



# Echem Rnx. Engg. CL 611

**Prof. Bharat Suthar**

Department of Chemical Engineering  
IIT Bombay, Mumbai, India, 400076

Lecture x  
**Transport in Ionic Solutions**

*bharat.k.suthar[at]iitb.ac.in*

Landline: +91 (22) 2576 7243

# Outline



## ☐ Transport in the ionic solutions

### ☐ Parameters:

- ☐ Diffusivity
- ☐ Conductivity
- ☐ Transference number

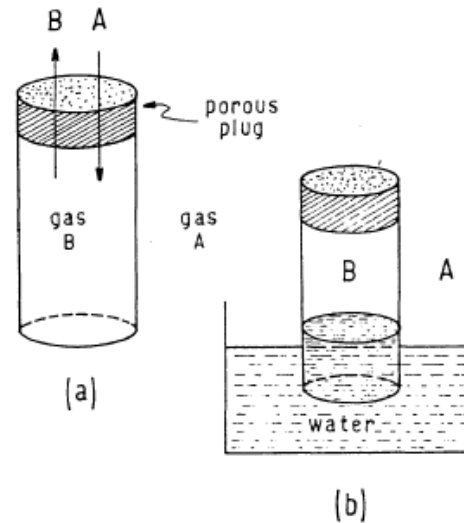
### ☐ Dilute solution theory

- ☐ Concentration gradient with 0 net current
  - ☐ To demonstrate we need to use combined flux equation
  - ☐ Nernst-planck equation
- ☐ Application of current on a symmetric cell
  - ☐ Reaction not possible
  - ☐ Reaction is present

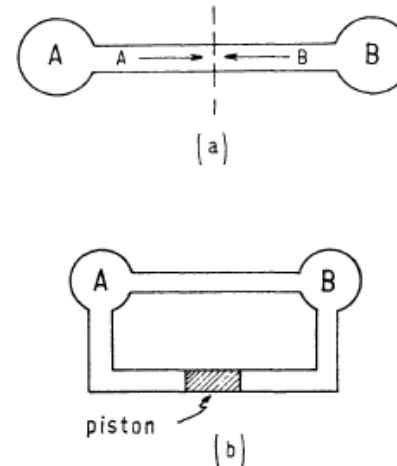
# Diffusion Process:

## *Example of coupled transport*

1. Systems used by Graham. Gas B in the tube diffuses through a porous plug into gas A (usually air) and A diffuses into the tube. In (b), the water level rises or drops depending on whether the molecular weight of B is less than or greater than that of A. (For more details see Section 6.1.1.1.)



2. (a) A system used by Graham and Loschmidt. Gases A and B are initially kept separate in two bulbs and then (by, for example, turning a stopcock) are allowed to interdiffuse. A porous plug may be used in the joining tube.  
(b) The gas chambers are joined by a second tube with a movable piston; then any change in pressure in the chambers resulting from the diffusion will be dissipated by movement of the piston. (For more details see Section 5.3.1.)



## Diffusion in Gases and Porous Media: Cunningham and Williams



# Fick's Law:

## Introduction

The transport of material by diffusion is due to the random thermal movement of molecules and is described by Fick's law:

$$\mathbf{J}_i = -D_i \nabla c_i, \quad (4.1)$$

$$J_{i,x} = -D_i \frac{dc_i}{dx}.$$

The flux defined here,  $\mathbf{J}$ , is the flux relative to the molar average velocity.

A more generalized form:

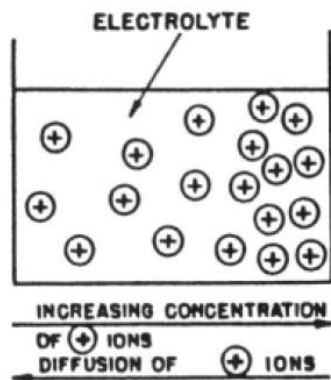
$$J_i = -B c_i \frac{d\mu_i}{dx}$$

$$\mu_i = \mu_i^0 + RT \ln c_i f_i$$

$$J_i = - \underbrace{BRT \left( 1 + \frac{d \ln f_i}{d \ln c_i} \right)}_{D?} \frac{dc_i}{dx}$$

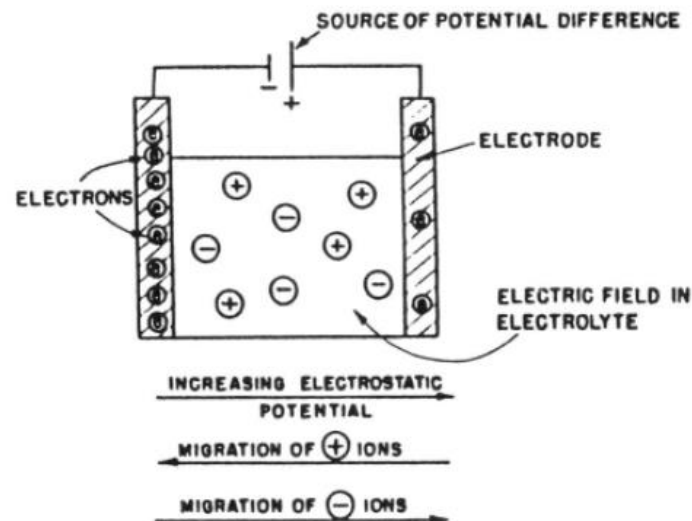
$f_i$  activity coefficient

# Diffusion vs Migration



**Fig. 4.1.** The diffusion of positive ions resulting from a concentration gradient of these ions in an electrolytic solution. The directions of increasing ionic concentration and of ionic diffusion are shown below the diagram.

$$J_{i,x} = -D_i \frac{dc_i}{dx}$$



**Fig. 4.2.** The migration of ions resulting from a gradient of electrostatic potential (i.e., an electric field) in an electrolyte. The electric field is produced by the application of a potential difference between two electrodes immersed in the electrolyte. The directions of increasing electrostatic potentials and of ionic migration are shown below the diagram.

migration or conduction

# Typical Diffusion Coefficients



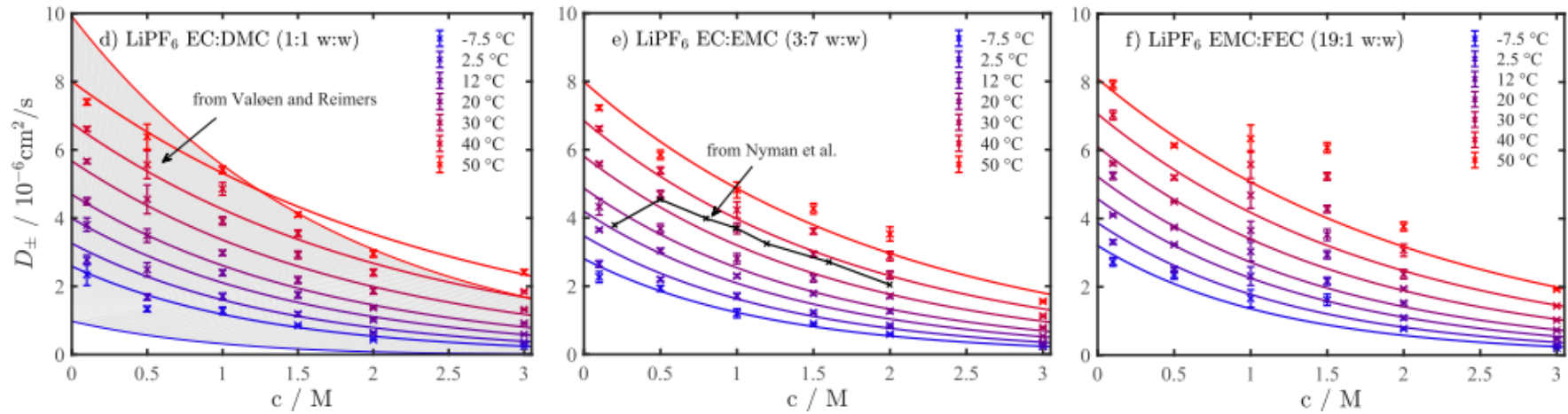
**TABLE 4.2**  
**Diffusion Coefficient  $D$  of Ions in Aqueous Solutions**

Ion	Diffusion Coefficient, ( $\text{cm}^2 \text{s}^{-1}$ )
$\text{Li}^+$	$1.028 \times 10^{-5}$
$\text{Na}^+$	$1.334 \times 10^{-5}$
$\text{K}^+$	$1.569 \times 10^{-5}$
$\text{Cl}^-$	$2.032 \times 10^{-5}$
$\text{Br}^-$	$2.080 \times 10^{-5}$

- Food for thought: What experiments can I perform to extract the diffusion coefficient of various ions?
- Since +ve and –ve ions are connected through electroneutrality, can I measure the  $D$  of individual ionic species?

# Diffusivity Measured for Li-ion Battery Elyt

*function of  $T$  and  $c$*



# Migration

❑ In solid metal conductor:

❖ Ohm's law

$$I = -\sigma \nabla \phi$$

$$I = \frac{\Delta V}{R}$$

❑ In ionic solutions:

❖ Migration:

❖ Force due to electric field  $\vec{F} = \underbrace{(z_i F)}_{q \left[ \frac{C}{\text{mol}} \right]} \underbrace{(-\nabla \phi)}_{\vec{E}}$

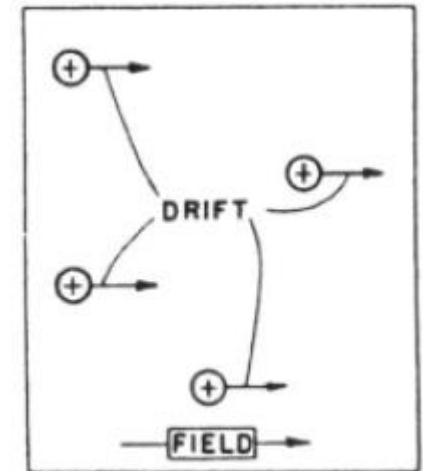
❖ Molar flux  $(N_i) \propto c_i$

❖ Using proportionality constant  $u_i$

$$N_i = \underbrace{u_i}_{\text{Prop. Const.}} \times c_i \times (z_i F)(-\nabla \phi)$$

$\phi$  is the potential in the solution, not the potential in the solid/electrodes

$$\vec{F} = q\vec{E}$$



(b) MACROSCOPIC VIEW





# Consider binary electrolyte

□ Molar fluxes of both ions (w/o conc. gradient):

□  $N_+ = u_+ \times c_+ \times (-z_+ F \nabla \phi)$

□  $N_- = u_- \times c_- \times (-z_- F \nabla \phi)$

□ Net current is due to both fluxes: (ignoring concentration gradient)

□  $i = \sum_i z_i F N_i$

□  $i = -(u_+ c_+ z_+^2 F^2 \nabla \phi + u_- c_- z_-^2 F^2 \nabla \phi)$

□  $i = - \underbrace{F^2 (u_+ c_+ z_+^2 + u_- c_- z_-^2)}_{\kappa} \nabla \phi$

□ Ionic conductivity

□  $\kappa = F^2 (u_+ c_+ z_+^2 + u_- c_- z_-^2)$

□ Units S/cm, battery electrolyte: ~10 mS/cm

□  $i = -\kappa \nabla \phi$

# Typical Conductivity Values



**TABLE 4.7**  
**Representative Values of Specific Conductivity**

Substance	Type of Conductor	Specific Conductivity ( $\text{S cm}^{-1}$ )	$T$ (K)
Copper	Metallic	$5.8 \times 10^5$	293
Lead	Metallic	$4.9 \times 10^5$	273
Iron	Metallic	$1.1 \times 10^5$	273
4 M $\text{H}_2\text{SO}_4$	Electrolytic	$7.5 \times 10^{-1}$	291
0.1 M KCl	Electrolytic	$1.3 \times 10^{-2}$	298
Xylene	Nonelectrolyte	$1 \times 10^{-19}$	298
Water	Nonelectrolyte	$4 \times 10^{-8}$	291

How do I measure the conductivity of solutions?

# Molar conductivity



## □ Ionic conductivity

$$\kappa = F^2(u_+c_+z_+^2 + u_-c_-z_-^2) \quad \text{Eq[1]}$$

Units S/cm, battery electrolyte: ~10 mS/cm

## □ Example:

□ Take KCl solution of concentration  $c$ .

□  $z_+ = z_- = 1$ , &  $c_+ = c_- = c$ , simplifies eqn 1 as follows:

$$\kappa = F^2(u_+ + u_-)c \quad \text{Eq [2]}$$

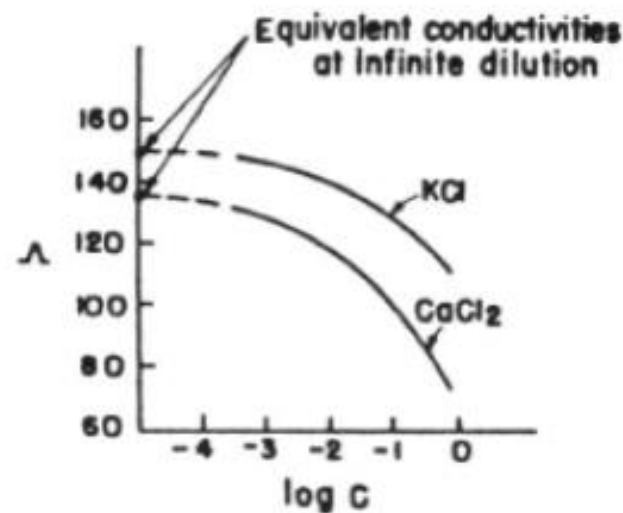
□ Conductivity is proportional to concentration, hence  $\kappa/c$  is supposed to be constant.

$$\kappa/c = F^2(u_+ + u_-) \quad \text{Eq [3]}$$

□  $\kappa/c$  is also known as molar conductivity ( $\Lambda_m$ )

□ Only at concentration below 0.1 mM, one see  $\Lambda_m$  to be constant.

Sym	Name	Units
$G$	Conductance	S or $1/\Omega$
$\rho$	Resistivity	cm/S
$\sigma, \kappa$	Specific conductivity	S/cm
$\Lambda_m$	Molar conductivity	$\text{S cm}^2/\text{mol}$
$\Lambda$	Equivalent conductivity	$\text{S cm}^2/(\text{mol eq})$



# Equivalent conductivity

## □ Ionic conductivity

$$\kappa = F^2(u_+c_+z_+^2 + u_-c_-z_-^2) \quad \text{Eq[1]}$$

Units S/cm, battery electrolyte: ~10 mS/cm

## □ Example:

□ Take  $\text{CaCl}_2$  solution of concentration  $c$ .

