



## EE 302: Control Systems

Instructor: VR Sule

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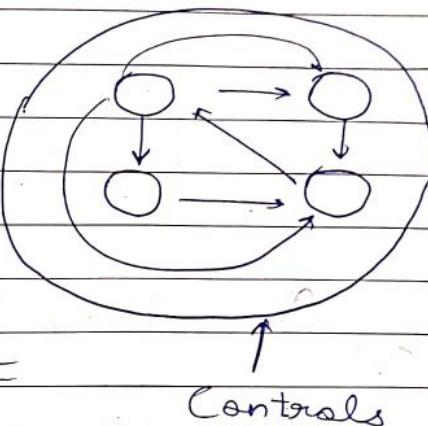
Syllabus: OL, CL Systems, Modelling & Repre.  
 Differential Equations, Transfer functions,  
 Block Diagram, Flow Graph, Root locus  
 Design, Stability Analysis, Design of  
 Controller and Observer.

B.1.19

- System: Interacting parts

Responses ←

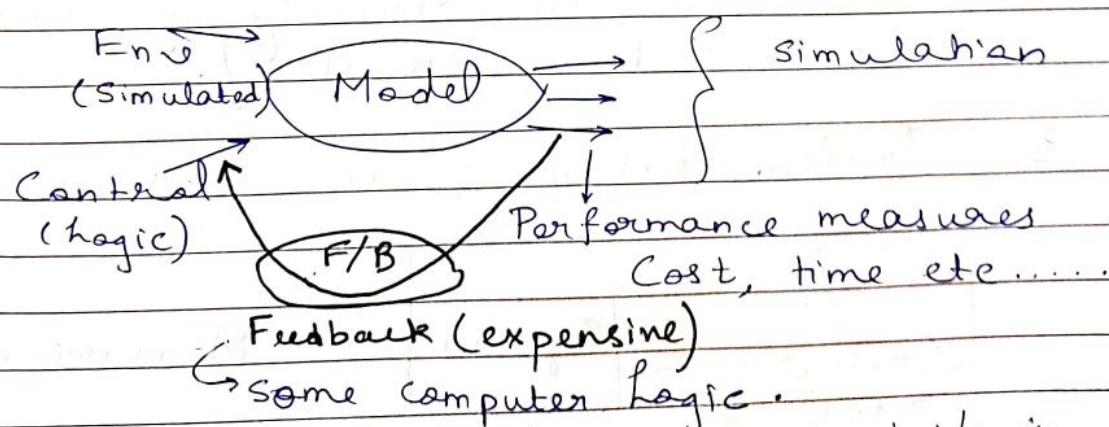
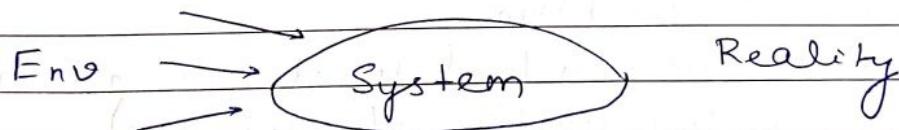
Environment



Controls

Causes → System → Effects  
 Uncontrolled Choices

→ What's a Simulation?

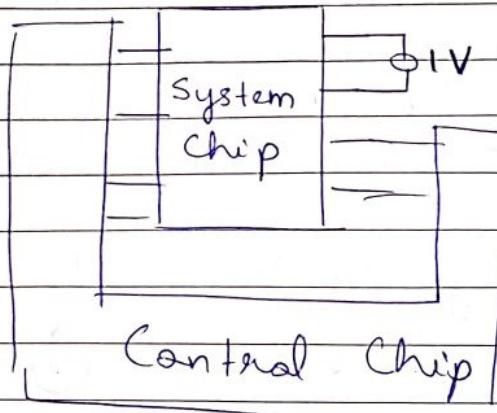


→ Feedback required when uncertainty in i/p -- o/p relations

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→ Recent Work: Physically Defined Control

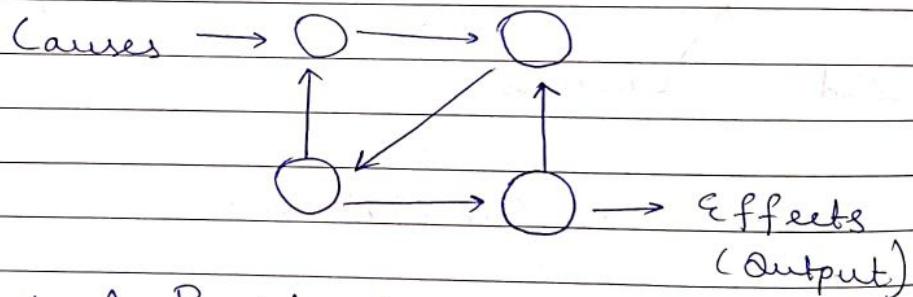


- Textbooks
- 1) Control Systems - Norman Nise
  - 2) Doyle, Francis, Tannenbaum: Feedback control theory
  - 3) Chua et al Linear & Non-Linear Networks
  - 4) Wolovich: Automatic Control Systems

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Recap

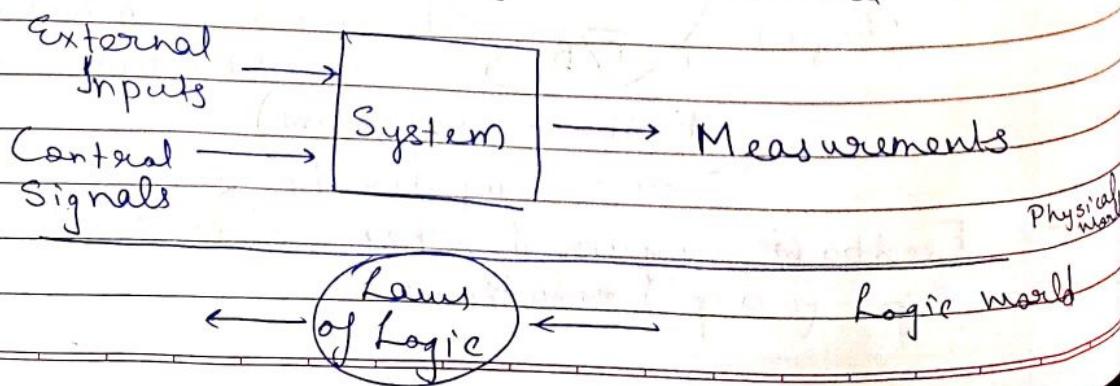
1. What is a System



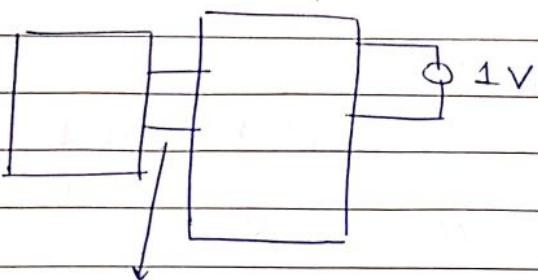
2. Control Problem:

- Change the control inputs to get desired outputs (quality of outputs)
- Under the uncertainty of external causes and system itself.

