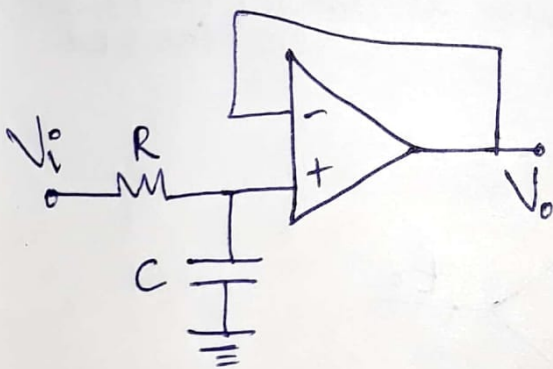


Low Pass filter (2nd order)

$$\frac{V_2}{V_1} = \frac{1/R_2 R_1 C_1 C_2}{s^2 + \left(\frac{1}{R_1 C_1} + \frac{1}{R_2 C_1} \right) s + \frac{1}{R_1 R_2 C_1 C_2}}$$

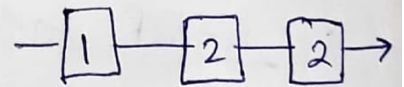
$$= \frac{\omega_0^2}{s^2 + (\omega_0/Q)s + \omega_0^2}$$



$$\frac{V_o}{V_i} = \frac{1}{1 + sRC}$$

1st order low pass

5th order



∴ For higher orders, just cascade these two filters.

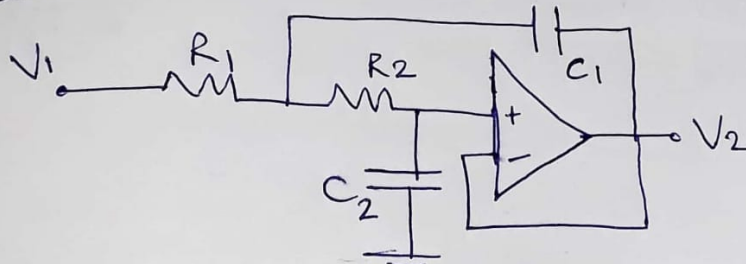
Impedance Transformation (To convert lp to hp)

Date

For $n=2$,

$$|T|^2 = \frac{K^2}{1+\omega^4} \Rightarrow |A_{\omega}|^2 = \frac{\omega^4}{1+\omega^4}$$

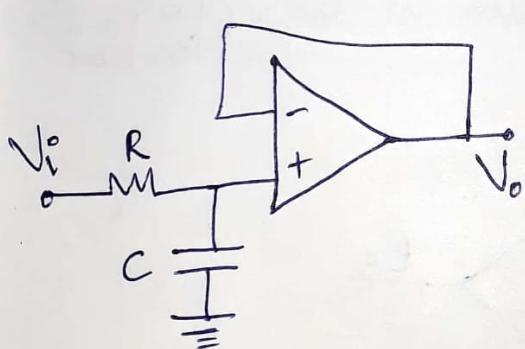
Sallen-Key Filter



Low Pass filter (2^{nd} order)

$$\frac{V_2}{V_1} = \frac{1/R_2 R_1 C_1 C_2}{s^2 + (1/R_1 C_1 + 1/R_2 C_1)s + 1/R_1 R_2 C_1 C_2}$$

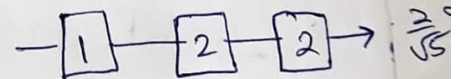
$$= \frac{\omega_o^2}{s^2 + (\omega_o/Q)s + \omega_o^2}$$



$$\frac{V_o}{V_i} = \frac{1}{1+SCR}$$

1st order low pass

5th order



∴ For higher orders, just cascade these two filters.

Impedance Transformation (To convert lp to hp)

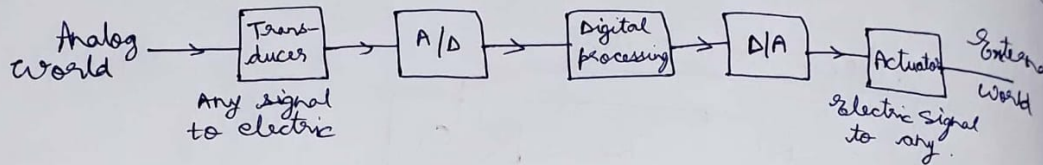
Notes:

$$\left. \begin{aligned} R &\equiv \frac{1}{1/R} \\ C &\equiv \frac{1}{1/C} \end{aligned} \right\} s \rightarrow \omega_o/s$$

