## Problem 3.24

The noncoherent carrier is

$$c(t) = A_c \cos(2\pi f_c t + \phi)$$

and the DSB-SC modulated wave is  $m(t)\cos(2\pi f_c t)$ . The composite signal is therefore

$$\begin{split} s(t) &= A_c \cos(2\pi f_c t + \phi) + m(t) \cos(2\pi f_c t) \\ &= [A_c \cos\phi + m(t)] \cos(2\pi f_c t) - A_c \sin\phi \sin(2\pi f_c t) \\ &= s_I(t) \cos(2\pi f_c t) - s_O(t) \sin(2\pi f_c t) \end{split}$$

where

$$s_I(t) = A_c \cos \phi + m(t)$$

$$s_O(t) = A_c \sin \phi$$

Applying the composite signal s(t) to an ideal envelope detector produces the output

$$a(t) = [s_I^2(t) + s_Q^2(t)]^{1/2}$$

$$= [(A_c \cos \phi + m(t))^2] + (A_c \sin \phi)^{21/2}$$

$$= [A_c^2 \cos^2 \phi + 2A_c \cos \phi m(t) + m^2(t) + A_c^2 \sin^2 \phi]^{1/2}$$

$$= [A_c^2 + 2A_c \cos \phi m(t) + m^2(t)]^{1/2}$$
(1)

(a) For  $\phi = 0$ , Eq. (1) reduces to

$$a(t) = \left[A_c^2 + 2A_c m(t) + m^2(t)\right]^{1/2}$$
  
=  $A_c + m(t)$  (2)

which consists of the message signal m(t) plus a dc bias equal to the carrier amplitude.

(b) For  $\phi \neq 0$  and  $|m(t)| \ll A_c/2$ , we may approximate Eq. (1) as follows:

$$a(t) \approx \left[A_c^2 + 2A_c \cos\phi m(t)\right]^{1/2}$$

$$= A_c \left[1 + \frac{2}{A_c} \cos\phi m(t)\right]^{1/2}$$
(3)

With  $|\cos\phi| \le 1$ , and  $|m(t)| << A_c/2$ , we may approximate Eq. (3) further as

$$a(t) \approx A_c \left[ 1 + \frac{1}{A_c} \cos \phi m(t) \right]$$

$$= A_c + \cos \phi m(t) \tag{4}$$

When  $\phi$  is close to zero, the detector output in Eq. (4) is very close to the value defined in Eq. (2). However, when  $\phi$  approaches 90°,  $\cos \phi$  approach zero, then the envelope detector output in Eq. (4) reduces to a dc component equal to  $A_c$  with no significant trace of the message signal m(t) being visible. If therefore the phase error  $\phi$  is variable, then the envelope detector output a(t) varies in a corresponding way, which could be undesirable.