

## Re view

### 1. Flyback converter :

⇒ Energy is stored in  $L_m$  & it is transfered to o/p

⇒ Isolated Buck – Boost control

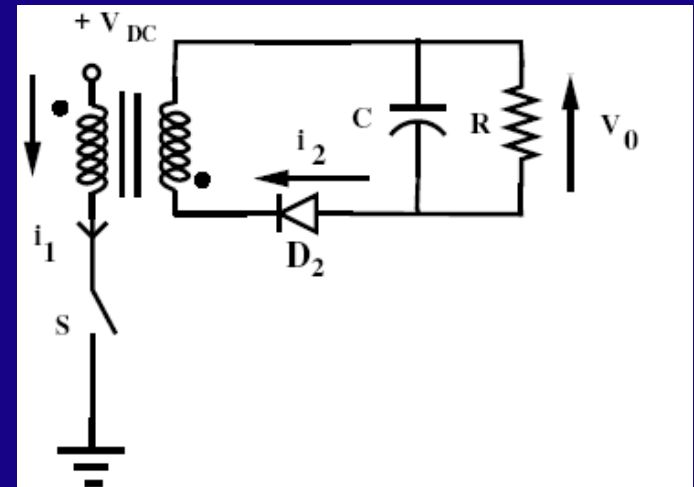
$$V_0 = V_{dc} \left( \frac{N_2}{N_1} \right) \frac{D}{(1-D)}$$

⇒ Operated in discontinuous mode (flux reseting)

⇒ Generally airgap is provided during the fabrication of transformer

⇒ Multiple o/p's are possible

⇒ Closed loop operation is a must



## Forward Converter

### With non-ideal transformer

$\Rightarrow \mu_r \neq \infty, R \rightarrow \text{finite}$

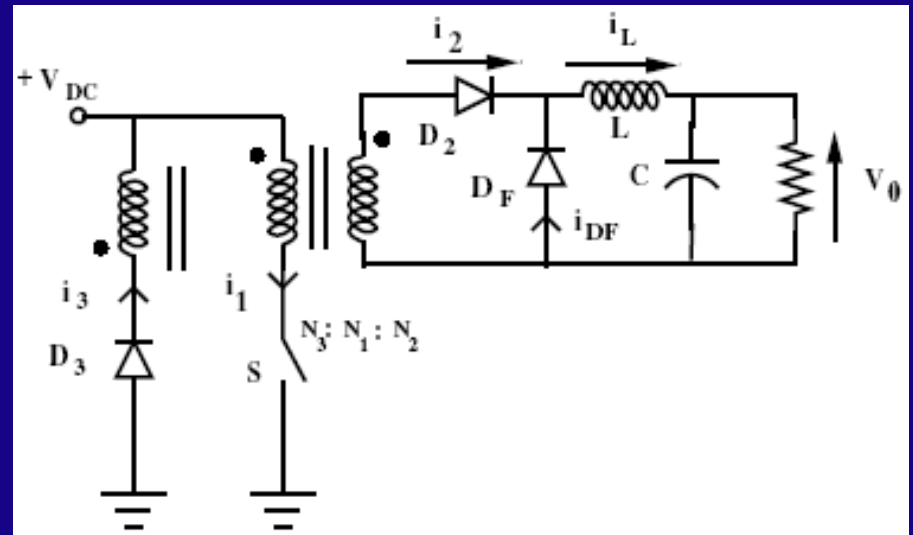
$\therefore$  magnetising current is finite.

