Re view

- 1. Buck, Boost, Buck Boost & Cuk' Inverter \rightarrow No isolation
- $\Rightarrow |V_{DC}| \& |V_0|$ can not be greatly different
- ⇒ Use a transformer & do not allow it to saturate

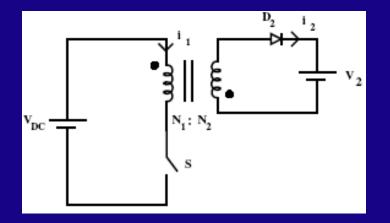
Close 'S' for 'DT' duration:

 $'i_1$ enters the dot in the primary.

$$i_2$$
 = 0, because of D_2

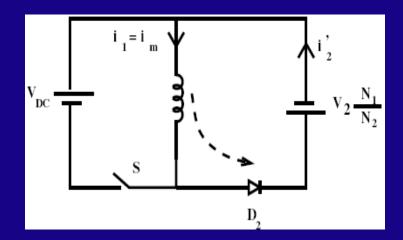


- 1 linearly with time.
- $'\phi'$ in the core also \uparrow linearly with time.



Open 'S'

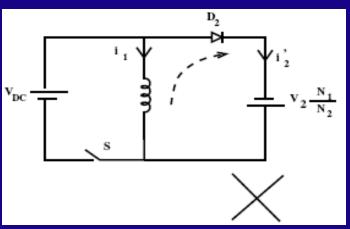
- \Rightarrow ' ϕ ' in the core must be continuous
- .. 'φ' due to i₂ should be in the same direction as that due to i₁ (they are not produced at the same time).



- \Rightarrow :. i₂ also enters the '•'
- i_1 & i_2' will flow simultaneously when 'S' is opened.
- \Rightarrow No path for i_m
- ⇒'V' spike across 'S'
- ⇒Instead of feeding power to another

 'V' source, connect a parallel

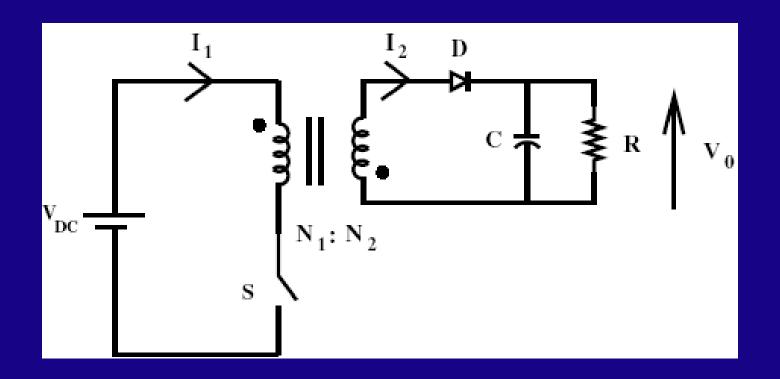
 combination of C & R
- ⇒ Fly back converter





FLYBACK CONVERTER:

Freewheeling diode also known as flywheel diode. Very popular upto 200 W.



Close S:

Current enters the dotted terminal.

l₂ should leave the dot in the secondary.

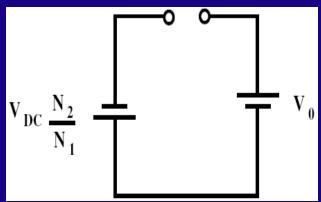
⇒ Not possible due to D

$$\therefore I_2 = 0$$
 $\therefore I_1 = I_s = I_m \rightarrow \text{only the magnetizing 'I'}$.

 $i_1 \& : \phi \uparrow linearly.$

'C' supplies power to the load.

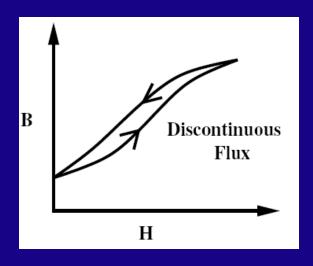
'V' across
$$N_1 = V_{DC}(\bullet ' is + ve)$$

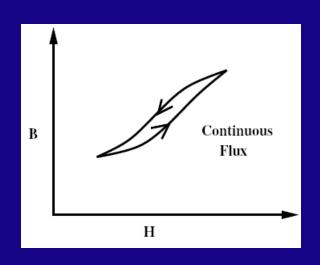


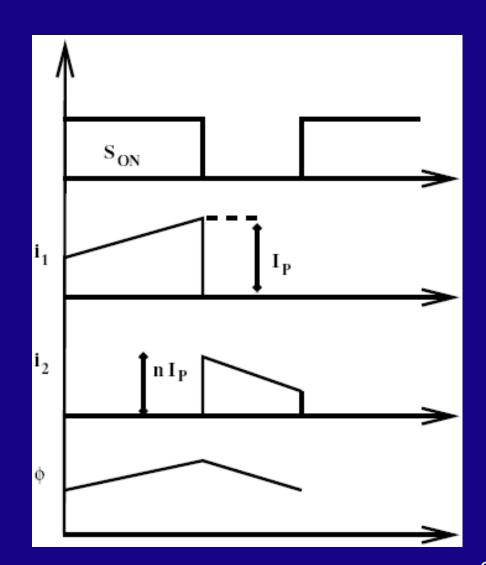
∴'V' induced in secondary =
$$V_{DC} \frac{N_2}{N_1}$$
 ('•' is + ve)

