

→ Laplace transforms.

$$\boxed{L(av + bw) = aL(v) + bL(w)}$$

$\Rightarrow M_L$ a matrix basis
(linear map = Matrix with basis)

$$\frac{d}{dt} (af(t) + bg(t)) = a \frac{df(t)}{dt} + b \frac{dg(t)}{dt}$$

If $f(t) = \sum_{i=0}^{\infty} a_i t^i$ $\{1, t, t^2, \dots\}$

Then $\frac{df(t)}{dt} = \sum_{i=0}^{\infty} i a_i t^{i-1}$

Term 0 → t^0 coefficient

$$a_0 \rightarrow t^0$$

$$2a_1 \rightarrow t^1$$

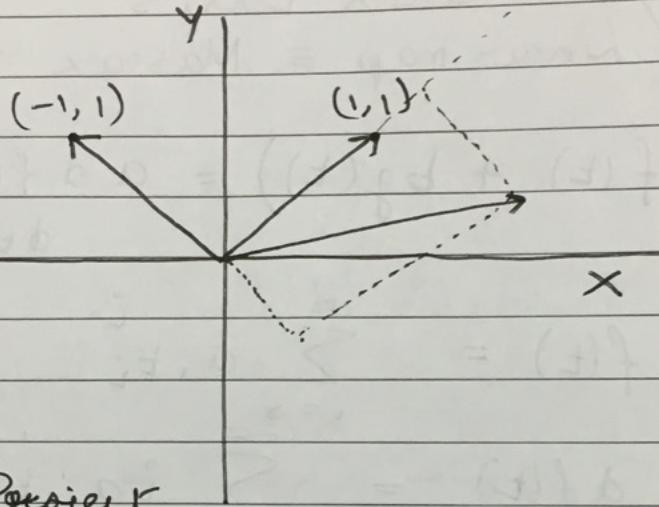
$$3a_2 \rightarrow t^2$$

$$4a_3 \rightarrow t^3$$

$$\begin{array}{c|ccccc|c} & 0 & 1 & 0 & \dots & & a_0 \\ & 0 & 0 & 2 & \dots & & a_1 \\ & 0 & 0 & 0 & 3 & \dots & \vdots \\ \hline i & 0 & 0 & 0 & 0 & \dots & a_i \end{array}$$

$\left(\frac{d^2}{dt^2}\right), \left(\frac{d^i}{dt^i}\right) \rightarrow$ Also Linear Maps.

$$\rightarrow \int f(t) dt, \quad \int (af(t) + bg(t)) dt, \\ a \frac{d}{dt} + b \int dt + c \frac{d^2}{dt^2}$$



Project

$$\text{stretch } \begin{pmatrix} 3 & 1 \\ 1 & 1 \end{pmatrix} \begin{pmatrix} 1 & 1 \\ -1 & 1 \end{pmatrix} - 1 \begin{pmatrix} -1 \\ 1 \end{pmatrix} \begin{pmatrix} -1 & 1 \\ 1 & 1 \end{pmatrix}$$

Not obvious what it does

$$\begin{bmatrix} 3 & 3 \\ 3 & 3 \end{bmatrix} - 1 \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = \begin{bmatrix} 2 & 4 \\ 4 & 2 \end{bmatrix}$$

Eigen Value Egn

$$Mv = \lambda v$$

then, $\lambda \rightarrow$ eigen value

$v \rightarrow$ eigen vector ($v \neq 0$)

$$\rightarrow L(v) = \lambda v$$

$$\frac{df}{dt} = \cancel{\lambda} \lambda f(t)$$

$$f(t) = ce^{\lambda t} \quad \{ ce^{\lambda t} \} \lambda \in \mathbb{C} \}$$

↓
family of solutions for

even for $D^i f = \lambda f$ & $\int f(t) dt = \cancel{f(t)}$

$$[g(t) \longmapsto \int g(t) e^{\lambda t} dt]$$

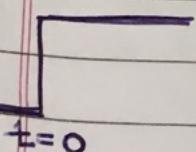
Analogy of dot product with function
 $\Rightarrow \int$ integrals.

→ Hence the motivation for Laplace trans.

$$L[f(t)] = F(s) = \int_0^\infty f(t) e^{-st} dt$$

Laplace examples

(ex)



$$u(t) = \begin{cases} 0 & \text{if } t < 0 \\ 1 & \text{o/w} \end{cases}$$

$$L[u(t)] = \frac{1}{s} = \int_0^\infty e^{-st} dt = \frac{1}{s} (1 - 0)$$

Ex 2)

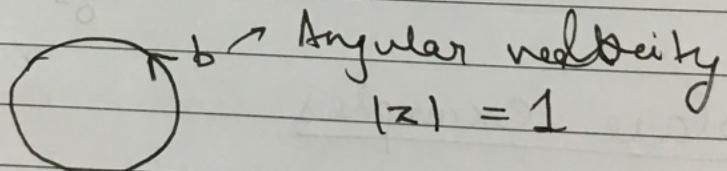
$$\begin{aligned} f(t) &= e^{at} \\ \mathcal{L}[f(t)] &= \int_0^\infty e^{at} e^{-st} dt \\ &= \frac{1}{s-a}, \quad s > a \end{aligned}$$

d.o.e, o.w

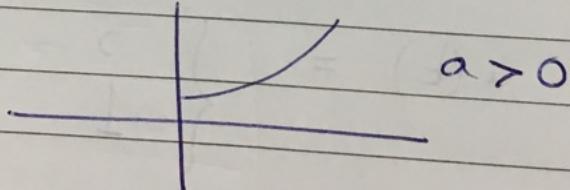
→ Introduce Complex Numbers

$$\begin{aligned} j^2 &= -1 \\ (a+jb)t \\ e^{jbt}, \quad a, b \in \mathbb{R} \end{aligned}$$

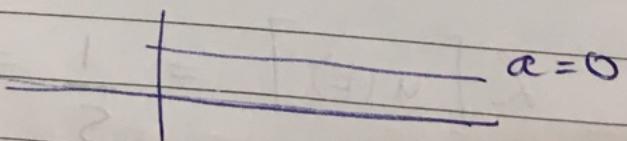
$$\rightarrow e^{jbt} = \cos(bt) + j \sin(bt)$$



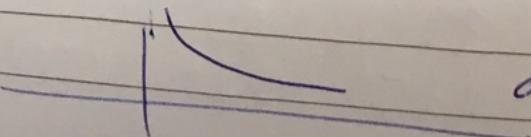
$$e^{at}$$



$$a=0$$



$$a < 0$$



$e^{(a+jb)t} = e^{at} \cos bt$ is just like
classmate

$$e^{-t} \sin t$$

~~Harmonic~~

Damped Oscillation.