3. Implementation of the Control



- Designing compensations is also a control problem

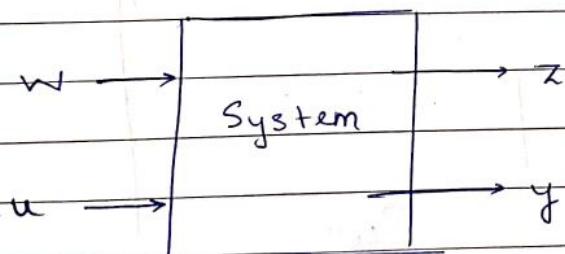


When both are connected they work well, else not

#### 4. Model of System

- Physical world reconstructed inside computer logic is called a Simulation
- Model along with environmental inputs is necessary for control.

#### Notation



- Labelling / Classification of I/Os  
overlap b/w different sets is allowed

w : exogenous inputs (ex. Ref. value)  
u : Control inputs

y : Response Measurements (for quality control)

z : Regulated outputs.

(outputs which determine the performance)

# Classes of Systems

## 1. Memoryless Systems :

Systems which react to inputs instantaneously

## 2. Systems with Memory

React to current inputs and past history of inputs

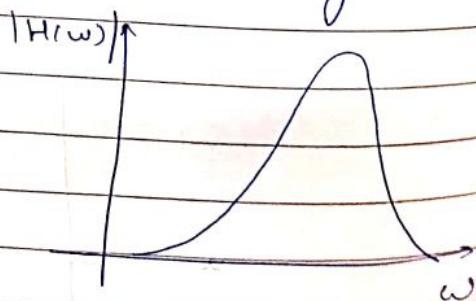
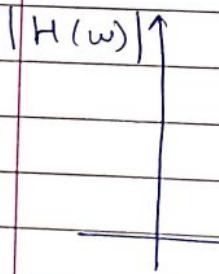
→ Encoded as the State of the system

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## Causal System :

- Whose state  $x(t)$  and outputs  $y(t)$  are dependent only on inputs  $w(\tau), u(\tau)$  for  $\tau \in (-\infty, t]$

- Weiner's Conditions for causality



Transfer function :  $R(s) = \frac{q(s)}{P(s)}$

$P(s) \neq 0$  polynomial

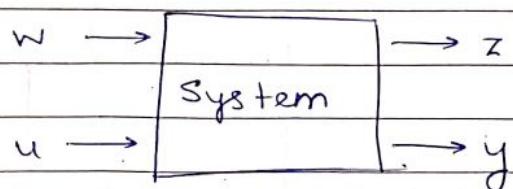
~~deg~~ Condition for Causality  
 $\deg(q(s)) \leq \deg(P(s))$

Book :

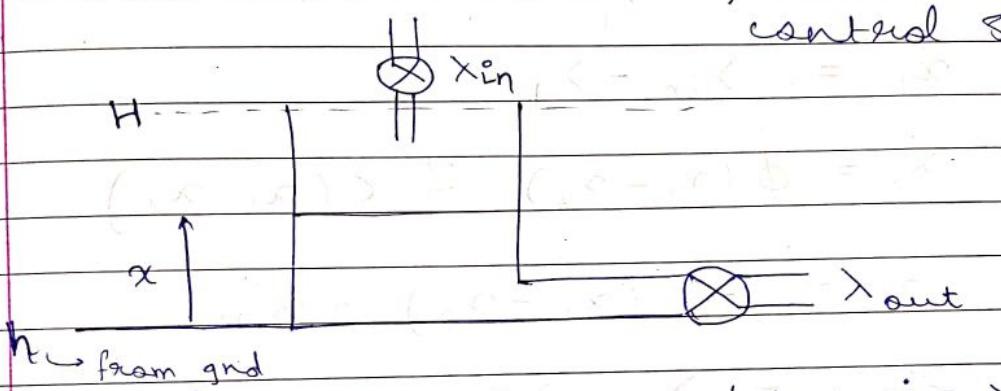
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## Examples of Systems

Recap : Four block model of a system



1. Dose tank / Flush tank / Water level control system



$$\dot{x} \propto \lambda_{in} - \lambda_{out}, \text{ take: } \dot{x} = \lambda_{in} - \lambda_{out}$$

$$\lambda_{out} = \phi(x(t)) \approx f x(t)$$

Non linear      Approx.

$$\lambda_{in} \in \{0, \lambda_{in}\}$$

State Space Model :

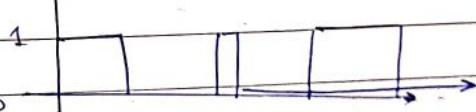
state  $x(t)$

input  $\lambda_{in}$  (our control)

external input  $\{0, 1\}$

$$h \leq x(t) \leq H$$

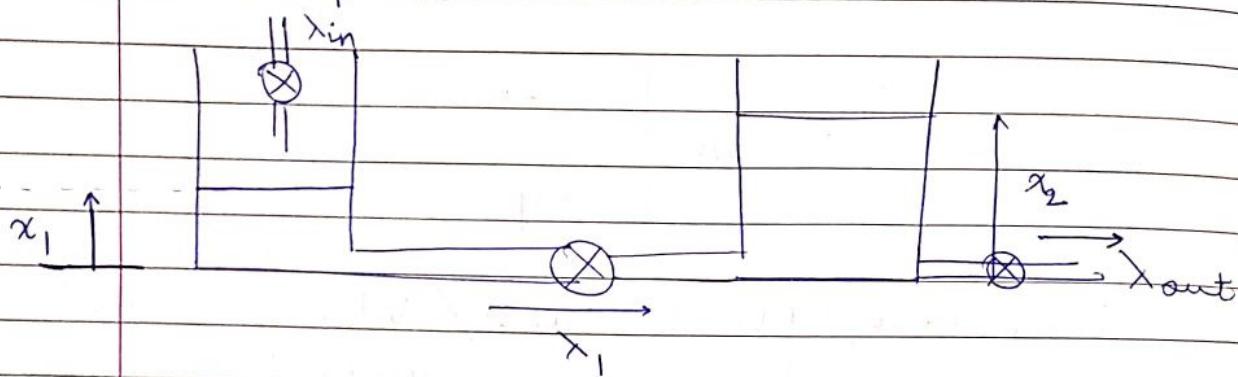
ON/OFF



Model is applicable for :-

- Inventory Control
- Warehouse Control
- Bank Account with spending
- Comm. Networks (Buffers)

