

## Why do we require variable DC supply

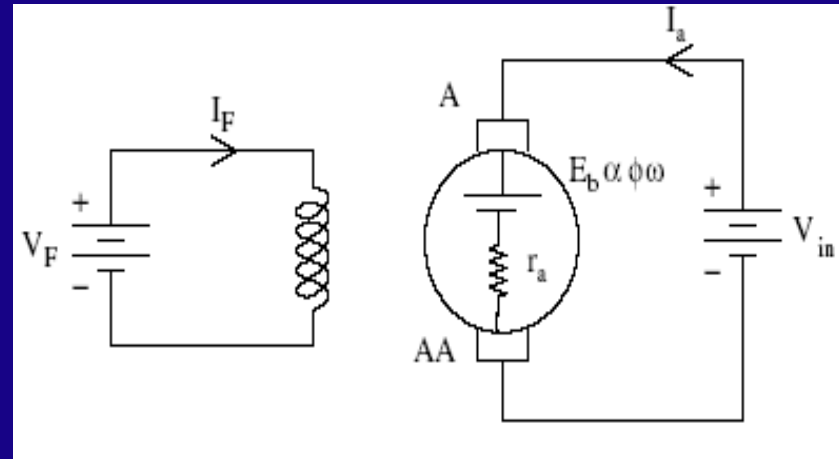
$$V_{in} = E_b + I_a r_a$$

$$E_b = k\phi\omega = kI_F\omega$$

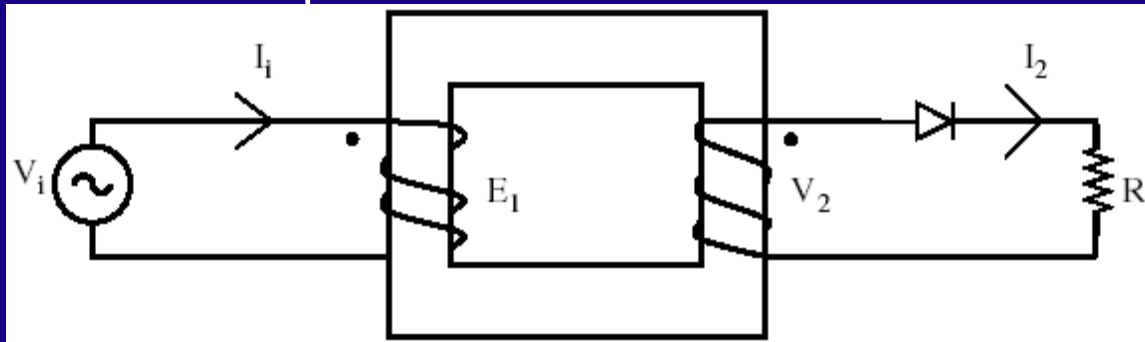
$$\therefore \omega = \frac{V}{kI_F} - \frac{I_a r_a}{kI_F}$$

$$\omega \propto V_{in}$$

$$\propto 1/I_F \quad \text{Both requires variable DC supply}$$



Input ' $V_i$ ' is sinusoidal



$\Rightarrow E_1$  &  $V_2$  are Sinusoidal.

$\Rightarrow i_2$  is non-sinusoidal.

$\Rightarrow$  Core flux can have a DC component in addition to a sinusoidal component.

