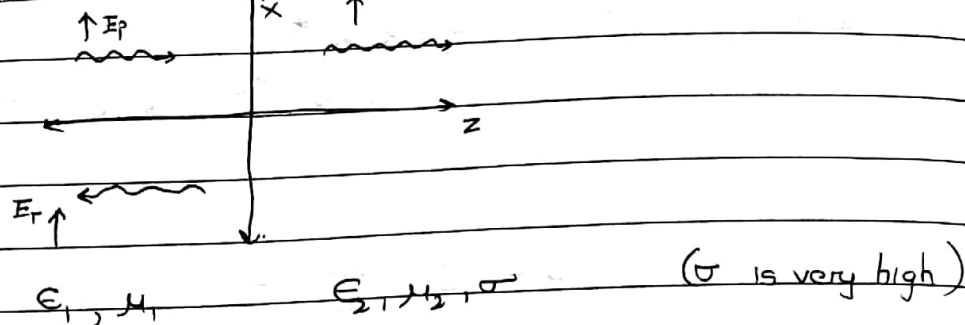


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A] → Lossless Medium - Conductor * Interface



- For medium 2, $\gamma = \alpha + j\beta = (1+j) \sqrt{\frac{\mu\omega\sigma}{2}}$

$$h_2 = \frac{j\omega\mu}{\gamma}$$

- For $z < 0$, (last lecture)

$$S^- = \hat{z} \frac{|E_r|^2}{h_1^*} [1 - |r|^2 + r - r^*] = (\vec{E}_i + \vec{E}_r) \times (\vec{H}_i + \vec{H}_r)^*$$

For $z > 0$

$$S^+ = \vec{E}_t \times \vec{H}_t^* = \hat{z} \frac{|E_0|^2 |T|^2 e^{-2\alpha z}}{h_2^*}$$

- Note :- $|T|^2 = \frac{2h_2}{h_1} (1 - |r|^2 + r - r^*)$

Proof:- LHS :- $T = \frac{2h_2}{h_1 + h_2}$

$$= \frac{2(a + jb)}{a + h_1 + jb}$$

$$|T|^2 = \frac{4(a^2 + b^2)}{(a + h_1)^2 + b^2}$$

$$LHS = RHS$$

$$\therefore S^+ = \hat{z} \frac{|E_0|^2}{h_1} \left[\underbrace{1 - |r|^2}_{\text{real}} + \underbrace{r - r^*}_{\text{imaginary}} \right] e^{-2\alpha z}$$

- At $z=0$, $S^+ = S^-$ ✓✓
- For $z > 0$, the power is getting attenuated exponentially with distance.

$$\begin{aligned} \text{Real Power (time-averaged)} &= \frac{1}{2} \operatorname{Re}(\vec{S} \cdot \hat{z}) \\ &= \frac{1}{2} \times \frac{|E_0|^2}{h_1} [1 - |r|^2] \end{aligned}$$

$$\rightarrow \text{For } z > 0, \quad \vec{J}_t = \sigma \vec{E}_t = \hat{z} E_0 T \sigma e^{-\alpha z}$$

$$\begin{aligned} \text{Real Power dissipated} &= \frac{1}{2} \int_{\text{vol}} \vec{E}_t \cdot \vec{J}_t^* dV \\ &= \frac{1}{2} \int_0^1 \int_0^1 \int_0^\infty \hat{z} E_0 T e^{-\alpha z} \cdot \hat{z} E_0^* T^* \sigma e^{-\alpha z} dz dy dx \end{aligned}$$

considering a 1×1 area in XY plane

$$= \frac{1}{2} \int_0^\infty |E_0|^2 |T|^2 \sigma e^{-2\alpha z} dz$$

$$= \frac{\sigma |E_0|^2 |T|^2}{2 \cdot 4\alpha}$$

$$\text{Real Power entering } z > 0, = \frac{1}{2} \operatorname{Re}(S^+ \cdot \hat{z}) \text{ at } z=0.$$

