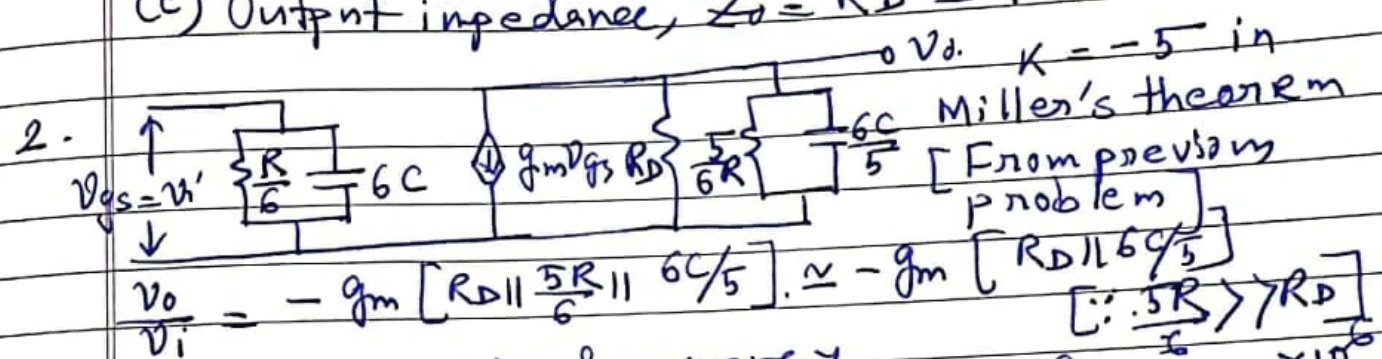


1. (a) Source terminal is common to both input and output.

(b) $I_{DS} = \frac{K_n'}{2} (V_{GS} - V_T)^2 = 5(5-1)^2 = 80 \text{ mA}$
 $V_{DS} = V_{DD} - I_{DS} R_D = 15 - 80 \times 0.125 = 5 \text{ V}$
 $V_{DS} > V_{GS} - V_T$, Transistor in satn.
 $g_m = K_n' (V_{GS} - V_T) = 10(5-1) = 40 \text{ mS}$
 $V_o = -g_m R_D V_i = -40 \times 0.125 \times 10^{-3} = -5 \times 10^{-3} \text{ V}$

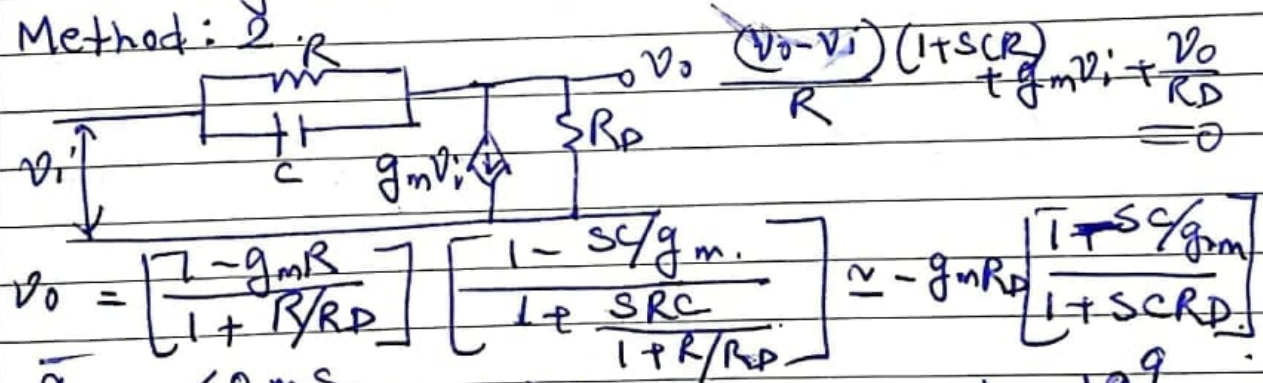
(c) Output impedance, $Z_o = R_D = 125 \Omega$



$\frac{V_o}{V_i} = -g_m [R_D \parallel \frac{5R}{6} \parallel \frac{6C}{5}] \approx -g_m [R_D \parallel \frac{6C}{5}]$ [$\because 5R \gg R_D$]
~~Corner~~ Corner 3dB frequency
 $\omega_0 = \frac{1}{R_D \cdot \frac{6C}{5}} = \frac{5}{6 C R_D} = \frac{5 \times 10^9}{6 \times 125} = 6.67 \times 10^6 \text{ rad/s}$

Actually, the gain can not come down to 28 dB with the given parameters.

Method: 2



$V_o = \left[\frac{1 - g_m R}{1 + R/R_D} \right] \left[\frac{1 - sC/g_m}{1 + \frac{sRC}{1 + R/R_D}} \right] \approx -g_m R_D \left[\frac{1 + sC/g_m}{1 + sC R_D} \right]$
 $g_m = 40 \text{ mS}$, $g_m R \gg 1$
 $R = 1 \text{ M}\Omega$, $R \gg R_D$
 $R_D = 125 \Omega$

Pole freq = $\frac{1}{C R_D} = \frac{10^9}{125} = 8 \times 10^6 \text{ rad/s}$
 Zero freq = $\frac{g_m}{C} = \frac{40 \times 10^{-3}}{6 \times 10^{-9}} = 6.67 \times 10^6 \text{ rad/s}$

The minimum gain = 0 dB

Maximum gain = 14 dB

The zero is near enough that the gain does not go to $14 - 28 = -14 \text{ dB}$

$$3. |I_{DS}| = 5 \text{ mA} \cdot g_m = \sqrt{2k'I_{DS}} = \sqrt{2 \times 10 \times 5} = 10 \text{ mS}$$

$$\mu = g_m r_o = g_m \frac{1}{\lambda I_{DS}} = \frac{10}{0.01 \times 5} = 200 \gg 1.$$

$$v_{o2} = \frac{\mu}{1+\mu} v_i \approx v_i$$

$$v_{o1} = \frac{-\mu v_i r_o}{r_o + r_o + (1+\mu)r_o} \approx -v_i$$

$$\frac{v_{o1} - v_{o2}}{v_i} \approx -2$$

$$4.(b) v_o = \frac{(1+\mu)(iR_s)r_o}{r_o + r_o + (1+\mu)R_s}, Z = \frac{v_o}{i} = \frac{(1+\mu)r_o R_s}{2r_o + (1+\mu)R_s}$$

$$\Rightarrow Z \approx \frac{\mu r_o R_s}{2r_o + \mu R_s} \approx \frac{g_m r_o^2 R_s}{2r_o + g_m r_o R_s} = \frac{g_m r_o R_s}{2 + g_m R_s}$$

$$g_m = 10 \text{ mS}$$

$$R_s = 1 \text{ k}\Omega$$

$$g_m R_s = 10 \gg 2$$

$$\approx r_o$$

$$= \frac{1}{\lambda I_{DS}} = 20 \text{ k}\Omega$$

$$(a) \cancel{I_{DS} = 5 \text{ mA}} \cdot \frac{k'}{2} (V_{GS} - V_T)^2 = 5 \Rightarrow V_{GS} = V_{GS2} = V_T + 1 \text{ V}$$

$$V_{DS} = V_{GS} - V_T \quad [\text{For minimum } V_{DD}]$$

$$V_{o2}(\text{DC}) = 1 \text{ V}$$

$$(a) I_{DS} = 5 \text{ mA}; \frac{k'}{2} (V_{GS} - V_T)^2 = 5, V_{GS} - V_T = 1$$

$$\Rightarrow V_{GS} = 2 \text{ V}$$

$$V_{DS} = V_{GS} - V_T \quad [\text{For minimum } V_{DD}]$$

$$= 1 \text{ V}$$

$$V_D = V_{DS} + I_D R_s = 1 + 5 \times 1 = 6 \text{ V} = 6 \text{ V}$$

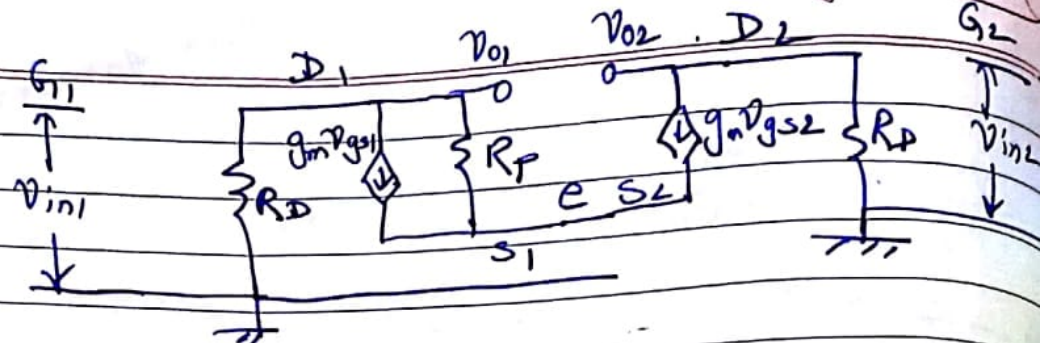
$$V_{G2} = V_{GS} + I_D R_s = 2 + 5 = 7 \text{ V}$$