Pri.  $AT = \text{Sec. } AT$

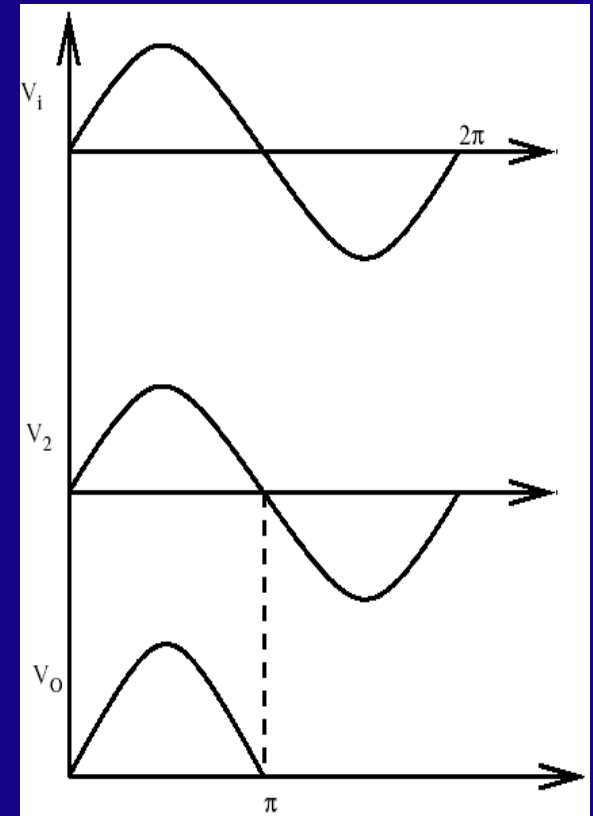
(Neglecting magnetizing Current)

Fourier Spectrum = DC component

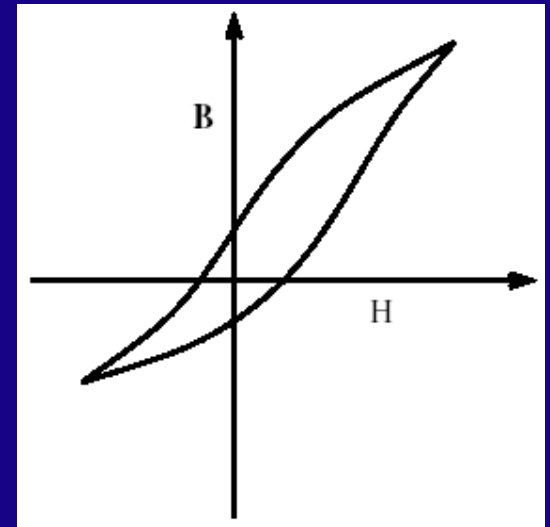
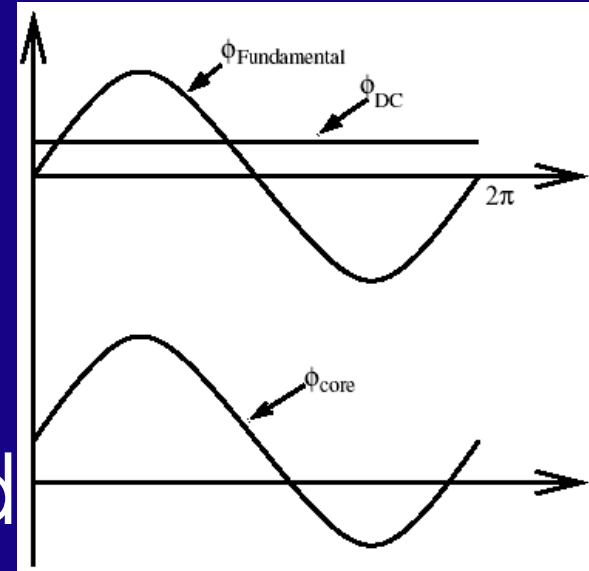
+  $x \sin \omega t$

+ Higher ' $\omega$ ' terms

For high frequency AC component in secondary there should be a high frequency component in primary.



- ⇒ No DC in primary.
- Flux in the core has a DC component.
- ⇒ Core may get saturated during some part of the cycle.
- ⇒  $i$  will be peaky, core loss & harmonics.