$\Rightarrow$  when  $i_2 = 0$ ,  $i_1 \neq 0$

$\Rightarrow$  magnetising current should be continuous

$\Rightarrow$  calls for a separate winding

$\Rightarrow$  should provide a path for the magnetising 'I' (similar to fly-back connection)



Close 'S'

$$i_1 = i_2' + i_m$$

$i_m \rightarrow$  magnetising current

'V' applied to  $L_m = V_{DC}$

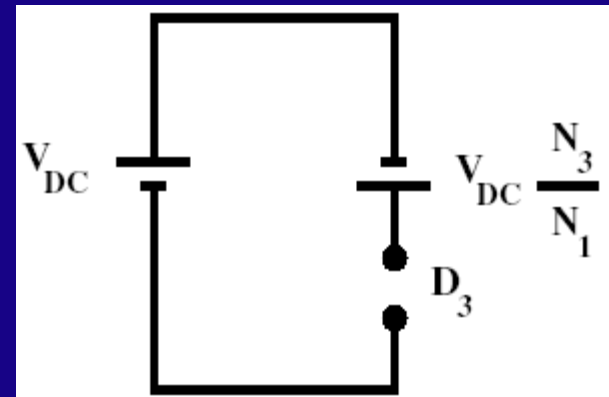
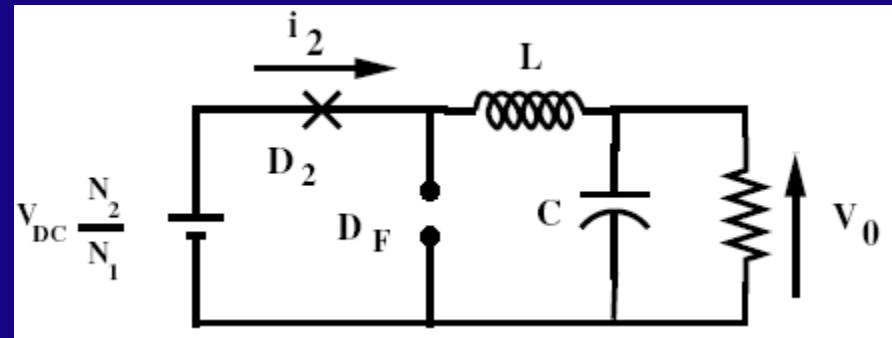
$\therefore i_m \uparrow$  linearly with time.

'V' induced in  $N_2$  supplies current to load ( $i_2$  can leave the dot)

'V' across  $D_F = V_{DC} \frac{N_2}{N_1}$

Right direction for  $i_3$  is to leave the dot.

$\Rightarrow$  not possible due to  $D_3$



OR: – 'V' induced in  $N_3 = V_{DC} \frac{N_3}{N_1}$  with ' $\bullet$ ' as +ve.

$$\therefore \text{'V' across } D_3 = -V_{DC} \left( 1 + \frac{N_3}{N_1} \right)$$

Open 'S'

$$i_1 = 0 \quad \therefore i_2 = 0$$

$i_m$  &  $i_L$  should be continuous  $\therefore i_L$  flows through  $D_F$ .

'V' across  $D_2 =$  'V' induced in  $N_2$

$\Rightarrow \frac{d\phi}{dt}$  is -ve  $\therefore$  all ' $\bullet$ ' are -ve

$\Rightarrow D_3$  starts conducting providing a path for  $i_m$

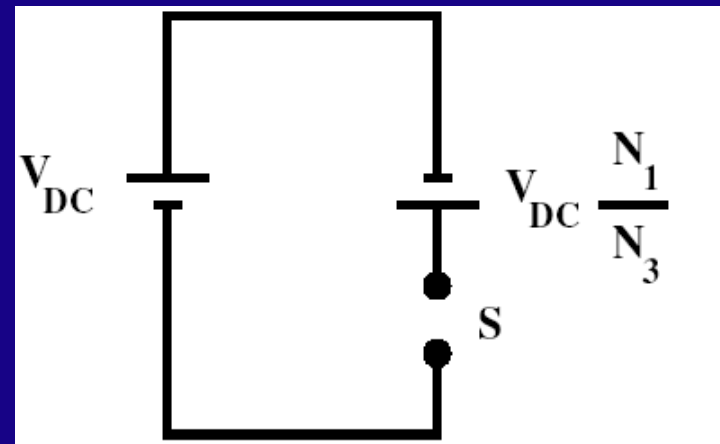
$$\text{Peak value of } i_m = I_m = \frac{V_{DC}}{L_m} DT$$