Open S:

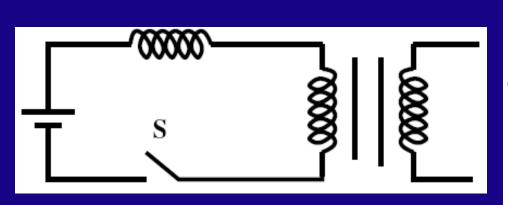
- 'φ' in the core must be continuous.
- \Rightarrow i₂ will flow in the sec. in such a way that direction of ' ϕ ' due to i₁ is same
- \Rightarrow i₂ enters the dot in secondary
- ⇒ Stored energy is transferred to the load
- \Rightarrow i₂ may or may not become zero
- \Rightarrow i₂ \neq 0 just prior to turn ON of 'S'
- \Rightarrow ' ϕ ' is continuous (unidirectional ' ϕ ')

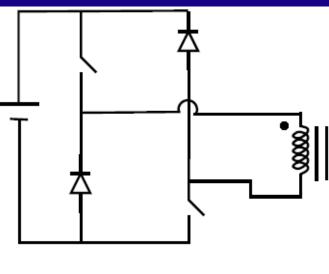






- ⇒ Generally operated in discontinuous mode because if accidentally D↑, core may saturate⇒'S' may fail
- ⇒ Airgap is provided in the airgap
- ⇒ Not tightly coupled⇒Leakage flux





⇒ Flux will follow the above path only if there is Volt.Sec./Turn balance

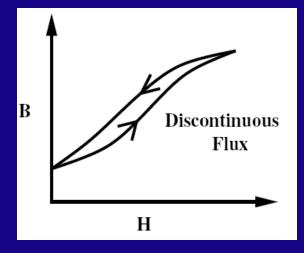
$$\uparrow$$
 in $d\phi = \downarrow$ in $d\phi$

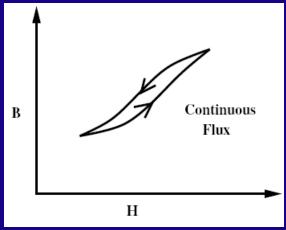
$$\uparrow \text{ in } d\phi = \frac{V_{DC}}{N_1} DT$$

$$\downarrow \text{ in } d\phi = \frac{V_0}{N_2} (1 - D)T$$

$$\therefore \frac{\mathbf{V}_0}{\mathbf{N}_2} (1 - \mathbf{D}) \mathbf{T} = \frac{\mathbf{V}_{DC}}{\mathbf{N}_1} \mathbf{D} \mathbf{T}$$

$$\therefore \mathbf{V}_0 = \mathbf{V}_{DC} \left(\frac{\mathbf{N}_2}{\mathbf{N}_1} \right) \left(\frac{\mathbf{D}}{1 - \mathbf{D}} \right)$$



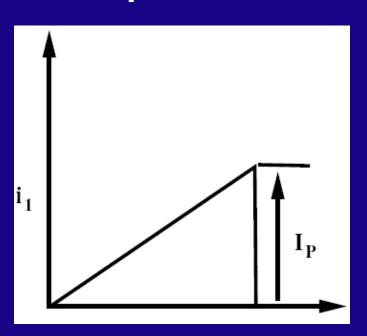


- $\Rightarrow |V_0| \& |V_{DC}|$ can be significantly different
- $\Rightarrow D_{\text{MAX}} = 0.5$
- \Rightarrow Choose $\frac{N_2}{N_1}$ suitably
- ⇒ Primary 'L' is a very important parameter

$$I_{P} = \frac{V_{DC}}{L_{1}}DT$$

$$\therefore \mathbf{P}_{\mathsf{in}} = \mathbf{V}_{\mathsf{DC}} \left[\frac{1}{2} \mathbf{I}_{\mathsf{P}} \frac{\mathsf{DT}}{\mathsf{T}} \right] \approx \mathbf{P}_{\!0}$$

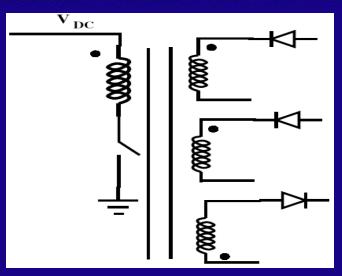
$$\therefore I_{P} = \frac{2P_{in}}{DV_{DC}} \approx \frac{2P_{0}}{DV_{DC}}$$



Advantage:

- 1) o/p can be significantly different.
- 2) Multiple o/p's are possible.
- 3) Isolation.

⇒Closed loop is a must



Various configuration:

