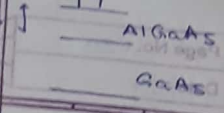


25-30 is ideal

30nm



20nm channel layer

III-V Transistor (High Electron Mobility Transistor)

n-MOS S/D : n-type (P) Substrate : p-type (B)

$\mu = 300-400 \text{ cm}^2/\text{V.s}$

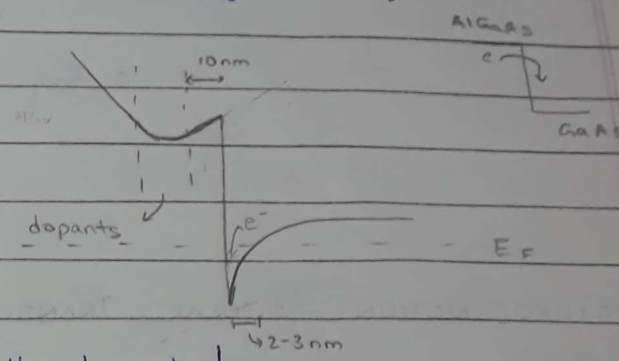
Bulk Mobility of Si = $1300-1500 \text{ cm}^2/\text{V.s}$

- Lattice vibration \rightarrow Phonon Scattering
- Doping \rightarrow Interphase Impurity Scattering
- \rightarrow Surface Scattering*

* Gradual Channel Approx : E are \perp and are non-interfering
 \rightarrow carrier-carrier scattering ($n^{1/3}$)

III-V Transistor has no impurity scattering

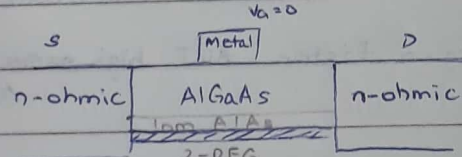
- 30% 10nm AlGaAs (undoped)
- 30% 10nm AlGaAs (n+) Si
- 30% 10nm AlGaAs (undoped)
- 5nm GaAs (undoped)



* carriers are separated from the dopants!

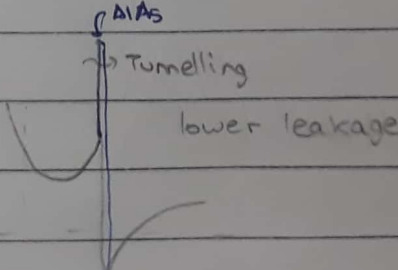
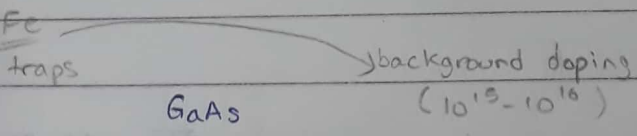
* 2-dimensional e^- gas (e^- are confined on the left by band offset right by electrostatic potential)

$E \sim kT (2 \times \frac{1}{2} k_B T)$



$V_T = -ve$: depletion mode

$V_T = +ve$: enhancement mode



$V_T \sim -(2-3)V$ Depletion Mode

* $V_T < 0$

* μ is high ($2500 \text{ cm}^2/\text{V.s}$)

$f \uparrow$ 300 GHz

$I_{DP} \rightarrow f \sim 600 \text{ GHz}$ but high gate leak

* better gate control (Much higher Transconductance g_m)

* Static Power Consumption $\neq 0$!

* Top undoped layer ensures gate current is minimal

Topic: _____
Date: _____

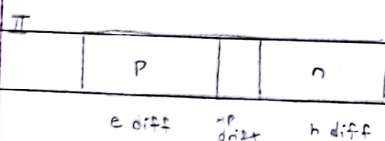
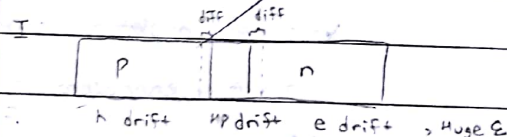
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Date: 24/10/17

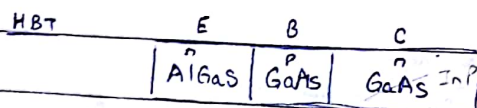
HMT \rightarrow used for power transistor

- * used as transceiver

- ↳ Lightly doped C (e^- will move through depl region faster BUT high series R_c)



↳ 200 GHz, 10^5 A/cm^2



(-) series resistance to of AlGaAs \uparrow (as high barrier contact is poor)

(*) Base doping can be slightly increased \Rightarrow lesser C \rightarrow faster device

- back current blocked by barrier
- more mobility so lesser time for recombination