$$\text{Peak value in } N_3 = I_m \frac{N_1}{N_3}$$

'V' applied to  $N_3 = V_{DC}$  (with ' $\bullet$ ' as -ve)

$$\therefore \text{Induced 'V' in } N_1 = V_{DC} \frac{N_1}{N_3}$$

$$\therefore \text{'V' across 'S' = } V_{DC} \left( 1 + \frac{N_1}{N_3} \right)$$



$\Rightarrow$  'V' induced in  $N_2 = V_{DC} \frac{N_2}{N_3}$  (with '•' as -ve)

$\therefore$  'V' rating of  $D_2 = V_{DC} \frac{N_2}{N_3}$

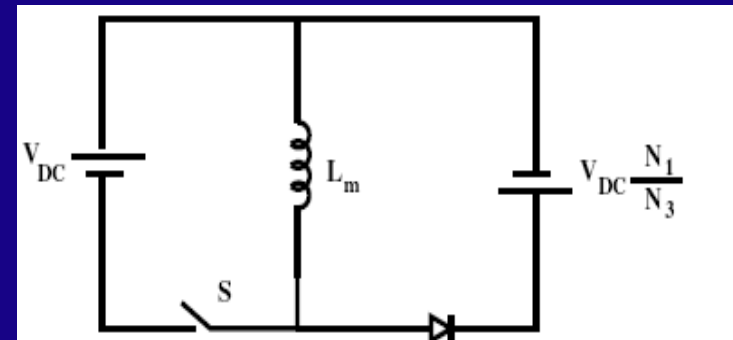
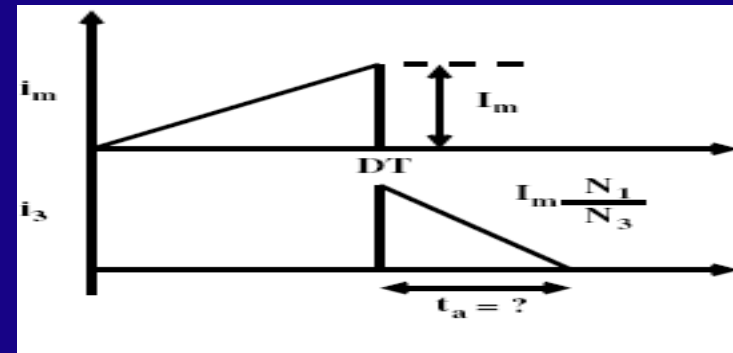
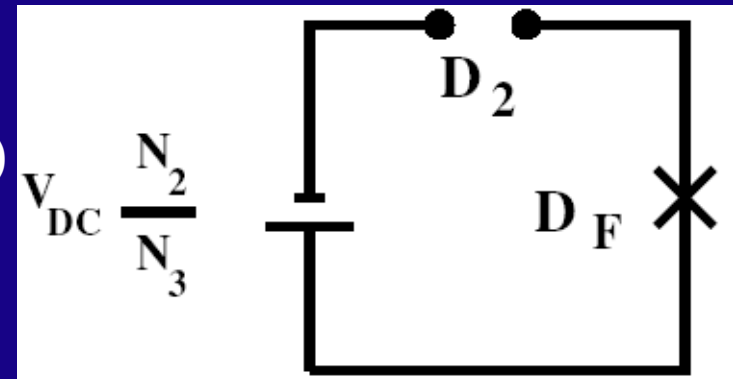
What is the value of  $N_3$  = ?