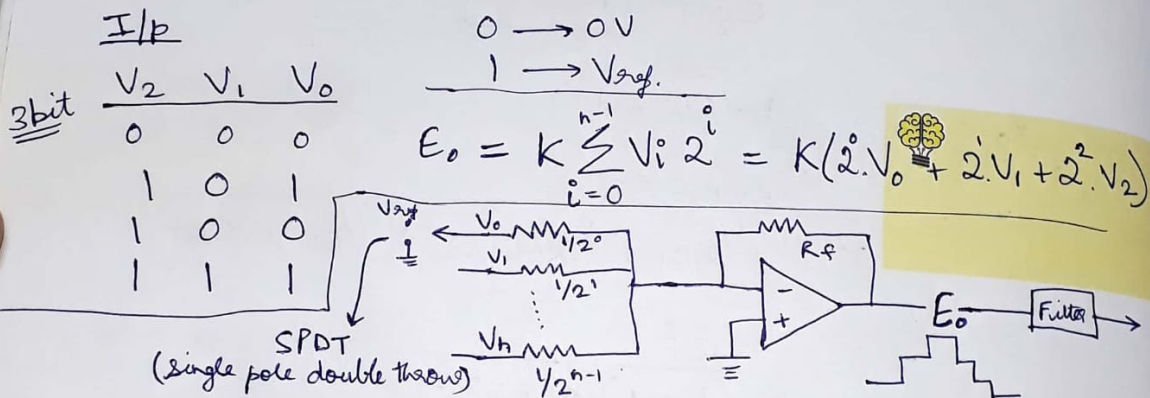


Date 16/6/18

D to A and A to D converter (Mixed Signal Processing)

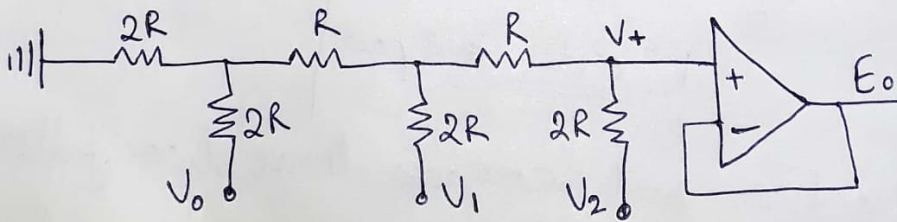


D to A



It is difficult to have the resistance values precisely & the range of resistance values is large (1Ω to $2^n\Omega$) for 8 bit