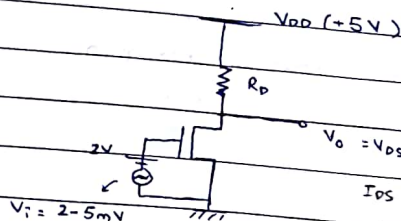
Even lesser resistance

* Prefer to use high E_g material (to minimize minority carriers)

$E_g \approx 10\text{eV}$

insulators are high E_g materials where right dopant hasn't been found

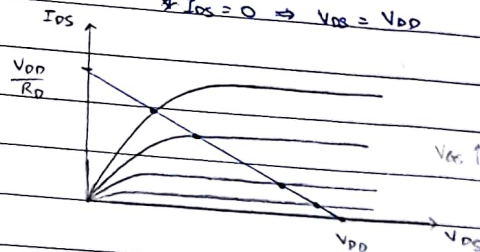
ANALOG MICROELECTRONICS



$$V_{DD} = V_{DS} + I_{DS} \times R_D$$

$$V_{DS} = 0 \Rightarrow I_{DS} = V_{DD}/R_D$$

$$I_{DS} = 0 \Rightarrow V_{DS} = V_{DD}$$



$$V_{in} \uparrow \rightarrow I_{DS} \uparrow \Rightarrow V_o (= V_{DD} - I_{DS} R_D) \downarrow$$

$$\frac{\partial V_o}{\partial V_{in}} = \text{Gain (A)}$$

$$I_{DS} = \frac{K'}{2} (V_{in} - V_T)^2$$

[Assuming MOS is in SAT.]

$$V_o = V_{DD} - I_{DS} R_D$$

$$V_o = V_{DD} - \frac{K'}{2} (V_{in} - V_T)^2 R_D \Rightarrow A = \frac{\partial V_o}{\partial V_{in}} = -K' (V_{in} - V_T) R_D$$

↳ circuit is not linear, all signals are not equally magnified

* Linearize the Gain $\Rightarrow V_{in} = V_{DC} + \hat{v}_{in} \sin \omega t, |\hat{v}_{in}| \ll |V_{DC}|$

$$V_o = V_{DC} + \hat{v}_{out} \sin \omega t$$

$$A = \frac{\partial V_o}{\partial V_{in}} = \frac{\partial V_{out}}{\partial V_{in}} = \frac{\hat{v}_{out}}{\hat{v}_{in}}$$

Transconductance, $g_m = \frac{\partial I_{DS}}{\partial V_{GS}}$

$$\rightarrow V_o = V_{DD} - I_{DS} R_D$$

$$\Rightarrow \frac{\partial V_o}{\partial V_{in}} = -\frac{\partial V_{DS}}{\partial V_{in}} R_D = -g_m R_D$$

NOTE: to maintain linearisation, V_{ac} should be small (small signal)

[Assuming MOS is in LIN]

$$I_{DS} = K' \left[(V_{in} - V_T) V_o - \frac{V_o^2}{2} \right]$$

$$-\frac{\partial I_{DS}}{\partial V_{in}} = -K' \left[V_o + (V_{in} - V_T) \frac{\partial V_o}{\partial V_{in}} - V_o \frac{\partial V_o}{\partial V_{in}} \right] = \frac{\partial V_o}{\partial V_{in}}$$

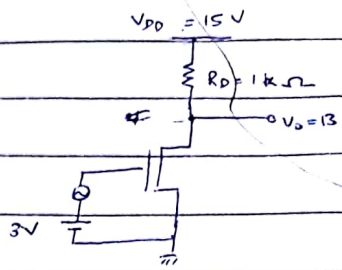
$$V_o = V_{DD} - I_{DS} R_D$$

$$\frac{\partial V_o}{\partial V_{in}} = -\frac{\partial I_{DS}}{\partial V_{in}} R_D$$

Design an amplifier with $\frac{\partial V_o}{\partial V_{in}} = -2$ $k' = 1 \text{ mA/V}$, $V_{DD} = 15$, $V_T = 1$

Choose $R_D = 1 \text{ k}\Omega \Rightarrow g_m = 2 \text{ mA/V}$
 $g_m = k' (V_{GS} - V_T) \Rightarrow V_{GS} = 3 \text{ V}$

CHECK $I_{DS} = \frac{10^{-3}}{2} (3-1)^2 = 2 \text{ mA}$



$V_o > V_{DD} - V_T \checkmark \text{ (SAT)}$

$\frac{\partial V_o}{\partial V_{in}} = -3$, $k' = 1 \text{ mA/V}$, $V_T = 1 \text{ V}$, $V_{DD} = 15 \text{ V}$. What is max gain.

$V_{DS} > V_{GS} - V_T \Rightarrow V_{DD} - I_{DS} R_D > V_{GS} - V_T \Rightarrow R_D < \frac{16 - V_{GS}}{\frac{k'}{2} (V_{GS} - 1)^2} \quad \text{--- (1)}$

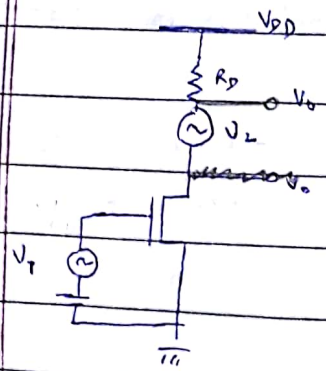
$R_D = \theta \frac{2(16 - V_{GS})}{k' (V_{GS} - 1)^2} \quad 0 \leq \theta \leq 1$

$A = -g_m R_D = -k' (V_{GS} - 1) R_D$
 $= -\theta \frac{2(16 - V_{GS})}{V_{GS} - 1}$

To ensure $|A V_{in}| \ll |V_o| \rightarrow$ we need extremely small V_{in} .

MIXER

$V_1 = A_1 \sin \omega_1 t$ $V_2 = A_2 \sin \omega_2 t \Rightarrow (\omega_1 - \omega_2), (\omega_1 + \omega_2)$

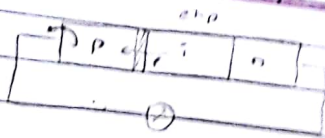


$I_D = k' \left[(V_{GS} - V_T) V_{DS} - \frac{V_{DS}^2}{2} \right]$

$V_o = V_{DD} - I_{DS} R_D$

$I_{DS} = k' \left[(V_{GS} - V_T + V_1) V_o - \frac{V_o^2}{2} \right]$

Design a potential well



POPULATION INVERSION

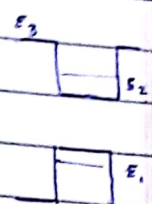
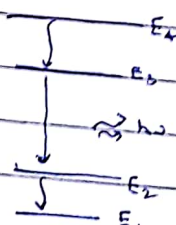
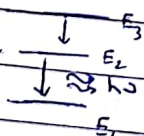
(Gas Laser)

HeNe, KrF, HeAr, HeCd

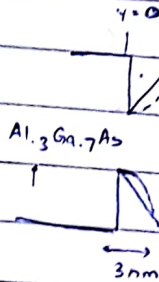
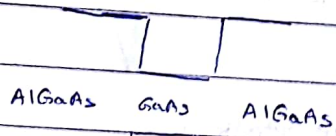
* A LASER can only 'lase' if there are more e^- at higher energy level than the lower energy level



stimulation emission CANNOT occur with 2 level system.

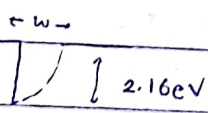


Modulation BW



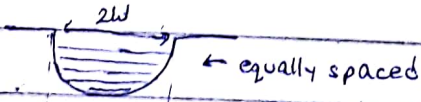
AlAs \rightarrow SeV
GaAs \rightarrow 1.19eV
 $\Delta E_c = -0.6E_g$

$Al_xGa_{1-x}As$ $x = 9/10$



$$x = my^2 \rightarrow m = \frac{2.16}{w^2}$$

$$E = \frac{h^2 k^2}{2m}$$

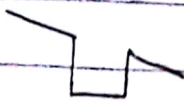


← equally spaced



← compressively spaced

Quantum Confined Stark Effect



graded QW



① efficiency ↓

15nm AlGaAs (undoped)

15nm

8-doped

Cheap way to develop harmonics



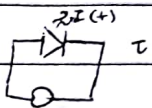
$$V_i = V \sin \omega t$$

$$V_o = A \sin(3\omega t)$$

$$I = I_0 \left(e^{\frac{qV \sin \omega t}{2kT}} - 1 \right)$$

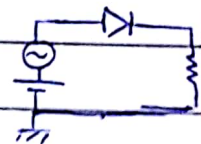
$$= I_0 \left(1 + \frac{qV}{2kT} + \frac{q^2 V^2}{8k^2 T^2} + \frac{q^3 V^3}{24k^3 T^3} + \dots \right)$$

keep large V



$I(t)$

To measure e

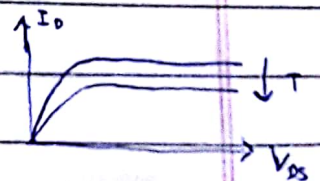


Thermal Run-Away of Diode

$$T \uparrow, I \uparrow \rightarrow I^2 R \uparrow$$

+ve feedback

I_n MOSFET



-ve feedback

$T \uparrow, \mu \downarrow$ (due to decrease in mobility)

$T \uparrow, V_T \downarrow$ (minority carrier conc. \uparrow with T)

in linear $I \uparrow$

in sat $I \downarrow$