$$\uparrow d\phi = \frac{V_{DC} DT}{N_1}$$

$$\downarrow d\phi = \frac{V_{DC}}{N_3} t_a$$

equating above equation,

$$t_a = \frac{N_3}{N_1} DT$$



For core flux to become zero,

$$t_a < (1 - D)T$$

$\therefore D$  must be limited to  $D_{\max}$  such that

$$\frac{N_3}{N_1} D_{\max} T = (1 - D_{\max}) T$$

$$\Rightarrow D_{\max} = \frac{1}{2} \quad \text{if } N_3 = N_1$$

If  $N_3 = N_1$ ,  $D > 0.5$  :-

$i_m$  will not become zero, because

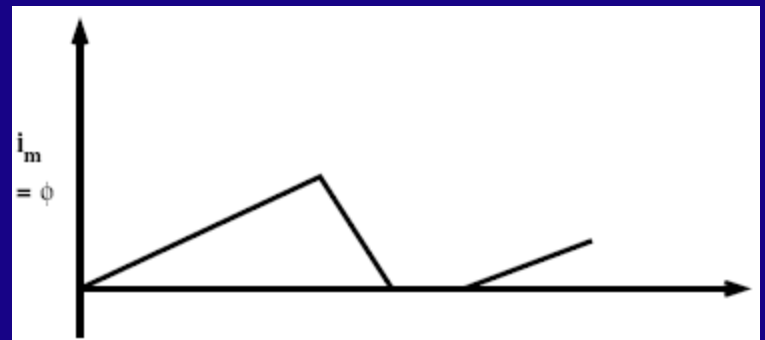
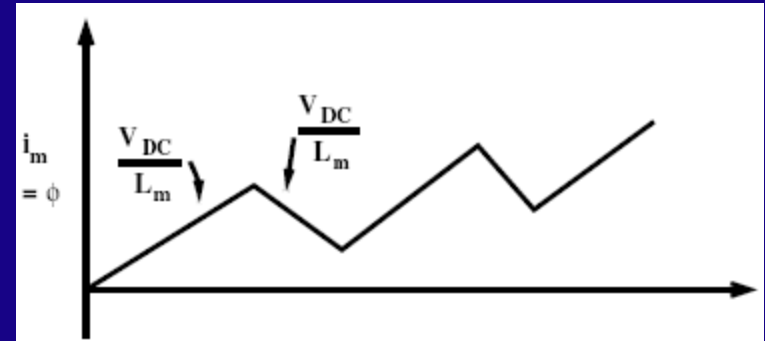
$+V_{DC}$  is applied for 'DT' &

