## Generation of Finite Difference Formulas on Arbitrarily Spaced Grids

## By Bengt Fornberg

Abstract. Simple recursions are derived for calculating the weights in compact finite difference formulas for any order of derivative and to any order of accuracy on one-dimensional grids with arbitrary spacing. Tables are included for some special cases (of equispaced grids).

1. Introduction. Previously published methods to generate finite difference weights (e.g., references [1]-[5]) have been of considerable complexity and often been limited to derivatives of low order on equidistantly spaced grids. The most ambitious attempt to tabulate weights for many orders of derivatives and to high orders of accuracy appears to be the work by Keller and Pereyra [4]. However, their algorithms (limited to equispaced grids) were very involved, and the resulting tables contain both isolated and systematic errors.

In the present study we describe two simple recursion relations which give the weights for any order of derivative (including the 0th derivative, corresponding to interpolation), approximated to any order of accuracy on an arbitrary grid in one dimension. Since, in general, only four arithmetic operations are needed to determine each weight, the main anticipated application of the present method is to dynamically changing grids. However, the method is also well suited to generate tables of weights. Such tables (in the special case of equispaced grids, up to the 4th derivative and up to 9 weights) are included in the cases of one-sided and centered approximations at a grid point and at a 'half-way point' between grid points.

**2. Notation, Algorithm.** Given  $M \ge 0$ , the order of the highest derivative we wish to approximate, and a set of N+1 grid points (at x-coordinates  $\alpha_0, \ldots, \alpha_N$ ;  $N \ge 0$ ), the problem is to find all the weights such that the approximations

$$\left. \frac{d^m f}{dx^m} \right|_{x=x_0} pprox \sum_{
u=0}^n \delta^m_{n,
u} f(lpha_
u), \qquad m=0,1,\ldots,M; \ n=m,m+1,\ldots,N,$$

become of optimal formal order of accuracy (in general of order n-m+1, although it can be higher in special cases). The following algorithm achieves this:

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Enter 
$$M, N, x_0, \alpha_0, \alpha_1, \alpha_2, \dots, \alpha_N$$

$$\delta_{0,0}^0 := 1$$

$$c1 := 1$$
for  $n := 1$  to  $N$  do
$$c2 := 1$$
for  $\nu := 0$  to  $n-1$  do
$$c3 := \alpha_n - \alpha_{\nu}$$

$$c2 := c2 \cdot c3$$
if  $n \le M$  then  $\delta_{n-1,\nu}^n := 0$ 
for  $m := 0$  to  $\min(n, M)$  do
$$\delta_{n,\nu}^m := ((\alpha_n - x_0)\delta_{n-1,\nu}^m - m\delta_{n-1,\nu}^{m-1})/c3$$
next  $m$ 
next  $\nu$ 
for  $m := 0$  to  $\min(n, M)$  do
$$\delta_{n,n}^m := \frac{c1}{c2}(m\delta_{n-1,n-1}^{m-1} - (\alpha_{n-1} - x_0)\delta_{n-1,n-1}^m)$$
next  $m$ 

$$c1 := c2$$
next  $n$ 

Notes. 1. If the array  $\delta_{n,\nu}^m$  initially is zero, the statement "if  $n \leq M$  then  $\delta_{n-1,\nu}^n := 0$ " can be omitted.

- 2. In the case of m = 0 (corresponding to interpolation formulas), expressions of the form 'zero\*(undefined number)' occur. The result is assumed to be zero.
- 3. The order in which the  $\alpha_{\nu}$  (all distinct) are given is significant (since the weights corresponding to all leading subsets of the  $\alpha_{\nu}$ 's are calculated). There is no restriction on  $x_0$  coinciding with any  $\alpha_{\nu}$ .
- **3. Derivation of the Algorithm.** For simplicity, assume we seek to approximate the derivatives at the point  $x_0 = 0$ . Let  $\{\alpha_0, \alpha_1, \dots, \alpha_N\}$  be distinct real numbers and denote