\therefore R-2R ladder D/A converter



Case I: $V_0 = V_1 = 0, V_2 = 1$,

Notes: $\therefore V_+ = \frac{V_2}{2}$

Case II: $V_0 = V_2 = 0, V_1 = 1$,

$\therefore V_+ = \frac{V_1}{4}$

Case III: $V_0 = 1, V_1 = V_2 = 0$

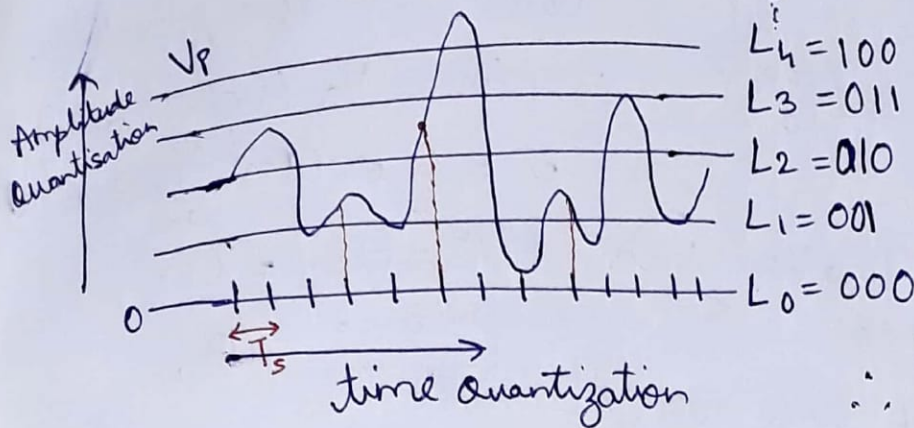
$\therefore V_+ = \frac{V_0}{8}$

$\therefore E_o = \frac{V_0}{8} + \frac{V_1}{4} + \frac{V_2}{2}$

Single Dual Notes: $\Sigma - \Delta$ Success

Date

A to D



$f_s = \frac{1}{T_s}$

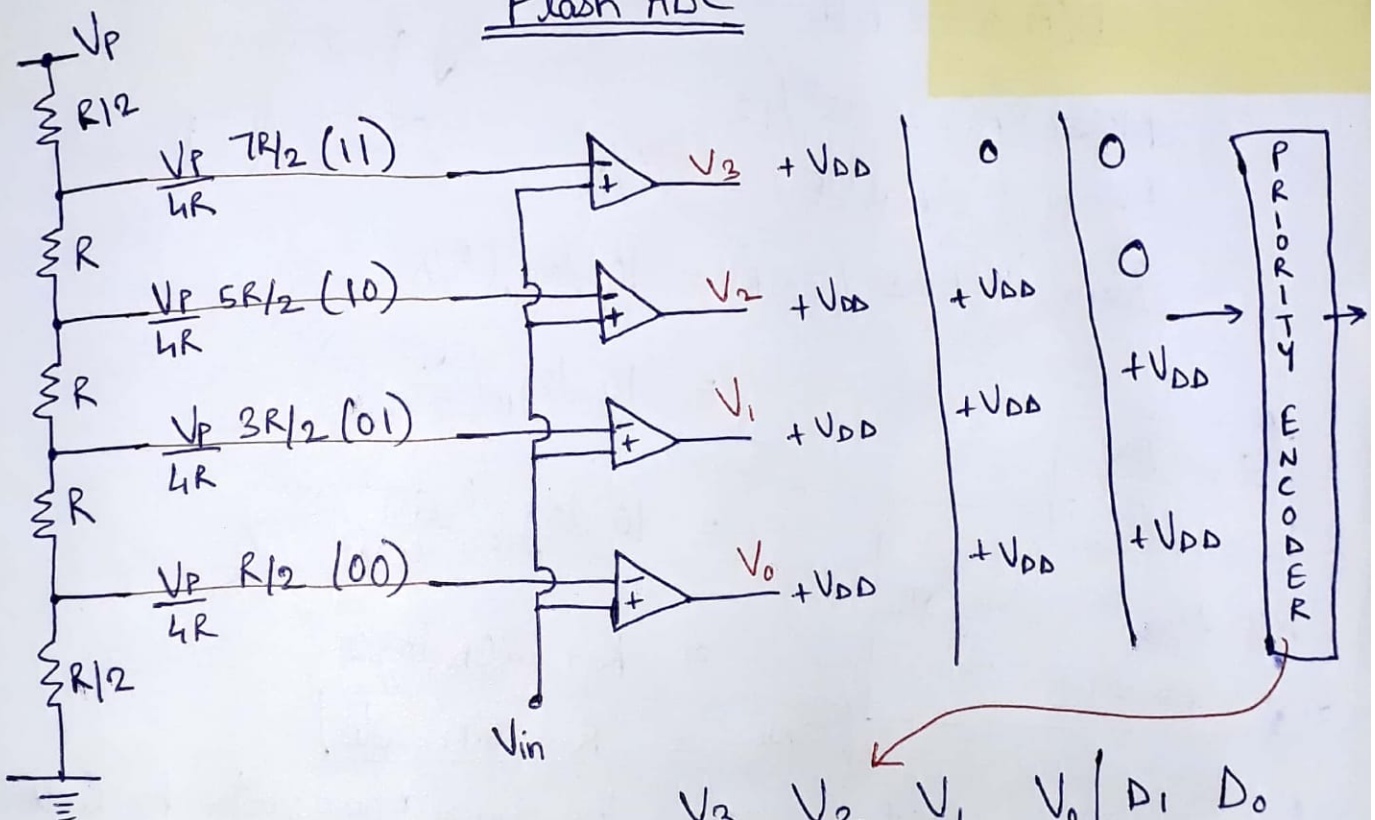
Sampling freq.
No. of samples taken per second.

$\therefore f_s > 2f_i$ highest freq. in input

or $f_s > 2(f_H - f_L)$ even works
(choose anti-aliasing filter appropriately)

f_L f_H

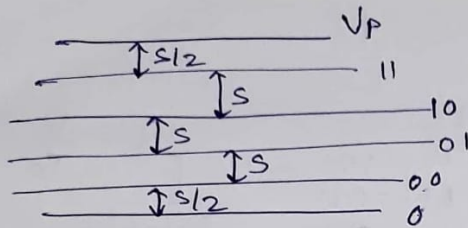
Flash ADC



Single Slope ADC
Multi Slope ADC

V_3	V_2	V_1	V_0	D_1	D_0
1	X	X	X	1	1
0	1	X	X	1	0

Date



$$\therefore S = \frac{V_P}{4}$$

\therefore Within a step, the signal can take any value with equal probability.

