

Review :

1) No. of pulses : odd multiples of 3 for synchronization (no sub harmonics)

$\frac{1}{2}$ wave symmetry (no even harmonics)

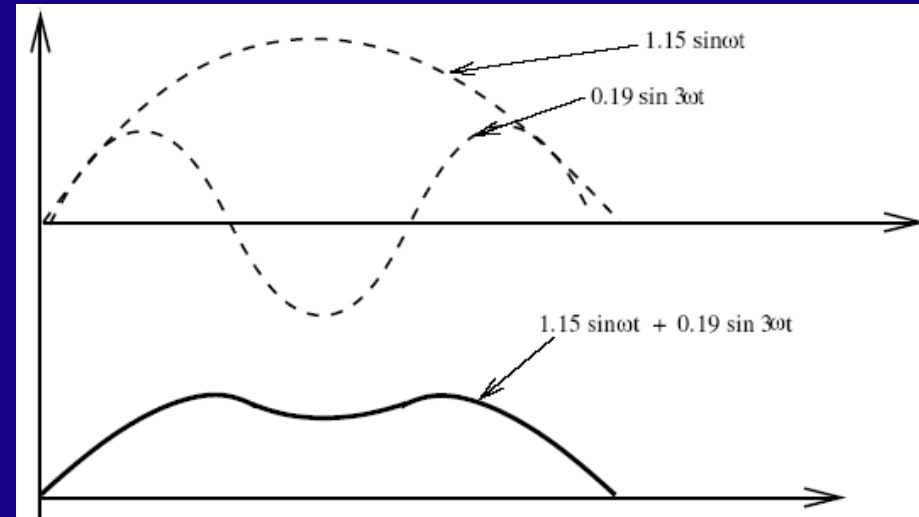
& 3- Φ symmetry

2) In sinusoidal PWM technique,
Predominant harmonic =

$$45 F_{\text{Sine}} \pm 2 F_{\text{Sine}} \dots \text{for } F_N = 45$$

3) DC utilization poor (Peak of the fundamental component of Line – line = $\frac{V_{\text{dc}}}{2} \sqrt{3}$)

4) Can be improved by adding 3rd harmonic component to the modulating wave.



Expression for modulating

$$\text{wave} = 1.15 \sin \omega t + 0.19 \sin 3\omega t$$

\therefore Peak fundamental component

$$\text{of } V_{L-L} = (1.15) \sqrt{3} \frac{V_{dc}}{2} = \underline{V_{dc}}$$

Harmonic elimination Techniques

Undesirable harmonics can be eliminated and fundamental can be controlled by creating notches at pre-determined angles

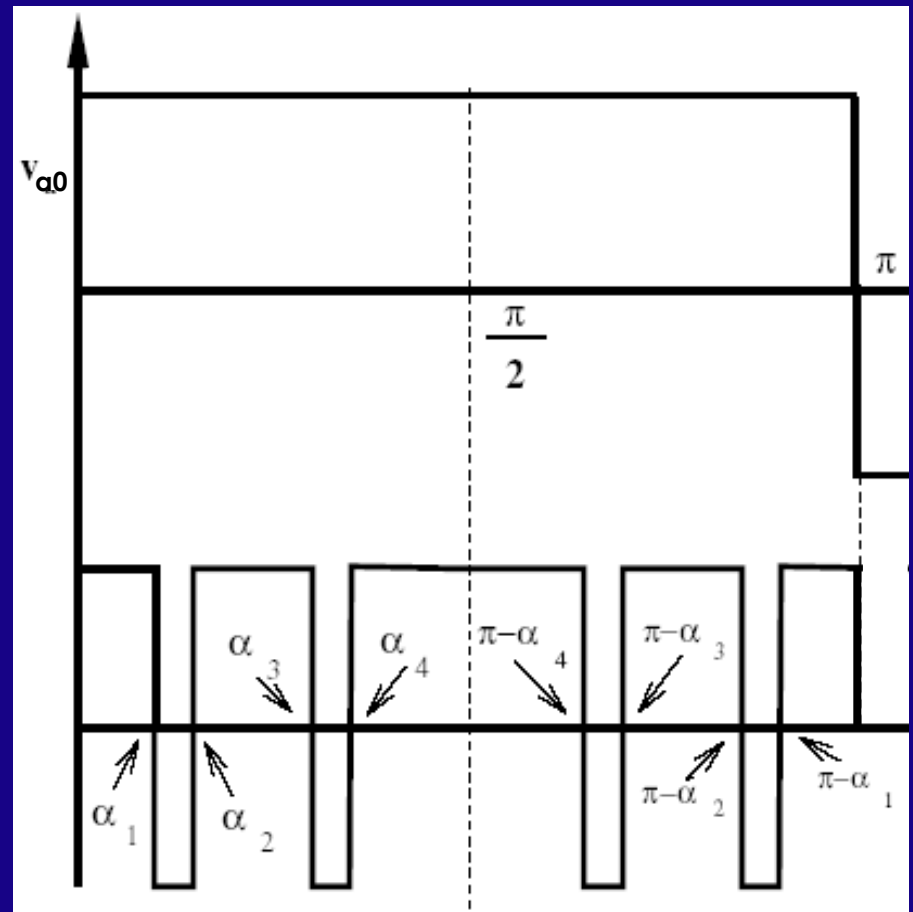
⇒ If 'n' switchings/ $\frac{1}{4}$ cycle