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Page _____

→ Inverse Laplace transform

$$f(t) = \frac{1}{2\pi j} \int_{\sigma_1 - j\infty}^{\sigma_1 + j\infty} F(s) e^{st} ds$$

Formulas

$$1) L[a f_1(t) + b f_2(t)]$$

$$= a F_1(s) + b F_2(s)$$

$$2) L[\cos \omega t] = L \left[\frac{e^{j\omega t} + e^{-j\omega t}}{2} \right]$$

$$= \frac{1}{2} \left[\frac{1}{s - j\omega} + \frac{1}{s + j\omega} \right]$$

$$\frac{1}{2} \left[\frac{1}{s - j\omega} + \frac{1}{s + j\omega} \right] = \frac{s}{s^2 + \omega^2}$$

$$3) L[\sin \omega t] = \frac{\omega}{s^2 + \omega^2}$$

$$4) \quad \mathcal{L} \left[\frac{d}{dt} f(t) \right] = \int_0^{\infty} \frac{df}{dt} e^{-st} dt$$

$$= e^{-st} f(t) \Big|_0^{\infty} + s \int_0^{\infty} f(t) e^{-st} dt$$

$$= * sF(s) - f(0^-) *$$

$$f(t) = \boxed{** u(t) \rightarrow \text{special case!}}$$

$$f(0^-) = \lim_{t \rightarrow 0^-} f(t) \qquad u(0^-) = 0$$

$$\rightarrow ** \mathcal{L} [\delta(t)] = \mathcal{L} \left[\frac{du(t)}{dt} \right] = 1 **$$

$$5) \quad \mathcal{L} \left[\int_{0^-}^t f(\tau) d\tau \right] = - \frac{e^{-st}}{s} \int_{0^-}^t f(\tau) d\tau \Big|_0^{\infty}$$

$$+ \frac{1}{s} \int_{0^-}^{\infty} f(t) e^{-st} dt$$

$$** \boxed{= \frac{F(s)}{s}} **$$

$$\mathcal{L}^{-1} \left[\frac{1}{s-a} \right] = e^{at}$$

$$\frac{P(s)}{q(s)} = \sum_i \frac{c_i}{(s-a_i)}$$

where $q(s) = \prod_i (s-a_i)$

$$c_j = \frac{P(a_j)}{\prod_{i \neq j} (a_j - a_i)}$$

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→ Recap,

Laplace transform

$$F(s) = \mathcal{L}[f(t)] = \int_0^\infty f(t) e^{-st} dt$$

→ Stan. formulas

$$\mathcal{L}\left[\frac{df}{dt}\right], \quad \mathcal{L}\left[\int_0^t f(\tau) d\tau\right]$$

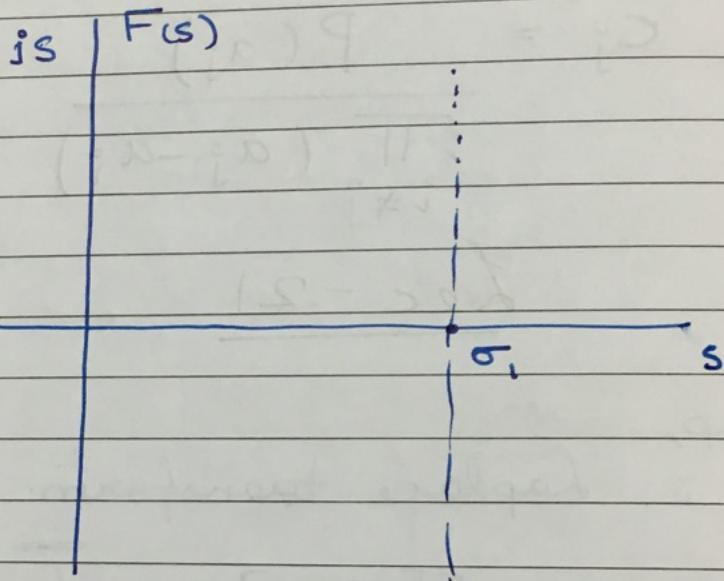
$$\mathcal{L}[e^{at}] = \int_0^\infty e^{-(s-a)t} dt = \frac{1}{s-a} \text{ if } s > a$$

$$= \cancel{\frac{1}{s-a}}$$

→ More on Inverse Laplace

$$\mathcal{L}^{-1}(F(s)) = \frac{1}{2\pi j} \int_{\sigma_1 - j\infty}^{\sigma_1 + j\infty} F(s) e^{st} ds$$

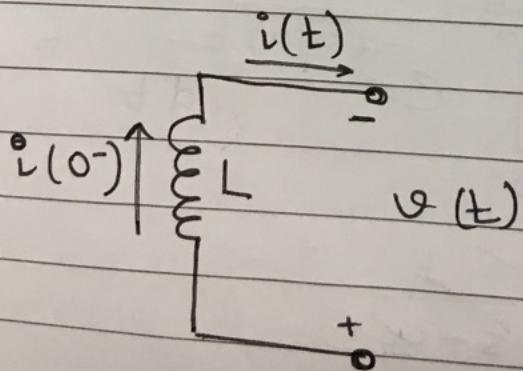
where $\sigma_1 > a \rightarrow$ leftmost pt. of defn.



→ But if we use

$$\mathcal{L}^{-1}[L(f(t))] = f(t)$$

→ Proof of Thvenin / Norton thms



$$v(t) = L \frac{di(t)}{dt}$$

$$V(s) = L \left(s I(s) - i(0^-) \right)$$

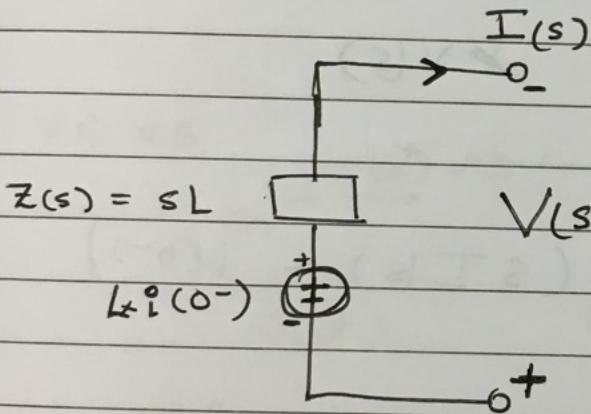
Aliter

$$\begin{aligned} i(t) &= \frac{1}{L} \int_{-\infty}^t V(\tau) d\tau \\ &= \frac{1}{L} \int_{0^-}^t V(\tau) d\tau + \frac{1}{L} \int_{-\infty}^{0^-} V(\tau) d\tau + i(0^-) \end{aligned}$$

\Rightarrow

$$I(s) = \frac{V(s)}{sL} + \frac{i(0^-)}{s}$$

\rightarrow Transformed ckt.