□  $z_+ = 2, z_- = 1, \& c_+ = c_-/2 = c$ ,

simplifies eqn 1 as follows:

$$\kappa = F^2(4u_+ + 2u_-)c \quad \text{Eq [2]}$$

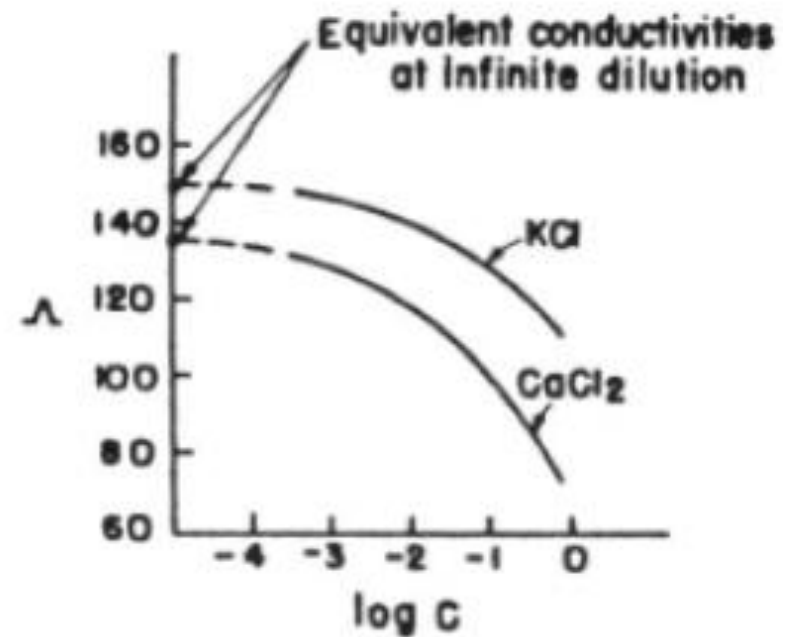
$$\kappa = F^2(2u_+ + u_-)2c \quad \text{Eq [2]}$$

□ Equivalent =  $2c$

□ **Equivalent conductivity is defined as**

$$\kappa/zc \ (\Lambda)$$

□ Only at concentration below 0.1 mM, one see  $\Lambda$  to be constant.

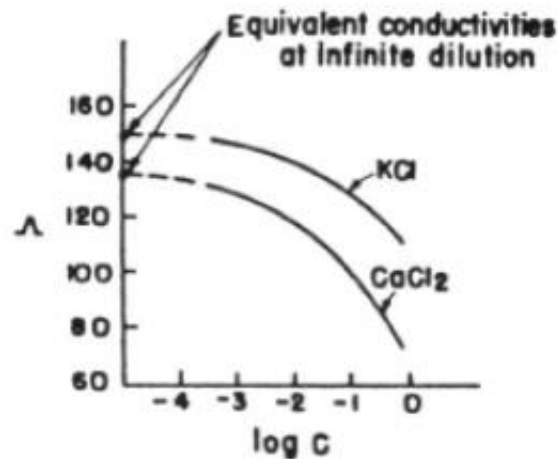


# Kohlrausch's Law at low concentrations

□ Kohlrausch's Law at low concentrations:

$$\Lambda = \Lambda^\circ - K \sqrt{c}$$

- Particularly for strong electrolytes.
- For weak elyt, where dissociation is not full, it is not fully applicable.

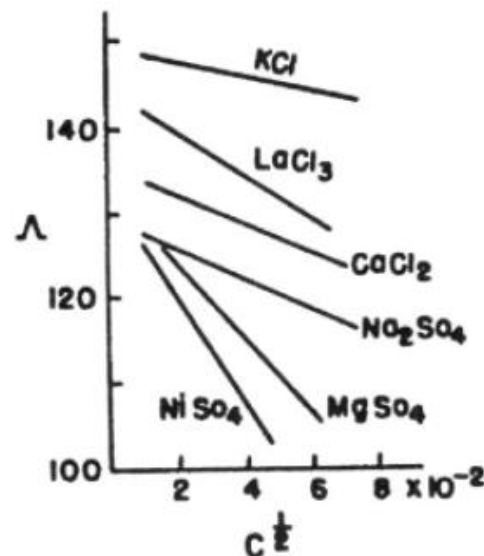


Example:

The figure shows the max concentration value of

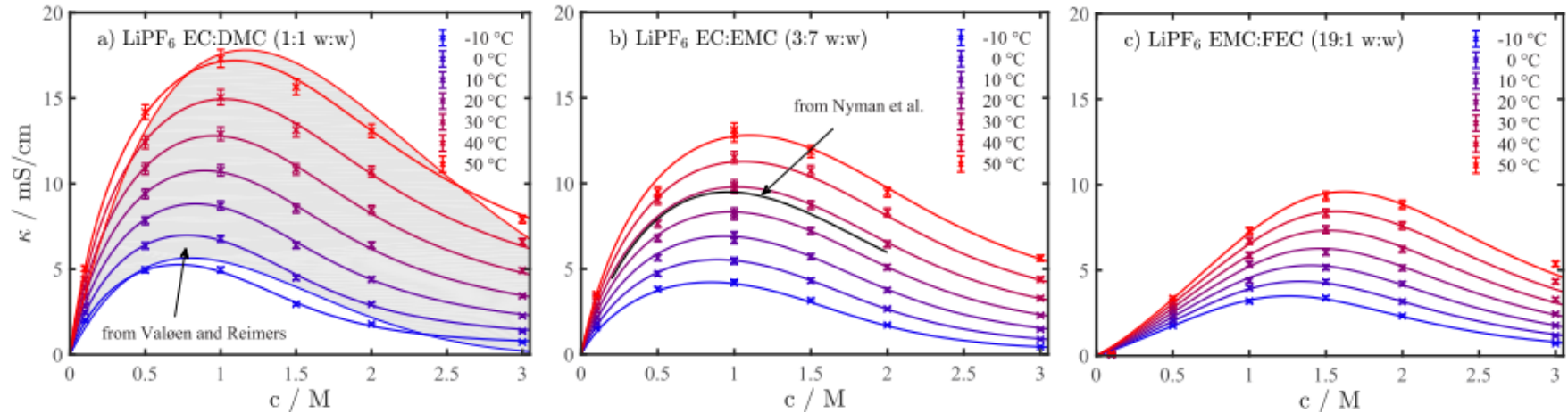
$$\sqrt{c} = 8 \times 10^{-2}$$

$$c = 6.4 \text{ mM}$$



# Conductivity for Li-ion Battery Elyt

*function of  $T$  and  $c$*



The measured conductivity at  $c > 10$  mM deviates significantly from the Kohlrausch law.

# Transference Number:

## Binary electrolyte (no conc. gradient)

$$\square i = - \underbrace{F^2(u_+c_+z_+^2 + u_-c_-z_-^2)}_{\kappa} \nabla \phi$$

☐ Ionic conductivity  $\kappa$

$$\square \kappa = F^2(u_+c_+z_+^2 + u_-c_-z_-^2)$$

☐ Units S/cm, battery electrolyte: ~10 mS/cm

☐ Current is being carried by two species:

☐ How much is due to single specie:

$$\square t_+ = \frac{u_+c_+z_+^2}{u_+c_+z_+^2 + u_-c_-z_-^2}$$

$$\square t_- = \frac{u_-c_-z_-^2}{u_+c_+z_+^2 + u_-c_-z_-^2}$$

$$\square t_+ + t_- = 1$$

☐ Generally:

$$\square \sum t_i = 1$$

# Transference Number:



**TABLE 4.16**

**Transport Numbers of Cations in Aqueous Solutions at 298 K in 0.1 *N* Solutions**

Electrolyte	HCl	LiCl	NaCl	KCl	KNO <sub>3</sub>	AgNO <sub>3</sub>	BaCl <sub>2</sub>
Transport number of cation, $t_+$	0.83	0.32	0.39	0.49	0.51	0.47	0.43

For Nafion the transference number  $t_+ = 1$

For solid state electrolyte for Li-ion battery,  $t_+ = 1$

For anionic exchange membrane,  $t_- = 1$



## ☐ Transport in the ionic solutions

### ☐ Parameters:

- ☐ Diffusivity
- ☐ Conductivity
- ☐ Transference number

### ☐ Dilute solution theory contd.

#### ☐ **Concentration gradient with 0 net current**

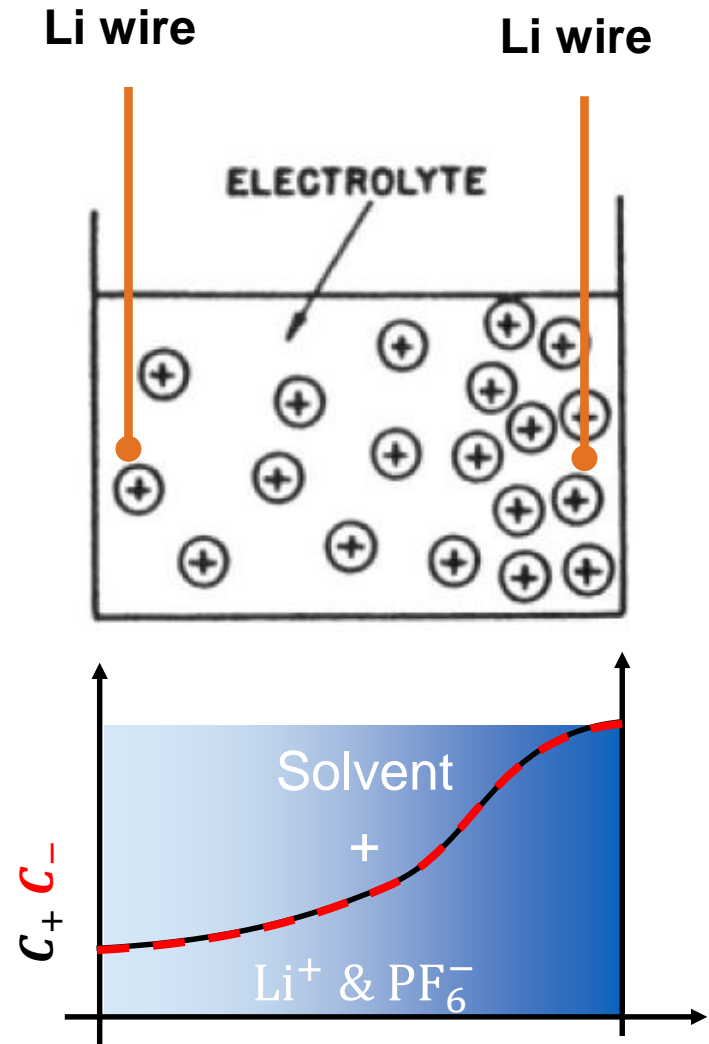
- ☐ To demonstrate we need to use combined flux equation
- ☐ Nernst-planck equation
- ☐ Application of current on a symmetric cell
  - ☐ Reaction not possible
  - ☐ Reaction is present

# Example: Concentration Gradient System



Case: Concentration gradient exists in the following system. No applied electric field.

- Is molar flux nonzero?
- Is current nonzero?
- What types of transport processes are taking place in this system?
- Will there be a potential gradient as well?
- Say its LiPF<sub>6</sub> system:
- If I dip a lithium wire at two different location, will I measure potential difference?
- If there is a potential gradient, will there be migration?



# NERNST-PLANCK EQUATION



$$\mathbf{N}_i = \underbrace{-z_i u_i F c_i \nabla \phi}_{\text{migration}} \quad \underbrace{-D_i \nabla c_i}_{\text{diffusion}} \quad + \quad \underbrace{c_i \mathbf{V}}_{\text{convection}}$$

N-P eqn is also referred to as dilute solution theory.

$$i = \sum_i z_i F N_i$$

$$\mathbf{i} = -F^2 \nabla \phi \sum_i z_i^2 u_i c_i - F \sum_i z_i D_i \nabla c_i + F \mathbf{v} \sum_i z_i c_i$$

$$\mathbf{i} = -F^2 \nabla \phi \sum_i z_i^2 u_i c_i - F \sum_i z_i D_i \nabla c_i$$

Charge balance: (assuming electroneutrality)

$$\nabla \cdot \mathbf{i} = 0$$

Special case:

When no current is flowing in the system:

$$i = 0$$

# Example revisited

When no current is flowing in the system:

$$i = 0$$

N-P relation:

$$i = -F^2 \nabla \phi \sum z_i^2 u_i c_i - F \sum z_i D_i \nabla c_i$$

$$0 = -F^2 \nabla \phi \sum z_i^2 u_i c_i - F \sum z_i D_i \nabla c_i$$

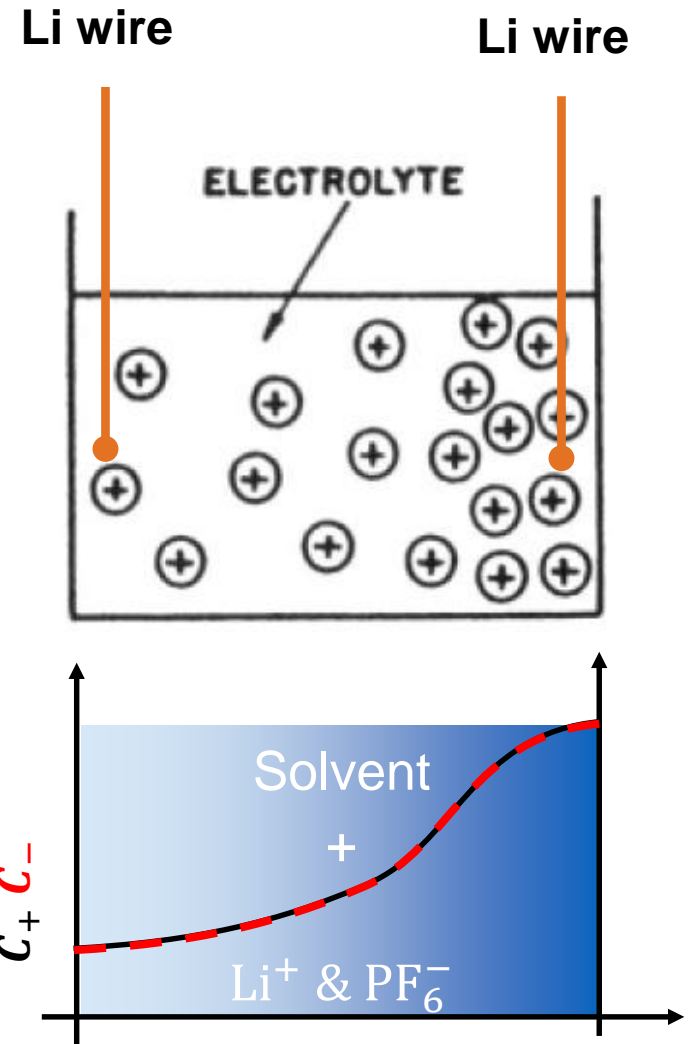
$$\nabla \phi = - \frac{\sum z_i D_i \nabla c_i}{F \sum z_i^2 u_i c_i}$$

Easy case:  $\text{Li}^+ \text{PF}_6^-$  with  $\nu_+ = \nu_- = 1$

$$c = c_+ = c_-$$

$$\nabla \phi = - \frac{\sum z_i D_i}{F \sum z_i^2 u_i} \nabla \ln c$$

*This is also termed as diffusion potential*





## ☐ Transport in the ionic solutions

### ☐ Parameters:

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### ☐ Dilute solution theory contd.

- ☐ Concentration gradient with 0 net current
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# N-P Equation: Dilute Solution Theory



Molar Flux:

$$\mathbf{N}_i = \underbrace{-z_i u_i F c_i \nabla \Phi}_{\text{migration}} - \underbrace{D_i \nabla c_i}_{\text{diffusion}} + \underbrace{c_i \mathbf{v}}_{\text{convection}}$$

Electroneutrality

$$\mathbf{i} = F \sum_i z_i \mathbf{N}_i$$
$$\mathbf{i} = -F^2 \nabla \Phi \sum_i z_i^2 u_i c_i - F \sum_i z_i D_i \nabla c_i + F \mathbf{v} \sum_i z_i c_i$$

Current in the solution:

$$\mathbf{i} = -F^2 \nabla \Phi \sum_i z_i^2 u_i c_i - F \sum_i z_i D_i \nabla c_i$$

Expression in terms of  $\kappa$  and  $D_i$ :  $\kappa = F^2 \sum_i z_i^2 u_i c_i$

Transference number:  $t_+$

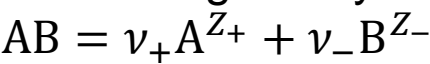
Thermodynamic factor:  $1 + \frac{d \ln f_+}{d \ln c_+}$



# Too many parameters:

How many parameters do I need to know the potential drop in the solution?

For the following binary soln



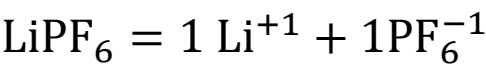
$$u_+$$

Mobility of + ions

$$u_-$$

Mobility of - ions

**Example:**



$$D_+$$

Diffusivity of + ions (N-E)

$$D_-$$

Diffusivity of – ions (N-E)

$$t_+$$

Transference number of + ions

$$t_-$$

Transference number of - ions

What are the fundamentally essential parameters to describe transport?

$$\kappa$$

Conductivity of electrolyte

What are the essential macro parameters to describe transport?

$$1 + \frac{d \ln f_+}{d \ln c_+}$$

Thermodynamic factor for + ions

$$1 + \frac{d \ln f_-}{d \ln c_-}$$

# Electrochemical Potential:



$$\begin{aligned} \mathbf{N}_i &= -u_i z_i F \times c_i (\nabla \Phi) - D_i \nabla c_i \\ \mathbf{N}_i &= -u_i z_i F \times c_i (\nabla \Phi) - D_i c_i \nabla \ln c_i \end{aligned} \quad \left. \vphantom{\begin{aligned} \mathbf{N}_i &= -u_i z_i F \times c_i (\nabla \Phi) - D_i \nabla c_i \\ \mathbf{N}_i &= -u_i z_i F \times c_i (\nabla \Phi) - D_i c_i \nabla \ln c_i \end{aligned}} \right\} \nabla c_i = c_i \nabla \ln c_i$$

Rearrangement: (take  $\nabla$  out)

$$\mathbf{N}_i = -c_i \times \nabla [u_i z_i F \cdot \Phi + D_i \ln c_i]$$

$$\mathbf{N}_i = -c_i \times \nabla \left[ u_i z_i F \cdot \Phi + \frac{D_i}{RT} RT \ln c_i \right]$$

$$\mathbf{N}_i = -c_i \times \frac{D_i}{RT} \nabla \left[ \underbrace{\frac{u_i RT}{D_i}}_{\text{N-E Relation}} z_i F \cdot \Phi + RT \ln c_i \right]$$

$$\mathbf{N}_i = -c_i \times \frac{D_i}{RT} \nabla \left[ \underbrace{z_i F \cdot \Phi + RT \ln c_i}_{\bar{\mu}_i \text{ Echem Pot.}} \right]$$

Flux can be expressed using one driving force  $\nabla \bar{\mu}_i$ !

$$\mathbf{N}_i = -c_i \times \frac{D_i}{RT} \nabla \bar{\mu}_i$$

$$\bar{\mu}_i = z_i F \cdot \Phi + \underbrace{\mu_i^0 + RT \ln c_i}_{\text{Chemical Pot.}}$$





## ☐ Transport in the ionic solutions

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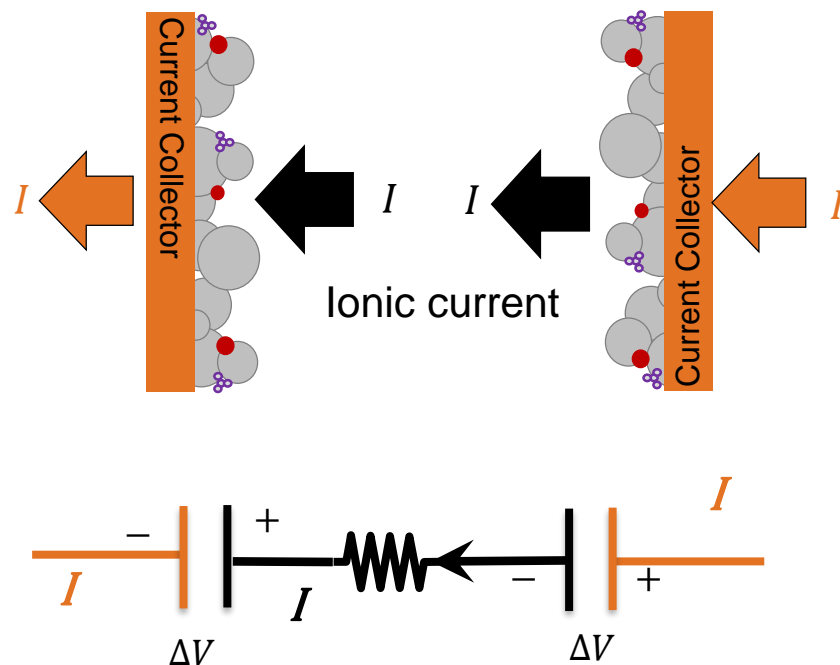
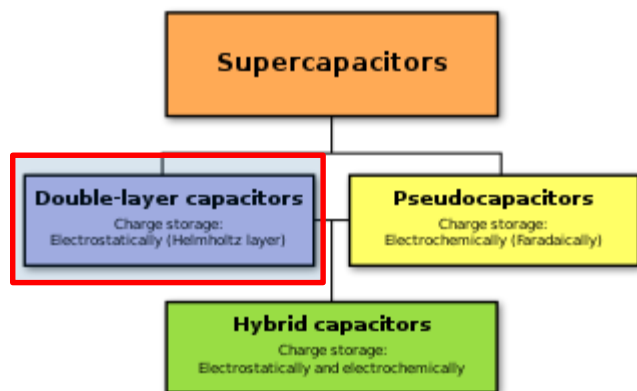
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- ☐ Concentration gradient with 0 net current
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  - ☐ Nernst-planck equation
- ☐ Application of current on a symmetric cell
  - ☐ Reaction not possible
  - ☐ Reaction is present

# Symmetric Cell: No Faradaic Rxn @ Interface



- ❑ Example:
  - ❑ Conductivity Cell
  - ❑ Supercapacitor



# Symmetric Cell: No Faradaic Rxn @ Interface



Molar Flux:

$$\mathbf{N}_i = \underbrace{-z_i u_i F c_i \nabla \Phi}_{\text{migration}} - \underbrace{D_i \nabla c_i}_{\text{diffusion}} + \underbrace{c_i \mathbf{v}}_{\text{convection}}$$

Current Eqn.

$$\mathbf{i} = F \sum_i z_i \mathbf{N}_i$$

$$\mathbf{i} = -F^2 \nabla \Phi \sum_i z_i^2 u_i c_i - F \sum_i z_i D_i \nabla c_i + F \mathbf{v} \sum_i z_i c_i$$

Electroneutrality

Current in the solution:

$$\mathbf{i} = -F^2 \nabla \Phi \sum_i z_i^2 u_i c_i - F \sum_i z_i D_i \nabla c_i$$

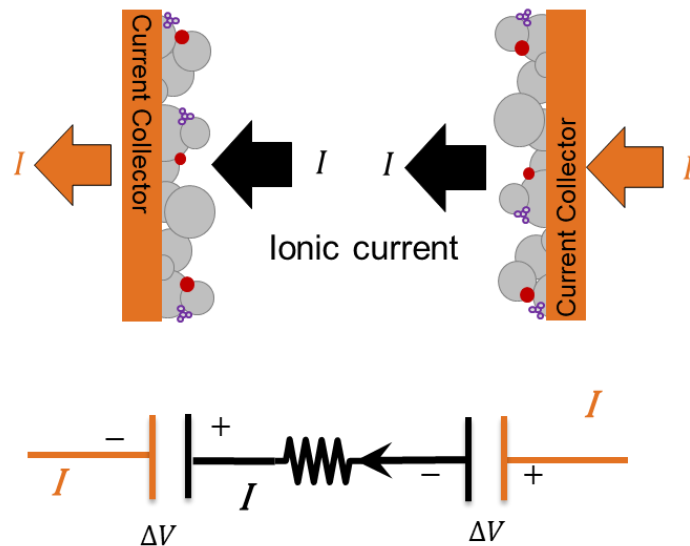
Expression in terms of  $\kappa$  and  $D_i$ :  $\kappa = F^2 \sum_i z_i^2 u_i c_i$

Modified Ohm's law (McInnis Equation)

$$\nabla \Phi = -\frac{\mathbf{i}}{\kappa} - \frac{F}{\kappa} \sum_i z_i D_i \nabla c_i$$

In the absence of conc. gradient (Ohm's law):

$$\nabla \Phi = -\frac{\mathbf{i}}{\kappa}$$



# Symmetric Cell: No Faradaic Rxn @ Interface



Conservation of charge:

$$\nabla \cdot \mathbf{i} = 0$$

Where  $i$  is given as:  $\nabla \Phi = -\frac{\mathbf{i}}{\kappa} - \frac{F}{\kappa} \sum_i z_i D_i \nabla c_i$

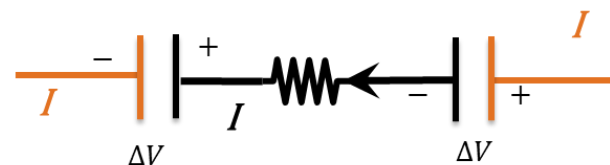
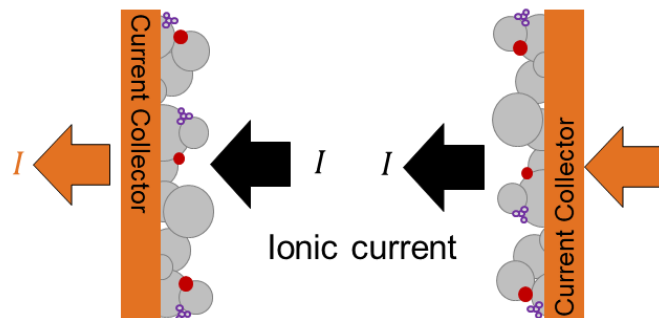
Gives the following expression:

$$\nabla \cdot (\kappa \nabla \Phi) + F \sum_i z_i \nabla \cdot (D_i \nabla c_i) = 0$$

When no concentration gradient exists:

$$\nabla^2 \Phi = 0$$

Ohm's Law





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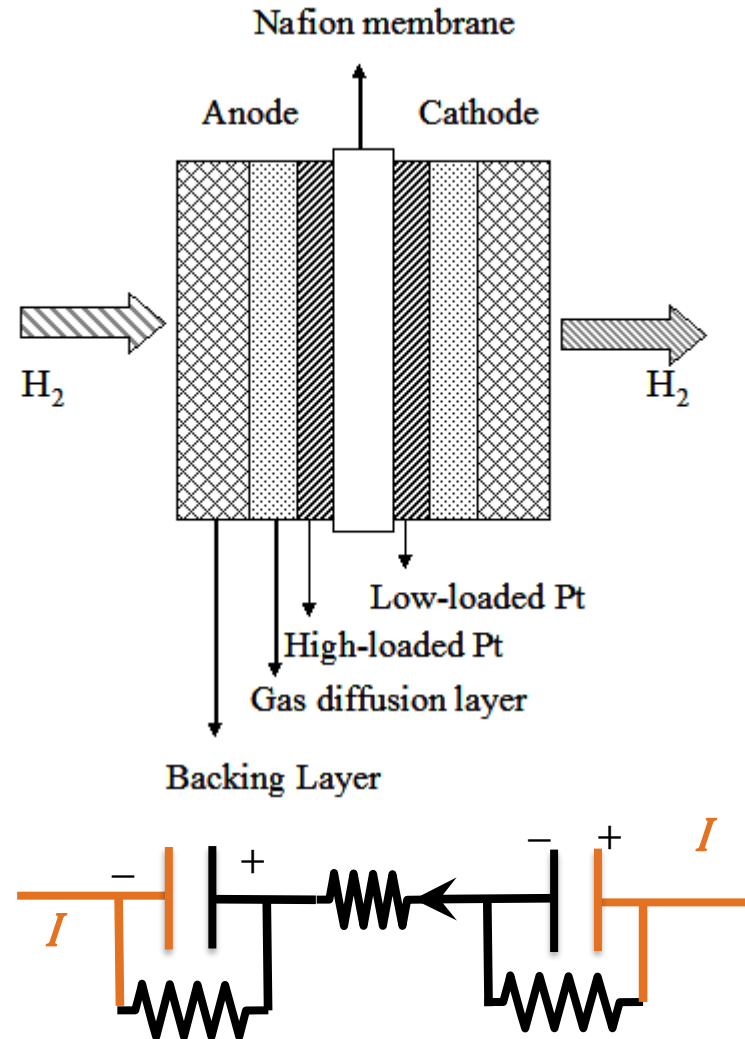
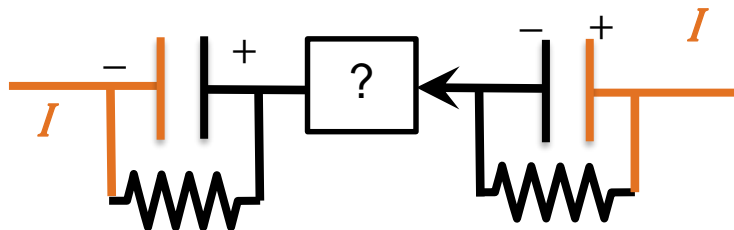
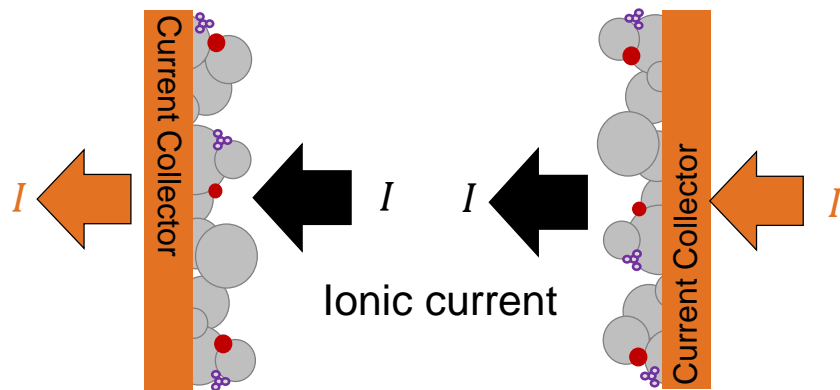
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# Faradaic Rxn @ Interface



Simple cases of symmetric cell  
Case of Battery



**Image:** Simple cases of symmetric cell Hydrogen pump experiment  
**Anodic oxidation of hydrogen in PEFCs at varying platinum loadings**  
G. Selvarania, Bincy Johnb, P. Sridhara, S. Pitchumania and A. K. Shukla

# Example: Li-Li symmetric cell



$$\underbrace{\frac{\partial c_i}{\partial t}}_{\text{Accumulation}} = \underbrace{-\nabla \cdot \mathbf{N}_i}_{\text{Net Input}} + \text{Bulk Rnx}$$

$$\frac{\partial c_i}{\partial t} = -\nabla \cdot (-z_i u_i F c_i \nabla \Phi - D_i \nabla c_i)$$

$$\frac{\partial c_i}{\partial t} = z_i u_i F \nabla \cdot (c_i \nabla \Phi) + D_i \nabla^2 c_i$$

Individual governing eqn.

$$\frac{\partial c_+}{\partial t} = z_+ u_+ F \nabla \cdot (c_+ \nabla \Phi) + D_+ \nabla^2 c_+$$

$$\frac{\partial c_-}{\partial t} = z_- u_- F \nabla \cdot (c_- \nabla \Phi) + D_- \nabla^2 c_-$$

$$\mathbf{i} = F \sum_i z_i \mathbf{N}_i$$

$$\mathbf{i} = -F^2 \nabla \Phi \sum_i z_i^2 u_i c_i - F \sum_i z_i D_i \nabla c_i$$

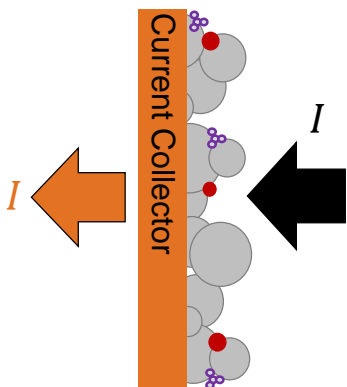
$$\mathbf{i} = -\kappa \nabla \Phi - F \sum_i z_i D_i \nabla c_i$$

**Current equation:**

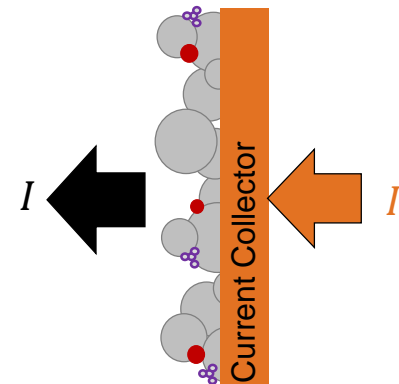
$$\mathbf{i} = -\kappa \nabla \Phi - F (z_+ D_+ \nabla c_+ + z_- D_- \nabla c_-)$$

# Complete System of Eqn.

Along with Boundary Conditions:



$$\begin{aligned}\frac{\partial c_+}{\partial t} &= z_+ u_+ F \nabla \cdot (c_+ \nabla \Phi) + D_+ \nabla^2 c_+ \\ \frac{\partial c_-}{\partial t} &= z_- u_- F \nabla \cdot (c_- \nabla \Phi) + D_- \nabla^2 c_- \\ \mathbf{i} &= -\kappa \nabla \Phi - F(z_+ D_+ \nabla c_+ + z_- D_- \nabla c_-)\end{aligned}$$



Only + reacts

$$\mathbf{i} = F z_+ \mathbf{N}_+$$

$$\mathbf{N}_- = 0$$

$$F z_+ \mathbf{N}_+ = F z_+ (-z_i u_i F c_i \nabla \Phi - D_i \nabla c_i) = i$$

$$\mathbf{N}_- = -z_i u_i F c_i \nabla \Phi - D_i \nabla c_i = 0$$

Only + reacts

$$\mathbf{i} = F z_+ \mathbf{N}_+$$

$$\mathbf{N}_- = 0$$

$$F z_+ \mathbf{N}_+ = F z_+ (-z_i u_i F c_i \nabla \Phi - D_i \nabla c_i) = i$$

$$\mathbf{N}_- = -z_i u_i F c_i \nabla \Phi - D_i \nabla c_i = 0$$



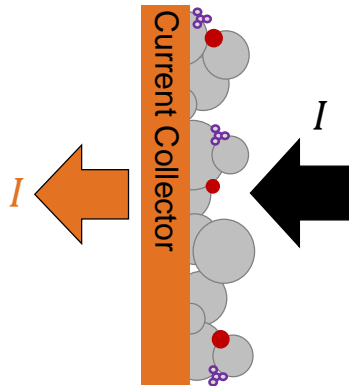
# Complete System of Eqn.

Along with Boundary Conditions:

Using Electroneutrality  $c_+ = c_-$

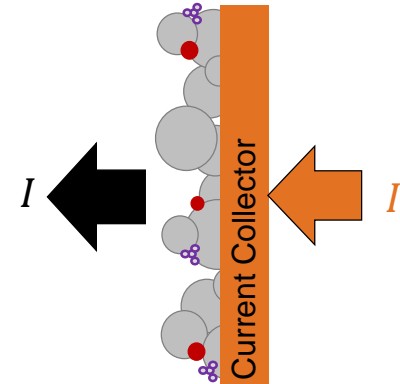
Elimination of potential from the governing equation.

Parameters used:  $t_+ = \frac{u_+ z_+}{u_+ z_+ - u_- z_-}$  &  $D = \frac{z_+ u_+ D_- - z_- u_- D_+}{z_+ u_+ - z_- u_-}$  and  $\kappa$



$$\frac{\mathbf{i}}{z_+ F} = \frac{D}{1 - t_+} \nabla c$$

$$\frac{\partial c}{\partial t} = D \nabla^2 c$$

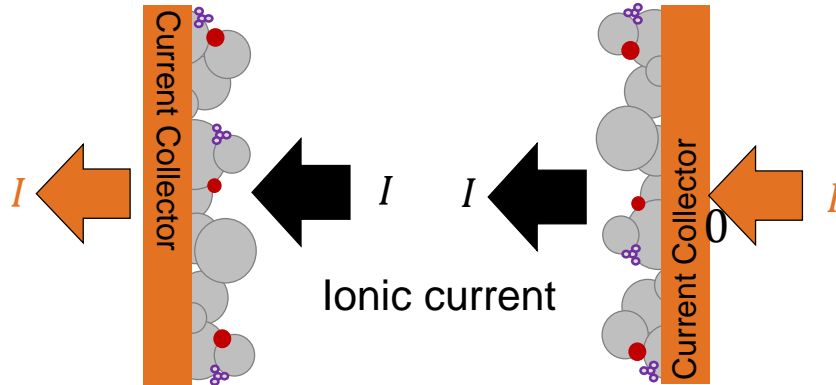


$$\frac{\mathbf{i}}{z_+ F} = \frac{D}{1 - t_+} \nabla c$$

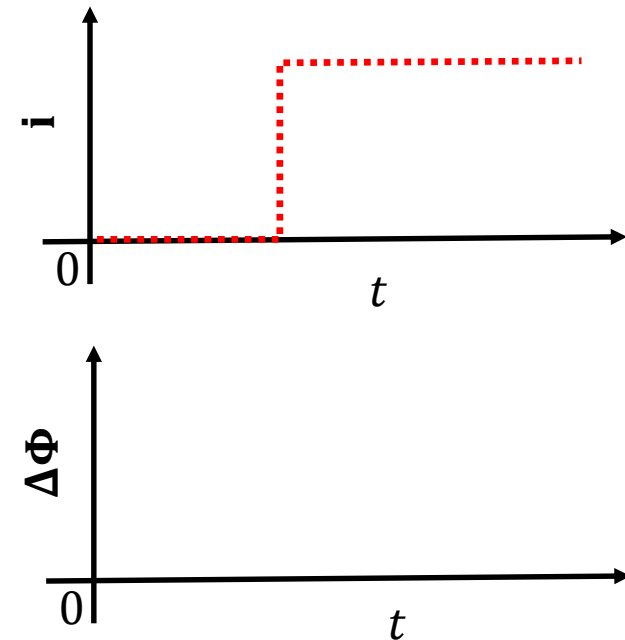
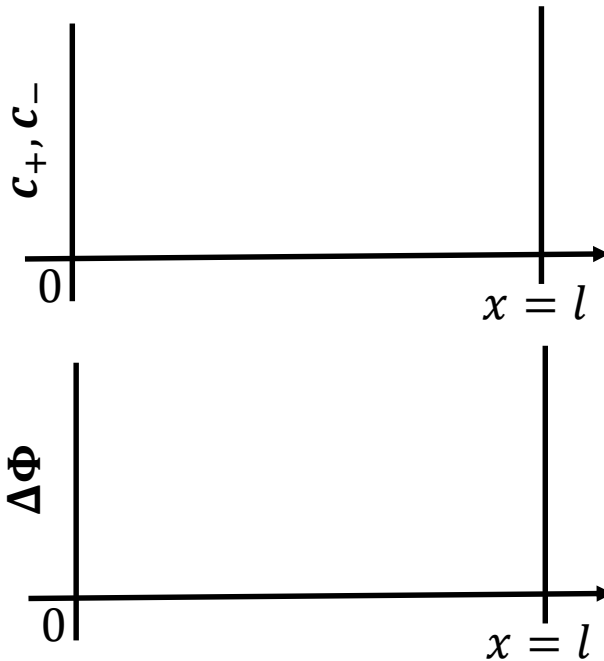
Solve for  $c(x, t)$  first, then integrate the following equation to get  $\phi$

$$\mathbf{i} = -\kappa \nabla \Phi - F(z_+ D_+ + z_- D_-) \nabla c_+$$

# Pictorial Description: Board work

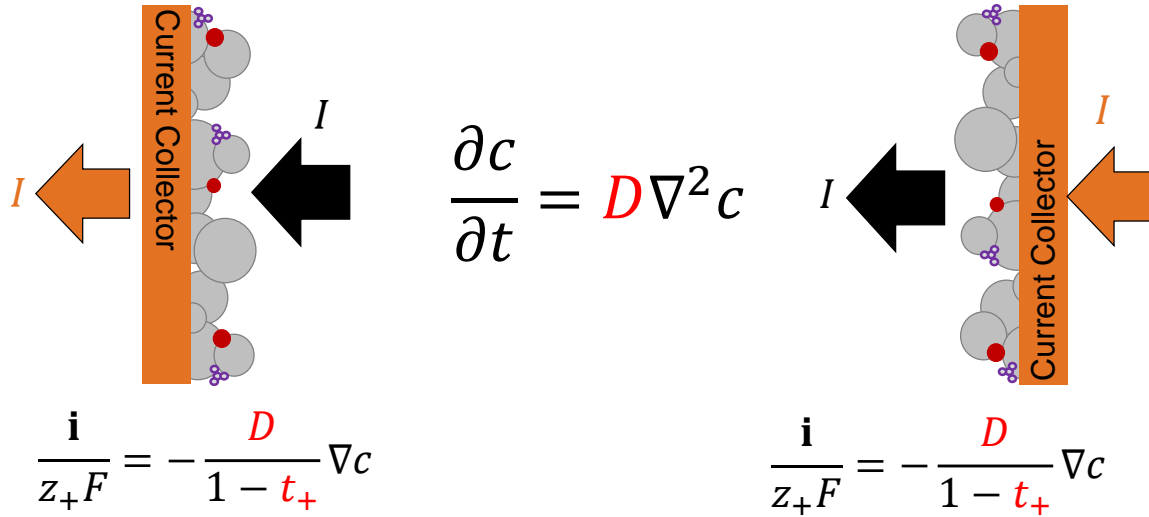


$c_+$  with  $x$  and  $t$   
 $c_-$  with  $x$  and  $t$   
 $i, \Phi$  with  $x$  and  $t$



# Complete System of Eqn.

Along with Boundary Conditions:



Solve for  $c(x, t)$  first, then integrate the following equation to get  $\phi$

$$i = -\kappa \nabla \Phi - F(z_+ D_+ + z_- D_-) \nabla c_+$$

$$\kappa = F^2 \sum_i z_i^2 u_i c_i = F^2 \left( \frac{z_-^2 D c_0}{2RT t_+} - \frac{z_+^2 D c_0}{2RT (1 - t_+)} \right)$$

For case when  $-z_- = z_+ = z$

$$\kappa = \frac{F^2 z^2 D c_0}{2RT} \left( \frac{1}{t_+} + \frac{1}{(1 - t_+)} \right) = \frac{F^2 z^2 c_0}{2RT} \frac{D}{t_+ (1 - t_+)}$$

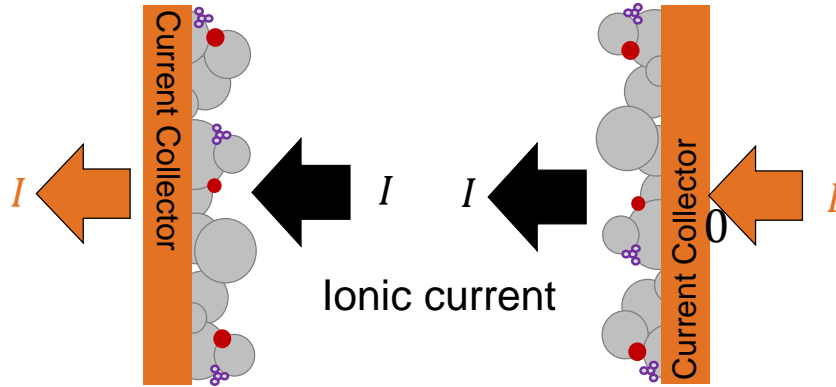
$$F \left( z_+ \frac{D}{2(1 - t_+)} + z_- \frac{D}{2t_+} \right)$$

For case when  $-z_- = z_+$

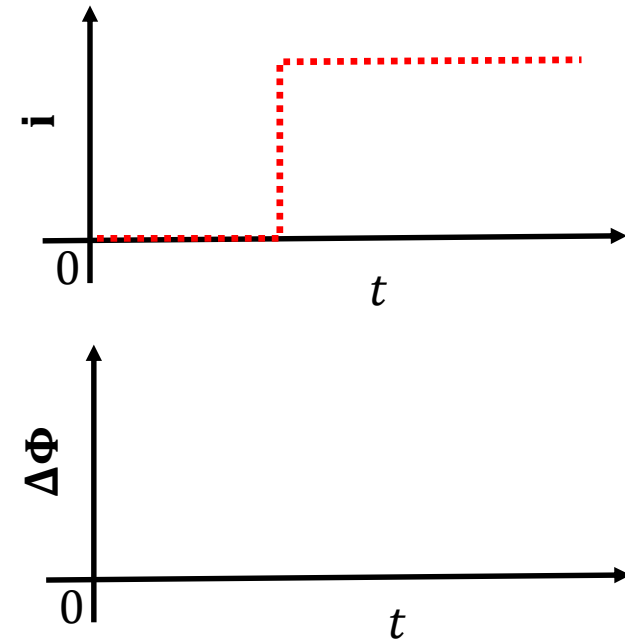
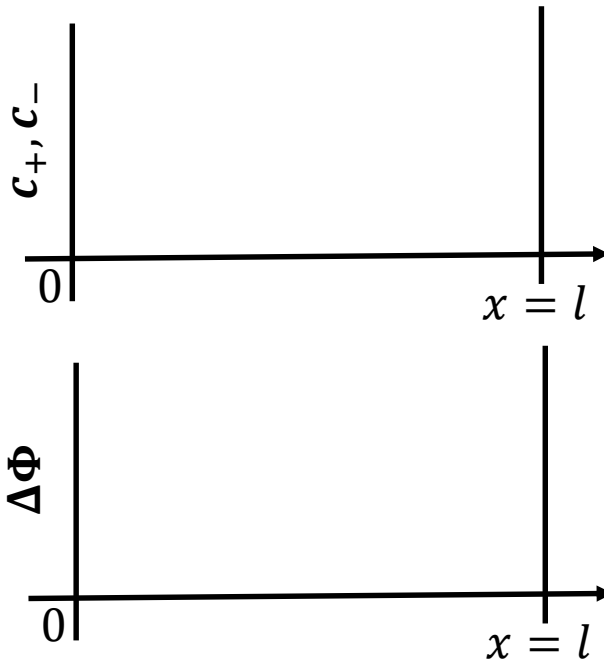
$$= \frac{F z D}{2} \left( \frac{1}{(1 - t_+)} + \frac{-1}{t_+} \right)$$

$$= -\frac{F z_+ D}{2} \left( \frac{1 - 2t_+}{(1 - t_+) t_+} \right)$$

# Pictorial Description: Board work



$c_+$  with  $x$  and  $t$   
 $c_-$  with  $x$  and  $t$   
 $i, \Phi$  with  $x$  and  $t$



# Parameters in Dilute Solution Theory



$D$  Given

$t_+$  Given

$$u_+ = \frac{D}{2RT(1 - t_+)}$$

$$u_- = \frac{D}{2RTt_+}$$

$$D_+ = u_+RT = \frac{D}{2(1 - t_+)}$$

$$D_- = u_-RT = \frac{D}{2t_+}$$

$$t_- = 1 - t_+$$

$$\mathbf{i} = -\kappa \nabla \Phi - F(z_+ D_+ + z_- D_-) \nabla c_+$$

$$\kappa = F^2 \sum_i z_i^2 u_i c_i$$

$$\kappa = F^2 \left( z_-^2 \frac{D}{2RTt_+} c_0 + z_+^2 \frac{D}{2RT(1 - t_+)} c_0 \right)$$

For case when  $-z_- = z_+$

$$= \frac{F^2 z^2 D c_0}{2RT} \left( \frac{1}{t_+} + \frac{1}{(1 - t_+)} \right)$$

$$= \frac{F^2 z^2 c_0}{2RT} \frac{D}{t_+(1 - t_+)}$$

$$F(z_+ D_+ + z_- D_-)$$

$$= F \left( z_+ \frac{D}{2(1 - t_+)} + z_- \frac{D}{2t_+} \right)$$

For case when  $-z_- = z_+$

$$= \frac{FzD}{2} \left( \frac{1}{(1 - t_+)} + \frac{-1}{t_+} \right)$$

$$= -\frac{Fz_+ D}{2} \left( \frac{1 - 2t_+}{(1 - t_+)t_+} \right)$$

# Typical Numbers!

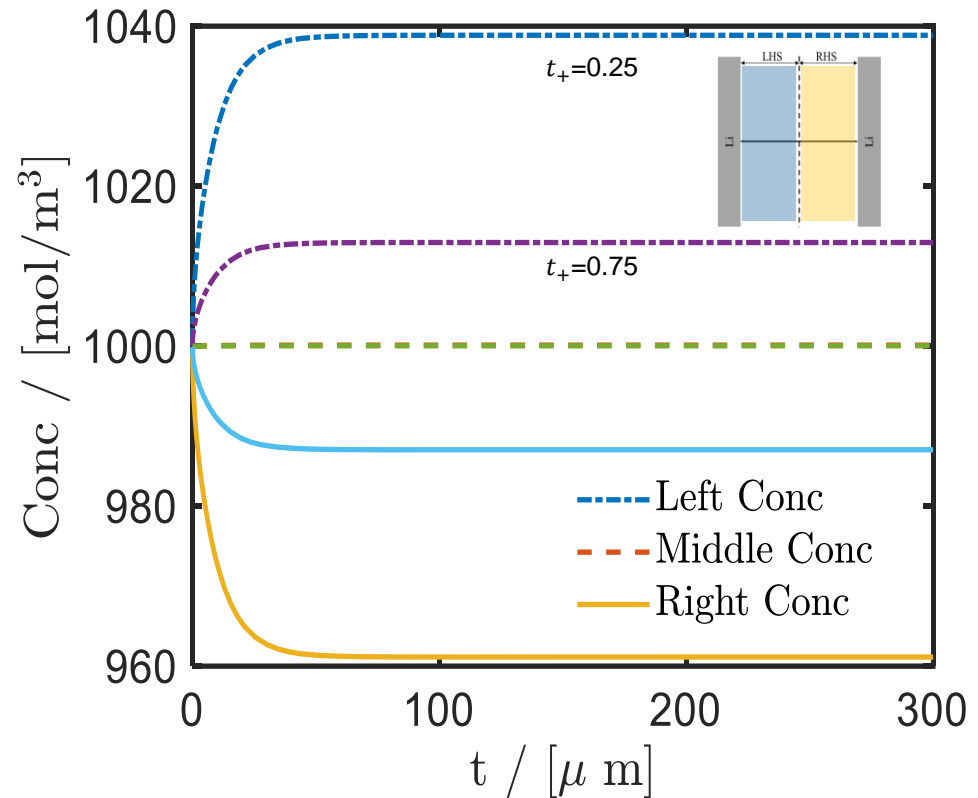
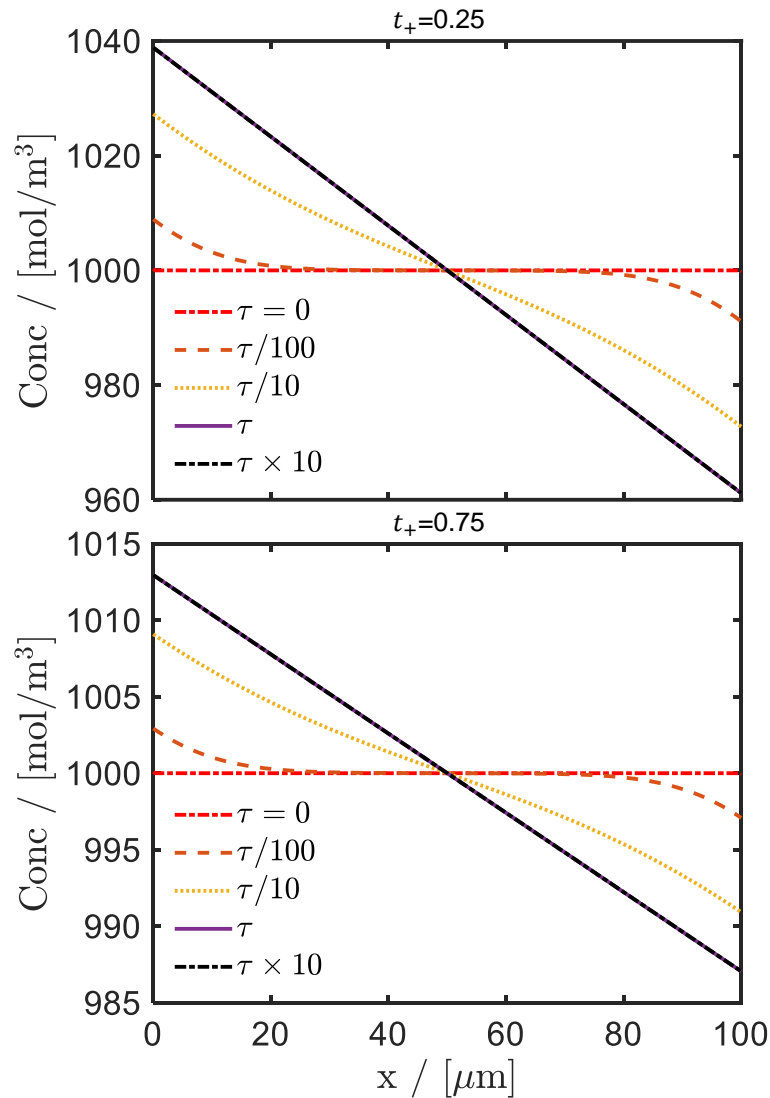


$z_+$	1 (e.g $\text{Li}^+$ )				
$z_-$	-1 (e.g $\text{PF}_6^-$ )				
$D$	1.00E-10 [ $\text{m}^2/\text{s}$ ]				
$t_+$	$\rightarrow 0$	$1/4$	$1/2$	$3/4$	$\rightarrow 1$
$t_-$	$\rightarrow 1$	$3/4$	$1/2$	$1/4$	$\rightarrow 0$
$u_+$	2.02E-14	2.69E-14	4.04E-14	8.07E-14	2.02E-10
$u_-$	2.02E-10	8.07E-14	4.04E-14	2.69E-14	2.02E-14
$D_+$	5.00E-11	6.67E-11	1.00E-10	2.00E-10	5.00E-07
$D_-$	5.00E-07	2.00E-10	1.00E-10	6.67E-11	5.00E-11
$\kappa$	$\rightarrow \infty$	1	0.75	1	$\rightarrow \infty$
$C_0$	1 molar				
$F(z_+D_+ + z_-D_-)$	-4.82E-02	-1.29E-05	0	1.29E-05	4.82E-02

# Transference No. 0.25 and 0.75



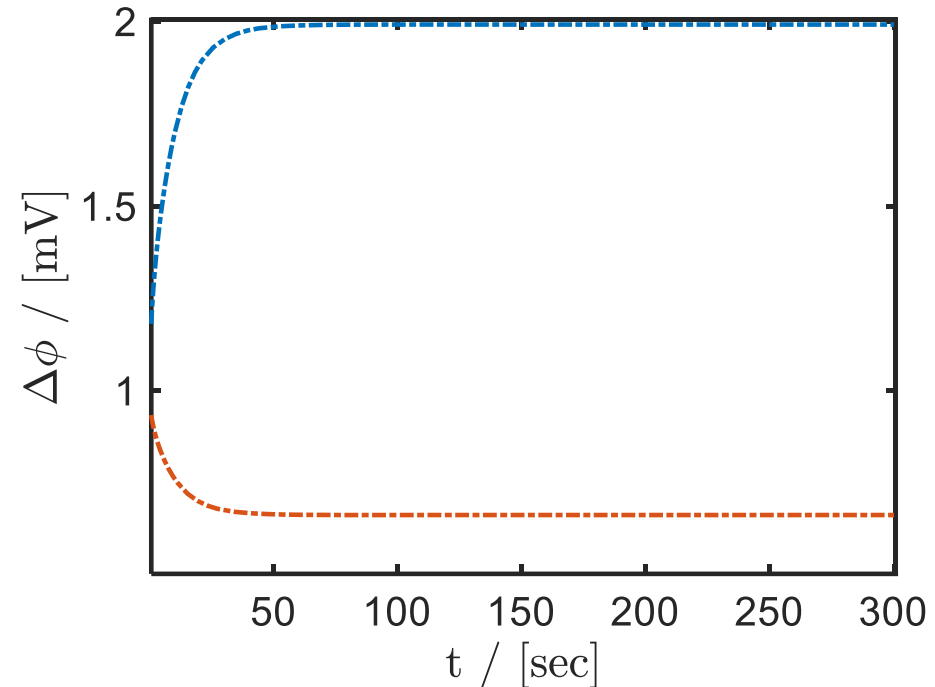
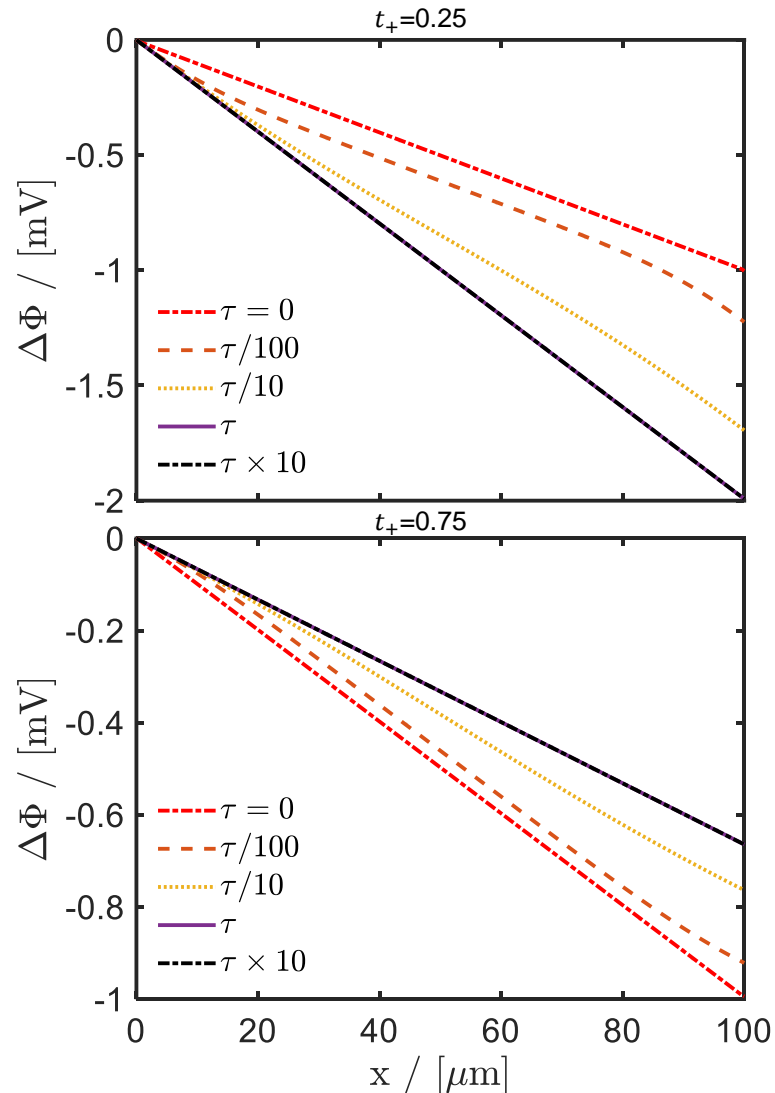
Development of concentration gradient with time:



# Transference No. 0.25 and 0.75



Potential drop across the separator with time:

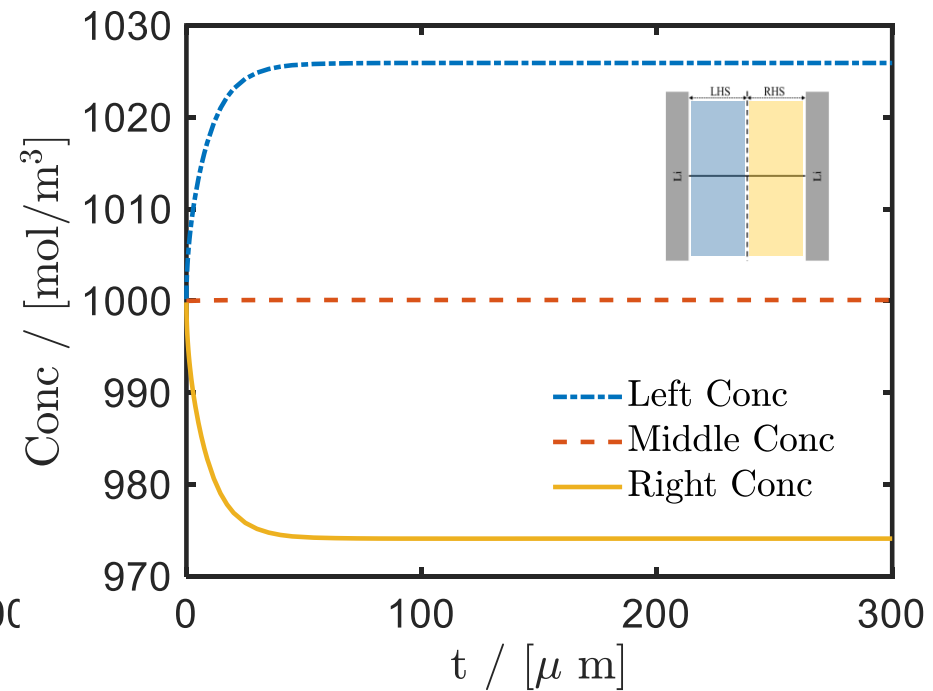
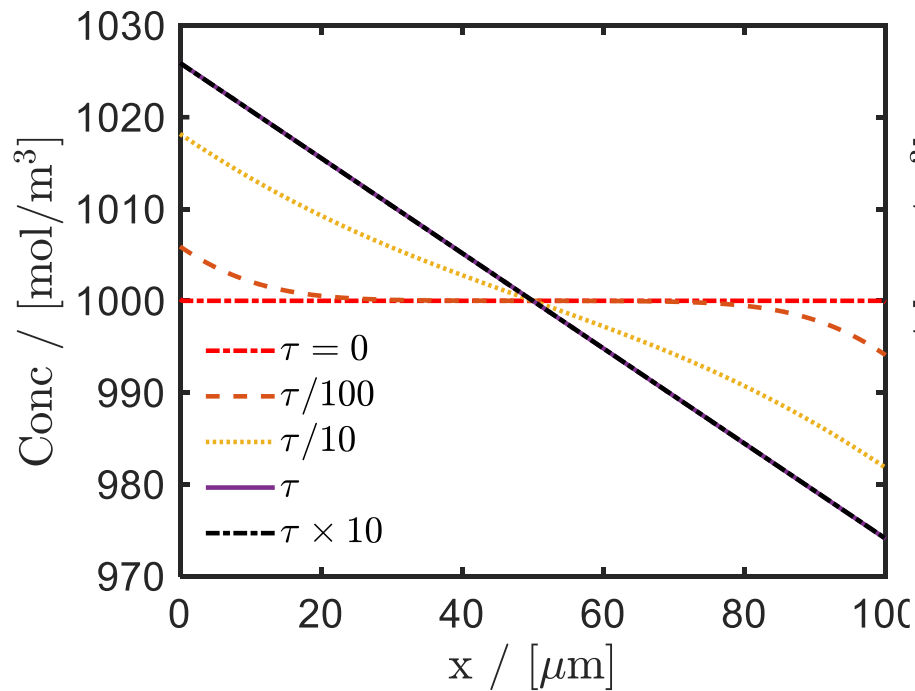




# Transference No. 0.5



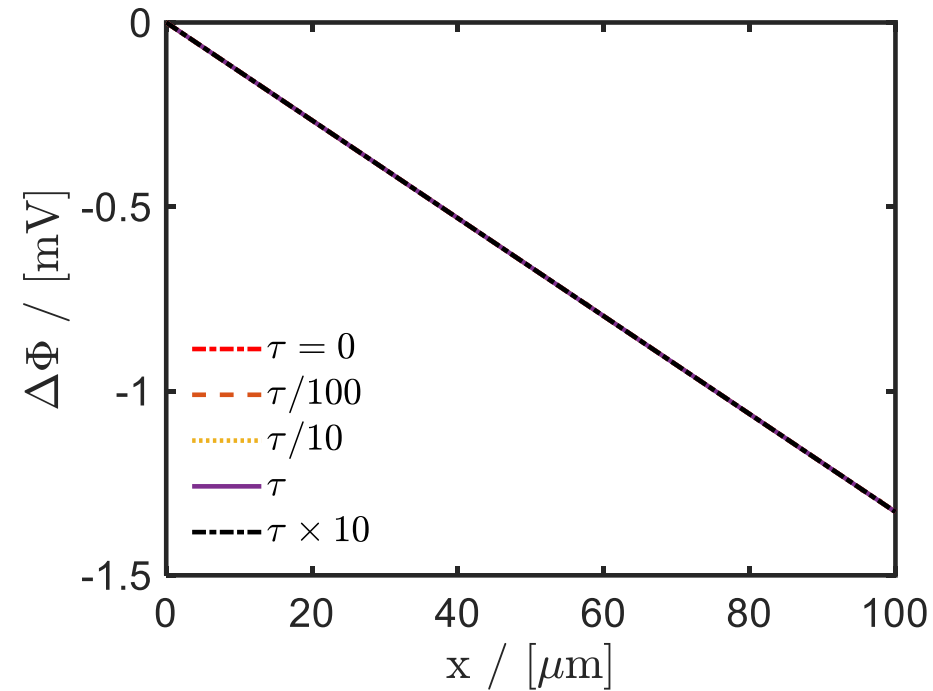
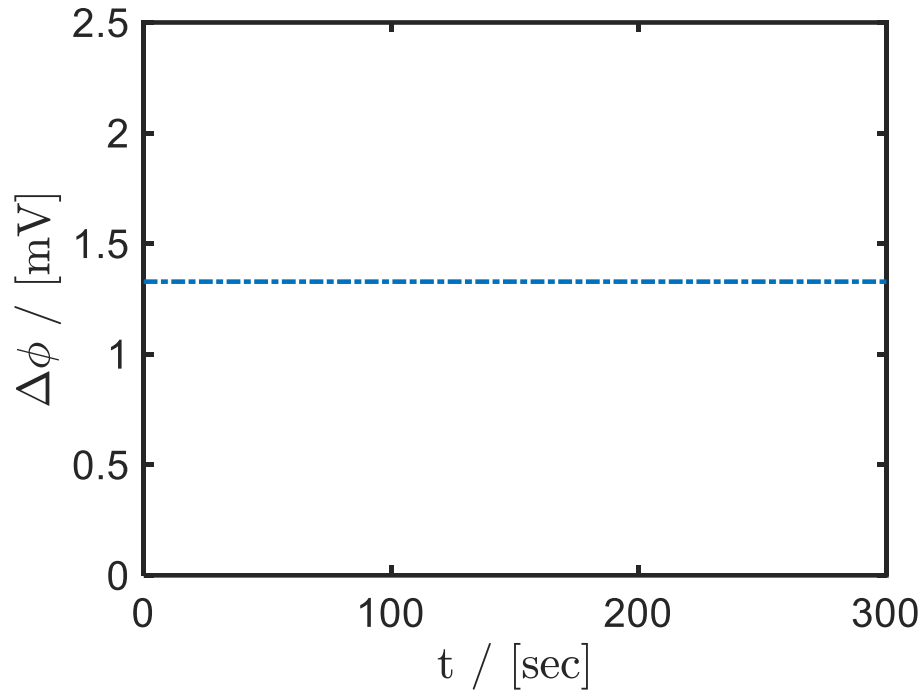
Development of concentration gradient with time:



# Transference No. 0.5

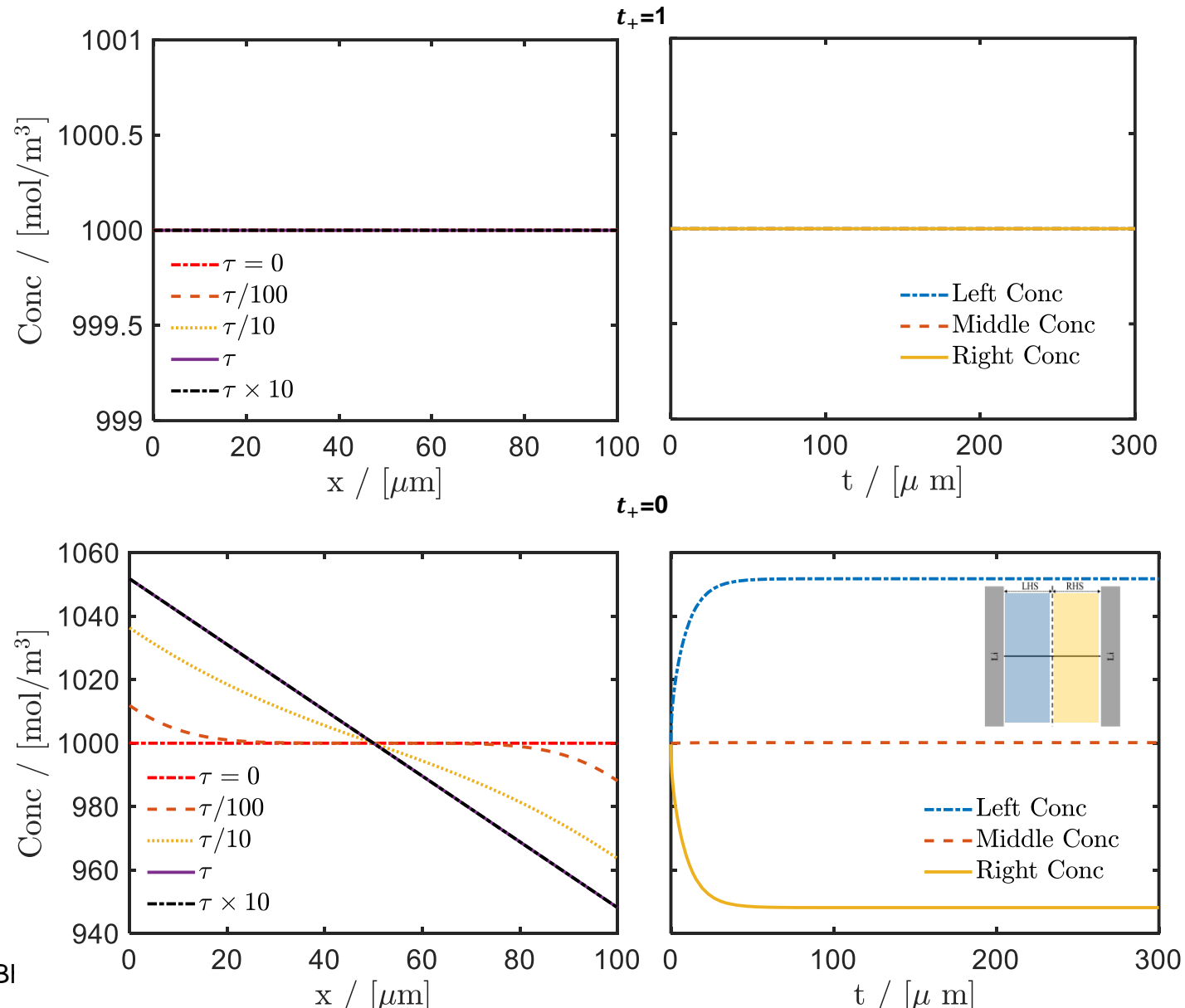


Potential drop across the separator with time:



# Transference No. 0 and 1

Development of concentration gradient with time:



# Excess Supporting Electrolyte



- ❑ Excess salt which is not involve in Rxn.
- ❑ What type of influence it will have?
  - ❑ There are more than 2 ionic species. E.g.  $\text{CuSO}_4$  and  $\text{H}_2\text{SO}_4$  in water

$$\mathbf{N}_i = \underbrace{-z_i u_i F c_i \nabla \phi}_{\text{migration}} \quad \underbrace{-D_i \nabla c_i}_{\text{diffusion}} \quad + \quad \underbrace{c_i \mathbf{v}}_{\text{convection}}.$$

- ❑ What can we say about  $N_i$  of nonreacting species.

- ❑ What is  $\nabla c_i$  of these species?

- ❑  $\nabla \phi$  drops down in the solution

$$\mathbf{N}_i = -\cancel{z_i u_i F c_i \nabla \phi} - D_i \nabla c_i + c_i \mathbf{v}$$

$$\frac{\partial c_i}{\partial t} + \mathbf{v} \cdot \nabla c_i = D_i \nabla^2 c_i.$$

$$\frac{\partial c_i}{\partial t} = D_i \nabla^2 c_i.$$

# Porous Media:



Highly porous



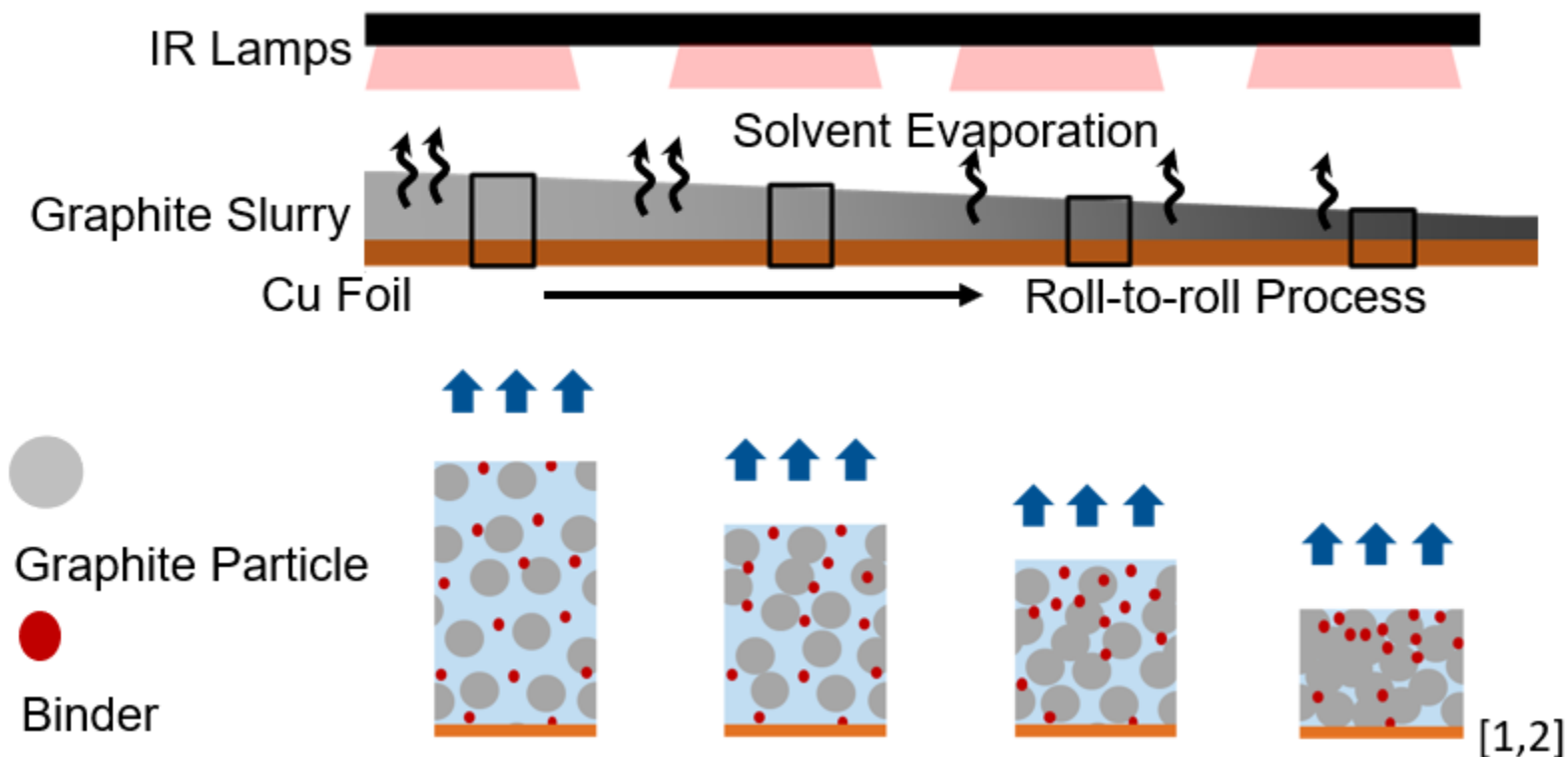
| shutterstock.com • 324598310

Not porous



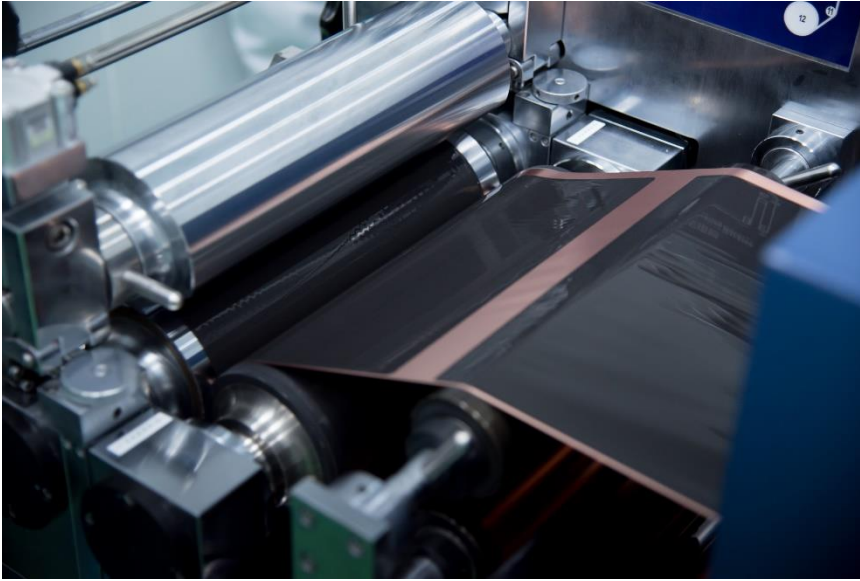
shutterstock.com • 1921723520

# How porous electrodes are made?

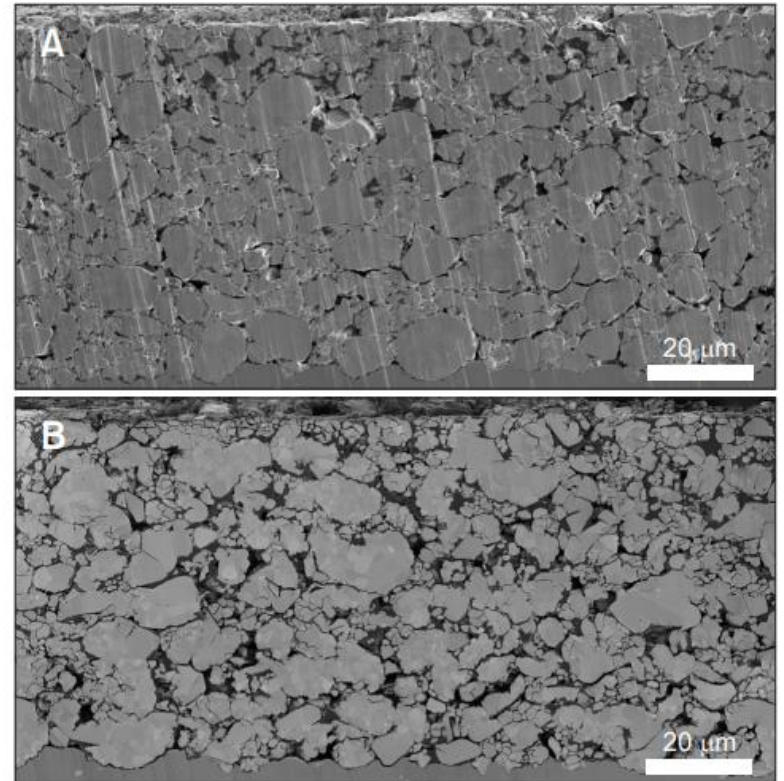
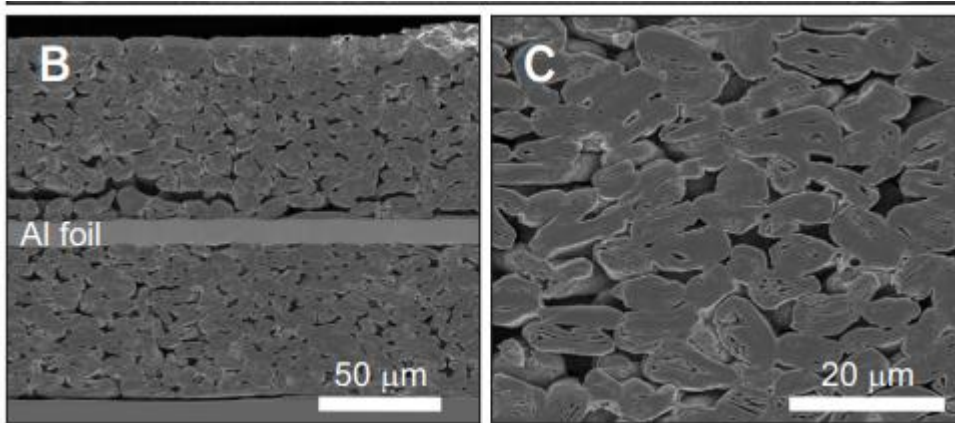


1. Muller et al., *J. Power Sources*, (2017)
2. Morasch et al., *J. Electrochem. Soc.*, (2018)

# Porous Electrode:



Cross section of battery electrode



<https://koreascience.kr/article/JAKO201720861274899.pdf>



# Porous Media: Separator vs Electrode



Dishwasher Plastic foam:  
Porous separator equivalent



<https://www.amazon.in/>

Dishwasher metal mesh, or  
metal foam  
Porous electrode equivalent



<https://www.recemat.nl/copper-foam/>

1. Which porous media can support electronic current?
2. Which porous media can provide double layer capacitance?





# Porous Electrode: Properties

- ☐ Volume Fractions:  $\varepsilon$
- ☐ Characteristic pore size
  - ☐ Pore size distribution
- ☐ Specific surface area:  $a \left[ \frac{m_{\text{BET}}^2}{m_{\text{electrode}}^3} \right]$
  
- ☐ Effective resistance ( $R_{\text{eff}}$ )
  - ☐ Tortuosity Factor ( $\tau$ )
  - ☐ McMullin number ( $N_m$ )
  
- ☐ Effective conductivity ( $\kappa_{\text{eff}}$ )
- ☐ Effective diffusivity ( $D_{\text{eff}}$ )

# Porous Electrode:



## Volume Fractions: $\varepsilon$

1. Definition
2. Void volume fraction (Porosity)
  1. Electrolyte volume fraction ( $\varepsilon_{\text{elyt}}$ )
3. Solid volume fractions
  1. Active material volume fraction ( $\varepsilon_{\text{AM}}$ )
  2. Binder (polymer) volume fraction ( $\varepsilon_{\text{Binder}}$ )
  3. Conductive carbon volume fraction ( $\varepsilon_{\text{CC}}$ )
4.  $\Sigma \varepsilon_i = 1$
5. For fuel cell void volume fraction and ionomer volume fractions both exists.
  1. Void volume fraction = mostly gas transport
  2. Ionomer volume fraction: mostly ion transport

Meaning of  $\varepsilon = 0$ , examples?

Meaning of  $\varepsilon = 1$ , examples?



# Porous Electrode:

## Specific Surface Area

1. Unit of  $\left[ \frac{\text{m}_{\text{BET}}^2}{\text{m}_{\text{superficial}}^3} \right]$
2. '*Electroactive*' surface area/volume element in the electrode.
  1. Should it be same for reaction and double layer capacitance?
  2. Conductive carbon based area, where should it be used?

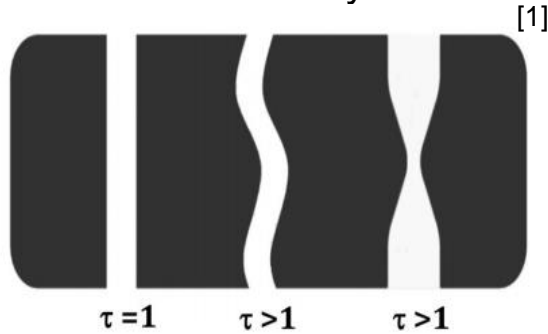
$$a \equiv \frac{\text{interfacial area}}{\text{superficial volume}}.$$

$$a = \frac{(\text{number of spheres})4\pi r^2}{\text{volume}} = \frac{\frac{V(1-\varepsilon)}{4/3\pi r^3}4\pi r^2}{V} = \frac{3(1-\varepsilon)}{r}.$$

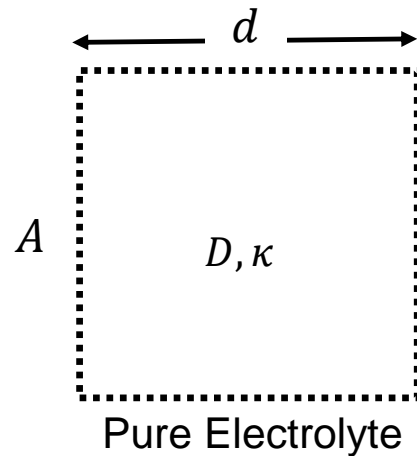
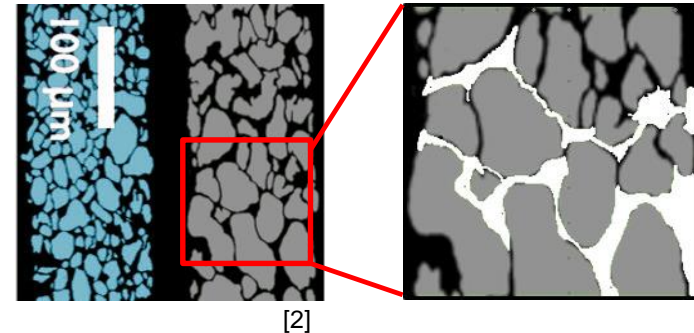
# Porous Electrode:



Tortuosity

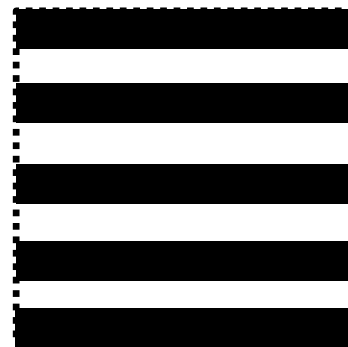


Tortuosity For Porous Media



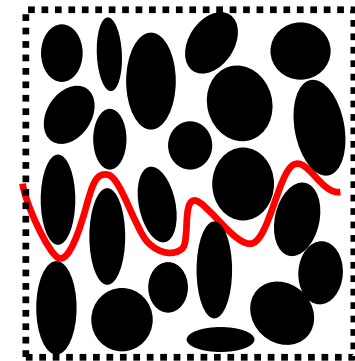
$$D_{\text{eff}} = D \quad \kappa_{\text{eff}} = \kappa$$

$$R_{\text{ion}} = d/(A\kappa_{\text{eff}})$$



$$D_{\text{eff}} = D\varepsilon \quad \kappa_{\text{eff}} = \kappa\varepsilon$$

$$R_{\text{ion}} = d/(A\kappa_{\text{eff}})$$



$$D_{\text{eff}} = D \frac{\varepsilon}{\tau} \quad \kappa_{\text{eff}} = \kappa \frac{\varepsilon}{\tau}$$

$$R_{\text{ion}} = d/(A\kappa_{\text{eff}})$$

1. Cooper et al., *J. Power Sources*, (2014)

2. Smith et al., *J. Electrochem. Soc.*, (2009).

# Porous Electrode:



How to measure the porosity by using mass of the electrode only?