## 2. Coupled tanks



$$\dot{x}_1 = \lambda_{in} - \lambda_1$$

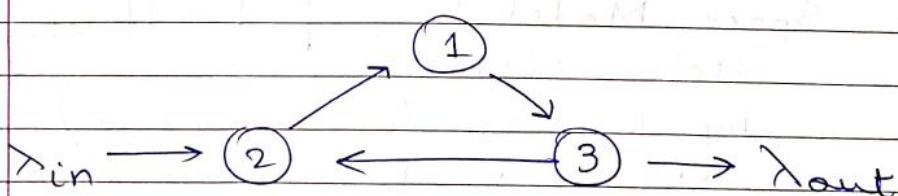
$$\lambda_1 = \phi(x_1, -x_2) \approx c(x_1 - x_2)$$

$$\dot{x}_1 = -c(x_1 - x_2) + \lambda_{in}$$

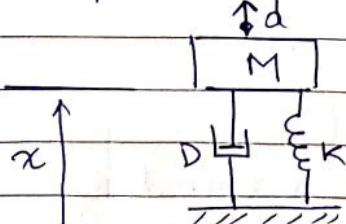
$$\dot{x}_2 = \lambda_1 - \lambda_{out}$$

$$\lambda_{out} \approx f x_2$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -c & c \\ c & -c \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \lambda_{in}$$



## 3. Suspension System

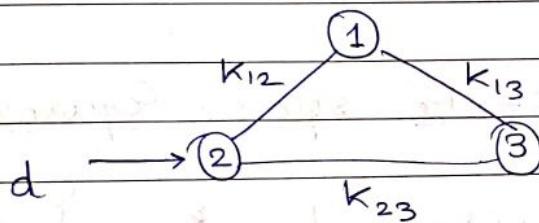


$$M \ddot{x} = -Mg - Dx - Kx + d$$

Let,  $x_1 = x$   $x_2 = \dot{x}_1$

$$\begin{bmatrix} \dot{x} \\ \ddot{x} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -K/M & -D/M \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ -g+d/M \end{bmatrix}$$

### Coupled Mass Systems



$$\vec{r}_1 = \begin{bmatrix} x_1 \\ y_1 \end{bmatrix} \quad \vec{r}_3 = \begin{bmatrix} x_3 \\ y_3 \end{bmatrix}$$

$$\ddot{\vec{r}}_1 = -k_{12} \vec{r}_1$$

$$\ddot{\vec{r}}_3 = -k_{13} (\vec{r}_3 - \vec{r}_1)$$

$$\ddot{\vec{r}}_2 = d$$

### Four Block Model of a system

$$\dot{x} = Ax + B_1 u + B_2 w$$

$$y = C_1 x + D_1 u + D_2 w$$

$$z = C_2 x + D_3 u + D_1 w$$

The interface ...  
half of the band gap, will ...  
uniformly distributed in ...  
However, assume symmetric ...  
than.

-1cm, kSi=12.

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## Background Assumed

1. Laplace transform
2. Solutions of Differential Equations
3. Impulse response, step response
4. Frequency Response plots
  - Gain
  - Phase
5. Network Theory basics

Chapter 2, Norman Nise → Also exam  
Numerical problems

→ Examples of state space equations

Circuits : Capacitor,  $L$ ,  $R$ ,  $\{$  energy storing  
 $\}$  controlled sources :  $V_{CVS}$ ,  $V_{CCS}$   
 $C_{CVS}$ ,  $C_{CCS}$

Transformers, Gyrator

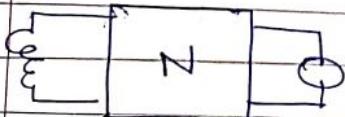
→ "Resistive"

Independent Sources : Voltage, Current

(choose the)  
State var.  
to be  
 $v_c$  and  $i_L$ )

$$v_c : \text{Cap. voltage} = C \frac{dv_c}{dt}$$
$$i_L : \text{Inductor voltage} = L \frac{di_L}{dt}$$

First order circuits

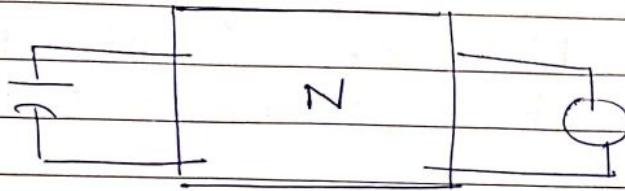


Resistive

First order circuits

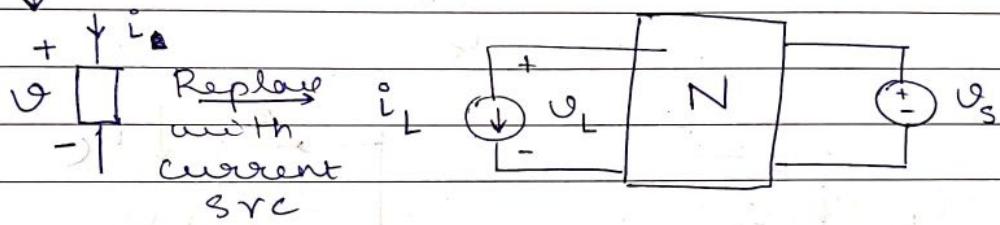
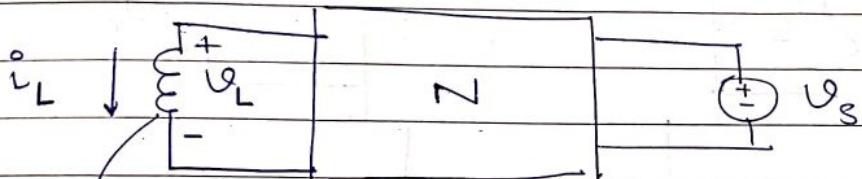
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First order  $\Rightarrow$  Single Inductor  
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 Youva Capacitor



### Sign Convention

1)