$$\text{Now, } S^+ = \hat{z} \frac{|E_0|^2 |T|^2}{h_2^*} e^{-2\alpha z}$$

$$n_2 = \frac{(1+j)\alpha}{\sigma} \Rightarrow \frac{1}{n_2^*} = \frac{\sigma}{2\alpha} (1-j)$$

$$\therefore S^+ = \hat{z} |E_0|^2 |T|^2 e^{-2\alpha z} \times \frac{\sigma}{2\alpha} (1+j)$$

$$\therefore \text{Power entering} = \frac{1}{2} \operatorname{Re}(S^+ \cdot \hat{z}) = \frac{|E_0|^2 |T|^2 \sigma}{4\alpha} \text{ at } z_0$$

• $\therefore \text{Real Power entering} = \text{Real Power dissipating} \quad \checkmark$

→ Perfect Conductor ($\sigma \rightarrow \infty$)

$$\delta_s \rightarrow 0, \quad \alpha \rightarrow \infty, \quad n_2 \rightarrow 0$$

• $\Gamma = \frac{n_2 - n_1}{n_2 + n_1} = -1$ ---- perfect reflection

• Because $\alpha \rightarrow \infty$, power in second medium dissipates instantaneously in a very very short distance.

$$\begin{aligned} \vec{E} &= \vec{E}_i + \vec{E}_r = \hat{x} E_0 [e^{-jk_0 z} - e^{+jk_0 z}] \\ &= -\hat{x} 2j E_0 \sin(k_0 z) \end{aligned}$$

$$\begin{aligned} \vec{H} &= \vec{H}_i + \vec{H}_r = \hat{y} \frac{E_0}{h_1} [e^{-jk_0 z} + e^{+jk_0 z}] \\ &= \hat{y} \frac{E_0}{h_1} 2 \cos(k_0 z) \end{aligned}$$

$$- S^- = \vec{E} \times \vec{H}^* = -\hat{z} j \frac{|E_0|^2}{h_1} 4 \cos(k_0 z) \sin(k_0 z)$$

- $\text{Re}(S^-) = 0 \quad \therefore$

No real power is being transmitted.

- Surface current density $= \vec{J}_s = \hat{n} \times \vec{H}^*$
 $= -\hat{z} \times \hat{y} \frac{E_0}{\eta_1} 2 \cos(k_y z)$
 $= \hat{x} \frac{2E_0}{\eta_1} \quad \text{at } z = 0$

* Standing Waves

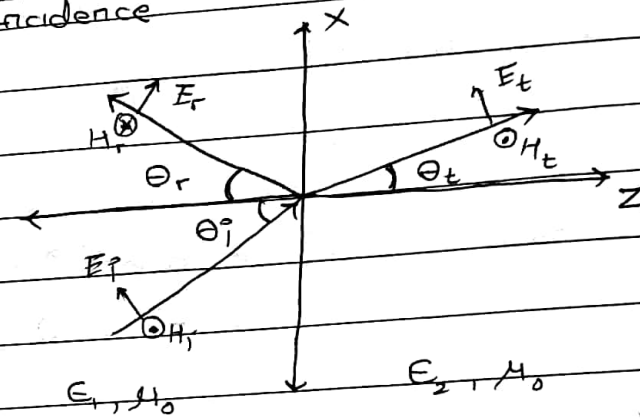
$$\begin{aligned} \vec{E} &= \vec{E}_i + \vec{E}_r = \hat{x} E_0 e^{-jk_y z} + \hat{x} \Gamma E_0 e^{jk_y z} \\ &= \hat{x} \underbrace{E_0 e^{-jk_y z}}_{\text{Travelling Wave}} \underbrace{(1 + \Gamma e^{+j2k_y z})}_{\text{Amplitude modulation of travelling wave}} \end{aligned}$$

- The variation of amplitude of travelling wave is the phenomenon of standing waves