$$V(s) = \frac{V_o}{s} \quad (\text{If } v(t) = V_o = \text{constant})$$

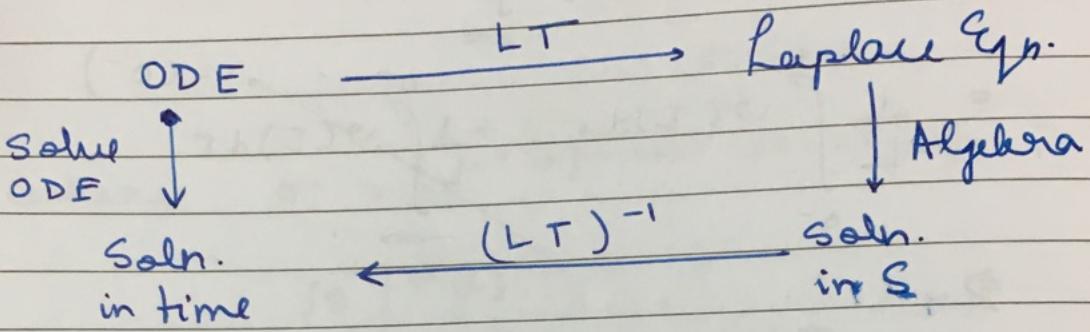
$$I(s) = \frac{V_o}{s^2 L} + \frac{i(0^-)}{s}$$

$$V(s) = \frac{V_o + i(0^-)sL}{s^2 L}$$

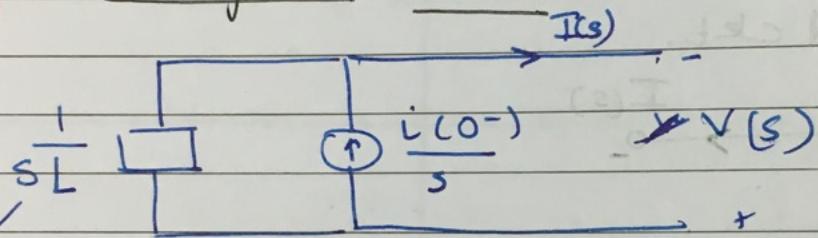
$$L^{-1}[I(s)] = i(t) = i(0^-) + \frac{V_o}{L} L^{-1}\left[\frac{1}{s^2}\right]$$

$$i(t) = i(0^-) + \frac{V_o}{L} t \quad \left(\because L[t] = \frac{1}{s^2} \right)$$

$$\rightarrow \text{Case 2: } v(t) = \sin(\omega t) \xrightarrow{\text{put } e^{j\omega t} - e^{-j\omega t}} \frac{e^{j\omega t} - e^{-j\omega t}}{2j}$$



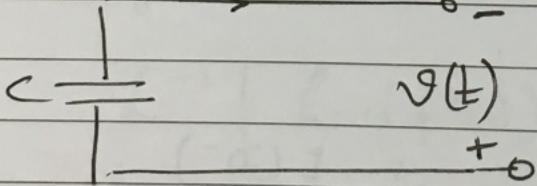
\rightarrow Transformed Circ



$$V(s) = L(sI(s)) - i(0^-)$$

$$i(t)$$

ex



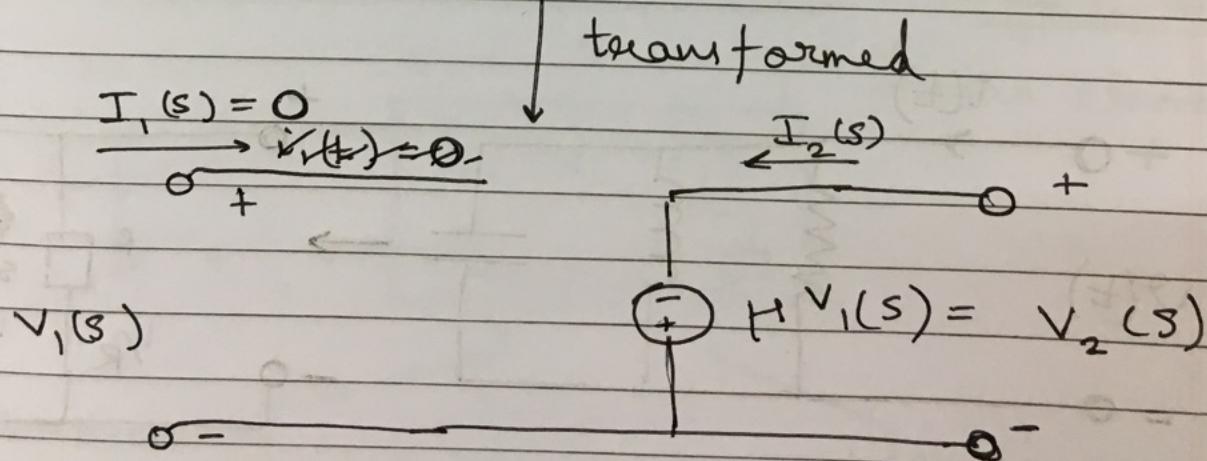
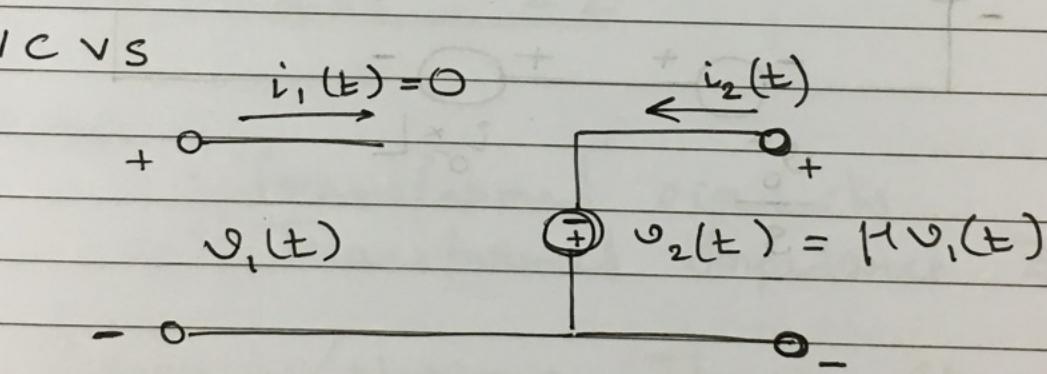
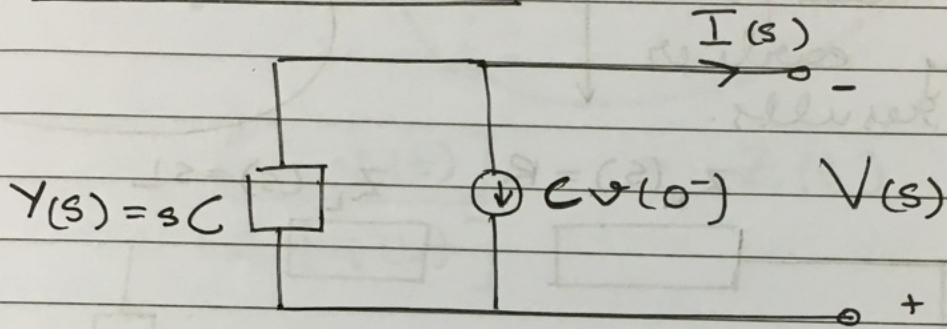
$$\begin{aligned} Z(s) &= \frac{1}{sC} & V(s) &= Y(s) = sC \\ \frac{V(0)}{s} - & \end{aligned}$$

