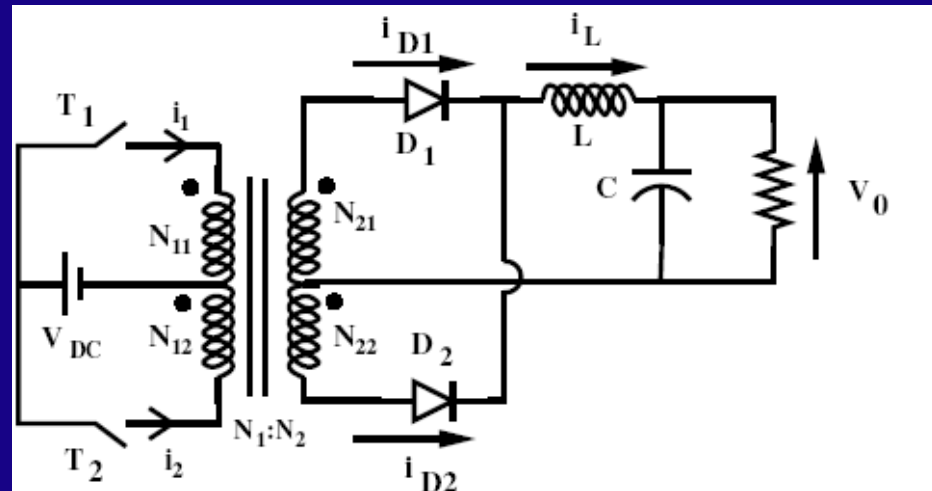


## Push – Pull converter :

$$N_{11} = N_{12} = \frac{N_1}{2}$$

$$N_{21} = N_{22} = \frac{N_2}{2}$$



From $t = 0$	to $t = \frac{DT}{2},$	$T_1$ is ON & $T_2$ is OFF
$t = \frac{DT}{2}$	to $t = \frac{T}{2},$	$T_1$ & $T_2$ are OFF
$t = \frac{T}{2}$	to $t = \frac{(1+D)T}{2},$	$T_2$ is ON & $T_1$ is OFF
$t = \frac{(1+D)T}{2}$	to $t = T,$	$T_1$ & $T_2$ are OFF

From  $0 < t < \frac{DT}{2}$   $T_1$  is ON

'V' across  $N_{11} = V_{11} = V_{DC}$  (with '•' as + ve)

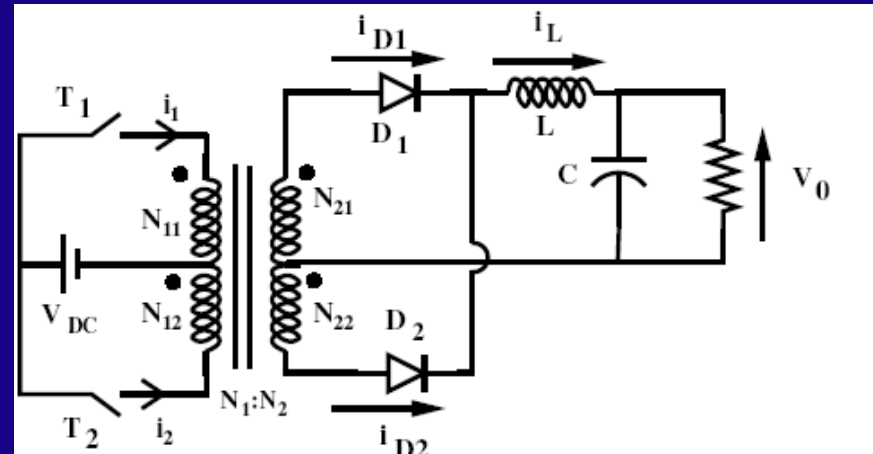
'V' across  $N_{12} = V_{12} = V_{DC}$

'V' across  $T_2 = 2V_{DC}$

$i_1$  enters the DOT

$i_{D1}$  can leave the DOT =  $i_L$

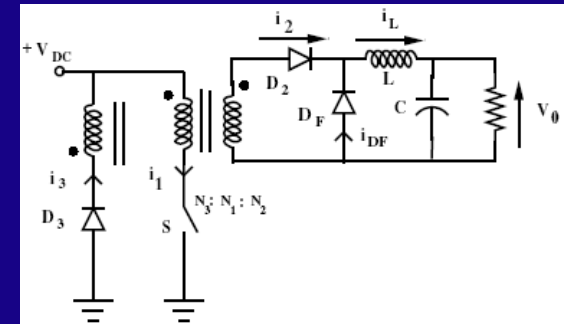
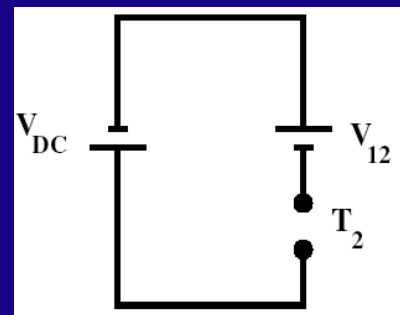
$i_{D2} = 0$