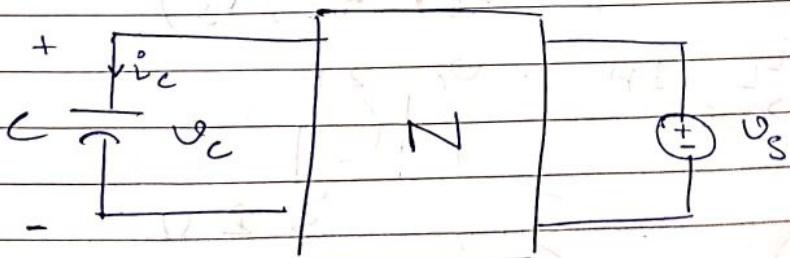


~~Y~~  $L \rightarrow$  Linear operators

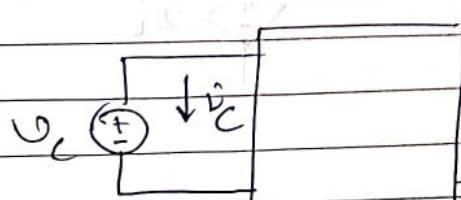
$$V_L = L(i_L, V_s)$$

$$L \frac{di_L}{dt} (= L(i_L, V_s))$$

2)



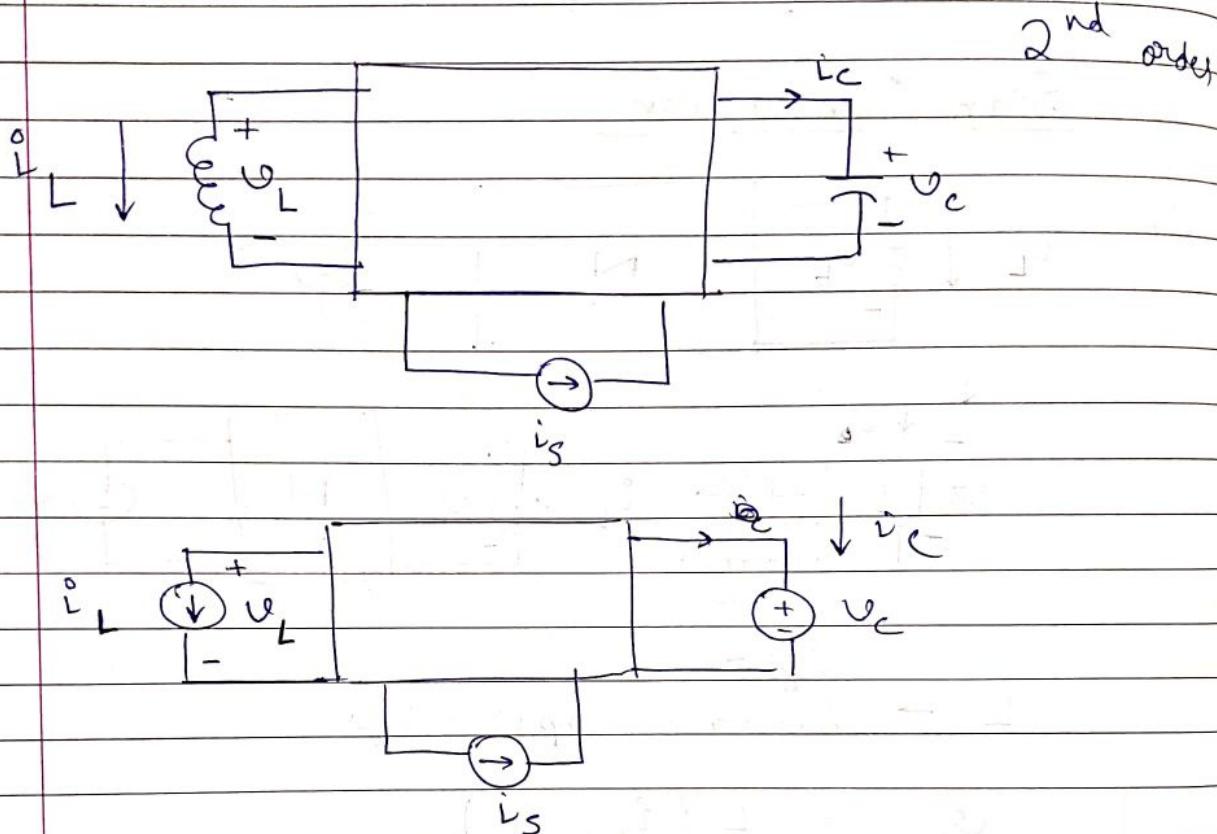
$$i_C = C \frac{dV_C}{dt}$$



$$C \frac{dV_C}{dt} = L(V_C, V_s)$$

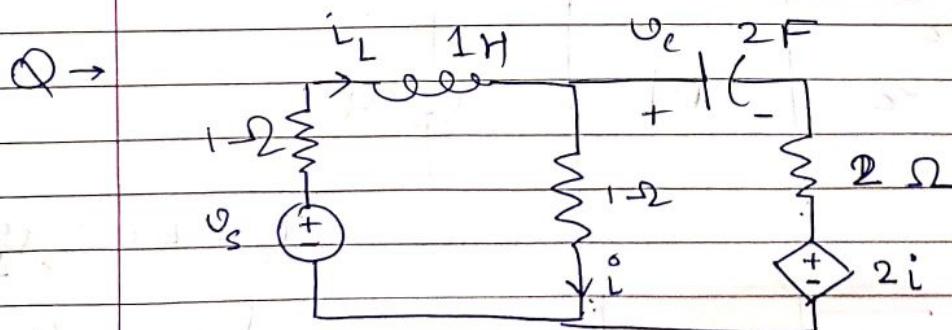
3)