- Standing Wave Ratio = $\frac{\text{Max Amplitude}}{\text{Min Amplitude}} = \frac{1 + |\Gamma|}{1 - |\Gamma|}$

B]

Oblique Incidence



$$E_1 < E_2 \quad (\text{Why?})$$

A Case I

Case I Parallel Polarization

 \vec{E} is in the plane of reflection-transmission

$$\vec{E}_i = E_0 (\hat{x} \cos \theta_i - \hat{z} \sin \theta_i) e^{-jk_1 (\hat{x} \sin \theta_i + \hat{z} \cos \theta_i)}$$

$$\vec{k}_i = k_1 (\hat{x} \sin \theta_i + \hat{z} \cos \theta_i)$$

$$\vec{r} = x\hat{x} + y\hat{y} + z\hat{z}$$

$$k_1 = \omega \sqrt{\mu_0 \epsilon_1}$$

$$\vec{H}_i = \frac{E_0}{\eta_1} \hat{y} e^{-jk_1 (\hat{x} \sin \theta_i + \hat{z} \cos \theta_i)}$$

$$\vec{E}_r = E_0 \Gamma (\hat{x} \cos \theta_r + \hat{z} \sin \theta_r) e^{-jk_1 (\hat{x} \sin \theta_r - \hat{z} \cos \theta_r)}$$

$$\vec{H}_r = \frac{E_0 \Gamma}{\eta_1} (-\hat{y}) e^{-jk_1 (\hat{x} \sin \theta_r - \hat{z} \cos \theta_r)}$$

$$\vec{E}_t = E_0 T (\hat{x} \cos \theta_t - \hat{z} \sin \theta_t) e^{-jk_2 (\hat{x} \sin \theta_t + \hat{z} \cos \theta_t)}$$

$$\vec{H}_t = \frac{E_0 T}{\eta_2} (\hat{y}) e^{-jk_2 (\hat{x} \sin \theta_t + \hat{z} \cos \theta_t)}$$

- At $z=0$, Continuity equations :- $E_{\text{te}} + E_{\text{tr}} = E_{\text{te}}$
 $H_{\text{ty}} + H_{\text{tr}} = H_{\text{ty}}$

$$E_0 \cos \theta_i e^{-jk_1 x \sin \theta_i} + \Gamma E_0 \cos \theta_r e^{-jk_1 x \sin \theta_r} = E_0 T \cos \theta_t e^{-jk_2 x \sin \theta_t}$$

$$\frac{E_0}{n_1} e^{-jk_1 x \sin \theta_i} - \frac{E_0 \Gamma}{n_1} e^{-jk_1 x \sin \theta_r} = \frac{E_0 T}{n_2} e^{-jk_2 x \sin \theta_t}$$

- For i & ii to be always valid, the exponents are equal.

$$\theta_i = \theta_r$$

$$k_1 \sin \theta_i = k_1 \sin \theta_r = k_2 \sin \theta_t$$

- Solve for Γ and T

$$T = \frac{2n_2 \cos \theta_i}{n_1 \cos \theta_i + n_2 \cos \theta_t}$$

$$\Gamma = \frac{n_2 \cos \theta_t - n_1 \cos \theta_i}{n_2 \cos \theta_t + n_1 \cos \theta_i}$$

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- The value of θ_i for which $\Gamma=0$ is called Brewster's Angle (θ_b)

$$\cos \theta_b = \frac{n_2 \cos \theta_t}{n_1}$$

Also use $k_1 \sin \theta_i = k_2 \sin \theta_t$

$$= \sqrt{\frac{\epsilon_1}{\epsilon_2}} \sqrt{1 - \sin^2 \theta_t}$$

$$= \sqrt{\frac{\epsilon_1}{\epsilon_2}} \sqrt{1 - \frac{k_1^2 \sin^2 \theta_b}{k_2^2}}$$