(3.1) 
$$\omega_n(x) := \prod_{k=0}^n (x - \alpha_k).$$

The polynomial

(3.2) 
$$F_{n,\nu}(x) := \frac{\omega_n(x)}{\omega'_n(\alpha_\nu)(x - \alpha_\nu)}$$

is the one of minimal degree which takes the value 1 at  $x = \alpha_{\nu}$  and 0 at  $x = \alpha_{k}$ ,  $0 \le k \le n$ ,  $k \ne \nu$ . For an arbitrary function f(x) and nodes  $x = \alpha_{\nu}$ , Lagrange's interpolation polynomial becomes

(3.3) 
$$p(x) := \sum_{\nu=0}^{n} F_{n,\nu}(x) f(\alpha_{\nu}).$$

The desired weights express how the values of  $[d^m p(x)/dx^m]_{x=0}$  vary with changes in  $f(\alpha_{\nu})$ . Since only one term in p(x) is influenced by changes in each  $f(\alpha_{\nu})$ , we find

(3.4) 
$$\delta_{n,\nu}^m = \left[ \frac{d^m}{dx^m} F_{n,\nu}(x) \right]_{x=0}.$$

Therefore, the nth degree polynomial  $F_{n,\nu}(x)$  can also be expressed as

(3.5) 
$$F_{n,\nu}(x) = \sum_{m=0}^{n} \frac{\delta_{n,\nu}^{m}}{m!} x^{m}.$$

From (3.2) follow (noting that  $\omega(x) = (x - \alpha_n)\omega_{n-1}(x)$  implies  $\omega'_n(x) = (x - \alpha_n)\omega'_{n-1}(x) + \omega_{n-1}(x)$ )

(3.6) 
$$F_{n,\nu}(x) = \frac{x - \alpha_n}{\alpha_{\nu} - \alpha_n} F_{n-1,\nu}(x)$$

and

$$(3.7) F_{n,n}(x) = \frac{\omega_{n-1}(x)}{\omega_{n-1}(\alpha_n)} = \frac{\omega_{n-2}(\alpha_{n-1})}{\omega_{n-1}(\alpha_n)} (x - \alpha_{n-1}) F_{n-1,n-1}(x) (n > 1).$$

By substituting the expansion (3.5) into (3.6) and (3.7), and by equating powers of x, the desired recursion relations between the weights are obtained:

(3.8) 
$$\delta_{n,\nu}^{m} = \frac{1}{\alpha_{n} - \alpha_{\nu}} (\alpha_{n} \delta_{n-1,\nu}^{m} - m \delta_{n-1,\nu}^{m-1})$$

and

(3.9) 
$$\delta_{n,n}^{m} = \frac{\omega_{n-2}(\alpha_{n-1})}{\omega_{n-1}(\alpha_{n})} (m\delta_{n-1,n-1}^{m-1} - \alpha_{n-1}\delta_{n-1,n-1}^{m}).$$

The relation

(3.10) 
$$\sum_{\nu=0}^{n} \delta_{n,\nu}^{m} = \begin{cases} 1, & m=0, \\ 0, & m>0, \end{cases}$$

could be used instead of (3.9) to obtain  $\delta_{n,n}^m$ . However, this would increase the operation count and might also cause a growth of errors in the case of floating-point arithmetic.

**4. Description of the Tables.** Special cases which commonly occur are centered and one-sided approximations on equidistant grids. The particular choices of  $\alpha_{\nu}$  used for Tables 1-4 correspond to grid spacings  $\Delta x = 1$ . For other values of  $\Delta x$ , these coefficients should be divided by  $(\Delta x)^m$  (where m, as before, is the order of the derivative).

TABLE 1

Some weights for centered approximations at a grid point (generated by setting  $M=4,~N=8,~x_0=0$  and  $\alpha_{\nu}=\{0,1,-1,2,-2,3,-3,4,-4\}$ ).

der ivative	Order of	Approximations at $x = 0$ ; x-coordinates at nodes:								
o v f e	o ā f y	-4	-3	-2	-1	0	1	2	3	4
0	8					1				
	2				$\frac{-1}{2}$	0	$\frac{1}{2}$			
	4			$\frac{1}{12}$	$\frac{-2}{3}$	0	$\frac{2}{3}$	$\frac{-1}{12}$		
1	6		$\frac{-1}{60}$	$\frac{3}{20}$	$     \begin{array}{r}       -1 \\       -2 \\       \hline       3 \\       -3 \\       \hline       4 \\       \hline       -4 \\       \hline       5 \\    \end{array} $	0	$\frac{3}{4}$	$\frac{-1}{12}$ $\frac{-3}{20}$	$\frac{1}{60}$	
	8	$\frac{1}{280}$	$\frac{-4}{105}$	$\frac{1}{5}$	$\frac{-4}{5}$	0	$\frac{4}{5}$	$\frac{-1}{5}$	$\frac{4}{105}$	$\frac{-1}{280}$
	2				1	-2	1			
	4			$\frac{-1}{12}$	$\frac{4}{3}$	$\frac{-5}{2}$	$\frac{4}{3}$	$\frac{-1}{12}$		
2	6		$\frac{1}{90}$	$\frac{-1}{12}$ $\frac{-3}{20}$	4/3 3/2 8/5	$\frac{-49}{18}$	$\frac{4}{3}$ $\frac{3}{2}$	$\frac{-1}{12}$ $\frac{-3}{20}$	$\frac{1}{90}$	
	8	$\frac{-1}{560}$	$\frac{8}{315}$	$\frac{-1}{5}$	<u>8</u> 5	$\frac{-205}{72}$	<u>8</u> 5	$\frac{-1}{5}$	$\frac{8}{315}$	$\frac{-1}{560}$
	2			$\frac{-1}{2}$	1	0	-1	$\frac{1}{2}$		
3	4		<u>1</u> 8	-1	13 8	0	$\frac{-13}{8}$	1	$\frac{-1}{8}$	
	6	$\frac{-7}{240}$	$\frac{\frac{1}{8}}{\frac{3}{10}}$	$\frac{-169}{120}$	$\frac{61}{30}$	0	$\frac{-61}{30}$	$\tfrac{169}{120}$	$\frac{-3}{10}$	$\frac{7}{240}$
	2			1	-4	6	-4	1		
4	4		$\frac{-1}{6}$	2	$\frac{-13}{2}$	$\frac{28}{3}$	$\frac{-4}{\frac{-13}{2}}$	2	$\frac{-1}{6}$	
	6	$\frac{7}{240}$	$\frac{-1}{6}$ $\frac{-2}{5}$	169 60	$\frac{-122}{15}$	<u>91</u> 8	$\frac{-122}{15}$	169 60	$\frac{-2}{5}$	$\frac{7}{240}$

TABLE 2 Some weights for centered approximations at a 'half-way' point (generated by setting  $M=4,~N=7,~x_0=0$  and  $\alpha_{\nu}=\{1/2,-1/2,3/2,-3/2,5/2,-5/2,7/2,-7/2\}$ ).

