

Q-1

End Sem Solution CL 611

1>

Diffusion: - Due to Concⁿ gradient of ions in solution

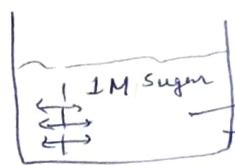
$$j_i = -D \frac{\partial c_i}{\partial x}$$

Migration: due to electrostatic potential gradient in electrolyte

$$\text{molar flux due to migration} = -z_i u_i F \nabla \phi$$

2> Self Diffusion Coeff

when there is no net diffusion of molecules (Uniform solⁿ).



Uniform solⁿ
No net diffusion

But there is ~~some~~ random movement of molecules, resulting in self diffusion coefficient.

Chemical diffusion coeff

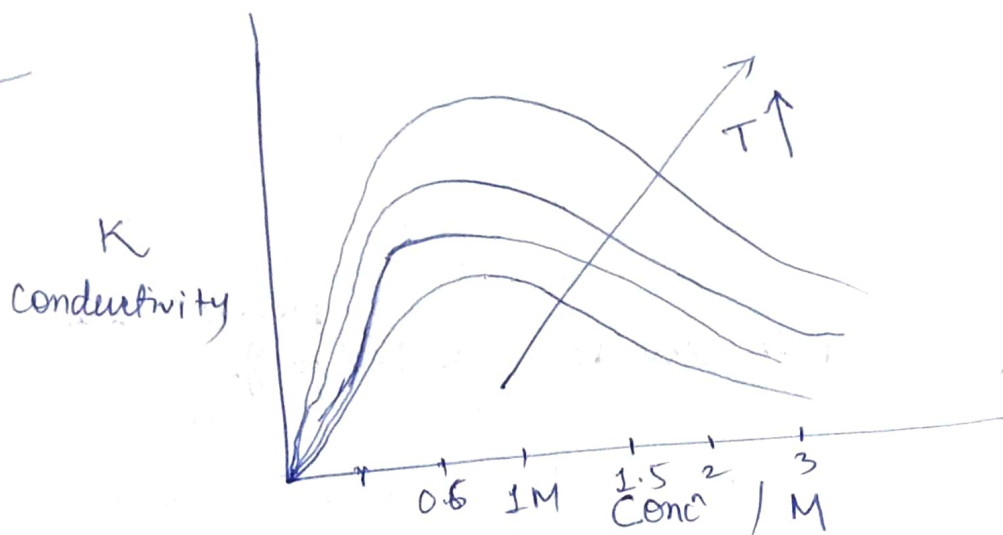
Due to net diffusion of molecules in solution (due to Concⁿ gradient)

$$D_{\text{chemical}} = D_{\text{self}} \left(1 + \underbrace{\frac{d \ln f_+}{d \ln c_+}} \right)$$

Thermodynamic

Fick's Law uses chemical diffusion factor coefficient.

3



4

KCl is commonly used because transference no. t_+ is nearly 0.5 [$t_+ = 0.49$, $t_- = 0.51$] hence the junction potential is zero (or near 0)

5

$t_+ \rightarrow$ fraction of current carried by ⁺ve ion, when there is no concⁿ gradient.

$t_+ = 1 \rightarrow$ Nafion Membrane

Solid state Electrolyte with fixed or immobile ⁻ve ions.

$t_+ = 0$

Anion exchange membrane
(⁺ve ions are immobile)

6

Thermodynamic factor,

$$= 1 + \frac{d \ln f_{\pm}}{d \ln C}$$

$f \rightarrow$ fugacity of ion in solution

$C \rightarrow$ concⁿ of ion

⑦ We prefer PEIS because, we want a fixed voltage of battery while doing EIS. If we do GIEIS, effectively we are charging or discharging the cell & potential ~~will~~ drift due to ocv (f.soc). Perturbation is kept small because to maintain linearity of the system. ($I \propto V$). It ensures accurate and reliable impedance measurement.

⑧ Cottrell Eqn,

describes time dependent current response of a system under diffusion controlled condition after a potential step is applied at a planar electrode.

$$i(t) = \frac{nFA C \sqrt{D}}{\sqrt{\pi t}}$$

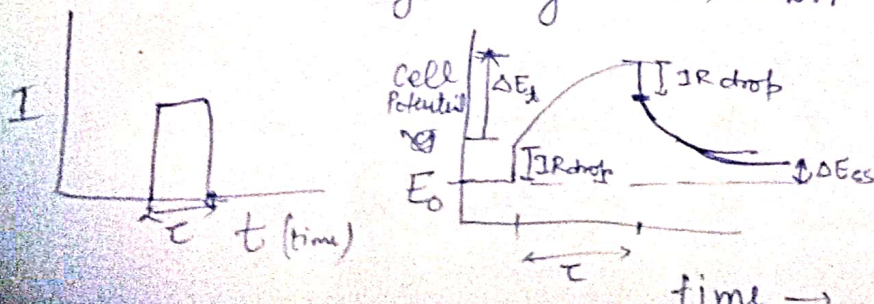
bulk concⁿ of electroactive species ($\frac{\text{mol}}{\text{cm}^3}$)
Diff. Coeff (cm^2/s)

$A \rightarrow$ Electrode Area (cm^2),

$$i(t) \propto \frac{1}{\sqrt{t}}$$

⑩ GITT Protocol →

Small current pulse applied for a short duration, followed by long relaxation period



$$D = \left(\frac{\Delta E_t}{\Delta E_{ss}} \right)^2$$

Diffusion Coeff

Q(2) Pourbaix Diagram (E vs pH)

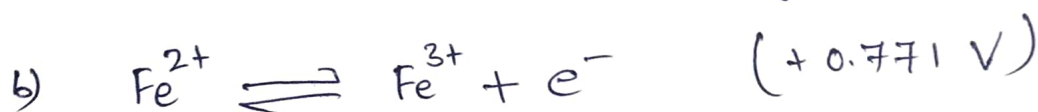


$$E = E^0 + \frac{RT}{nF} \ln \left(\frac{[\text{Fe}^{2+}]}{a_{\text{Fe}}} \right)$$

$$= -0.44 - \frac{0.0591}{n} \log \left(\frac{1}{[\text{Fe}^{2+}]} \right)$$

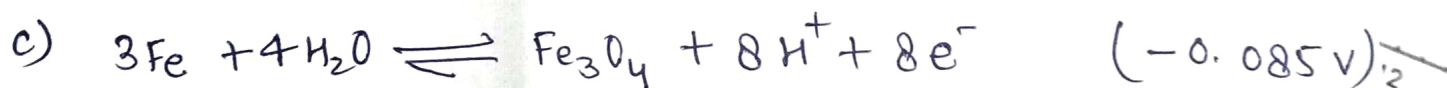
$$\therefore [\text{Fe}^{2+}] = 1 \text{ M}, \log 1 = 0$$

$$\therefore E = -0.44 \text{ V} \quad \left\{ \text{Horizontal line} \right\}$$



$$E = 0.771 + \frac{0.0591}{1} \log \left(\frac{[\text{Fe}^{3+}]}{[\text{Fe}^{2+}]} \right)$$

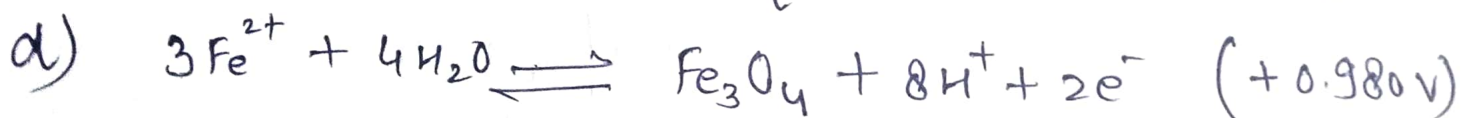
$$E = 0.771 \text{ V} \quad \left\{ \text{Horizontal line} \right\}$$



$$E = -0.085 - \frac{0.0591}{8} \log \left(\frac{1}{[\text{H}^+]^8} \right)$$

$$E = -0.085 - 0.0591 \text{ pH}$$

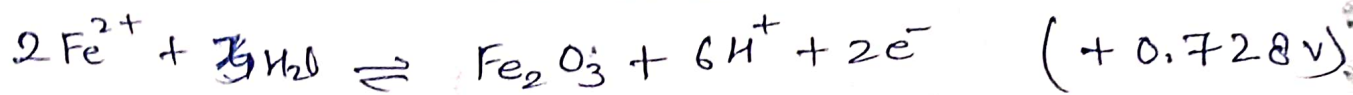
$$\text{sloped line} \quad \left\{ \text{slope} = -0.0591 \right\}$$



$$E = 0.980 - \frac{0.0591}{2} \log \left(\frac{1}{[\text{H}^+]^8} \right)$$

$$= 0.980 - 0.2364 \text{ pH}$$

Sloped line Intercept slope

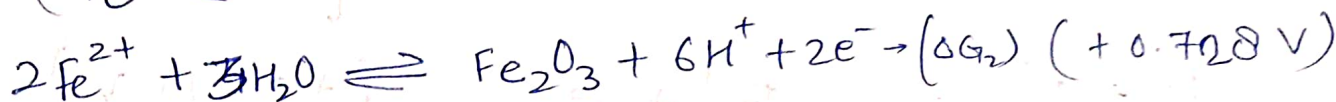
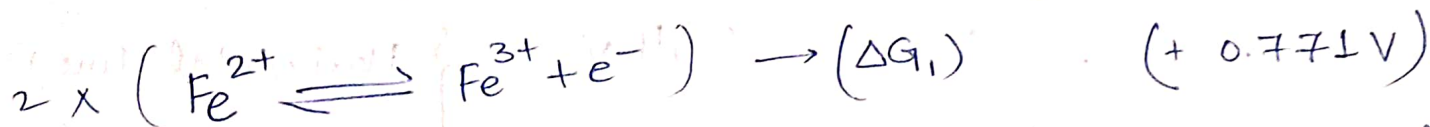


$$E = 0.728 - \frac{0.0591}{2} \log \left(\frac{1}{[\text{H}^+]^6} \right)$$

$$E = \underbrace{0.728}_{\text{Intercept}} - \underbrace{0.1773}_{\text{slope}} \text{pH}$$



We will find the potentials using eq (b) & eq (e)



$$\Delta G = \Delta G_2 - 2\Delta G_1$$

$$-2F U^\theta = -\{0.728 - 2 \times 0.771\}$$

$$-2F U^\theta = -2F \cdot (0.728) - 2\{-1 \cdot F(0.771)\}$$

$$U^\theta = +0.043 \text{ V}$$

Stability Product $\leftarrow K_{sp} = \frac{[\text{Fe}_2\text{O}_3][\text{H}^+]^6}{[\text{H}_2\text{O}]^3 [\text{Fe}^{3+}]^2} = [\text{H}^+]^6$

Since $K_{sp} = e^{\frac{nF U^\theta}{RT}}$

$$K_{sp} = e^{\frac{2 \times 96485 \times (+0.043)}{8.314 \times 298}}$$

$$= \frac{0.0001}{0.0001}$$

$$K_{sp} = \frac{2.8 \times 10^{-47}}{1.7475^6} = [H^+]^6$$

$$[H^+] = \frac{2.8 \times 10^{-47}}{1.7475^6}$$

$$pH = -\log[H^+] = 0.242$$

so, we will get a vertical line at $pH = -0.242$

g) $Fe_3O_4 + 3H_2O \rightleftharpoons 3Fe_2O_3 + 2H^+ + 2e^-$ (+0.221 V)

$$E = +0.221 - \frac{0.0591}{2} \log\left(\frac{1}{[H^+]^2}\right)$$

$$E = 0.221 - 0.0591 pH$$

h) $3HFeO_2 \rightleftharpoons Fe_3O_4 + H_2O + OH^- + 2e^-$ (-1.819 V)

$$E = -1.819 - \frac{0.0591}{2} \log[OH^-]$$

$$= -1.819 - 0.02955 pOH$$

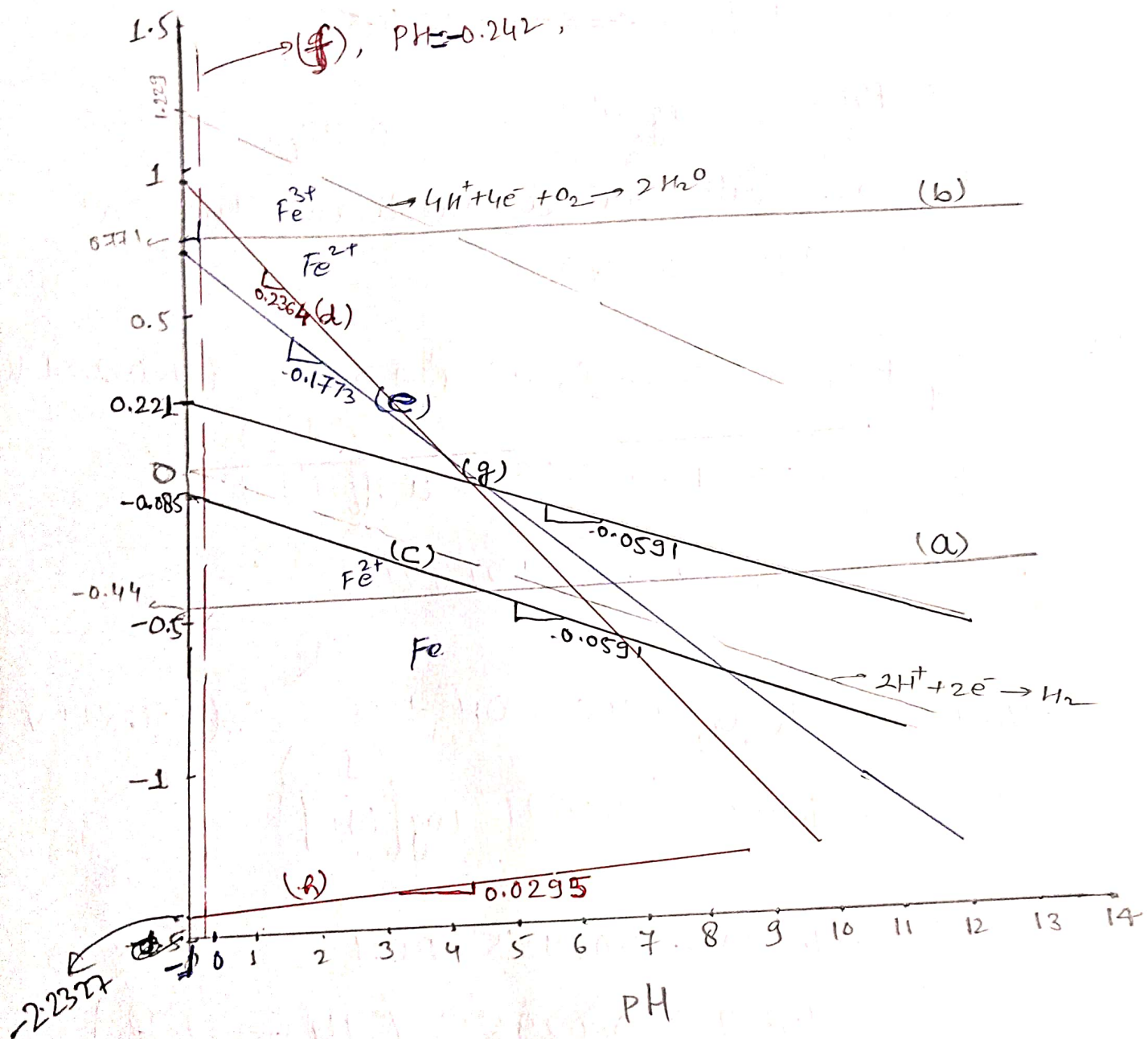
$$= -1.819 - 0.02955 (14 - pH)$$

$$= -2.2327 + 0.0295 pH$$

$$2.8 \times 10^{-47} = [H^+]^6$$

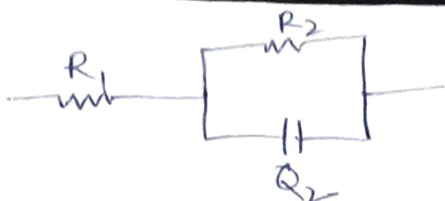
$$[H^+] = (2.8 \times 10^{-47})^{1/6}$$

$$-\log(1.74)$$



Refer to ppt uploaded for detailed analysis of pourbaix diagram.

③



① Impedance Response

$$Z = R_1 + Z_{\text{parallel}}$$

$$Z_1 = R_1$$

$Z_{\text{parallel}} =$ parallel sum of R_2 & Z_{Q_2}

$$Z_{Q_2} = \frac{1}{Q_2(j\omega)^n}$$

$$Z_{\text{parallel}} = \frac{R_2 \cdot \frac{1}{Q_2(j\omega)^n}}{R_2 + \frac{1}{Q_2(j\omega)^n}}$$

$$\therefore Z = R_1 + \frac{R_2 \cdot \frac{1}{Q_2(j\omega)^n}}{R_2 + \frac{1}{Q_2(j\omega)^n}}$$

where $n =$ constant phase element
 $n \approx 0.8 - 0.95$ [$n < 1$]
 for pure capacitor, $n = 1$

②

At $\omega \rightarrow \infty$

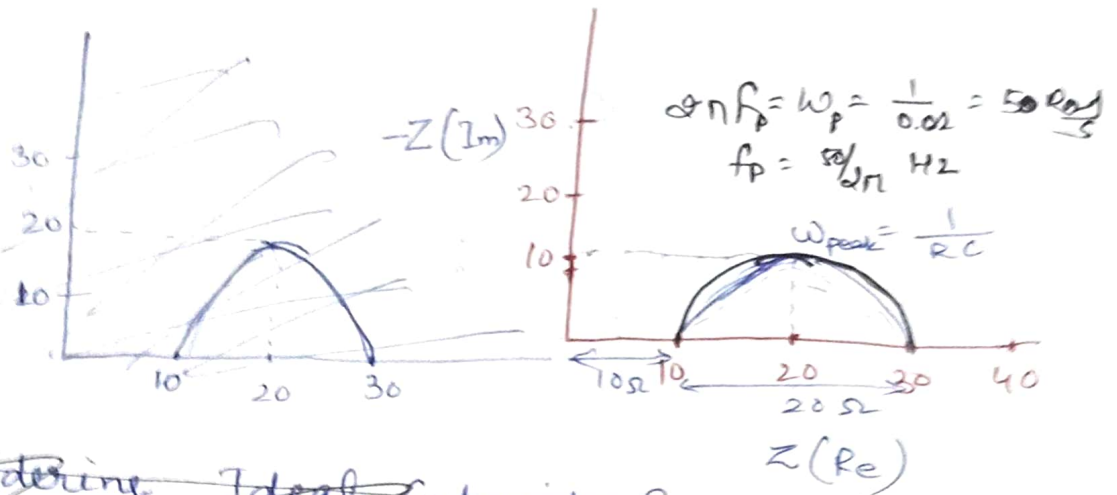
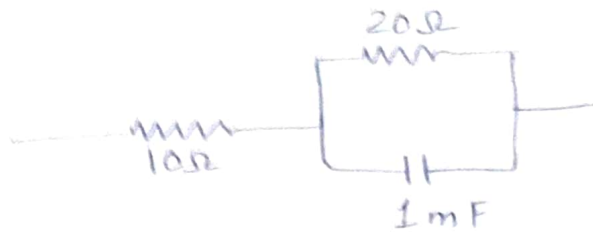
$$Z = R_1$$

capacitor offers zero impedance
 current will not flow through R_2

At $\omega = 0$

capacitor offer ∞ impedance. All current flow through R_2

$$Z = R_1 + R_2$$



~~response plot is considering Ideal capacitor [$Q=C, n=1$]
 for Real capacitor [$n < 1$], γ coordinate of
 peak frequency will be less than 10
 depending on value of n . $f_p = \frac{50}{2\pi} = 7.9577$~~

d)

Time Constant:

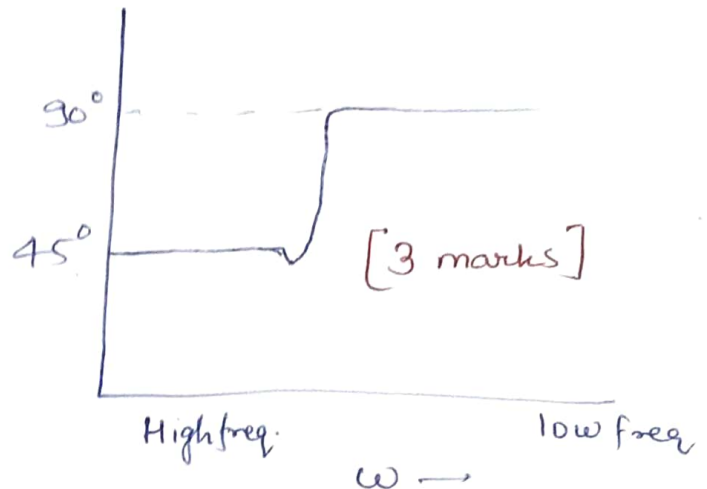
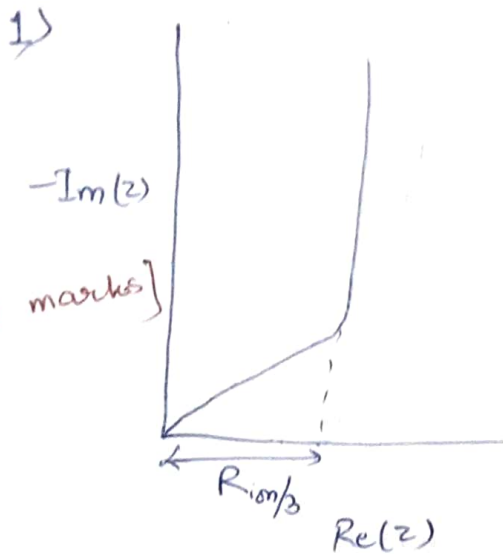
$$\begin{aligned}
 \tau &= R_2 \times Q_2 \\
 &= 20 \Omega \times 1 \text{ mF} \\
 &= 20 \text{ mS}
 \end{aligned}$$

$$\boxed{\tau = 0.02 \text{ S}}$$

for derivation, Refer Quiz(3) Question 1 solution uploaded on Moodle

[10 marks for derivation]

$$Z = \frac{R_{ion} \coth \sqrt{i\omega R_{ion} C_{de}}}{\sqrt{i\omega R_{ion} C_{de}}}$$



Bode Plot

At $\omega \rightarrow \infty$, $\coth(\sqrt{i\omega R_{ion} C_{de}}) \approx 1$

$$Z = \frac{R_{ion} \coth \sqrt{i\omega R_{ion} C_{de}}}{\sqrt{i\omega R_{ion} C_{de}}}$$

$$Z = \sqrt{\frac{R_{ion}}{\omega C_{de}}} \frac{1}{\sqrt{i}}$$

[3 marks]

$$\underline{Z_{\omega \rightarrow \infty} = \sqrt{\frac{R_{ion}}{\omega C_{de}}} \frac{1}{\sqrt{2}} (1-i)}$$

45° line behaviour

At $\omega = 0$

$$\coth(x) = \frac{1}{x} + \frac{x}{3} + \dots$$

[2 marks]

$$Z = \frac{R_{ion}}{\sqrt{i\omega R_{ion} C_{de}}} \left[\frac{1}{\sqrt{i\omega R_{ion} C_{de}}} + \frac{\sqrt{i\omega R_{ion} C_{de}}}{3} \right]$$

$$= \frac{R_{ion}}{i\omega R_{ion} C_{de}} + \frac{R_{ion}}{3} = \frac{R_{ion}}{3} + \frac{1}{i\omega C_{de}}$$

(90° line Capacitor behaviour)

③ find R_{ion} from Nyquist plot

Make symmetric cell using identical electrodes (same thickness, porosity, loading) and a separator. Using blocking electrolyte (No intercalation, $R_{ct} = 0$)



Get Nyquist Response, find $2 \frac{R_{ion}}{3}$ (2 identical electrodes)

[5 marks]

$$R_{ion} = \frac{d}{A K_{eff}}$$

$\frac{d}{A K_{eff}}$ (2 identical electrodes)
 $\frac{d}{A K_{eff}}$ thickness of electrode
 $\frac{d}{A K_{eff}}$ porosity
 $\frac{d}{A K_{eff}}$ Tortuosity
 $\frac{d}{A K_{eff}}$ Conductivity of pure electrolyte
 Area of electrode
 Note: thickness (d) is of electrode only (excluding Cu foil)

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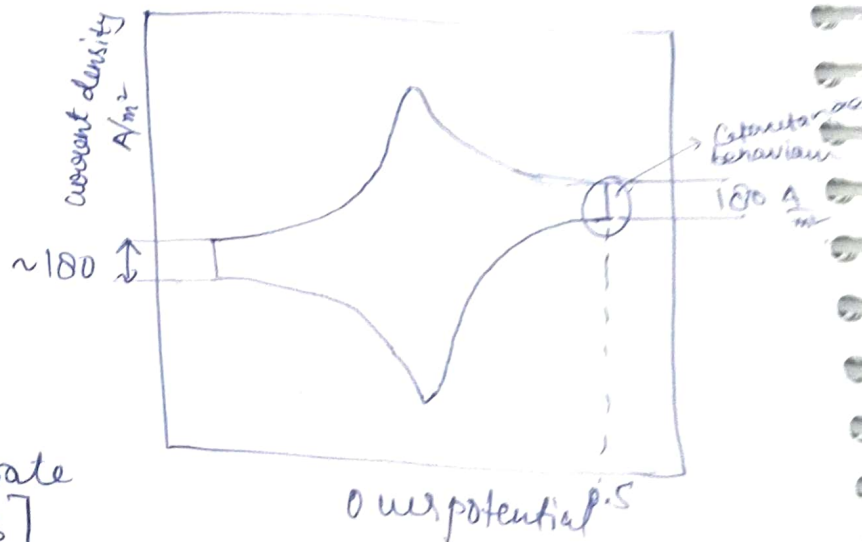
Q.5

From plot given,

①

$$i \approx 180 \text{ A/m}^2$$

$$\text{Overpotential} \approx 0.5 \text{ V}$$



[5 marks]

$$i = C_{de} \times \nu$$

\downarrow \downarrow
 [A] [F] scan rate [V/s]

scan rate is needed for calculation of

$$\text{areal Capacitance} \left[\frac{F}{m^2} \right]$$

Since scan rate not given, everyone who attempted it nicely, will get full of marks

b

$$\Delta E_p \approx \frac{0.059}{n}$$

~~Δ~~

$$n = \frac{0.059}{0.058} \approx 1$$

[5 marks]

$$\boxed{n = 1}$$

$$(6) \quad \frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2} \quad \text{--- (0)}$$

$$\text{Let } \eta = \frac{x}{g(t)} \quad \text{--- (1)}$$

$$\frac{\partial C}{\partial t} = \frac{\partial C}{\partial \eta} \frac{\partial \eta}{\partial t} = -\frac{x g'}{g^2} \frac{\partial C}{\partial \eta} \quad \text{--- (2)}$$

$$\frac{\partial C}{\partial x} = \frac{\partial C}{\partial \eta} \cdot \frac{\partial \eta}{\partial x} = \frac{1}{g} \frac{\partial C}{\partial \eta}$$

$$\frac{\partial^2 C}{\partial x^2} = \frac{1}{g^2} \frac{\partial^2 C}{\partial \eta^2} \quad \text{--- (2)}$$

$$\therefore \frac{\partial C}{\partial t} = -\frac{x g'}{g^2} \frac{\partial C}{\partial \eta} = \frac{D}{g^2} \frac{\partial^2 C}{\partial \eta^2}$$

$$\frac{\partial^2 C}{\partial \eta^2} + \frac{x g'}{D} \frac{\partial C}{\partial \eta} = 0$$

$$x = \eta g \rightarrow \text{from eqn (1)}$$

$$\frac{\partial^2 C}{\partial \eta^2} + \frac{\eta g g'}{D} \frac{\partial C}{\partial \eta} = 0$$

$$\text{Let } \frac{g g'}{D} = C_1$$

$$\boxed{\frac{\partial^2 C}{\partial \eta^2} + \eta C_1 \frac{\partial C}{\partial \eta} = 0}$$

$$\text{Let } \frac{\partial C}{\partial \eta} = \phi$$

 \Rightarrow

$$\boxed{\frac{\partial \phi}{\partial \eta} + \eta C_1 \phi = 0}$$

$$\left(\frac{\partial \phi}{\phi} \right) = -\int \eta C_1 d\eta$$

$$\ln \phi = -C_1 \frac{\eta^2}{2} + \ln C_2$$

$$\text{at } \eta=0, \phi=0 \rightarrow C_2=0$$

$$\phi = C_2 e^{-C_1 \eta^2 / 2}$$

$$\Rightarrow \frac{dC}{d\eta} = C_2 e^{-C_1 \eta^2 / 2}$$

$$\text{erf}(\eta) = \frac{2}{\sqrt{\pi}} \int_0^{\eta} e^{-\eta^2} d\eta$$

comparing: $C_2 = \frac{2}{\sqrt{\pi}}$, $C_1 = 2$

\therefore ~~$C = C_{\infty}$~~

$$C = C_{\infty} \text{erf}(\eta^2)$$

[5 marks] {For full derivation}

Those who have only shown steps from Fuller, will get 2 marks

② $gg' = \frac{1}{2} (g^2)' = DC_1$

$$(g^2)' = 2DC_1$$

$$g^2 = 2DC_1 t + C_3 = 4Dt + C_3$$

at $t=0$, $g=0 \therefore C_3=0$

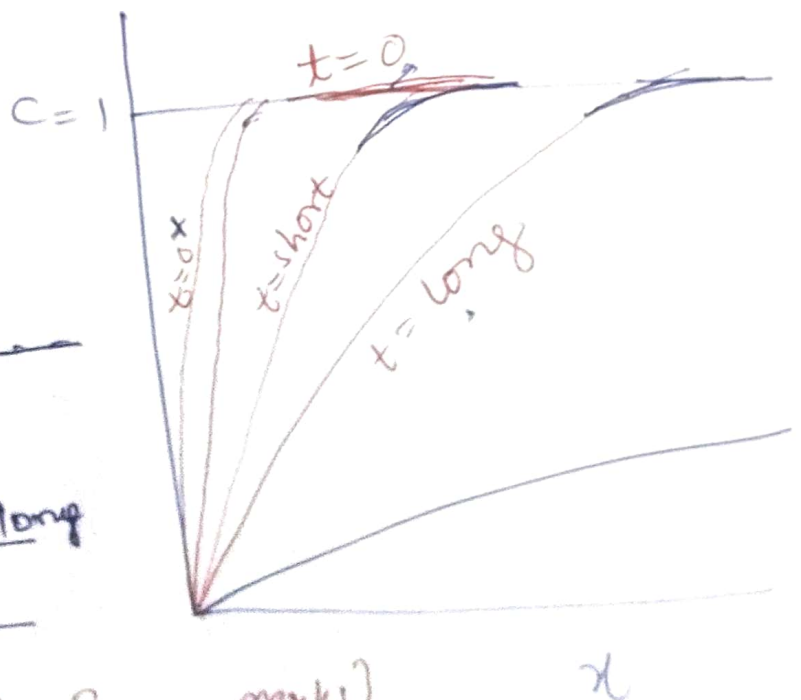
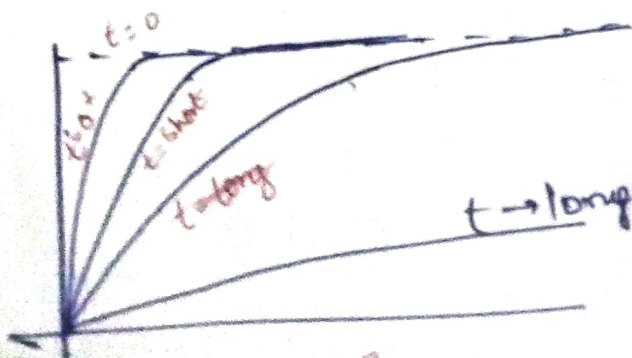
$$g = \sqrt{4Dt} = 2\sqrt{Dt}$$

[5 marks]

$$C = C_{\infty} \text{erf}(\eta^2) = C_{\infty} \text{erf}\left(\frac{x^2}{4Dt}\right)$$

③

③ System will not reach steady state



[3 + 2 marks] for S.S. answer

$$i = D \frac{dc}{dx}$$

$$\frac{i}{nF} = D \cdot \frac{1}{\delta} \frac{dc}{dn}$$

$$i = \frac{D n f}{\delta} \frac{dc}{dn} \Big|_{n=0}$$

$$= \frac{D n f}{\delta} c_{\infty} \frac{d}{dn} (\text{erf}(\eta^2)) \Big|_{n=0}$$

$$= \frac{D n f}{2\sqrt{Dt}} c_{\infty} \cdot \frac{2}{\sqrt{\pi}}$$

$$i = \frac{n F \sqrt{D} c^{\infty}}{\sqrt{\pi t}}$$

[5 marks]

7 (a) At 100% SOC (Anode @ $x=0.9$
Cathode @ $y=0.5$)

$$\text{Anode} \approx 0.07 \text{ V}$$

$$\text{Cathode} = 4.2$$

[2 marks]

$$V_{\text{cell}} = 4.2 - 0.07 = 4.13 \text{ V}$$

(b) At 0% SOC

$$\text{Anode} (x=0.1) = 0.2 \text{ V}$$

$$\text{Cathode} (y=0.98) = 3.59 \text{ V}$$

$$V_{\text{cell}} = 3.59 - 0.2 \approx 3.39 \text{ V}$$

[3 marks]

(c)

At 50% SOC

Anode: ~~range~~ $x = 0.1 - 0.9$
 Cathode: $y = 0.98 - 0.5 \rightarrow 0.1 \text{ SOC}$

At 50% SOC

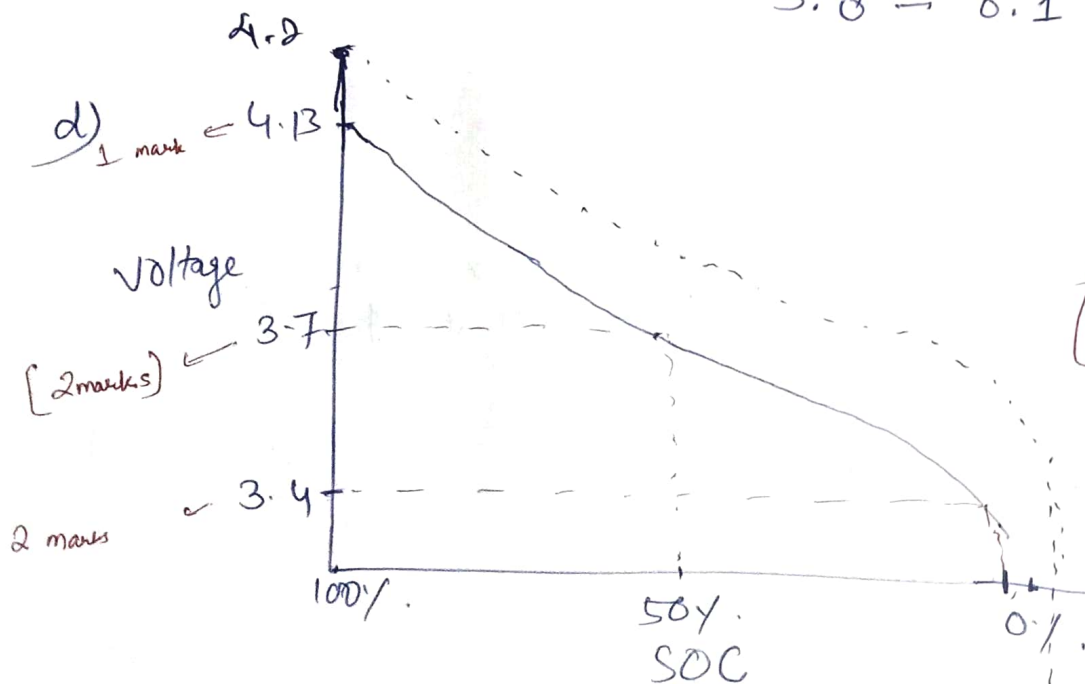
~~$y_{\text{cathode}} = 0.5 + \frac{0.48}{2} = 0.74$~~
 Cathode potential = ~~3.8 V~~
 $(\because \Delta y 0-100\% = 0.48 (0.98 - 0.5))$

Anode, $x = 0.1 + \frac{0.8}{2} = 0.5 \rightarrow 2 \text{ marks}$

$(\because \Delta x (0-100\%) = 0.8)$

Anode potential = 0.1 V

$V_{\text{cell @ 50\% SOC}} = \frac{0.74 - 0.5}{3.8 - 0.1} = 0.24 \text{ V}$
 $3.8 - 0.1 = 3.7 \text{ V} \rightarrow 1 \text{ mark}$



[5 Total marks]

(e) At 0% SOC, Anode = 0.2 V
 Cathode = 3.59 V

when 50% Anode particles are lost, charging the battery upto 50% SOC will

correspond to 100% SOC of ~~original~~ Anode ($0.07V$).

But Cathode will be at 50% SOC ($3.80V$) at that time.

Maximum Cell voltage will be ($3.80 - 0.07 = 3.73V$)

when we further charge battery (since cathode is half empty), Anode potential will go down further and will cross below $0V$ at some SOC, and plating will start.