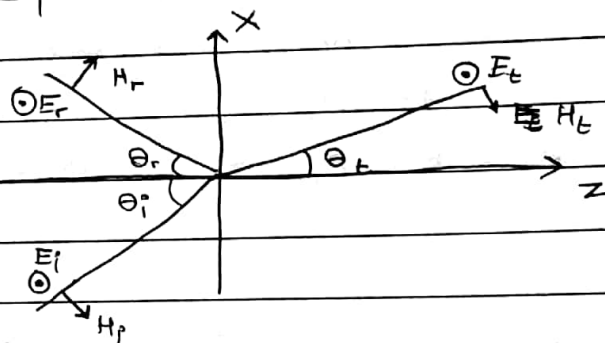
$$\cos \theta_b = \sqrt{\frac{\epsilon_1}{\epsilon_2}} \sqrt{1 - \frac{\epsilon_1 \sin^2 \theta_b}{\epsilon_2}}$$

$$\sin \theta_b = \frac{1}{\sqrt{1 + \epsilon_1/\epsilon_2}}$$

Note:- After reflection, the sense of direction of \vec{E} (leftwards or rightwards) changes.
This will not happen in case of perpendicular polarization.

Case 2 Perpendicular Polarization

\vec{H} is in the plane of reflection-transmission.



★ In perpendicular polarization, the direction of circular polarization reverses after reflection (RHCP \leftrightarrow LHCP)

$$\begin{aligned} \vec{E}_i &= \hat{y} E_0 e^{-jk_1(x \sin \theta_i + z \cos \theta_i)} \\ \vec{H}_i &= \frac{E_0}{h_1} (-\hat{x} \cos \theta_i + \hat{z} \sin \theta_i) e^{-jk_1(x \sin \theta_i + z \cos \theta_i)} \end{aligned}$$

$$\begin{aligned} \vec{E}_r &= \Gamma E_0 \hat{y} e^{-jk_1(x \sin \theta_r - z \cos \theta_r)} \\ \vec{H}_r &= \frac{\Gamma E_0}{h_1} (\hat{x} \cos \theta_r + \hat{z} \sin \theta_r) e^{-jk_1(x \sin \theta_r - z \cos \theta_r)} \end{aligned}$$

$$\begin{aligned} \vec{E}_t &= \hat{y} E_0 T e^{-jk_2(x \sin \theta_t + z \cos \theta_t)} \\ \vec{H}_t &= \frac{E_0 T}{h_2} (-\hat{x} \cos \theta_t + \hat{z} \sin \theta_t) e^{-jk_2(x \sin \theta_t + z \cos \theta_t)} \end{aligned}$$

- Continuity at $z=0$. :- i) $E_{iy} + E_{ry} = E_{ty}$
ii) $H_{ix} + H_{rx} = H_{tx}$

• Results :-

i) $k_1 \sin \theta_i = k_2 \sin \theta_r = k_2 \sin \theta_t$

ii) $\theta_i = \theta_r$

iii) $R = \frac{n_2 \cos \theta_i - n_1 \cos \theta_t}{n_2 \cos \theta_i + n_1 \cos \theta_t}$, $T = \frac{2n_2 \cos \theta_i}{n_2 \cos \theta_i + n_1 \cos \theta_t}$

• Brewster's Angle :-

$$n_2 \cos \theta_i = n_1 \cos \theta_t$$

$$\sin^2 \theta_i (\underbrace{n_1^2 k_1^2 - n_2^2 k_2^2}_{\text{always zero}}) = (n_1^2 - n_2^2) k_2^2$$