By similar analysis for top pMOS, $V_{DS} = -1$,

$$V_{DD} = V_S = V_D + 1 = 6 + 1 = 7 \text{ V}$$

$$\text{and } V_{G1} = 5 \text{ V}$$

5.



$$\frac{v_{o1}}{R_D} + g_m v_{gs1} + \frac{v_{o1} - e}{R_P} = 0$$

$$\frac{v_{o2}}{R_D} + g_m v_{gs2} = 0$$

$$\frac{v_{o1} - e}{R_P} + g_m v_{gs1} + g_m v_{gs2} = 0 \quad \left| \begin{array}{l} v_{gs1} = v_{i1} - e \\ v_{gs2} = v_{i2} - e \end{array} \right.$$

$$\Rightarrow e = \frac{v_{o1} + g_m R_P (v_{i1} + v_{i2})}{1 + 2g_m R_P}$$

$$= \frac{v_{o1}}{1 + 2g_m R_P} + \frac{v_{i1} + v_{i2}}{2}$$

$$= \frac{v_{o1}}{1 + 2g_m R_P} + v_{cm}$$

$$[g_m R_P \gg 1]$$

$$\left[\begin{array}{l} v_{i1} - v_{i2} = v_{dm} \\ \frac{v_{i1} + v_{i2}}{2} = v_{cm} \end{array} \right]$$

$$v_{gs1} = v_{i1} - e$$

$$= v_{i1} - \frac{v_{o1} + g_m R_P (v_{i1} + v_{i2})}{1 + 2g_m R_P}$$

$$= \frac{v_{i1} (1 + g_m R_P) - g_m R_P v_{i2} - v_{o1}}{1 + 2g_m R_P}$$

$$\approx \frac{v_{i1}}{2} - \frac{v_{i2}}{2} - \frac{v_{o1}}{1 + 2g_m R_P} \approx \frac{v_d}{2} - \frac{v_{o1}}{2g_m R_P}$$

$$v_{gs2} \approx -\frac{v_d}{2} - \frac{v_{o1}}{2g_m R_P}$$

$$v_{o2} = -g_m R_D v_{gs2}$$

$$\Rightarrow \frac{v_{o1} R_D}{2R_P} - v_{o2} = -g_m R_D \frac{v_d}{2}$$

$$v_{o2} = -g_m R_D \left[a v_{i2} - b v_{i1} - \frac{v_{o1}}{1+2g_m R_P} \right]$$

classmate

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$$a+b=1 \quad a = \frac{1+g_m R_P}{1+2g_m R_P}$$

$$a-b = \frac{1}{1+2g_m R_P} \cdot b = \frac{g_m R_P}{1+2g_m R_P}$$

$$v_{o2} \left[1 + \frac{g_m R_D}{1+2g_m R_P} \right] = -g_m R_D \left[-b v_{i1} + a v_{i2} \right]$$

$$v_{o1} = -v_{o2}$$

$$\frac{v_{o1} - v_{o2}}{2} = -2v_{o2}$$

$$= + \frac{2g_m R_D}{1 + \frac{g_m R_D}{1+2g_m R_P}} \left[-b v_{i1} + a v_{i2} \right]$$

$$= \alpha \cdot \left[-b \cdot \left(\frac{v_d}{2} + v_{cm} \right) + a \left(-\frac{v_d}{2} + v_{cm} \right) \right]$$

$$= \alpha \left[-\frac{v_d}{2} (b+a) + v_{cm} (a-b) \right]$$

$$= -\frac{\alpha}{2} v_d (a+b) + \alpha (a-b) v_{cm}$$

$$A_{DM} = -\frac{\alpha}{2} (a+b) = -\frac{\alpha}{2} = -\frac{g_m R_D}{1 + \frac{g_m R_D}{1+2g_m R_P}}$$

$$A_{CM-DM} = \alpha (a-b) = \frac{2g_m R_D}{1 + \frac{g_m R_D}{1+2g_m R_P}}$$

$$= \frac{2g_m R_D}{1 + 2g_m R_P + g_m R_D}$$

$$\approx \frac{2R_D}{2R_P + R_D}$$

$$= \frac{R_D/R_P}{1 + R_D/2R_P}$$

$$|CMRR| = \frac{a-b}{a+b} \cdot \frac{1}{2} \left(\frac{a+b}{a-b} \right) = \frac{1}{2(1+2g_m R_P)}$$