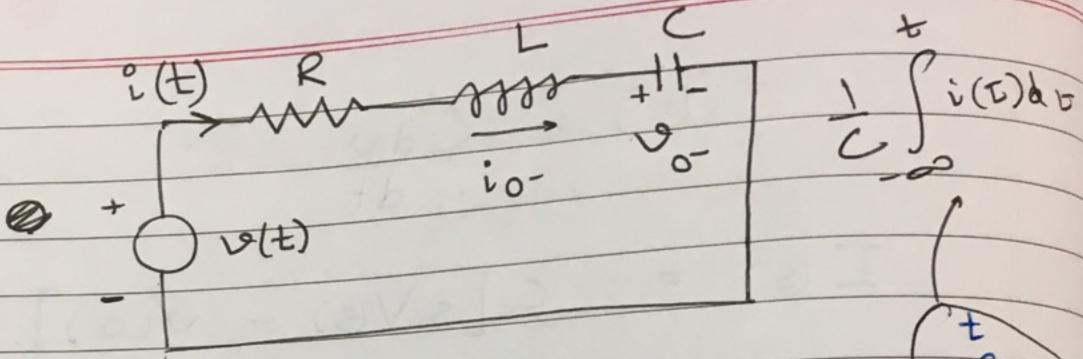
$$i(t) = C \frac{dv}{dt}$$

$$I(s) = C [sV(s) - v(0^-)]$$

$$V(s) - \frac{v(0^-)}{s} = \frac{I(s)}{sC}$$

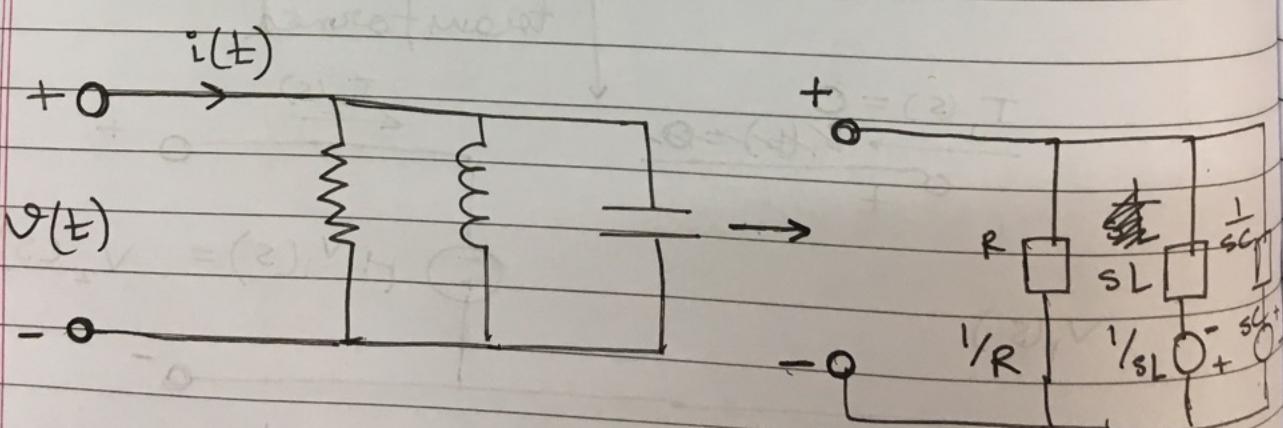
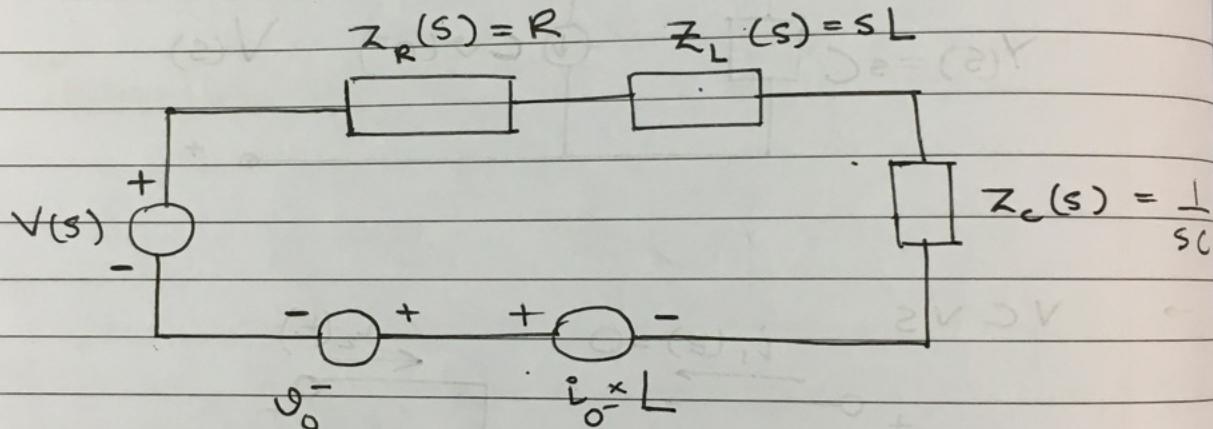
Transformed circuit



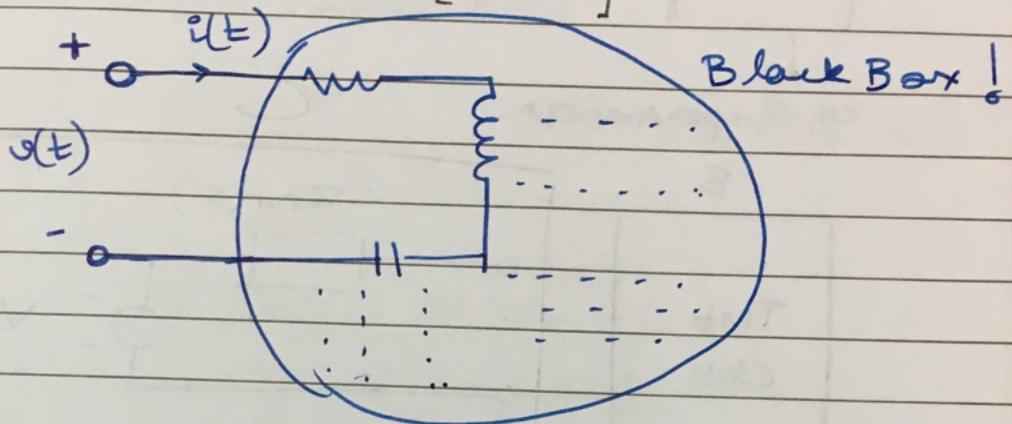


$$\text{KVL : } v(t) = R i(t) + L \frac{di}{dt} + \frac{1}{C} \int_{-\infty}^t i(\tau) d\tau + v_o^-$$

transform
using earlier
results.