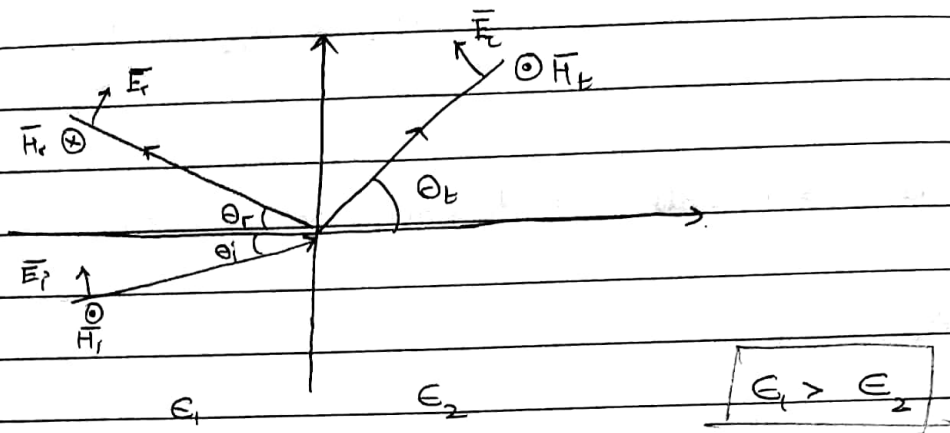
Brewster's angle does not exist.

* Polarization lenses :-

★ At Brewster's angle, the wave is polarized only in one direction (parallel, not perpendicular).

Hence, reflected wave ~~is~~ is not received by the lens

Case 3 Total (Internal) Reflection.



- For critical angle $\theta_i = \theta_c$, $\theta_t = \frac{\pi}{2}$

Since $k_1 \sin \theta_i = k_2 \sin \theta_t$, $\sin \theta_c = \frac{k_2}{k_1} = \sqrt{\frac{\epsilon_2}{\epsilon_1}}$

- Consider $\theta_i > \theta_c$

$$\Rightarrow \sin \theta_t > 1$$

$$\Rightarrow \cos \theta_t = \sqrt{1 - \sin^2 \theta_t} \text{ ----- Imaginary}$$

Let $k_2 \sin \theta_t = \beta$ and $k_2 \cos \theta_t = j\alpha$

$$E_t = E_0 T \left(\frac{j\alpha}{k_2} \hat{x} - \frac{\beta}{k_2} \hat{z} \right) e^{-j\beta x} e^{\alpha z}$$

$$H_t = \frac{E_0 T}{h_2} \left(\hat{y} \right) e^{-j\beta x} e^{\alpha z}$$

α is negative
 \Rightarrow Attenuation of E_t, H_t in medium 2.

Use Helmholtz's Equation:-

$$\nabla^2 H_t + k_2^2 H_t = 0$$

$$(-\beta^2 + \alpha^2 + k_2^2) H_t = 0$$

$$\therefore \alpha^2 - \beta^2 + k_2^2 = 0$$

The expressions for E_i, H_i, E_r, H_r remain as seen in case (

- Use continuity at $z = 0$

$$- k_1 \sin \theta_i = k_2 \sin \theta_r = \beta = k_2 \sin \theta_t \quad \dots \text{equating exponents}$$

$$\theta_i = \theta_r \quad \dots \text{as before}$$

- Two simultaneous equations for Γ and T .

$$\frac{E_i}{h_1} - \frac{E_r}{h_1} = \frac{E_t}{h_2} \quad E_i \cos \theta_i + E_r \cos \theta_r = \frac{E_t}{k_2} \cos \theta_t$$

$$\text{Solve: } \Gamma = \frac{n_2 \left(\frac{j\alpha}{k_2} \right) - h_1 \cos \theta_i}{n_2 \left(\frac{j\alpha}{k_2} \right) + h_1 \cos \theta_i}, \quad T = \frac{2 h_2 \cos \theta_i}{h_2 \left(\frac{j\alpha}{k_2} \right) + h_1 \cos \theta_i}$$

$$\text{Note: } |\Gamma| = 1$$

$$- \text{Now, } \bar{S}_i = \bar{E}_i \times \bar{H}_i^* = \frac{|E_0|^2}{h_1} (\hat{z} \cos \theta_i + \hat{x} \sin \theta_i)$$

$$\bar{S}_r = \bar{E}_r \times \bar{H}_r^* = -\frac{|E_0|^2}{h_1} |\Gamma|^2 (\hat{z} \cos \theta_i - \hat{x} \sin \theta_i)$$

$$\begin{aligned} \text{Real Power transmitted} &= \text{Re} \left((\bar{E}_i + \bar{E}_r) \times (\bar{H}_i + \bar{H}_r)^* \right) \\ &= \bar{S}_i + \bar{S}_r \quad (\text{seen previously}) \end{aligned}$$