2 port Network, Constant Source  
get their seen port

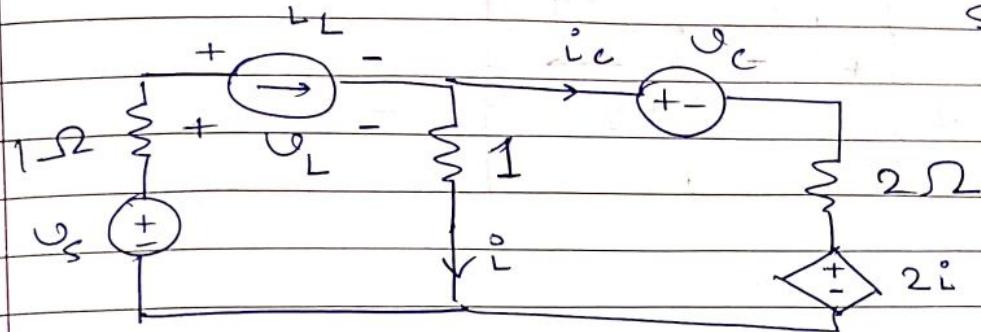


$$v_L = f_1(i_L, v_C, i_S)$$

$$i_C = f_2(i_L, v_C, i_S)$$

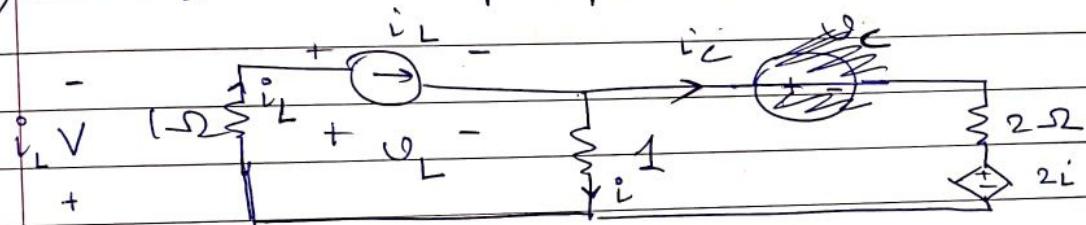


→ Convert to current src / voltage source



→ Find  $V_L$ ,  $i_c$

1)  $V_L$ : 3 Superposition K.V.L's



$$\overset{\circ}{i}_c + \overset{\circ}{i} = \overset{\circ}{i}_L$$

$$\overset{\circ}{i} = 2\overset{\circ}{i}_c + 2\overset{\circ}{i}$$

$$-\overset{\circ}{i} = 2\overset{\circ}{i}$$

$$\overset{\circ}{i}_c + 2\overset{\circ}{i}_c \quad \overset{\circ}{i} = -2\overset{\circ}{i}_c$$

$$-\overset{\circ}{i}_c = \overset{\circ}{i}_L$$

$$\overset{\circ}{i} = 2\overset{\circ}{i}_L$$

$$V_L = -\overset{\circ}{i}_L - \overset{\circ}{i}$$

Get in the form,

$$\begin{bmatrix} \frac{dV_c}{dt} \\ \frac{di_L}{dt} \end{bmatrix} = \begin{bmatrix} a_1 & a_2 \\ a_3 & a_4 \end{bmatrix} \begin{bmatrix} V_c \\ i_L \end{bmatrix} + \begin{bmatrix} b_1 \\ b_2 \end{bmatrix} U_s$$

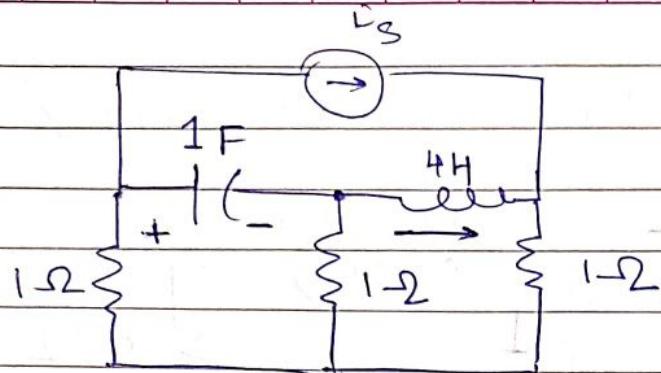
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2)



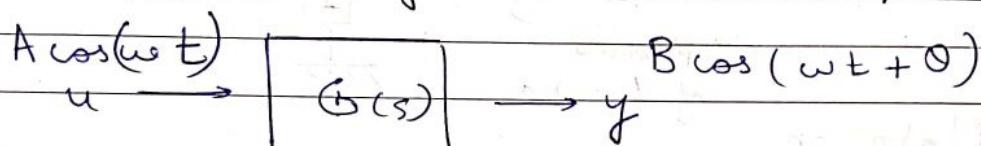
2)

# Modeling of LTI (Linear Time Invariant) Systems

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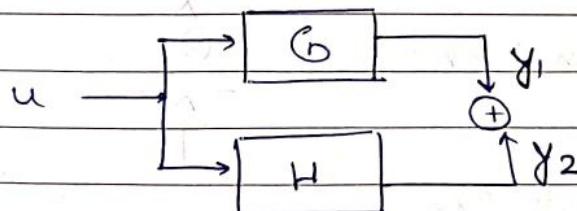
- Norman Nise, Chap 1, examples / classification of some common control systems
- In time domain : Linear constant coefficient differential Equations (LCCDE's)
- In frequency / Laplace domain : These are transfer functions

## Block Diagrams / Transfer functions

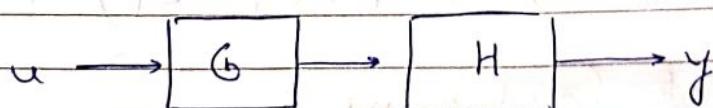


$$G(s) = \frac{y(s)}{u(s)}$$

1) Sum of Systems : ~~of~~

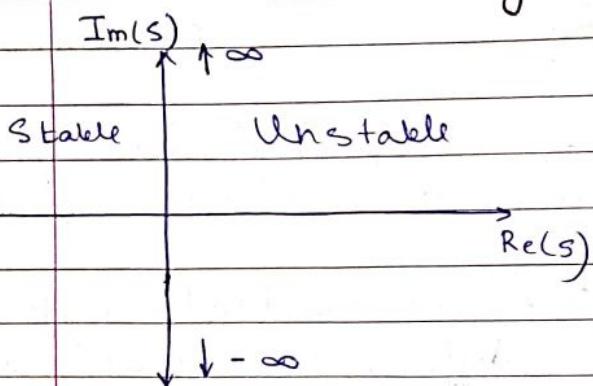


2) Cascade



$\mathcal{S}$  : Set of Stable Systems

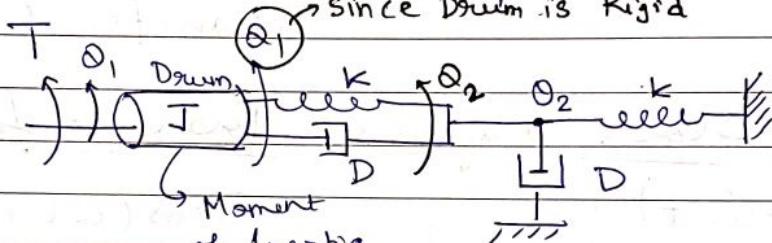
# Stability & Laplace transform



(Q1)

LCCDE's

State-space equations

Notation

Time domain

$$\ddot{\theta}_1$$

$$\ddot{\theta}_2$$

$$\ddot{T}$$

Freq. domain

$$\theta_2(s) \text{ or } \hat{\theta}_2$$

$$T(s) \text{ or } \hat{T}$$

Transfer function:

$$\frac{\hat{\theta}_2}{\hat{T}}$$

(1)