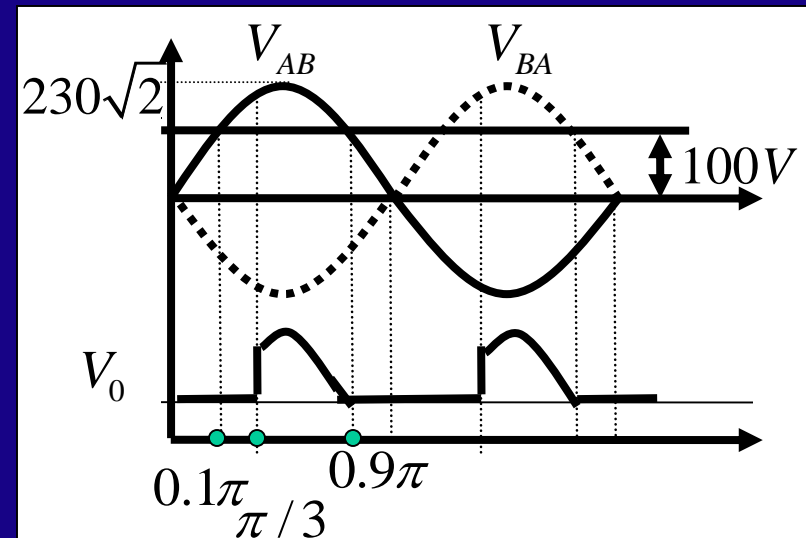
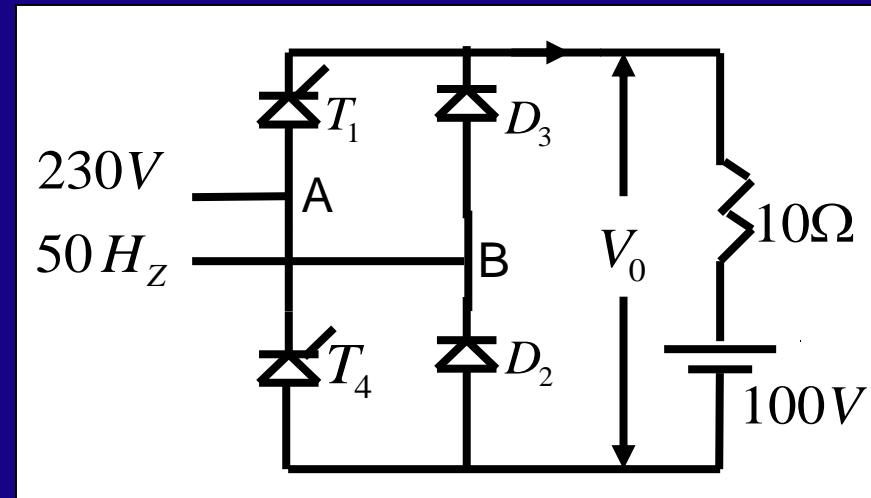
2. For the circuit shown in fig. determine average value of load current for  $\alpha = 60^\circ$

What is the new value of average current flowing through load if a large 'L' is connected in series with the load

Neglect the device drop

a) R-E Load:

$$\alpha_{\min} = \sin^{-1} \left( \frac{100}{230 * \sqrt{2}} \right) = 18^\circ = 0.1\pi^c$$





Minimum value of  $\alpha$  can be  $18^\circ$

But it is triggered at  $60^\circ$

It will turn off  $= \pi - \alpha_{\min} = 162^\circ$

$\Rightarrow 0 \text{ to } 60^\circ :- V_0 = E$

$60^\circ \text{ to } 162^\circ :- V_0 = V_m \sin \omega t$

$162^\circ \text{ to } 360 :- V_0 = E$

$\therefore$  Av. line voltage

$$= \frac{1}{\pi} \left[ \int_0^{\pi/3} E d\omega t + \int_{\pi/3}^{0.9\pi} V_m \sin \omega t d\omega t + \int_{0.9\pi}^{\pi} E d\omega t \right]$$

$$= 193.45 \text{ V}$$

$$\therefore \text{Av. value of load current } I_{av} = \frac{193.45 - 100}{10} = 9.345 \text{ A}$$

- b With large inductance in series with the load current becomes continuous.

$$\alpha = 60^\circ$$

$$\begin{aligned} \text{Av. value of o/p Voltage} &= \frac{230\sqrt{2}}{\pi} (1 + \cos \alpha) \\ &= 155 \text{ V} \end{aligned}$$