⇒ (n-1) harmonics are eliminated & magnitude of fundamental can be controlled

⇒ 4 switchings/(1/4) cycle

$(\alpha_1, \alpha_2, \alpha_3, \alpha_4)$

$$\alpha_1 < \alpha_2 < \alpha_3 < \alpha_4 < \frac{\pi}{2}$$



- ⇒ 3 significant harmonics = 0
- ⇒ fundamental can be controlled
- ⇒ square wave has quarter wave odd symmetry
- ⇒ Coefficient of the fundamental & harmonic components are given by

$$b_n = \frac{4}{n\pi} \left\{ 1 + 2 \sum_{k=1}^m (-1)^k \cos(n \alpha_k) \right\}$$

Assume that there are 5 switchings/ $\frac{1}{4}$ cycle

\Rightarrow 4 harmonics can be made zero

\Rightarrow In 3 phase, 3 wire system, triple harmonics can be ignored.

So harmonics to be eliminated are 5th, 7th, 11th and 13th.

$$b_1 = \frac{4}{\pi} \{1 - 2\cos\alpha_1 + 2\cos\alpha_2 - 2\cos\alpha_3 + 2\cos\alpha_4 - 2\cos\alpha_5\}$$

$$b_5 = \frac{4}{5\pi} \{1 - 2\cos 5\alpha_1 + 2\cos 5\alpha_2 - 2\cos 5\alpha_3 + 2\cos 5\alpha_4 - 2\cos 5\alpha_5\} = 0$$

$$b_7 = \frac{4}{7\pi} \{1 - 2\cos 7\alpha_1 + 2\cos 7\alpha_2 - 2\cos 7\alpha_3 + 2\cos 7\alpha_4 - 2\cos 7\alpha_5\} = 0$$

$$b_{11} = \frac{4}{11\pi} \{1 - 2\cos 11\alpha_1 + 2\cos 11\alpha_2 \dots \dots \dots - 2\cos 11\alpha_5\} = 0$$

$$b_{13} = \frac{4}{13\pi} \{1 - 2\cos 13\alpha_1 + 2\cos 13\alpha_2 \dots \dots \dots - 2\cos 13\alpha_5\} = 0$$

⇒ Non – linear transcendental equations

⇒ Solve numerically

⇒ choose required value for b_1
→ fundamental component

$$\alpha_1 = 10.514, \alpha_2 = 23.228$$

$$\alpha_3 = 29.289, \alpha_4 = 46.421$$

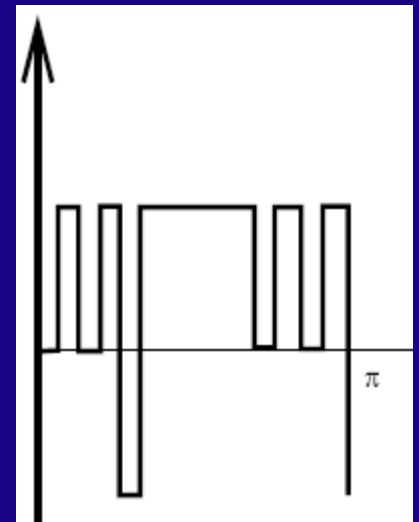
$$\alpha_5 = 50.157$$

$$b_1 = 0.986 \text{ p.u.}$$

⇒ Immediate Dominant Harmonic
'V' gets AMPLIFIED

A well designed PWM strategy should have the following:

- 1) No pulse of opposite polarity in $\frac{1}{2}$ cycle of line-line voltage waveform
 \Rightarrow large ripple current



2) Sub-harmonics=0 (PWM waveform must be synchronized with its own fundamental)

\Rightarrow Pulse No. = integer

$\Rightarrow \frac{1}{2}$ wave, $\frac{1}{4}$ wave, 3- Φ symmetry

\Rightarrow Do not allow different phases to switch simultaneously

⇒ The PWM inverter can be thought of as 3 separate driver stages which creates each phase waveform independently.

⇒ At any given instant, 1,2,3 devices may be either turned ON/OFF.

Using space vector PWM technique, it is proposed to achieve the above.