Write Diff. eqn.

$$T = J_1 \ddot{\theta}_1 + D(\dot{\theta}_1 - \dot{\theta}_2) + K(\theta_1 - \theta_2)$$

$$K(\theta_2 - \theta_1) + D(\dot{\theta}_2 - \dot{\theta}_1) + D\dot{\theta}_2 + K\theta_2 = 0$$

Initial Conditions

$$\theta_1(0) = \theta_2(0) = 0$$

2)

# Chapter 2 Examples

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$$\ddot{\theta}_1 + s^2 J \hat{\theta}_1 + sD(\hat{\theta}_1 - \hat{\theta}_2) + K(\hat{\theta}_1 - \hat{\theta}_2)$$

(2) Take Laplace transforms

$$\ddot{\theta} = s^2 J \hat{\theta}_1 + (\hat{\theta}_1 - \hat{\theta}_2)(Ds + K)$$

$$K(\hat{\theta}_2 - \hat{\theta}_1) + sD(\hat{\theta}_2 - \hat{\theta}_1) + sD\hat{\theta}_2 + K\hat{\theta}_2 = 0$$

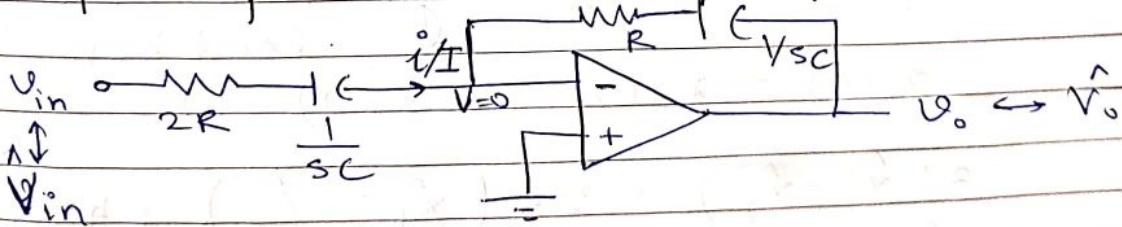
$$= 2(K + sD)(\hat{\theta}_2) - (K + sD)\hat{\theta}_1$$

$$\Rightarrow \hat{\theta}_1 = 2\hat{\theta}_2$$

$$\Rightarrow \ddot{\theta} = 2s^2 J \hat{\theta}_2 + \hat{\theta}_2(Ds + K)$$

$$\Rightarrow G(s) = \frac{\hat{\theta}_2}{\ddot{\theta}} = \left( \frac{1}{2Js^2 + Ds + K} \right)$$

2) Op-Amp Ckt Transfer function



$i \leftrightarrow I(s)$   
time domain      freq domain

find the transfer function:

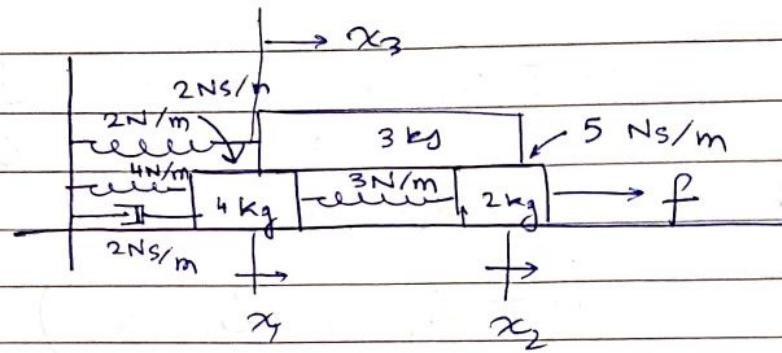
$$\frac{\hat{V}_o}{\hat{V}_{in}} = - \frac{\hat{V}_o}{\left( R + \frac{1}{sC} \right)} \Rightarrow - \left( R + \frac{1}{sC} \right) \frac{\hat{V}_o}{\hat{V}_{in}}$$

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→ Find the transfer function

$$2\ddot{x}_2 = f - 3x_2 - 5(x_2 - x_3)$$

$$\text{Block 2} \quad f = 2\ddot{x}_2 + 3x_2 + 5(x_2 - x_3) + 3(x_2 - x_1)$$

$$\text{Block 1} \quad 3(\dot{x}_1 - \dot{x}_2) + 2(\dot{x}_1 - \dot{x}_3) + 4x_1 + 2\dot{x}_1 + 4\ddot{x}_1 = 0$$

$$\text{Block 3} \quad 2x_3 - 2\dot{x}_3 + (\dot{x}_3 - \dot{x}_1) \times 2 + (\dot{x}_3 - \dot{x}_2) \times 5 + 3\ddot{x}_3$$

→ Laplace transforming with zero initial condition (I.C.)

$$x_1(0) = x_2(0) = x_3(0) = 0$$

$$3(\hat{x}_1 - \hat{x}_2) + 2s(\hat{x}_1 - \hat{x}_3) + 4\hat{x}_1 + 2s\hat{x}_1 + 4s^2\hat{x}_1$$

$$= (4s^2 + 2s + 7)\hat{x}_1 - 3\hat{x}_2 - 2s\hat{x}_3 = 0$$

$$-3\hat{x}_1 + (2s^2 + 5s + 3)\hat{x}_2 - 5s\hat{x}_3 = \hat{F}$$

$$-2s\hat{x}_1 + 6s\hat{x}_2 - 5s\hat{x}_3 + (3s^2 + 7s + 2) = 0$$

$$\begin{bmatrix} 4s^2 + 2s + 7 & -3 & -2s \\ -3 & 2s^2 + 5s + 3 & -5s \\ -2s & -5s & 3s^2 + 7s + 2 \end{bmatrix}$$

$$x \begin{bmatrix} \hat{x}_1 \\ \hat{x}_2 \\ \hat{x}_3 \end{bmatrix} = \begin{bmatrix} 0 \\ \hat{F} \\ 0 \end{bmatrix}$$

→ Solution beyond this?