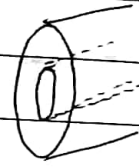
$$= \frac{|E_0|^2}{h_1} \cancel{2 \sin \theta_i} \hat{x}$$

- No power is being transmitted along Z , into medium 2

$$\begin{aligned} - \text{Also, } \bar{S}_t &= \bar{E}_t \times \bar{H}_t^* \\ &= \frac{|E_0|^2 |T|^2}{h_z} e^{2\alpha z} \left(\frac{j\alpha}{k_z} \hat{z} + \frac{\beta}{k_z} \hat{x} \right) \end{aligned}$$

- Z component is imaginary \Rightarrow No real power flowing
- Standing wave along Z direction.

* Coaxial Cables

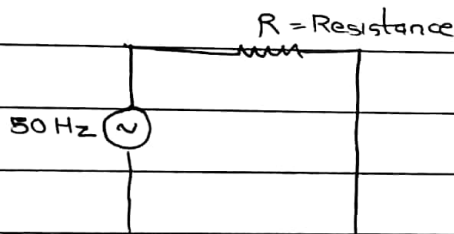


\vec{E} is in radial direction.

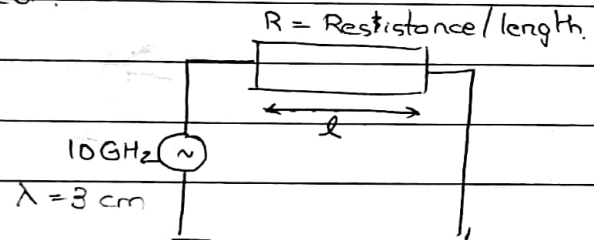
\vec{H} is in tangential (concentric circular) direction

* Distributed Circuits

When wavelengths of EM waves become ^{comparable to circuit size} ~~large~~, we cannot assume circuit elements to be localized.



Lumped-element
circuit



Distributed
circuit

- When studying distributed circuits, we cannot assume two points connected by a conductor to be at same potential.

$$\begin{array}{ccc} \varphi(z, t) & & \varphi(z + \Delta z, t) \\ \downarrow & \text{---} & \downarrow \\ \psi(z, t) & \text{---} & \psi(z + \Delta z, t) \end{array}$$

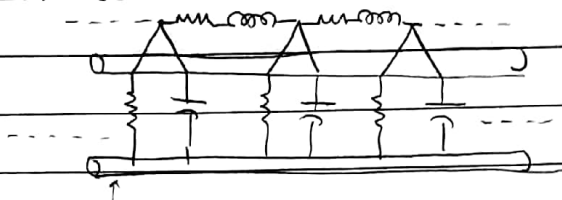
Define L, C, R, G to be inductance, capacitance, resistance, conductance per unit length.

- This happens in transmission lines, which run for several kilometres, because wavelength is comparable to length.

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→ Transmission Lines

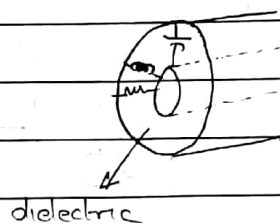
- R, L, C are all distributed. There are some R, L, C between two wires as well, outer and inner conductors of coaxial cables