$-V_{DC}$  is applied for  $(1-D)T$

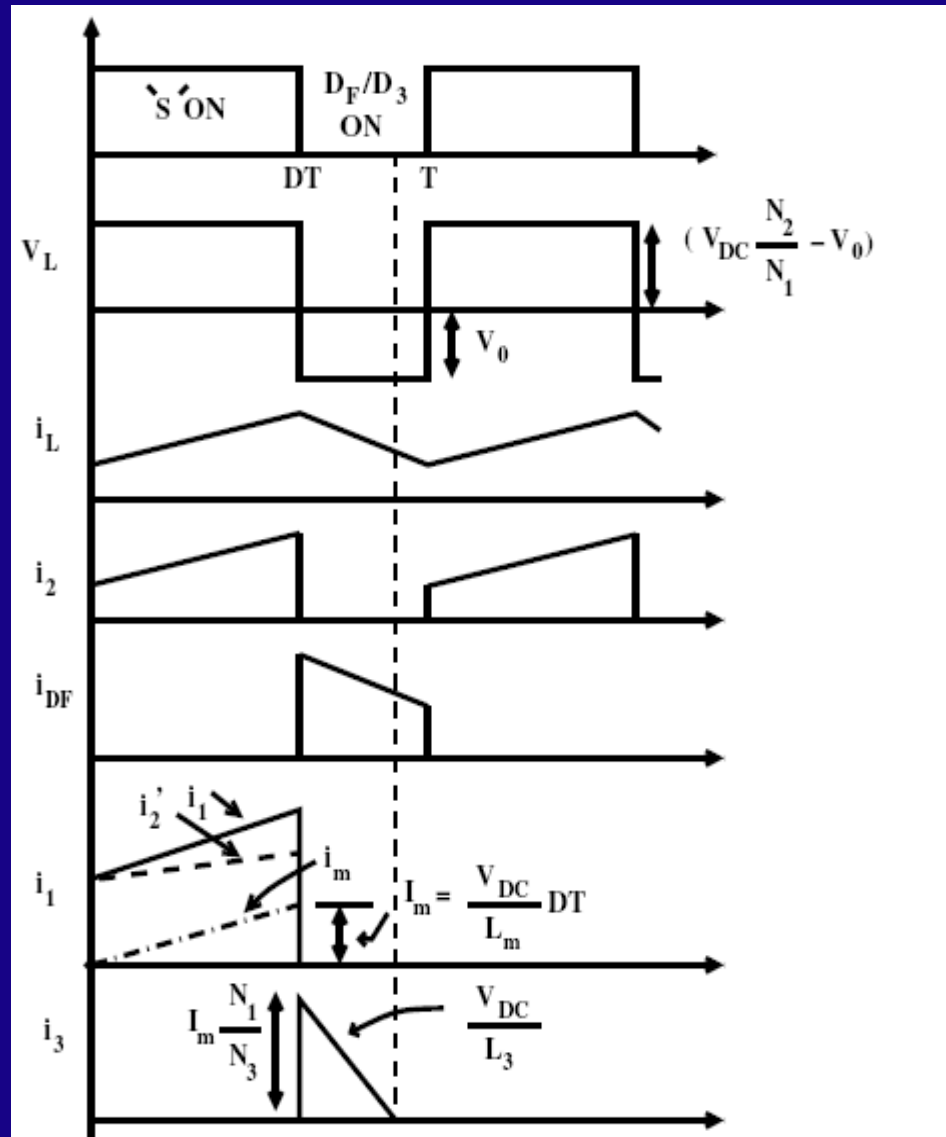
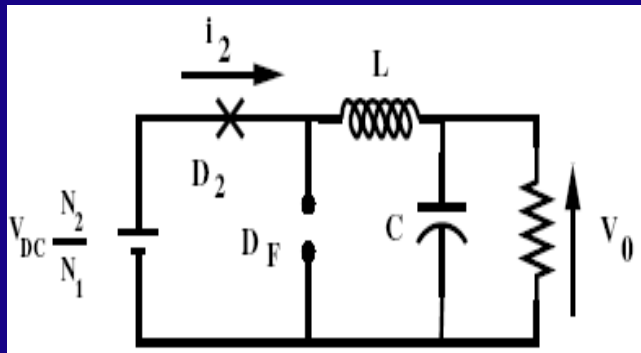
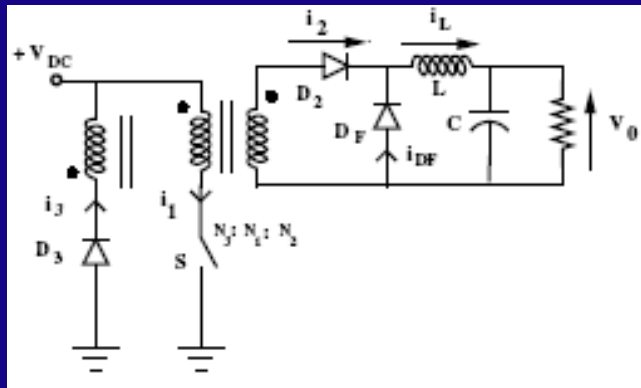
$\Rightarrow$  slope is the same

