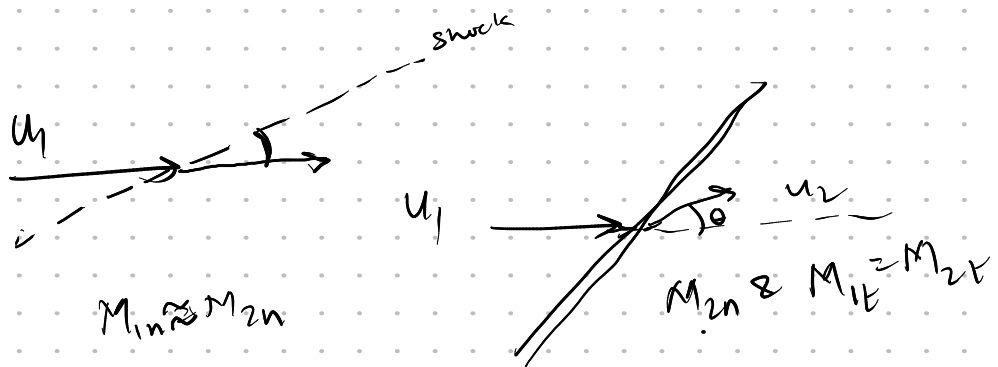


$$\frac{\Delta s}{R} = \frac{s_2 - s_1}{R} \bigg|_G = 0$$

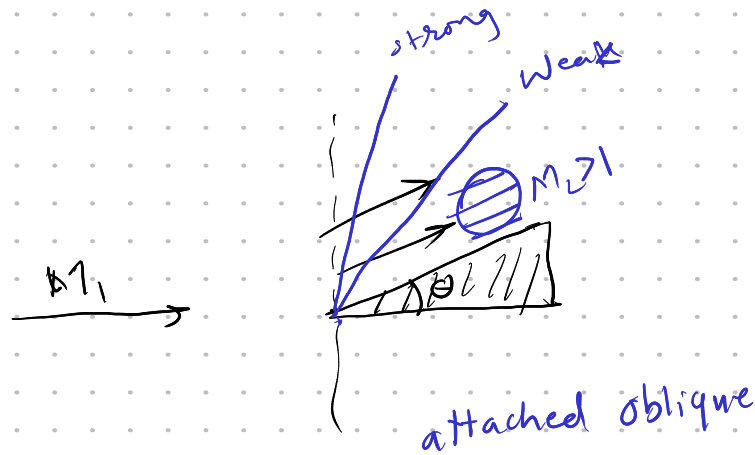
As  $\beta \downarrow$ ,  $\frac{\Delta s}{R} \downarrow$  for a given  $\gamma, M_1$

As  $\beta \downarrow$ ,  $\frac{P_2}{P_1} \downarrow$ ,  $\frac{T_2}{T_1}$ ,  $\frac{s_2}{s_1}$ ,  $\frac{P_{02}}{P_{01}}$

For  $M_1' < M_1$ ,



Q:- So I know that for given  $\theta$  (flow deflection), I have two possible values of  $\beta$  and corresponding two possible shocks (strong & weak). So which one will occur?



→ Both shocks are feasible. But strong shocks are unstable and hence very improbable.