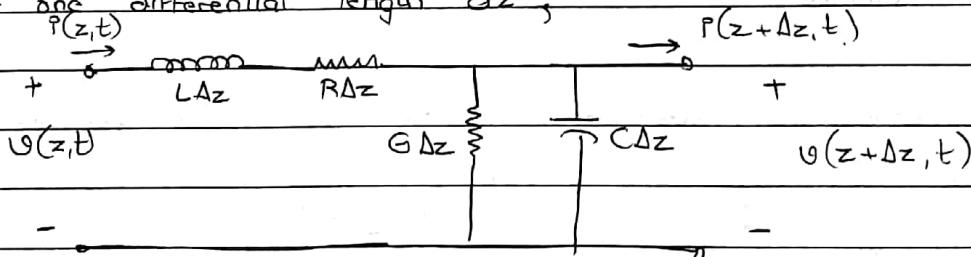
Series R, L

Parallel G, C

- Coaxial Cables have C, G along radial direction



- For one differential length dz ,



$$V(z, t) - i(z, t)RAz =$$

- $L, R, G, C \sim H/m, \Omega/m, S/m, F/m$

$$V(z, t) - i(z, t)RAz - LAz \frac{\partial i(z, t)}{\partial t} = V(z + \Delta z, t) \quad \text{--- KVL}$$

$$\lim_{\Delta z \rightarrow 0} \frac{V(z + \Delta z, t) - V(z, t)}{\Delta z} = -Ri(z, t) - L \frac{\partial i(z, t)}{\partial t}$$

$$\therefore \frac{\partial V(z, t)}{\partial z} = -Ri(z, t) - L \frac{\partial i(z, t)}{\partial t}$$

$$\bullet \quad -v(z+\Delta z, t)G - C \frac{\partial v(z+\Delta z, t)}{\partial t} = \lim_{\Delta z \rightarrow 0} \frac{i(z+\Delta z, t) - i(z, t)}{\Delta z}$$

$$\therefore \quad \boxed{\frac{\partial i(z, t)}{\partial z} = -G v(z, t) - C \frac{\partial v(z, t)}{\partial t}} \quad \text{--- KCL}$$

- $v(z, t) = V(z)e^{j\omega t}$ and $v(z, t) = V(z)\cos\omega t$ are both solutions for the voltage. Similarly, $i(z, t) = I(z)e^{j\omega t}$ and $i(z, t) = I(z)\cos\omega t$.

- Substitute in KVL.

$$\frac{\partial V(z)}{\partial z} = -(R + j\omega L) I(z)$$

- Substitute in KCL

$$\frac{\partial I(z)}{\partial z} = -(G + j\omega C) V(z)$$

- These equations are similar to Maxwell's equations. Hence, we also have counterparts of Helmholtz's equation.

$$\begin{aligned} \frac{\partial^2 V(z)}{\partial z^2} &= -(R + j\omega L) \frac{\partial I(z)}{\partial z} \\ &= (R + j\omega L)(G + j\omega C) V(z) \end{aligned}$$

Write $\gamma = \sqrt{(R + j\omega L)(G + j\omega C)} = \alpha + j\beta = \text{'Propagation constant'}$

$$\therefore \quad \frac{\partial^2 V(z)}{\partial z^2} = \gamma^2 V(z)$$

Voltage wave travelling backwards,

$$V(z) = \underbrace{V_0^+ e^{-\gamma z}}_{\text{Voltage wave travelling forward}} + V_0^- e^{\gamma z}$$

Voltage wave travelling forward

$$\text{ii } \frac{\partial^2 I(z)}{\partial z^2} = \gamma^2 I(z)$$

$$\therefore I(z) = I_0^+ e^{-\gamma z} + I_0^- e^{+\gamma z}$$

• Substitute these in previous equations.

$$\frac{\partial V(z)}{\partial z} = -(R + j\omega L) I(z)$$

$$-\gamma V_0^+ e^{-\gamma z} + \gamma V_0^- e^{+\gamma z} = -(R + j\omega L) (I_0^+ e^{-\gamma z} + I_0^- e^{+\gamma z})$$

$$\therefore -\gamma V_0^+ = -(R + j\omega L) I_0^+, \quad \gamma V_0^- = -(R + j\omega L) I_0^-$$

$$\therefore I_0^+ = \frac{V_0^+ \gamma}{R + j\omega L}$$

$$I_0^- = \frac{-V_0^- \gamma}{R + j\omega L}$$

Define 'characteristic impedance' $= Z_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$