$$Z(s) = \frac{L[v(t)]}{L[i(t)]} = Z(s)$$



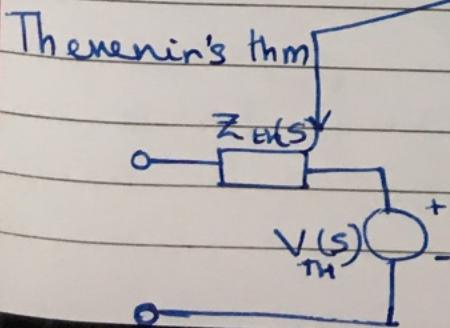
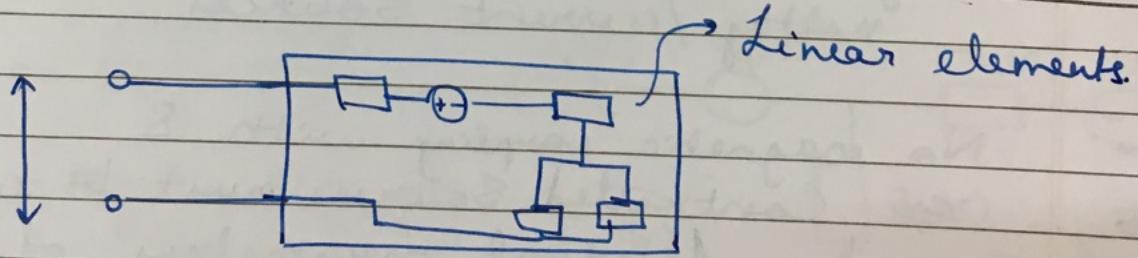
$$\frac{L[v(t)]}{L[i(t)]} = Z(s)$$

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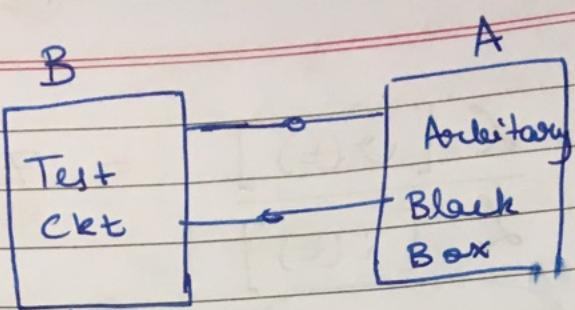
→ Recap

- Transformed circuits
- Transformed Impedance $Z(s)$

Thévenin / Norton's Thm's Chap 9, Malinenko

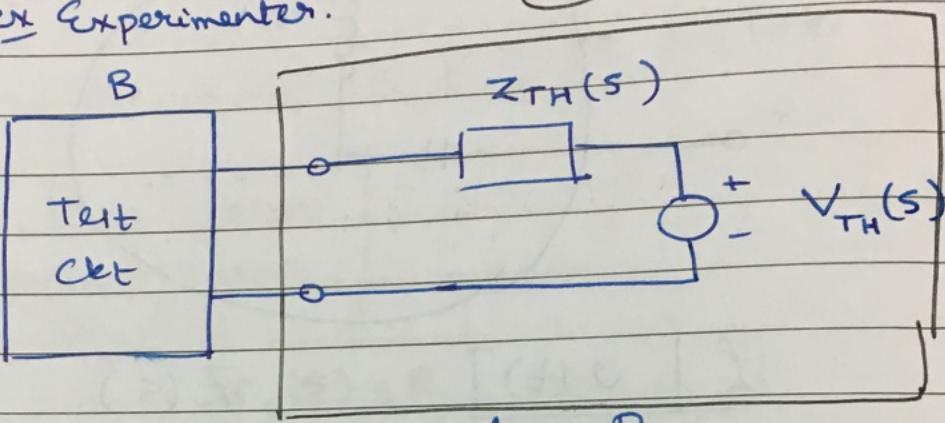


Norton's Thm.



ex Experimenter.

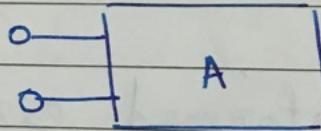
C



→ A, C indistinguishable for B.

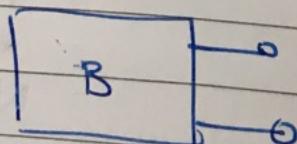
→ Conditions that A and B must satisfy
(Valkenbery)

A



- All elements must be linear
- May include Independent / Dependant voltage/current sources
- No magnetic coupling with B
- Controlled Sources must be controlled by Internal parameters of A

B



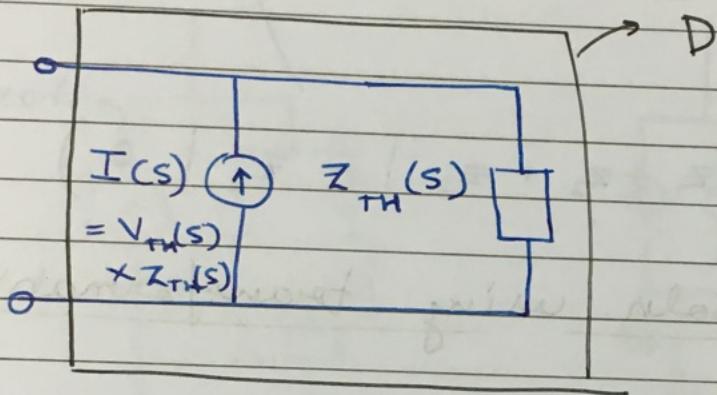
- No coupling to A

Thm [Thévenin thm]