'V' across  $N_{21} = V_{21} = V_{DC} \frac{N_2}{N_1}$  = 'V' across  $N_{22}$

'D<sub>2</sub>' is off

$\therefore$  'V' across  $D_2 = 2V_{DC} \frac{N_2}{N_1}$



$i_{D2}$  enters the dot

$\Rightarrow i_{D1}$  can leave the dot

$\therefore$  If  $D_2$  conducts  $D_1$  will also conduct.

'V' across secondary = 0 ( $N_2$  turns)

'V' across primary = 0 ( $N_1$  turns)

$$N_{21} \frac{d\phi}{dt} - i_{D1} r = V_{01}$$

$$N_{22} \frac{d\phi}{dt} + i_{D2} r = -V_{01}$$

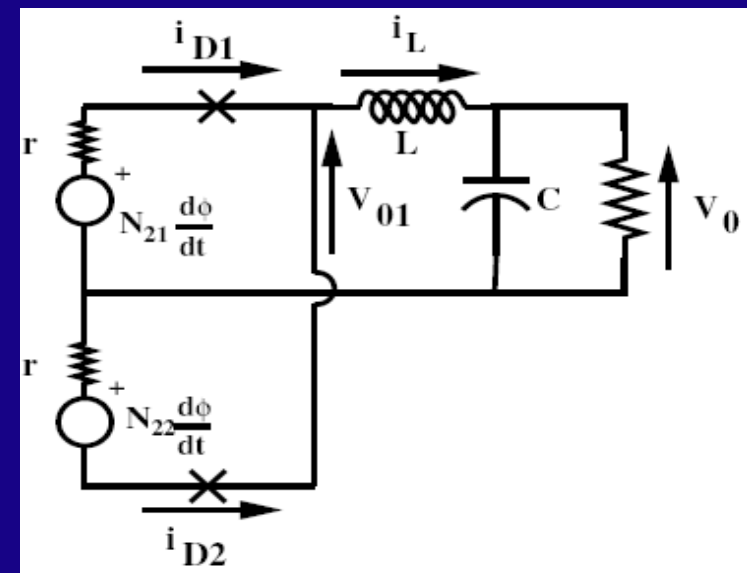
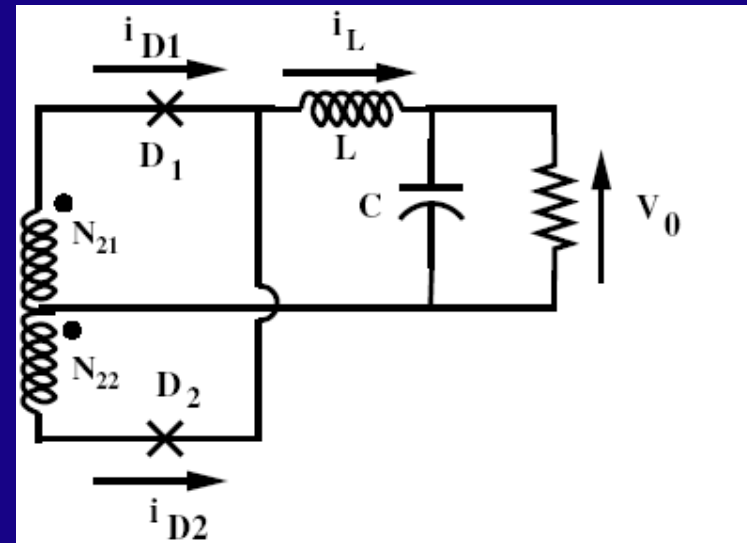
$$\therefore N_2 \frac{d\phi}{dt} = -(i_{D2} - i_{D1})r, \quad N_{21} = N_{22} = N_2 / 2$$

$i_{D2}$  should be  $> i_{D1}$ ,

$$i_{D1} : i_{D2} = i_L / 2$$

$$\Rightarrow V_{01} = 0 \quad \therefore V_L = -V_0,$$

$$\therefore \text{av. 'V' across } L = 0$$



$$V_0 = V_{DC} \frac{N_2}{N_1} D, \quad D \rightarrow \text{duty cycle of each switch} = \frac{T_{on}}{T_s / 2}$$

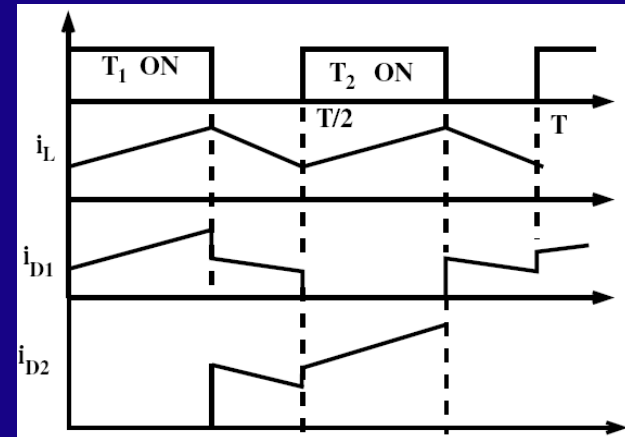
$$V_0 = 2V_{DC} \frac{N_2}{N_1} D, \quad D = \frac{T_{on}}{T_s}, 0 < D < 0.5$$

at  $T/2 < t < (1+D)T/2$ , close  $T_2$ ,

$$V_{12} = -V_{DC} \text{ (with '•' as -ve)}$$

$i_L$  flows through  $D_2$  &  $D_1$  can not conduct

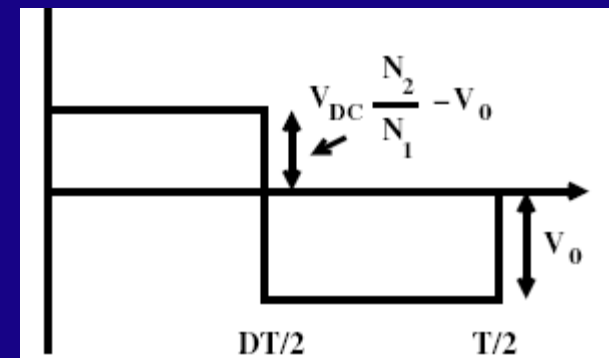
Open  $T_2$ : Both  $D_1$  &  $D_2$  conduct



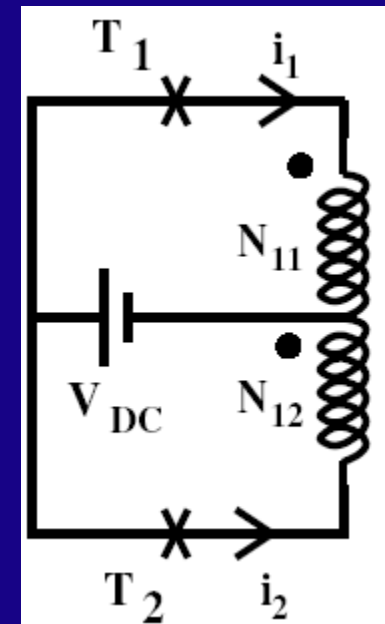
Limitations of push – pull converter :

In a practical circuit, two halves of push – pull converter are not the same

⇒ Primary winding may differ by a fraction of a turn



- ⇒ Switches may have slightly different saturation voltage
- ⇒ B – H curve is not traversed symmetrically
- ⇒ A dc flux in the core
- ⇒ Core imbalance
- ⇒ Flux walking to one direction
- ⇒ Sudden demand in load controller  $\uparrow D$  to max. value
- ⇒  $i$  &  $\therefore H \uparrow$
- ⇒ Core may saturate
- ⇒ Dead time between  $T_1$  &  $T_2$  :  
If both are ON flux produced by  $i_1$  &  $i_2$  opposes each other
- ⇒ If  $L_1 = L_2 = M$
- 'i' in the core is limited by 'r'.