1) Find Determinant of  $P(s)$ ; use Gramer's Rule  
 $\det(P(s)) \neq 0$

2) Invert the Matrix

$$P(s)^{-1} = \frac{\text{adj } P(s)}{\det P(s)}$$

### State Space Equations

• 2<sup>nd</sup> order state space system

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -6 & -5 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$y = \cancel{[1 \ 0]} \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$u \rightarrow \text{input}, y \rightarrow \text{output}$

$$\textcircled{a} \quad \begin{aligned} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= -6x_1 - 5x_2 + u \\ y &= x_1 \end{aligned} \quad \begin{aligned} s\hat{x}_1 &= \hat{x}_2 \\ \hat{x}_2 &= -6\hat{x}_1 - 5\hat{x}_2 + \hat{u} \\ \hat{y} &= \hat{x}_1 \end{aligned}$$

$$\text{T.F.} = \frac{\hat{y}}{\hat{u}} \quad X = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\begin{aligned} s\hat{x}_1 &= \hat{x}_2 \\ s\hat{x}_2 &= -6\hat{x}_1 - 5\hat{x}_2 + \hat{u} \\ \hat{y} &= \hat{x}_1 \end{aligned}$$

$$\textcircled{b} \quad \begin{aligned} 6s\hat{x}_1 &= -6\hat{x}_1 + \hat{u} \\ s^2\hat{x}_1 &= -6\hat{x}_1 - 5s\hat{x}_1 + \hat{u} \\ (s^2 + 5s + 6)\hat{x}_1 &= \hat{u} \end{aligned}$$

$$\left| \begin{array}{l} \hat{y} = \frac{1}{s^2 + 5s + 6} \hat{u} \end{array} \right| \quad \begin{matrix} \Leftrightarrow \\ \text{equivalent} \\ \text{to} \end{matrix} \quad \left[ \begin{array}{cc|c} 0 & 1 & 0 \\ -6 & -5 & 1 \end{array} \right]$$

$$\left[ \begin{array}{c|c} A & b \\ \hline c & d \end{array} \right] = \left[ \begin{array}{cc|c} 0 & 1 & 0 \\ -6 & -5 & 1 \\ \hline 1 & 0 & 0 \end{array} \right]$$

$$\begin{aligned} \dot{x} &= Ax + Bu \\ y &= Cx + Du \end{aligned} \quad \rightarrow \text{After LT}$$

$$\Rightarrow \begin{matrix} \hat{x} \\ \hat{y} \end{matrix} = A \hat{x} + B \hat{u} \\ \quad \quad \quad \hat{y} = C \hat{x} + D \hat{u}$$

$$\hat{x} = (sI - A)^{-1} B \hat{u}$$

$$\hat{y} = (C(sI - A)^{-1} B + D) \hat{u}$$

$$\left[ \begin{array}{c|c} A & B \\ \hline C & D \end{array} \right] \rightarrow T(s) = \hat{y}$$

→ On why  $(sI - A)$  exists,

$$= \begin{bmatrix} s & -1 \\ 6 & -s+5 \end{bmatrix}$$

$$= \frac{\text{adj}(sI - A)}{\det(sI - A)}$$

$$\det(sI - A) = s(s+5) + 6 \\ = s^2 + 5s + 6$$

Complete this.

$$[1 \ 0] \begin{bmatrix} \dots & \dots \end{bmatrix}$$

# State Space Model

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$$\dot{x} = Ax + bu$$

$$y = \cancel{c}x + cx + du$$

zero state condition  $x(0) = 0$

$$\begin{aligned}\hat{x} &= LT \text{ of } x(t) \\ \hat{y} &= " " y(t) \\ \hat{u} &= " " u(t)\end{aligned}$$

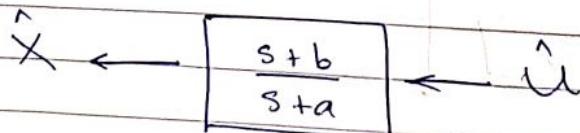
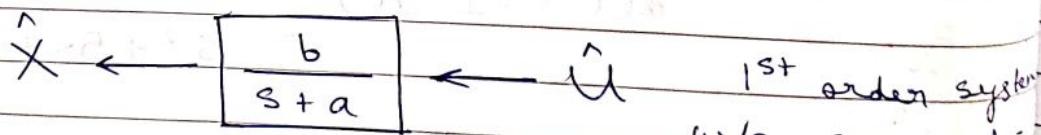
$$\hat{x} = (sI - A)^{-1} b \hat{u}$$

$$\hat{y} = [c(sI - A)^{-1} b + d] \hat{u}$$

$$\frac{\hat{y}}{\hat{u}} = (c(sI - A)^{-1} b + d)$$

$$\frac{\hat{y}}{\hat{u}} = \frac{c \text{adj}(sI - A)b}{\det(sI - A)} + d$$

$$\dot{x} = -ax + bu$$



→ Analysis

$$\hat{y} = -ay + bu$$

$$s\hat{Y} - y_{10} = -a\hat{Y} + b\hat{u}$$

$$\hat{Y} = \frac{y(0)}{(s+a)} + \frac{b}{(s+a)} \hat{u}$$

$$y(t) = e^{-at} y(0) + L^{-1}\left(\frac{b}{(s+a)} \hat{u}\right)$$

$f(t), g(t) \leftrightarrow F(s), G(s)$

$$\begin{aligned} & L^{-1}(F(s)G(s)) \\ &= \int_0^{\infty} f(t-\tau) g(\tau) d\tau \\ &= \int_0^t f(t-\tau) g(\tau) d\tau \\ &\quad \text{since } f(t) = 0 \text{ for } t < 0 \end{aligned}$$

$t - \tau \geq 0 \Rightarrow \tau \leq t$  for non zero part

→ Using Inverse convolution formula

$$y(t) = e^{-at} y_0 + b \int_0^t e^{-a(t-\tau)} u(\tau) d\tau$$

↓                      ↓

zero input response    zero state response

### Response Parameters

→ Step response :



$$\hat{Y} = \left(\frac{b}{s+a}\right) \frac{1}{s}$$

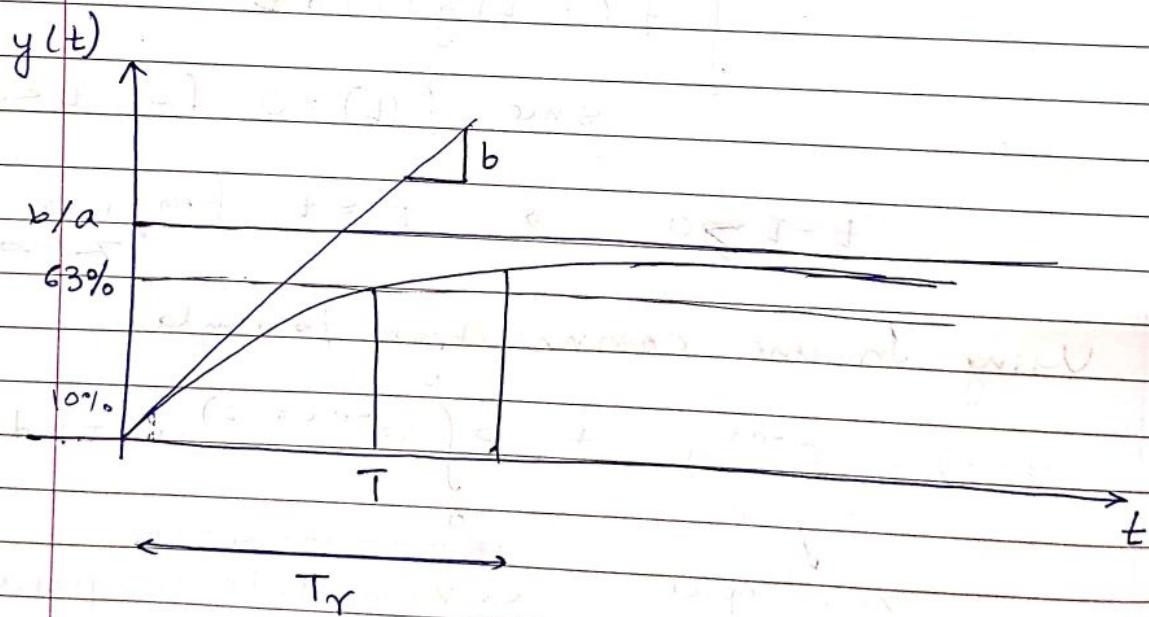
→ Using partial fraction expansion

$$\frac{b}{s(s+a)} = \frac{b/a}{s} + \frac{b/(-a)}{(s+a)}$$

$$\Rightarrow y(t) = L^{-1} \left( \frac{b/a}{s} + \frac{b/(-a)}{s+a} \right)$$

$$= \frac{b}{a} - \frac{b}{a} e^{-at} \quad t \geq 0$$

$$= \frac{b}{a} (1 - e^{-at})$$



→ Parameters

① Time Constant ( $T$ )

$$T = \frac{1}{a} \quad \text{for } \frac{b}{a} = 1$$

② Rise Time ( $T_r$ )

Time taken to rise from 10% to 90%

(3)

### Settling time ( $T_s$ )

Time taken to reach within 2% of settling value.

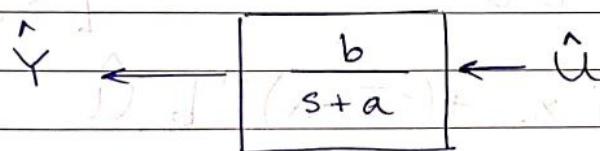
22.1.19

First order system solution:

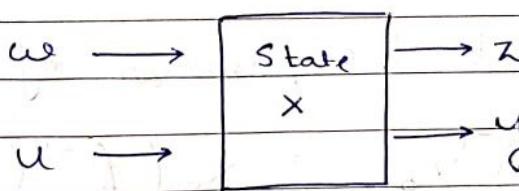
$$\dot{x} = -ax + bu$$

$$x(t) = e^{-at} y_0 + \int_0^t e^{-a(t-\tau)} u(\tau) d\tau$$

$$\text{Step Response } y(t) = \frac{b}{a} (1 - e^{-at})$$



### Notation Convention



→ State-space description of above,

$$x = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}$$

$$u = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ \vdots \\ u_m \end{bmatrix}$$

$$y = \begin{bmatrix} \cdot \\ \cdot \\ \cdot \end{bmatrix}$$

$$\begin{aligned} \dot{x} &= Ax + Bu \\ y &= Cx + Du \end{aligned}$$

$$\begin{array}{c} A, B = \text{real Matrices} \\ n \times n \\ n \times m \\ n \times m \\ C, D \\ p \times n \\ p \times m \end{array}$$

→ Simplified Single Input - Single output sys.

$$\dot{x} = Ax + bu$$

$$y = cx + du$$

$$\begin{bmatrix} A & b \\ c & d \end{bmatrix}$$

$$\hat{Y} = e^{(sI-A)^{-1}}b + d$$

~~$$\dot{x} = Ax + bu$$~~

$$x(0) = x_0$$

$$\hat{x} = \begin{bmatrix} \hat{x}_1 \\ \hat{x}_2 \\ \vdots \\ \hat{x}_n \end{bmatrix}$$

$$s\hat{x} - x_0 = A\hat{x} + b\hat{u}$$

$$\hat{x} = (sI - A)^{-1}x_0 + (sI - A)^{-1}b\hat{u}$$

$$\hat{Y} = c\hat{x} + d\hat{u}$$

→ Let  $\Phi(t)$  be the function of time s.t.

$$\mathcal{L}^{-1}(sI - A)^{-1}x_0 = x_0(\mathcal{L}^{-1}(sI - A)^{-1})$$

$$\mathcal{L}(\Phi(t)) = (sI - A)^{-1}$$

$\Phi(t)$  is also a solution of the Mat. Eqn

$$\dot{Z} = AZ$$

$$Z(0) = I$$

$$s\hat{Z} - I = A\hat{Z}$$

$$\hat{Z} = (sI - A)^{-1}$$

→ What does the notation mean

$$z(t) = [z_{ij}(t)]$$

$$\mathcal{L}(z(t)) = [\mathcal{L}(z_{ij}(t))]$$

$$\dot{z} = Az \quad z(0) = I$$

↪ A homogeneous differential equation  
since no forcing functions

→ Properties (proven later) of  $\Phi(t)$

$\Phi(t)$  satisfies

$$1. \quad \Phi(0) = I \quad 2. \quad \frac{d\Phi(t)}{dt} = A\Phi(t)$$

$$3. \quad \Phi(t+s) = \Phi(t)\Phi(s) \quad 4. \quad \Phi(-t) = (\Phi(t))^{-1}$$

$$5. \quad \det(\Phi(t)) = ? \quad (\text{Extra})$$

ex

$$A = \begin{bmatrix} 0 & 1 \\ -6 & -5 \end{bmatrix} \quad A + I = \dots$$

$$(sI - A)^{-1} = \begin{bmatrix} s & -1 \\ -6 & s+5 \end{bmatrix}^{-1}$$

$$= \frac{1}{(s^2 + 5s + 6)} \begin{bmatrix} s+5 & 1 \\ -6 & s \end{bmatrix}$$

$$\mathcal{L}^{-1}(sI - A)^{-1} = \frac{1}{(s+2)(s+3)} \begin{bmatrix} s+5 & 1 \\ -6 & s \end{bmatrix}$$