→ Under alone conditions

exists $Z_{th}(s)$ and $V_{th}(s)$ s.t
 $A \equiv C$

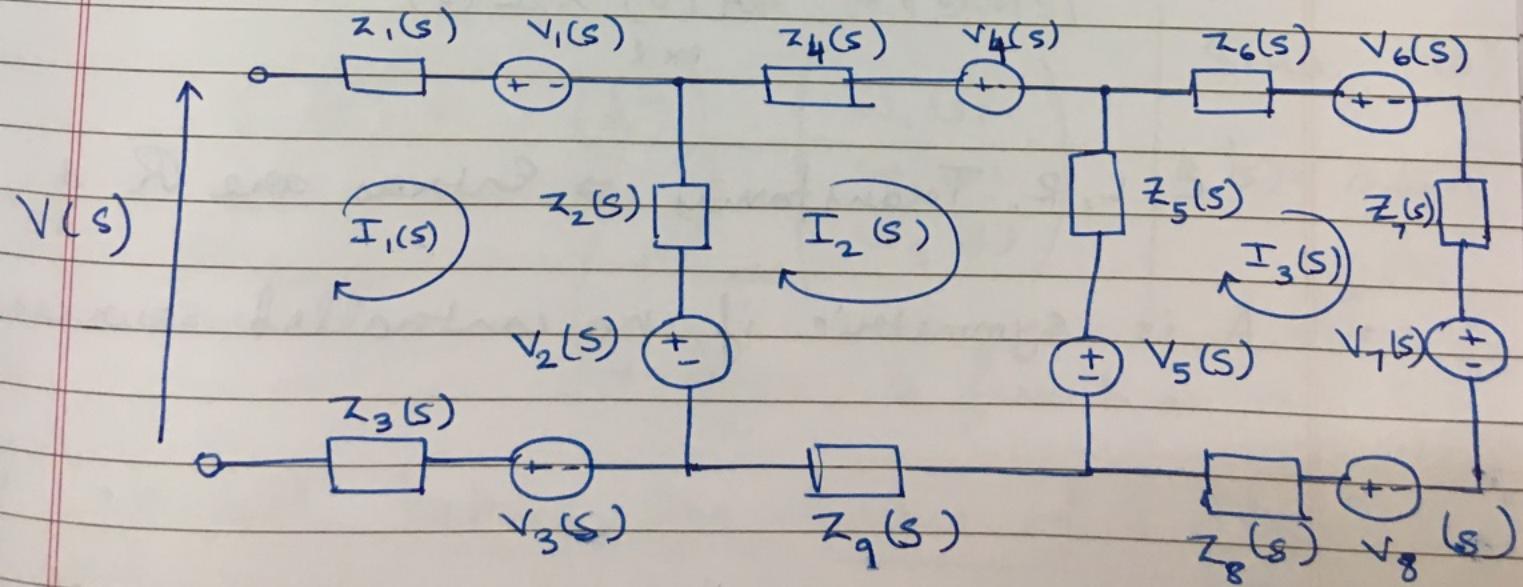
Norton's thm



exists $Z_{th}(s)$, $I(s)$ s.t.

$$D \equiv A.$$

Thm : Thévenin \Leftrightarrow Norton



→ General App. → Set to 0 $\Rightarrow I_{Th}(s) \rightarrow 0$

Gives $V(s)$

$$\begin{matrix} \left(\begin{array}{c} V_1(s) \\ V_2(s) \\ V_3(s) \end{array} \right) = A_{3 \times 3} \left(\begin{array}{c} I_1(s) \\ I_2(s) \\ I_3(s) \end{array} \right) & \text{where } A = \left(\begin{array}{ccc} -V_1(s) - V_2(s) + V_3(s) & & \\ V_2(s) - V_4(s) - V_5(s) & & \\ V_5(s) - V_6(s) - V_7(s) + V_8(s) & & \end{array} \right) \end{matrix}$$

$a_1 = (z_1 + z_2 + z_3 | -z_2 | 0)$ share no edges!

→ General soln. using transformations

$$\overline{\theta(t)} = A_{l \times l} \overline{i(t)}$$

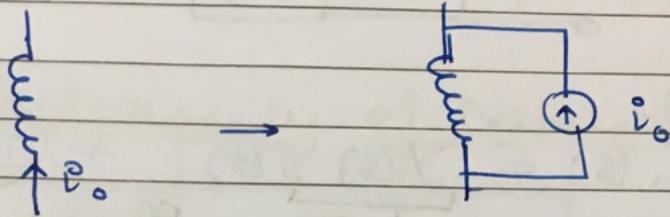
\downarrow
 $|E| - |N| + 1$

$$\overline{V(s)} = A(s) \times \overline{I(s)}$$

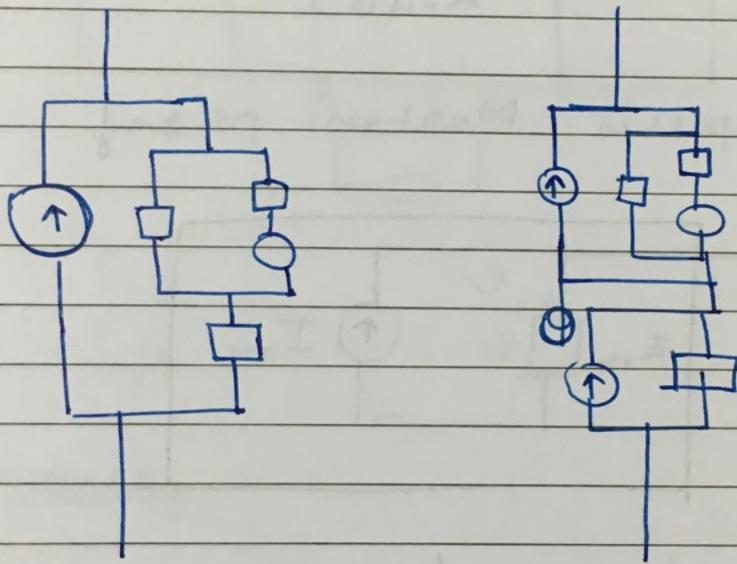
C, L, R, Transformers \Rightarrow Entries are $R, \frac{d}{ds}$

→ A is symmetric if no controlled sources

→ Inductor with initial conditions



→ Another case.



Conclusions

$$\overline{I}(s) = A^{-1}(s) \overline{V}(s)$$

$$I_1(s) = \begin{pmatrix} A^{-1} \\ 1 \end{pmatrix} \begin{pmatrix} w_1(s) \\ w_2(s) \\ w_3(s) \end{pmatrix}$$

Sine. (s)

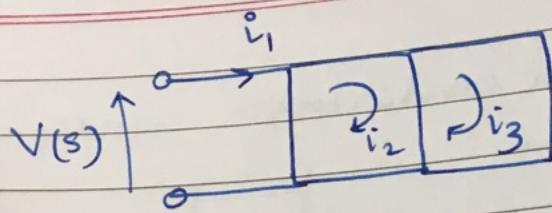
$A^{-1}(s) = \frac{\text{adj } A}{|A|}$

(s)

1st row 1st row

Again, a function of (s)

→ Recall : taking the Inverse of a Matrix



Sources inside
the network
Sources give
this.