$$\therefore I_0^+ = \frac{V_0^+}{Z_0}, \quad I_0^- = \frac{-V_0^-}{Z_0}$$

$$* \quad \gamma = \alpha + j\beta$$

Lossless medium $\therefore \alpha = 0$

$$\Rightarrow R = G = 0$$

$$\Rightarrow \gamma = j\beta = j\omega \sqrt{LC}$$

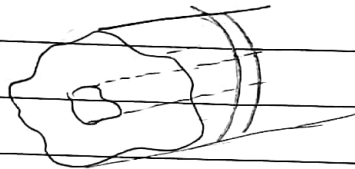
$$\beta = \omega \sqrt{LC}, \quad Z_0 = \sqrt{\frac{L}{C}}$$

$$\text{Wavelength} = \lambda = \frac{2\pi}{\beta}$$

$$\text{Phase velocity} = v_p = \frac{1}{\sqrt{LC}}$$

I CALCULATING G.R.L.C

Consider an arbitrary cable.



$$\text{Total Magnetic energy} = \frac{1}{2} \int_{\text{vol}} \vec{B} \cdot \vec{H}^* d\vec{v} \quad \leftarrow \begin{array}{l} \text{CS volume (length } l, \\ \text{area } S) \end{array}$$

$$= \frac{\mu}{2} \int_{\text{vol}} \vec{H} \cdot \vec{H}^* d\vec{v}$$

Time averaged

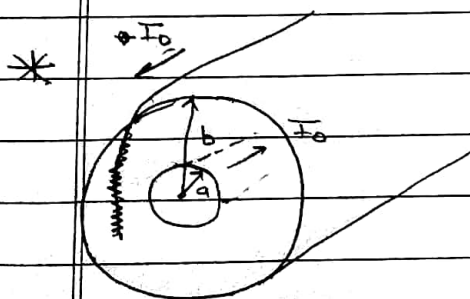
$$\text{Magnetic energy stored per unit length} = \frac{\mu}{4} \int_S \vec{H} \cdot \vec{H}^* dS$$

$\frac{1}{2}$ comes from \cos^2 from $\vec{H} \cdot \vec{H}^*$

$$\text{This should be equal to } \frac{1}{2} \left(\frac{1}{2} L |I_0|^2 \right)$$

because I is sinusoidal

$$\therefore \boxed{L = \frac{\mu}{|I_0|^2} \int_S \vec{H} \cdot \vec{H}^* dS}$$



$$\left. \begin{aligned} \vec{E} &= \frac{V_0 e^{-\gamma z} \hat{S}}{S \ln(b/a)} \\ \vec{H} &= \frac{I_0 e^{-\gamma z} \hat{\phi}}{2\pi S} \end{aligned} \right\} \text{for } a < S < b$$

--- Proof later

$S < a$ is solid metal

$S = b$ is hollow metal

Outside $S = b$, $E = H = 0$

$H = 0$ by Ampere's law

($I_{\text{enc}} = 0$, because equal and opposite currents are flowing)

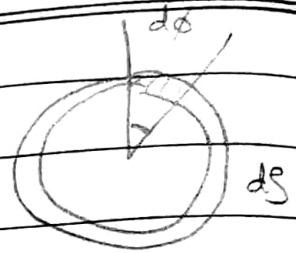
P.T.O

$$\text{Find } L = \frac{\mu}{|I_0|^2} \int \vec{H} \cdot \vec{H}^* ds$$

$$\hookrightarrow I_0 = I_0 e^{-\alpha z}$$

$$= \frac{\mu}{I_0^2 e^{-2\alpha z}} \int_a^b \int_0^{2\pi} \frac{I_0^2 e^{-2\alpha z}}{4\pi^2 s^2} s ds d\phi$$

$$= \frac{\mu}{2\pi} \ln(b/a)$$



$$ds = (s d\phi)$$