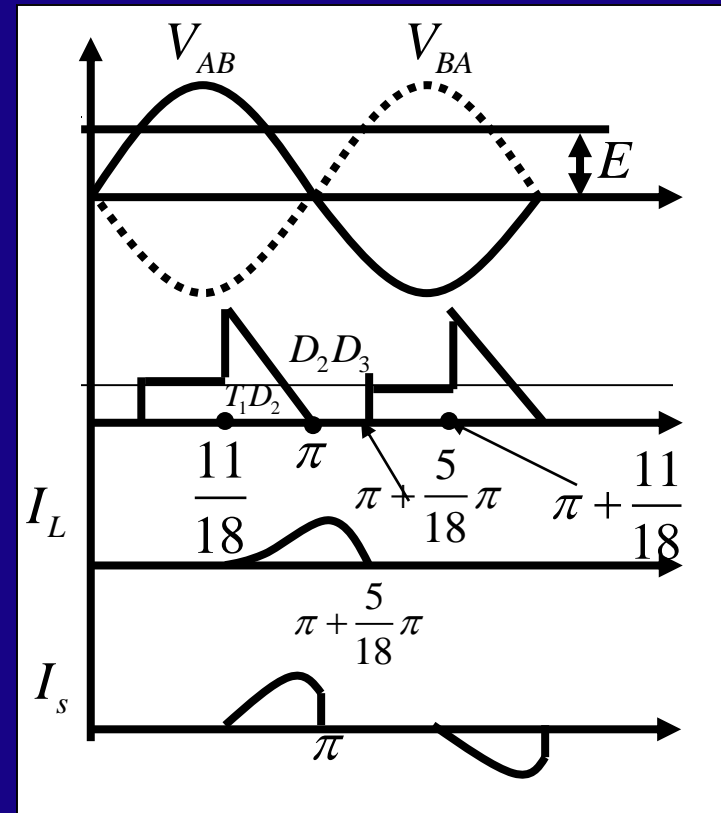
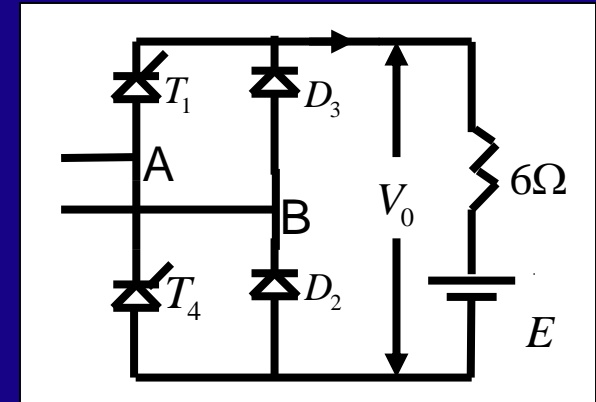
$$\text{Av. value of } I = \frac{155 - 100}{10} = 5.5 \text{ A}$$

3. Av. value of  $I_L = 1.8A$

Triggering angle is maintained at  $110^\circ$   
current becomes zero at  $50^\circ$  beyond the  
zero crossing.

Sketch the load current and  
applied average voltage  
waveform.

$$\alpha_{\min} = \sin^{-1} \left[ \frac{E}{V_m} \right]$$





From  $\frac{11}{18}$  to  $\pi$  radian  $T_1$  &  $D_2$  conduct

$$V_0 = V_i$$

From  $\pi$  to  $\left(\pi + \frac{5}{18}\pi\right)$

$V_0 = 0 \because D_2$  &  $D_3$  conducting

$$V_{av} = \frac{1}{\pi} \left[ \int_{\frac{11\pi}{18}}^{\pi} V_m \sin \omega t d\omega t + \int_{\pi}^{\pi + \frac{5\pi}{18}} 0 d\omega t + \int_{\pi + \frac{5\pi}{18}}^{\pi + \frac{11\pi}{18}} E d\omega t \right]$$
$$= \frac{1}{\pi} \left[ 230\sqrt{2} \left( \cos \frac{11\pi}{18} + 1 \right) + \frac{\pi}{3} E \right]$$

$$\therefore V_{av} = 68.12 + \frac{E}{3}$$

$$\therefore I_{av} = \frac{V_{av} - E}{R}, \quad I_{av} = 1.8A, R = 6\Omega$$

$$\therefore E = 85.9V$$