der i va r t i ve r t f e	Order of	Approximations at $x = 0$ ; x-coordinates at nodes: -7/2 $-5/2$ $-3/2$ $-1/2$ $1/2$ $3/2$ $5/2$ $7/2$								
	2	- ,,-			1/2	$\frac{1}{2}$				
	4			$\frac{-1}{16}$	2 9 16	2 9 16	<u>-1</u>			
	_		2				$\frac{-1}{16}$	2		
0	6		$\frac{3}{256}$	$\frac{-25}{256}$	$\tfrac{75}{128}$	$\frac{75}{128}$	$\frac{-25}{256}$	$\frac{3}{256}$		
	8	$\frac{-5}{2048}$	$\frac{49}{2048}$	$\frac{-245}{2048}$	$\frac{1225}{2048}$	$\frac{1225}{2048}$	$\frac{-245}{2048}$	$\frac{49}{2048}$	$\frac{-5}{2048}$	
	2				-1	1				
	4			$\frac{1}{24}$	$\frac{-9}{8}$	<u>9</u>	$\frac{-1}{24}$			
1	6		$\frac{-3}{640}$	$\frac{25}{384}$	$\frac{-75}{64}$	75 64	$\frac{-25}{384}$	$\frac{3}{640}$		
	8	$\frac{5}{7168}$	$\frac{-49}{5120}$	$\frac{245}{3072}$	$\frac{-1225}{1024}$	$\frac{1225}{1024}$	$\frac{-245}{3072}$	$\frac{49}{5120}$	$\frac{-5}{7168}$	
		7106	3120					3120	7108	
	2			$\frac{1}{2}$	$\frac{-1}{2}$	$\frac{-1}{2}$	$\frac{1}{2}$			
2	4		$\frac{-5}{48}$	$\frac{13}{16}$	$\frac{-17}{24}$	$\frac{-17}{24}$	13 16	$\frac{-5}{48}$		
	6	$\frac{259}{11520}$	$\frac{-499}{2304}$	$\frac{1299}{1280}$	$\frac{-1891}{2304}$	$\frac{-1891}{2304}$	$\frac{1299}{1280}$	$\frac{-499}{2304}$	$\frac{259}{11520}$	
	2			-1	3	-3	1			
3	4		<u>1</u> 8	$\frac{-13}{8}$	$\frac{17}{4}$	$\frac{-17}{4}$	13 8	$\frac{-1}{8}$		
	6	$\frac{-37}{1920}$	$\frac{499}{1920}$	$\frac{-1299}{640}$	1891 384	$\frac{-1891}{384}$	1299 640	$\frac{-499}{1920}$	$\frac{37}{1920}$	
	2		$\frac{1}{2}$	$\frac{-3}{2}$	1	1	$\frac{-3}{2}$	$\frac{1}{2}$		
4	4	$\frac{-7}{48}$	<u>59</u> 48	$\frac{-45}{16}$	<u>83</u> 48	<u>83</u> 48	$\frac{-45}{16}$	59 48	$\frac{-7}{48}$	

TABLE 3 Some weights for one-sided approximations at a grid point (generated by setting  $M=4,\ N=8,\ x_0=0$  and  $\alpha_{\nu}=\{0,1,2,3,4,5,6,7,8\}$ ).