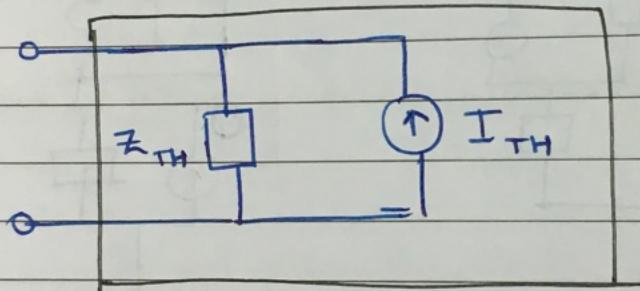
$$I_1(s) = \underbrace{Y(s)V(s)}_{\text{Passive Elements give this}} + \boxed{I_{TH}(s)}$$

Reason:

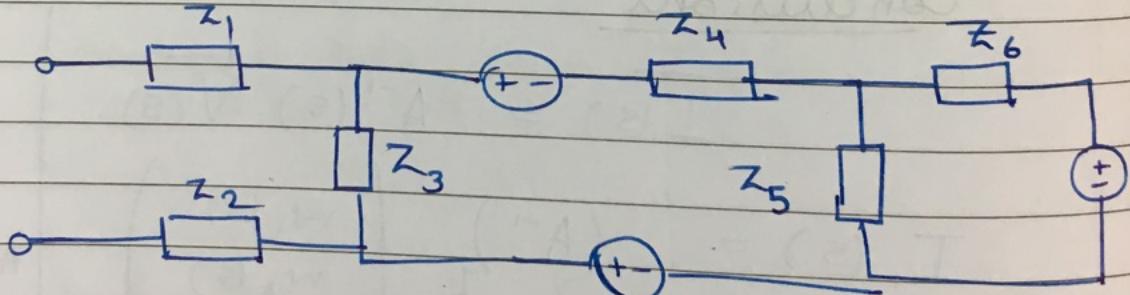
$$Y(s) = \frac{1}{Z_{TH}(s)}$$

(Passive multiplied by external $V(s)$)

→ Completes Norton proof



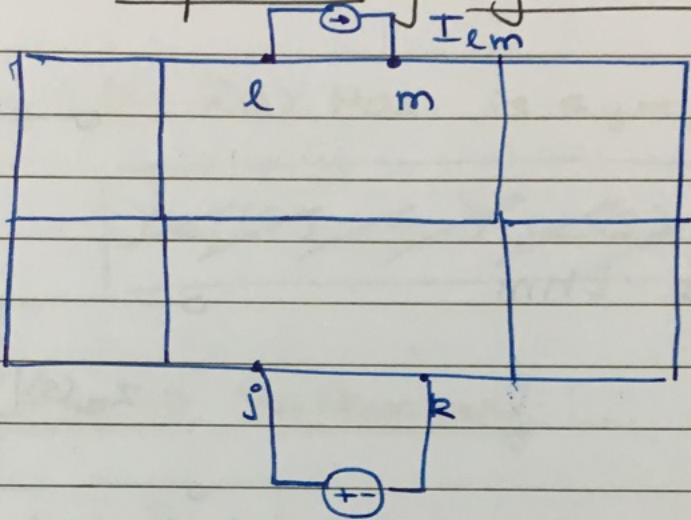
→ Algorithm we get from insight



To find $Z_{TH}(s)$ short all voltage sources, open all current sources. Use series-parallel rules for combining impedances.

$$Z = \left((Z_5 \parallel Z_6 + Z_4) \parallel Z_3 \right) + Z_1 + Z_2$$

Reciprocity of Networks



$$\begin{matrix} i_{lm} \\ i_{jk} \end{matrix}$$

$$\begin{matrix} v_{jk} \\ v_{lm} \end{matrix}$$

Reciprocity

- Behaviours of i_{lm} as a function of v_{jk} is the same as behaviours of i_{jk} as a function of v_{lm}
- Holds if Impedance matrix is symmetric . i.e. no controlled sources.

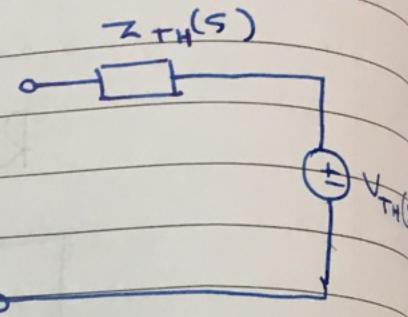
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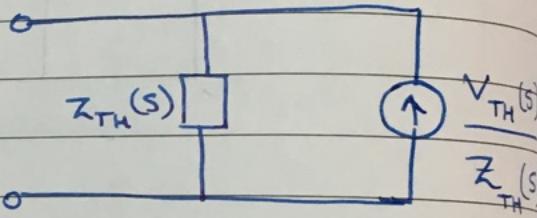
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Recap

Thevenin's thm



Norton's thm



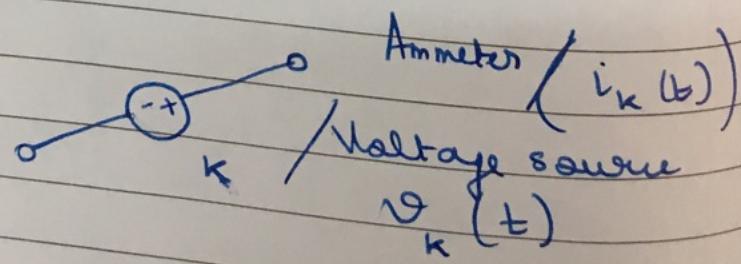
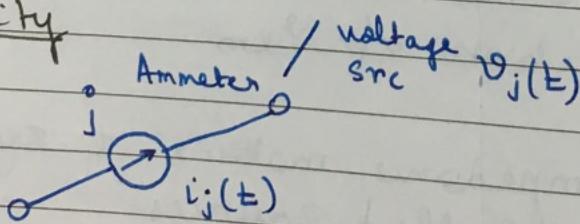
Proof Idea

$$\bar{V}(s) = \left(-Z_{ij}(s) \right) \bar{I}(s)$$

- Loop Analysis

$$\bar{I}(s) = \left(Z(s) \right)^{-1} \bar{V}(s)$$

Reciprocity



$$\frac{I_j(s)}{V_k(s)} = Y_{jk}(s)$$



Interchange roles of edges

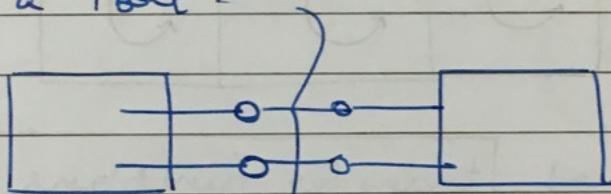
$$\frac{I_{k \leftarrow}(s)}{V_j(s)} = Y_{k \leftarrow j}(s)$$

Reciprocity (If $Z(s)$ Mat. is sym.) says (~~Reciprocity~~)

$$\boxed{Y_{kj}(s) = Y_{jk}(s)} \quad Y_{kj}(s) = Y_{jk}(s)$$

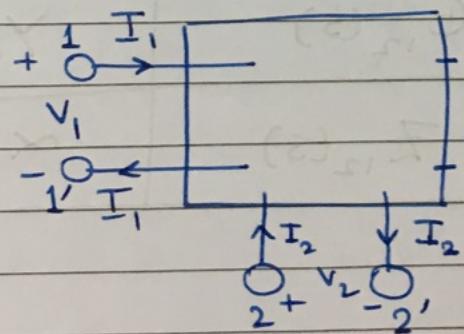
Chap 10 Network Theory

→ Nature of a Port:



→ we need two branches (1 \propto) for non zero current to flow b/w

→ Port:

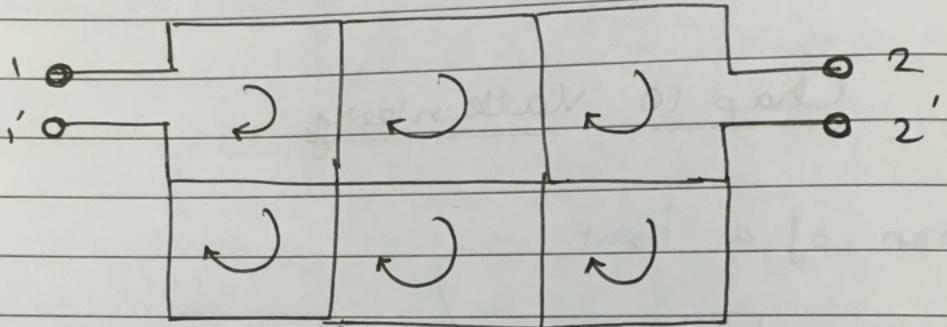


Two terminals with same current going in and out is a port.