$$\therefore f(n) = 1/s \text{ (Uniform dist.)}$$

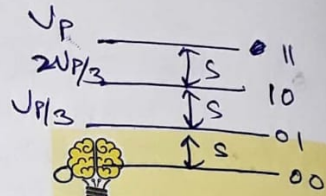
$$\bar{n} = 0 \text{ or } E(n) = \int_{-s/2}^{s/2} n \left(\frac{1}{s}\right) dn = 0$$

Quantization Error $\therefore \text{Var} = E(x^2) - E(x)^2 = E(x^2)$

$$\text{Var.} = s^2/12$$

\therefore A lower step size is desirable.

Higher Quantization error $\Leftarrow S = \frac{V_P}{3}$



17/4/18

$$D/A \leftrightarrow A/D$$

$$\text{Noise (N)} = s^2/12$$

$$\text{Energy of signal (E)} = V^2/2$$

$$\text{Signal to noise ratio (SNR)} = 10 \log_{10}(E/N)$$

$$= 10 \log_{10}\left(\frac{V^2 \cdot 12}{2 \cdot s^2}\right)$$

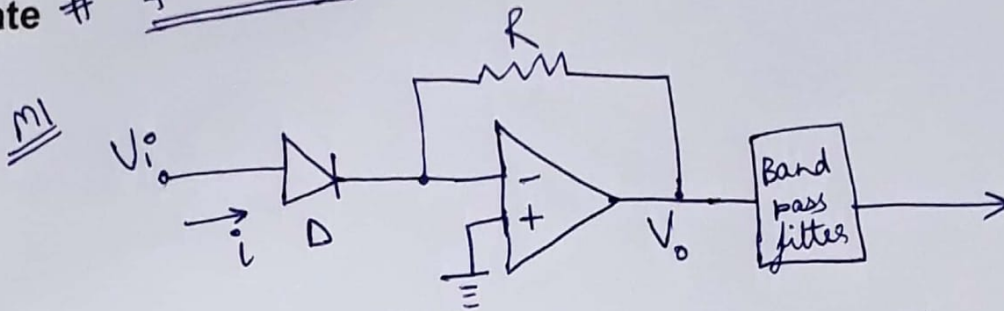
$$= 10 \log_{10}\left(\frac{6V^2 \cdot 2^{2n}}{4V^2}\right)$$

$$= K + 20n \log 2$$

$$\text{SNR} = K + 6n \text{ dB}$$

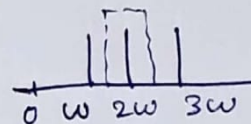
\therefore Adding 1 bit, improves the signal noise ratio by 6dB.

Date # $f \rightarrow 2f$



$$\begin{aligned} i &= I_0 e^{V_i / n k T} \\ &= -\frac{V_o}{R} \end{aligned} \quad \left. \vphantom{\begin{aligned} i &= I_0 e^{V_i / n k T} \\ &= -\frac{V_o}{R} \end{aligned}} \right\} \begin{aligned} V_o &= -I_0 R e^{V_i / n k T} \\ &= -I_0 R \left[1 + \frac{V_i}{n k T} + \frac{V_i^2}{2 n^2 k^2 T^2} + \dots \right] \end{aligned}$$

Filter out the $2f$ freq.

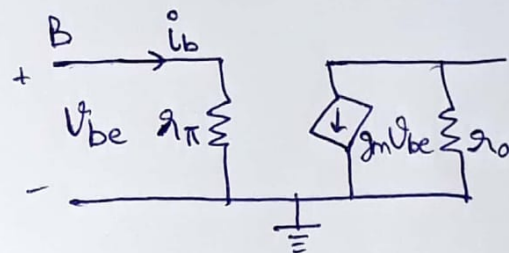
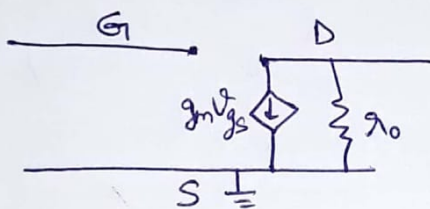


For, $V_i = V_A \sin \omega t$

Take square wave with $0, 2\omega, 4\omega$ frequencies & then filter out just 2ω freq.



BJT & MOS



$$i_c = \beta i_b, \quad \beta = g_m r_{\pi}$$

Bi CMOS \rightarrow CMOS + BJT.

Stability

$$A\beta = 1 \rightarrow$$

\therefore \uparrow gain & phase margin for stability