de or i de a r t i o f e	Order acy			mations a						
o i f e	o c f y	0	1	2	3	4	5	6	7	8
0	∞	1								
	1	-1	1							
	2	$\frac{-3}{2}$	2	$\frac{-1}{2}$						
	3	$\frac{-11}{6}$	3	$\frac{-3}{2}$	$\frac{1}{3}$					
	4	$\frac{-25}{12}$	4	-3	$\frac{4}{3}$	$\frac{-1}{4}$				
1	5	$\frac{-137}{60}$	5	-5	$\frac{10}{3}$	$\frac{-5}{4}$	$\frac{1}{5}$			
	6	$\frac{-49}{20}$	6	$\frac{-15}{2}$	$\frac{20}{3}$	$\frac{-15}{4}$	<u>6</u> 5	$\frac{-1}{6}$		
	7	$\frac{-363}{140}$	7	$\frac{-21}{2}$	$\frac{35}{3}$	$\frac{-35}{4}$	$\frac{21}{5}$	$\frac{-7}{6}$	$\frac{1}{7}$	
	8	$\frac{-761}{280}$	8	-14	<u>56</u> 3	$\frac{-35}{2}$	<u>56</u> 5	$\frac{-14}{3}$	<u>8</u> 7	$\frac{-1}{8}$
	1	1	-2	1						
	2	2	<b>-5</b>	4	-1					
	3	$\frac{35}{12}$	$\frac{-26}{3}$	$\frac{19}{2}$	$\frac{-14}{3}$	$\frac{11}{12}$				
2	4	$\frac{15}{4}$	$\frac{-77}{6}$	$\frac{107}{6}$	-13	$\frac{61}{12}$	$\frac{-5}{6}$			
	5	$\frac{203}{45}$	$\frac{-87}{5}$	$\frac{117}{4}$	$\frac{-254}{9}$	$\frac{33}{2}$	$\frac{-27}{5}$	$\frac{137}{180}$		
	6	<u>469</u> 90	$\frac{-223}{10}$	$\frac{879}{20}$	$\frac{-949}{18}$	41	$\frac{-201}{10}$	$\frac{1019}{180}$	$\frac{-7}{10}$	
	7	$\frac{29531}{5040}$	$\frac{-962}{35}$	$\frac{621}{10}$	$\frac{-4006}{45}$	<u>691</u> 8	$\frac{-282}{5}$	$\frac{2143}{90}$	$\frac{-206}{35}$	363 560
	1	-1	3	-3	1					
:	2	$\frac{-5}{2}$	9	-12	7	$\frac{-3}{2}$				
	3	$\frac{-17}{4}$	$\frac{71}{4}$	$\frac{-59}{2}$	$\frac{49}{2}$	$\frac{-41}{4}$	$\frac{7}{4}$			
3	4	$\frac{-49}{8}$	29	$\frac{-461}{8}$	62	$\frac{-307}{8}$	13	$\frac{-15}{8}$		
	5	$\frac{-967}{120}$	$\frac{638}{15}$	$\frac{-3929}{40}$	$\frac{389}{3}$	$\frac{-2545}{24}$	$\frac{268}{5}$	$\frac{-1849}{120}$	$\frac{29}{15}$	
	6	$\frac{-801}{80}$	349 6	$\frac{-18353}{120}$	$\frac{2391}{10}$	$\frac{-1457}{6}$	$\frac{4891}{30}$	$\frac{-561}{8}$	$\frac{527}{30}$	$\frac{-469}{240}$
	1	1	-4	6	-4	1				
	2	3	-14	26	-24	11	- <b>2</b>			
4	3	35 6			$\frac{-242}{3}$		-19	$\frac{17}{6}$		
	4	$\frac{28}{3}$	$\frac{-111}{2}$		$\frac{-1219}{6}$			$\frac{82}{3}$		
	5	1069 80	<u>-1316</u> 15	15289 60	$\frac{-2144}{5}$	10993	$\frac{-4772}{15}$	2803 20	$\frac{-536}{15}$	967 240

TABLE 4 Some weights for one-sided approximations at a 'half-way' point (generated by setting M=4, N=8,  $x_0$ =0 and  $\alpha_{\nu}$ ={-1/2, 1/2, 3/2, 5/2, 7/2, 9/2, 11/2, 13/2, 15/2}).

der i va er tive f	Orac cur	Approximations at $x = 0$ ; x-coordinates at nodes:								
o i f e	r u o a f y	-1/2	<i>x</i> -coord	inates at 3/2	nodes: 5/2	7/2	9/2	11/2	13/2	15/2
<u> </u>	1	1		- O/ <b>-</b>				11/2	10/2	10/2
	2	$\frac{1}{2}$	$\frac{1}{2}$							
	3	<u>3</u>	$\frac{3}{4}$	$\frac{-1}{8}$						
	4	$\frac{5}{16}$	$\frac{15}{16}$	$\frac{-5}{16}$	$\frac{1}{16}$					
0	5	$\frac{35}{128}$	$\frac{35}{32}$	$\frac{-35}{64}$	$\frac{7}{32}$	$\frac{-5}{128}$				
	6	63 256	$\frac{315}{256}$	$\frac{-105}{128}$	$\frac{63}{128}$	$\frac{-45}{256}$	$\frac{7}{256}$			
	7	$\frac{231}{1024}$	$\frac{693}{512}$	$\frac{-1155}{1024}$	$\frac{231}{256}$	$\frac{-495}{1024}$	$\frac{77}{512}$	$\tfrac{-21}{1024}$		
	8	$\frac{429}{2048}$	$\frac{3003}{2048}$	$\frac{-3003}{2048}$	$\frac{3003}{2048}$	$\frac{-2145}{2048}$	$\frac{1001}{2048}$	$\frac{-273}{2048}$	$\frac{33}{2048}$	
	9	$\frac{6435}{32768}$	6435 4096	$\frac{-15015}{8192}$	9009 4096	$\frac{-32175}{16384}$	5005 4096	$\frac{-4095}{8192}$	$\frac{495}{4096}$	$\frac{-429}{32768}$
	2	-1	1							
	3	$\frac{-23}{24}$	$\frac{7}{8}$	$\frac{1}{8}$	$\frac{-1}{24}$					
	4	$\frac{-11}{12}$	$\frac{17}{24}$	3 8	$\frac{-5}{24}$	$\frac{1}{24}$				
1	5	$\frac{-563}{640}$	$\frac{67}{128}$	143 192	$\frac{-37}{64}$	$\frac{29}{128}$	$\frac{-71}{1920}$			
	6	$\frac{-1627}{1920}$	$\frac{211}{640}$	59 48	$\frac{-235}{192}$	$\frac{91}{128}$	$\frac{-443}{1920}$	31 960		
	7	$\frac{-88069}{107520}$	2021 15360	28009 15360	$\frac{-6803}{3072}$	5227 3072	$\frac{-12673}{15360}$	3539 15360	$\frac{-3043}{107520}$	
	8	$\frac{-1423}{1792}$	$\frac{-491}{7168}$	7753 3072	$\frac{-18509}{5120}$	3535 1024	$\frac{-2279}{1024}$	953 1024	$\frac{-1637}{7168}$	2689 107520
	1	1 3	$-2 \\ -7$	1 5	<u>-1</u>					
	2	$\frac{3}{2}$	$\frac{-7}{2}$ -14	$\frac{5}{2}$	$\frac{-\frac{1}{2}}{-5}$	_7				
2	3	24 95	3 -269	49	-85	24 59	_3			
	4	48 12139	48 -6119	3091	-1759	$\frac{33}{48}$ $1211$	$\frac{16}{16}$ -919	739		
	5	5760 25333	960 -80813	384 2553	$\frac{288}{-21457}$	384 14651	960 -3687	5760 8863	-211	
	6	$\overline{11520}$ 81227	11520 -67681	256 34151	2304 -16747	2304 5669	1280 -76621	11520 1699	2304 -5647	21719
-		35840	8960	2880	1280	512	11520	640	8960	322560
	1 2	-1 -2	3 7	-3 -9	1 5	-1				
	3	$\frac{-23}{8}$	$\frac{91}{8}$	$\frac{-71}{4}$	55 4	$\frac{-43}{8}$	$\frac{7}{8}$			
3	4	$\frac{-29}{8}$	127 8	-29	115 4		43 8	$\frac{-3}{4}$		
	5	$\frac{-8197}{1920}$		$\frac{-27219}{640}$		$\frac{-15043}{384}$		$\frac{-10099}{1920}$	$\frac{1237}{1920}$	
	6	$\frac{-2317}{480}$	$\frac{47707}{1920}$	$\frac{-7443}{128}$	$\tfrac{158471}{1920}$			$\frac{-40087}{1920}$	1961 384	$\frac{-357}{640}$
	1	1	-4	6	-4	1				
	2	$\frac{5}{2}$	$\frac{-23}{2}$	21	-19	$\frac{17}{2}$	$\frac{-3}{2}$			
4	3	$\frac{101}{24}$	$\frac{-87}{4}$	$\frac{373}{8}$	$\frac{-319}{6}$	$\frac{273}{8}$	$\frac{-47}{4}$	$\frac{41}{24}$		
	4	$\frac{287}{48}$	$\frac{-1639}{48}$	$\frac{1341}{16}$	$\frac{-5527}{48}$	$\frac{4613}{48}$	$\frac{-783}{16}$	$\frac{677}{48}$	$\frac{-85}{48}$	
	5	14861 1920	$\frac{-1447}{30}$	21299 160	$\frac{-25651}{120}$	42119 192	$\frac{-2951}{20}$	30437 480	$\frac{-1903}{120}$	1127 640

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