- Thevenin/Norton: Work in 1 port case
single $Z_{TH}(s)$ & $V_{TH}(s)$
- To Analyse a ckt as a black - box with
> 1 ports we need to extend it.

Extended Thevenin / Norton Thm

Ex 10.



- Types of transfer functions possible
↳ experiments

(Inputs)	(Outputs)	Form Numer.
Form Denomin.	$V_2(s)$	$I_2(s)$
$V_1(s)$	$G_{12}(s)$	$Y_{12}(s)$
$I_1(s)$	$Z_{12}(s)$	$\chi_{12}(s)$

$$Z_{TH} = \frac{V(s)}{I(s)} = Z_{11}(s)$$

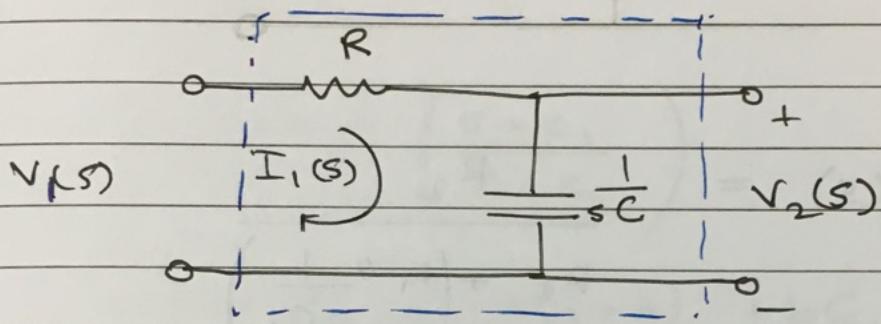
↓
At port 1

→ Indexing :

$$G_{12}(s) = V_2(s) / V_1(s)$$

$$Y_{12}(s) = I_2(s) / V_1(s)$$

Ex 10.3



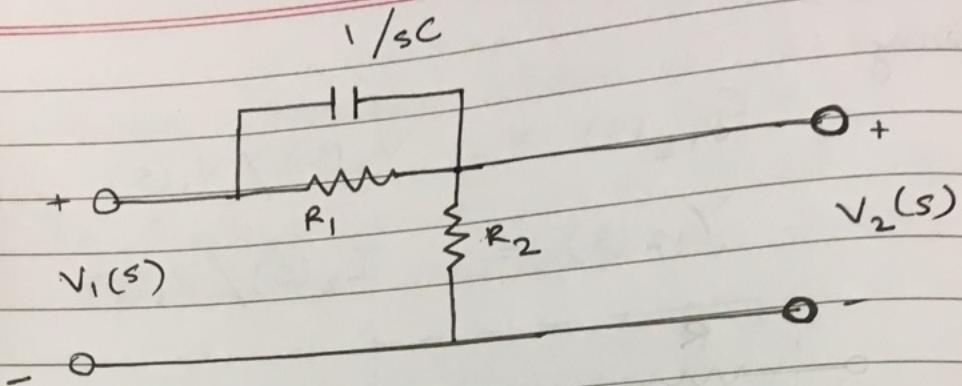
$$G_{12}(s) = \frac{1}{g_{21}(s)}$$

$$\begin{aligned} G_{12}(s) &= \frac{V_2(s)}{V_1(s)} = \frac{\left(\frac{1}{sC}\right) \times I_1(s)}{\left(R + \frac{1}{sC}\right) \times I_1(s)} \\ &= \frac{1}{RC} \end{aligned}$$

$$Y_{11}(s) = \frac{I_1(s)}{V_1(s)} = \frac{1}{R + \frac{1}{sC}}$$

$$\boxed{= \frac{1 \times s}{R \left(s + \frac{1}{RC} \right)}} = \frac{1}{Z_{TH_1}(s)}$$

E+5)



$$G_{1,2}(s) = \frac{R_2}{R_2 + \left(R_1 // \frac{1}{sC} \right)}$$

$$= \frac{R_2}{R_2 + \left(\frac{R_1 / sC}{R_1 + \frac{1}{sC}} \right)}$$

ct

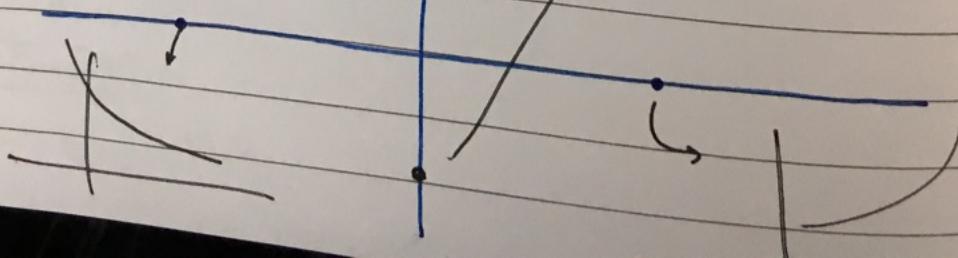
- Claim: All transfer functions are of the form $\frac{P(s)}{q(s)}$ where P, q are polynomials.
- Taken to be true.
- What values can s take?

Am: Complex Numbers.

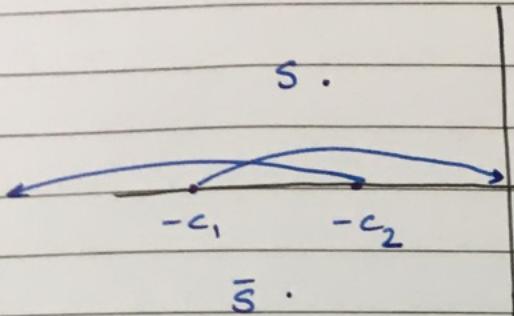
$$\cos(\omega t) = \frac{e^{j\omega t} + e^{-j\omega t}}{2}$$

\mathbb{C} plane

Pair of equidistant
⇒ (Sinusoid)



Poles & Zeros



Thinking of transfer
functions as conformal
mappings.

or

$$G_{12}(s) = \left(\frac{s + c_1}{s + c_2} \right)$$

$$f(z, t) = z(1-t) + t G_{12}(s)$$