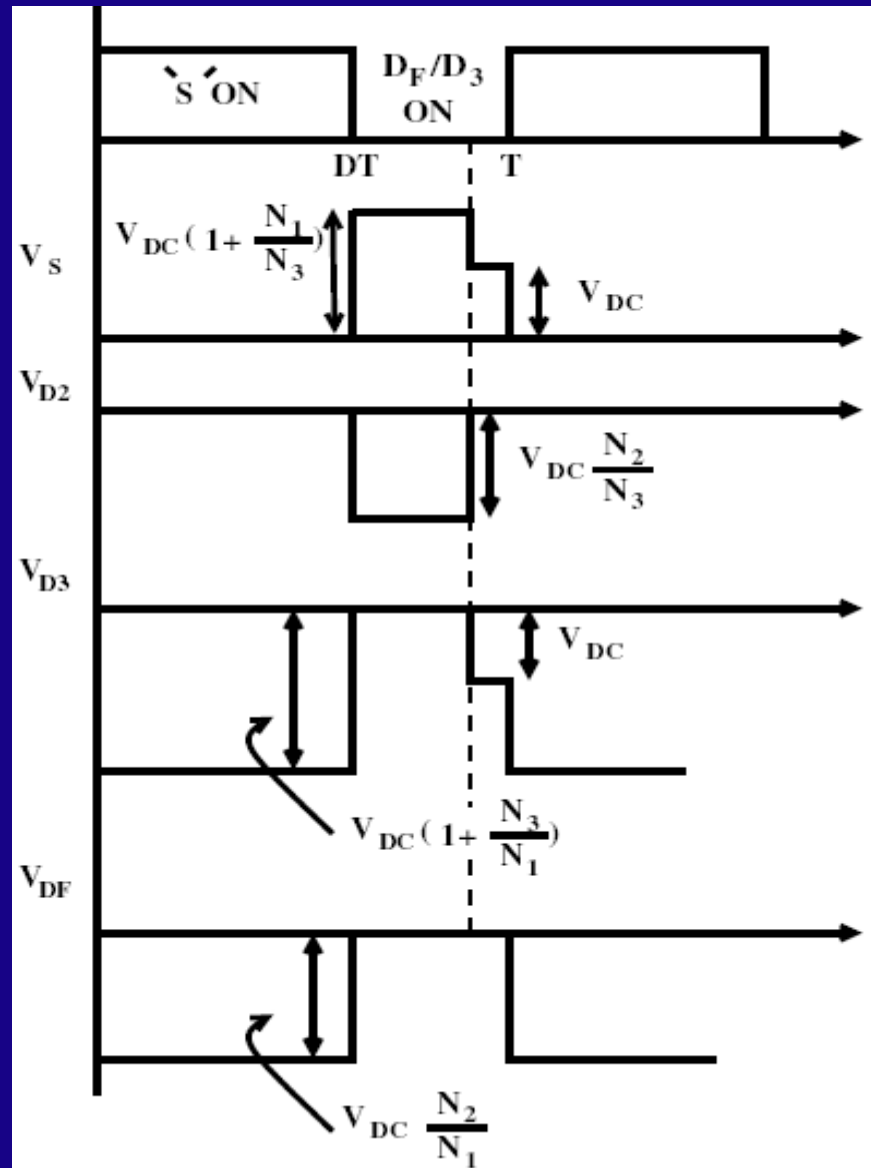
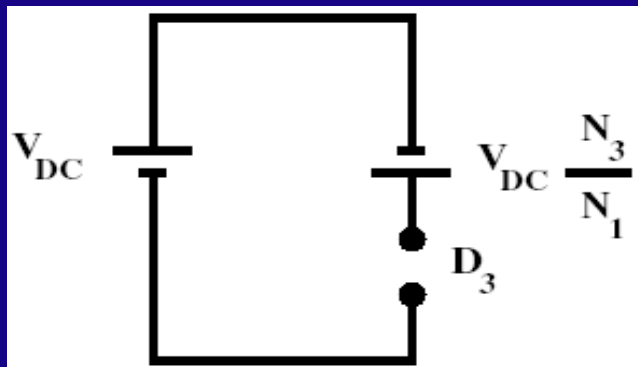
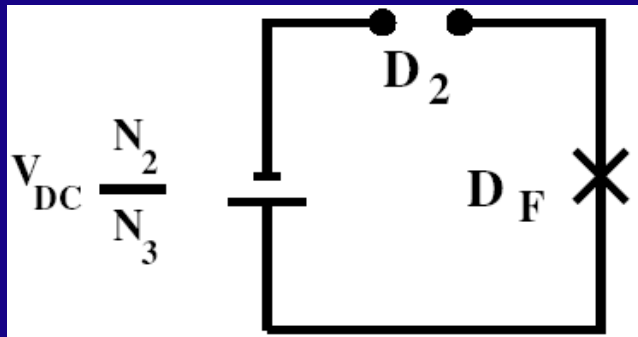
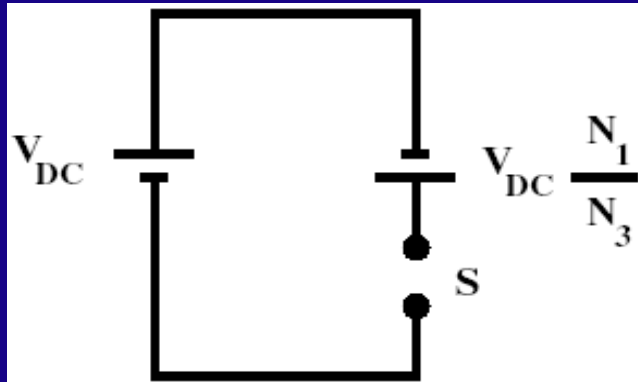
$\rightarrow$  core will saturate