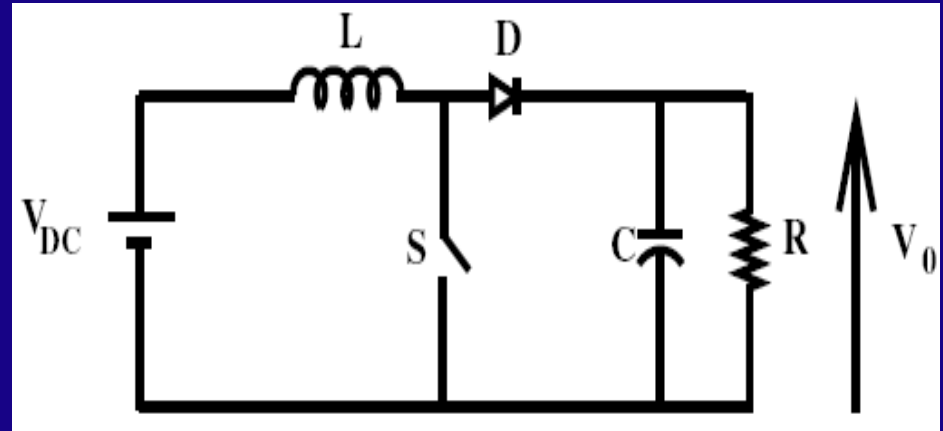




In 1960's → Linear Regulators

→ Simple

→ Low  $\eta$



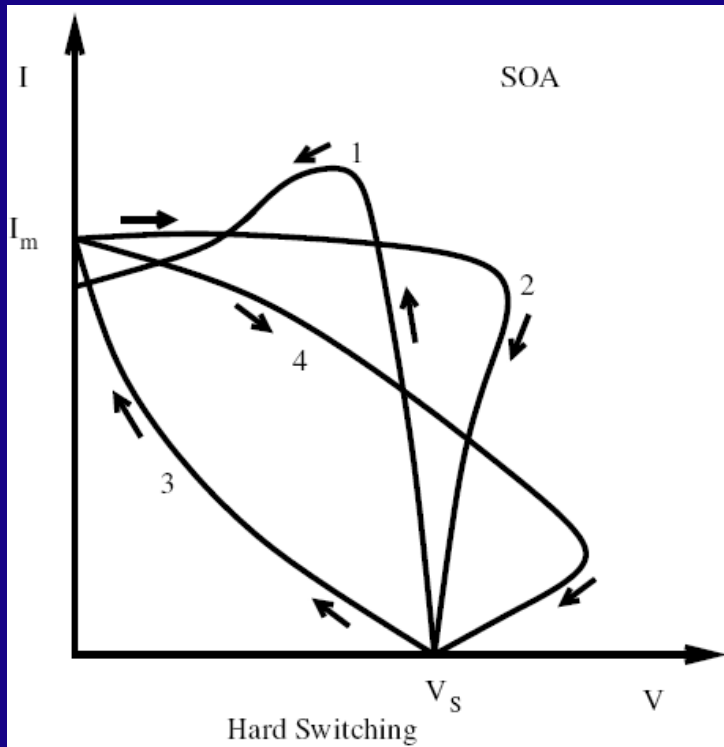
Switch Mode Conversion  $\Rightarrow$  Vary ' $D$ ' (ON/T) to control ' $V_0$ '

→ P.W.M. Control

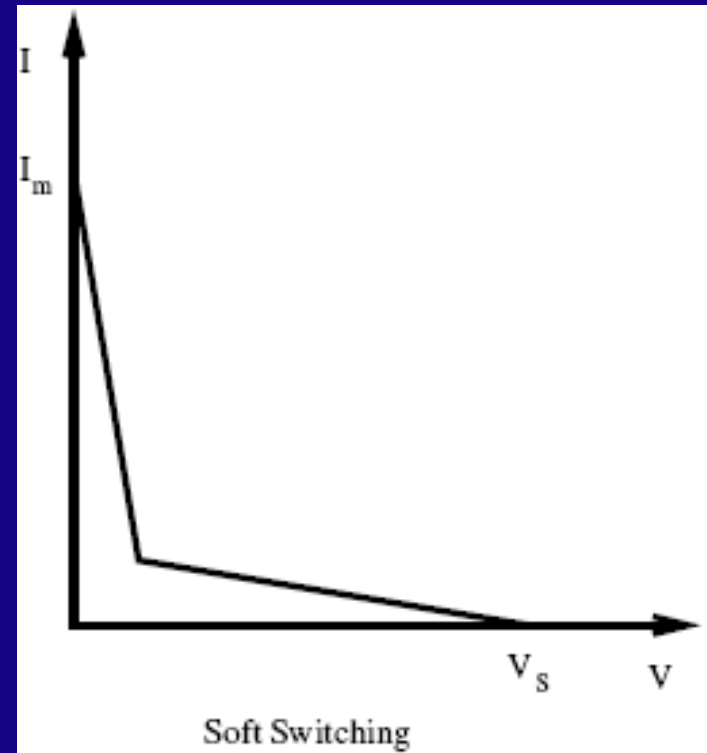
If ' $i$ ' is continuous, switches are required to turn ON/OFF the entire inductor ' $i$ '.

$\Rightarrow \frac{di}{dt}$  &  $\frac{dv}{dt}$  is very high

$\Rightarrow$  Hard Switching



Hard Switching



Soft Switching

Turn-On

Turn-Off

Without Snubber

1

2

With Snubber

3

4

SOA : Safe Operating Area

$V_s$  = Supply Voltage

$I_m$  = Maximum Current