$\rightarrow \therefore$  For  $D < 0.5$ , discontinuous (flux) conduction











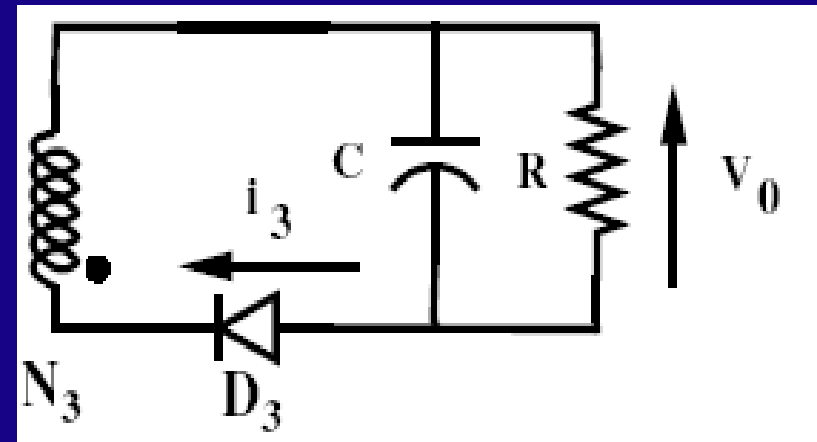
## Special Cases:

⇒ Primary & tertiary winding form a flyback converter

(C & R are replaced by  $V_{DC}$ )

⇒ No need to connect to  $V_{DC}$   
instead connect to C||R

OR : Using 2 – winding transformer

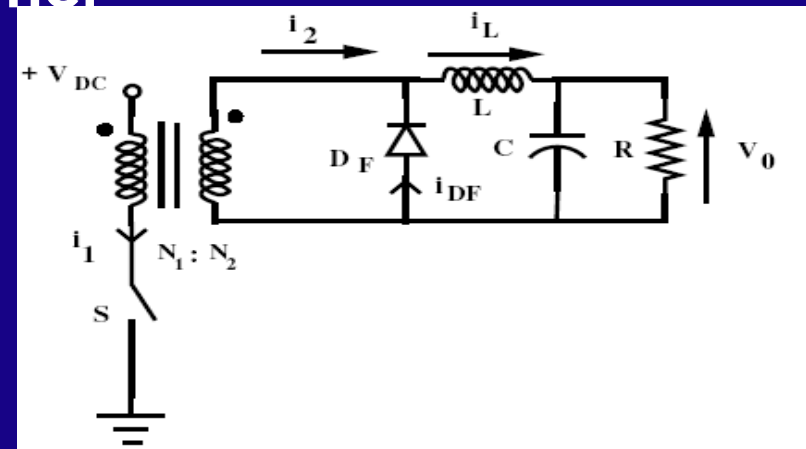


## Close 'S'

$i_1$  enters the dot

$i_2$  can leave the dot

$$I_1 = I_m + I'_2$$



## Open 'S'

$i_m$  &  $i_L$  should be continuous

For continuity of flux,  
right direction

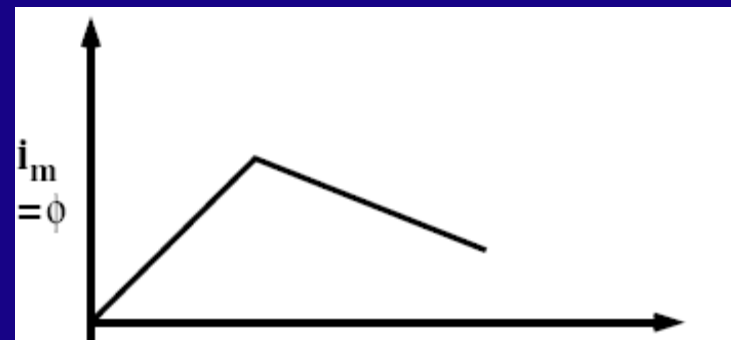
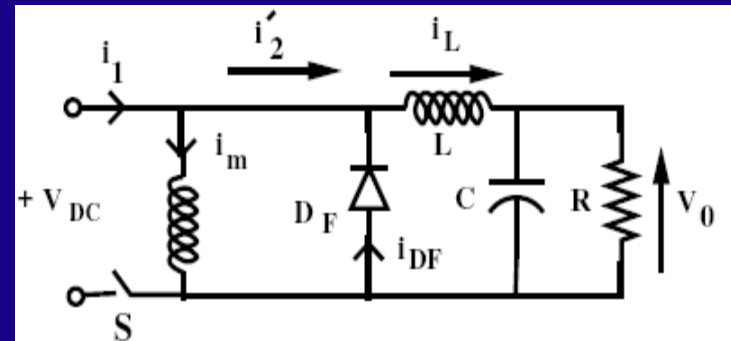
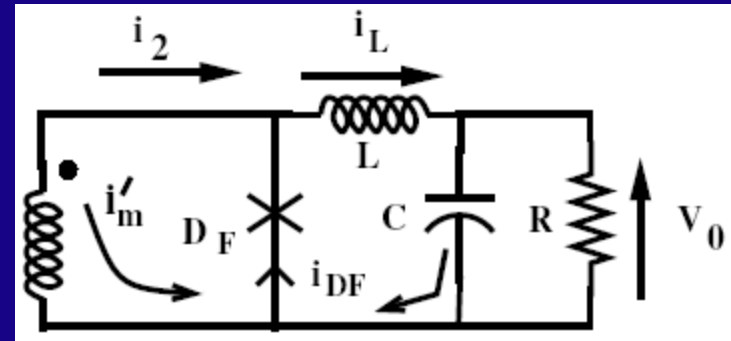
for ' $i$ ' in secondary  
(when ' $S$ ' is opened)  
is to enter the dot.

⇒ Possible.

⇒ ' $i$ ' in  $D_F = i'_m + i_L$

⇒ But ↓ of  $d\phi$  is very slow

⇒ Next cycle core may saturate



If  $L_f$  is not present

' $V_0$ ' appears directly  
across secondary

⇒ Affect the energy transfer

⇒ Do not allow ' $V_0$ '  
to appear across ' $N_2$ '

⇒ Use ' $L_f$ '

⇒  $i_L$  must be continuous

⇒ Use  $D_F$

⇒ Operation in the 1<sup>st</sup> quadrant only