Does tortuosity depend on porosity?

Is tortuosity a geometric factor?

# Porous Electrode:



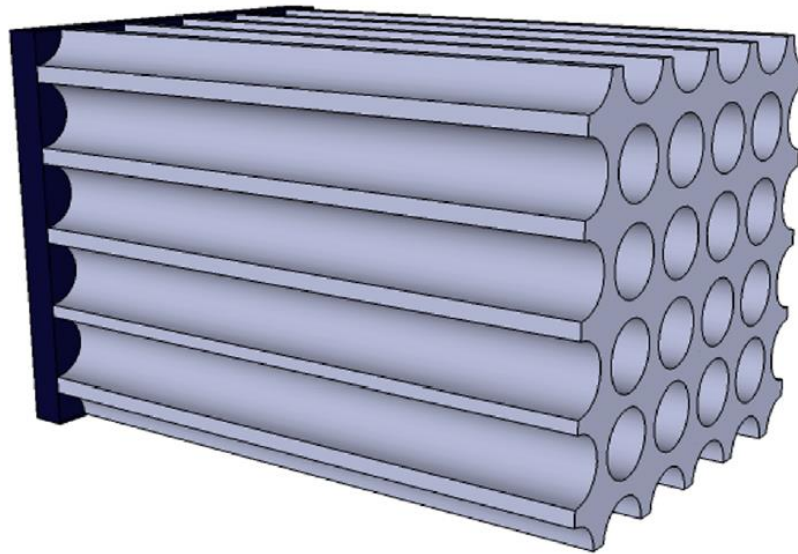
## McMullin Number

1. Ratio of tortuosity to porosity ( $N_m = \tau/\varepsilon_{\text{elyt}}$  or  $N_m = \tau/\varepsilon_{\text{ionomer}}$ )
2. Used when the deconvolution of porosity and tortuosity is not straight forward
  1. E.g. fuel cell electrode where ionomer volume fraction may not be known exactly.

# Ideal Porous Electrode

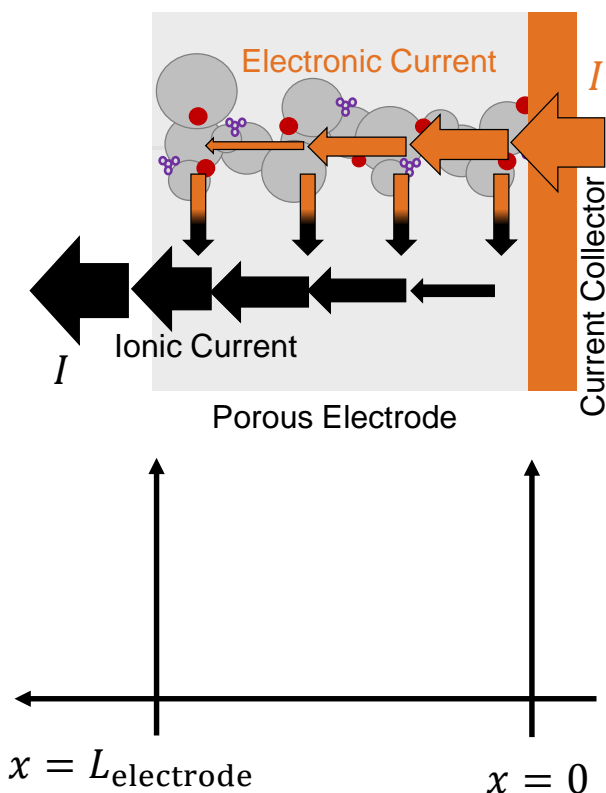


Tortuosity = 1, straight pores with uniform cross section area



**Figure 5.1** Straight pores of an idealized porous electrode.

# Transport in Porous Media



$$i_1(x = 0) = \frac{I}{A} \left[ \frac{A}{m_{x-\text{sec}}^2} \right]$$

A cross section area (x-sec)

$$i_2(x = L) = \frac{I}{A}$$

$$i_1(x) + i_2(x) = \frac{I}{A}$$

Derivative wrt x.

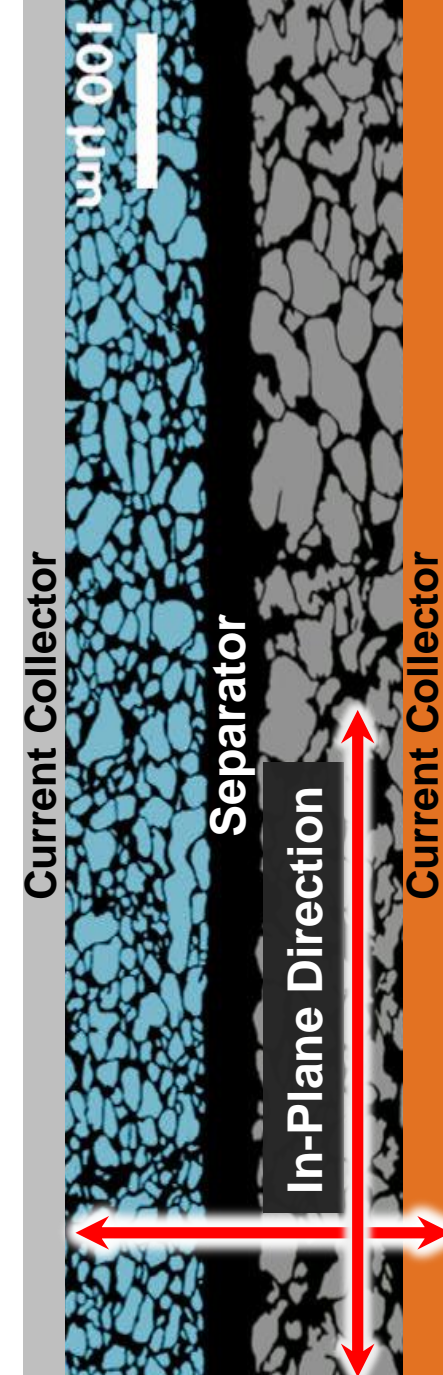
$$\nabla \cdot i_1(x) + \nabla \cdot i_2(x) = 0$$

What does  $\nabla \cdot i_1(x)$  represent?

- Reaction and double layer current
- Source or sink terms

$$\nabla \cdot i_1(x) = -ai_n$$

$$\nabla \cdot i_2(x) = \underbrace{ai_n}_{\left[ \frac{m_{\text{BET}}^2}{m^3} \times \frac{A}{m_{\text{BET}}^2} = \frac{A}{m^3} \right]}$$





# Transport in Porous Media



Analogy of flow in pipe.

# Species Balance Equations



For electrolyte only (no porous media)

$$\frac{\partial c_i}{\partial t} = -\nabla \cdot \mathbf{N}_i + \mathcal{R}_i.$$

$$\mathbf{N}_i = \underbrace{-z_i u_i F c_i \nabla \phi}_{\text{migration}} \quad \underbrace{-D_i \nabla c_i}_{\text{diffusion}} \quad + \quad \underbrace{c_i \mathbf{v}}_{\text{convection}}.$$

For porous media:

$$\frac{\partial \epsilon c_i}{\partial t} = -\nabla \cdot \mathbf{N}_i + \mathcal{R}_i.$$

$$\mathbf{N}_i = -\epsilon D_i \nabla c_i - \epsilon z_i u_i F c_i \nabla \phi + \epsilon c_i \mathbf{v},$$

$$\mathcal{R}_i = a j_n, \quad j_n = -\frac{s_i}{nF} i_n.$$

$$\frac{\partial \epsilon c_i}{\partial t} = -\nabla \cdot \mathbf{N}_i - a \frac{s_i}{nF} i_n = -\nabla \cdot \mathbf{N}_i - \frac{s_i}{nF} \nabla \cdot \mathbf{i}_2.$$

# EIS of a symmetric cell



Demo

# Next



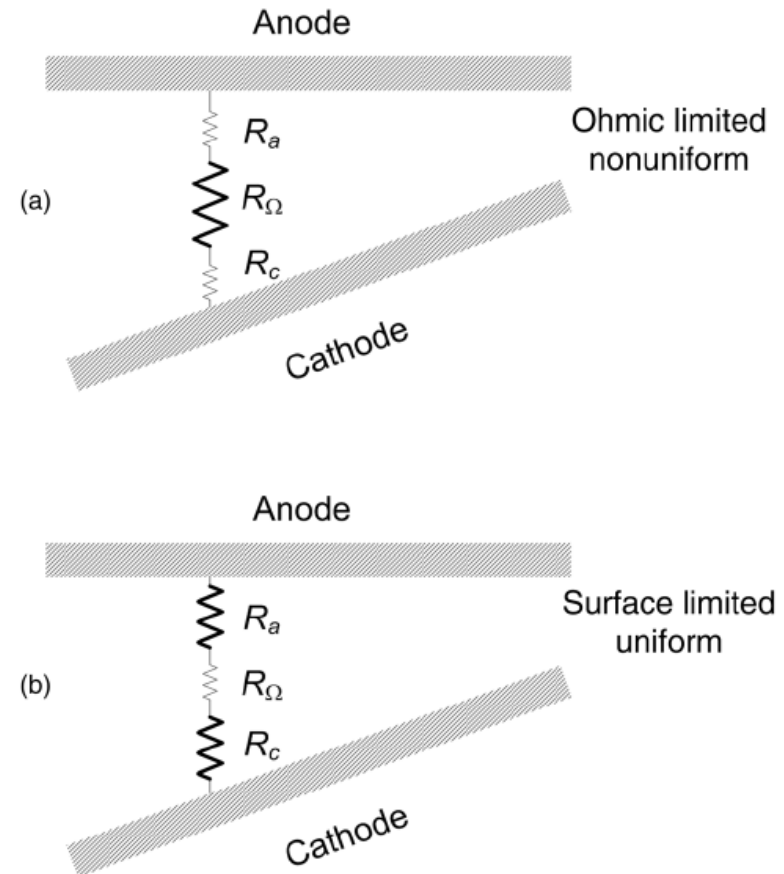
Current distribution (4.7 in Fuller Book)

# Current Distribution



*“Current distribution refers to how the current density varies across the surface of an electrode.”<sup>1</sup>*

- Uniform current density
- Uniform deposition vs nonuniform deposition
- Relative weightage of ohmic and reaction resistance



**Figure 4.11** Ohmic and charge-transfer (surface) resistances.

# Current Distribution: No Conc Gradient



Ohmic resistance:  $R_{\Omega} = \frac{L}{A\kappa}$

Charge transfer resistance:  $R_{ct} = \frac{1}{A} \frac{d\eta_s}{di}$

Wagner Number =  $Wa = \frac{R_{ct}}{R_{\Omega}} = \frac{\kappa}{L} \frac{d\eta_s}{di}$ ,

BV Kinetics

$$i = i_o \left[ \exp \frac{\alpha_a F}{RT} \eta_s - \exp \frac{-\alpha_c F}{RT} \eta_s \right],$$

Wa

Linear kinetics :  $Wa = \frac{\kappa}{L_c} \frac{RT}{F} \frac{1}{i_o(\alpha_a + \alpha_c)}$ .

Tafel kinetics :  $Wa = \frac{RT\kappa}{FL_c} \frac{1}{|i_{avg}| \alpha_c}$ .

- $Wa \gg 1$  Kinetics dominate Uniform current density
- $W \rightarrow 0$  Ohmic resistance dominate, Non-uniform current density

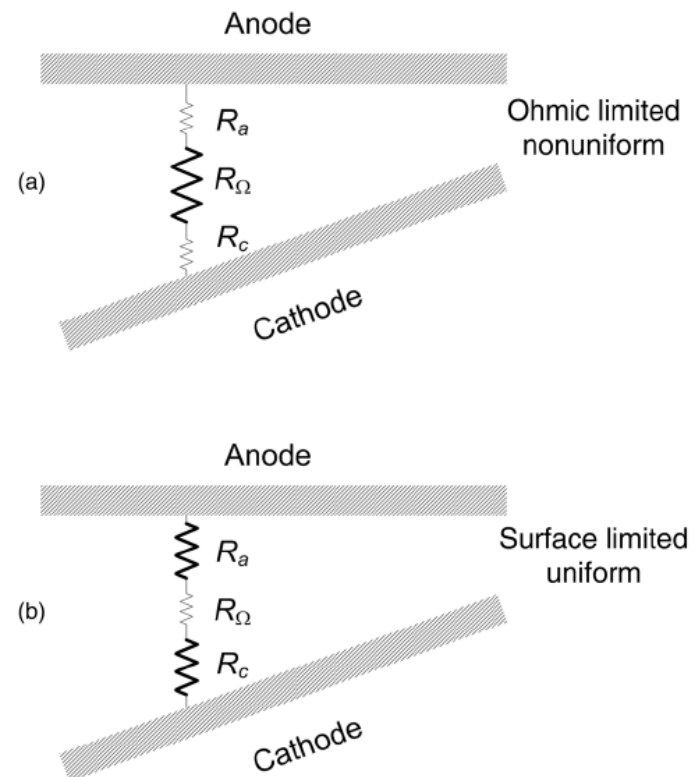


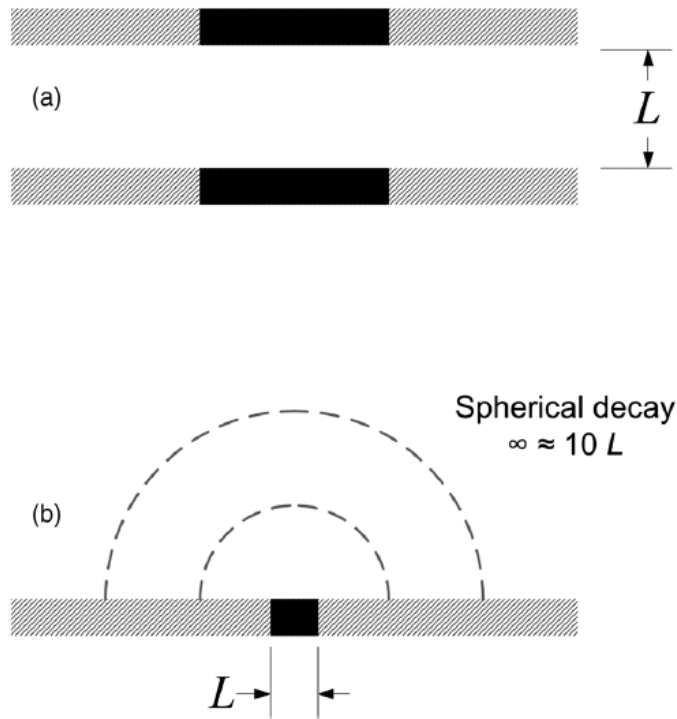
Figure 4.11 Ohmic and charge-transfer (surface) resistances.

# Influencing factors for $Wa$



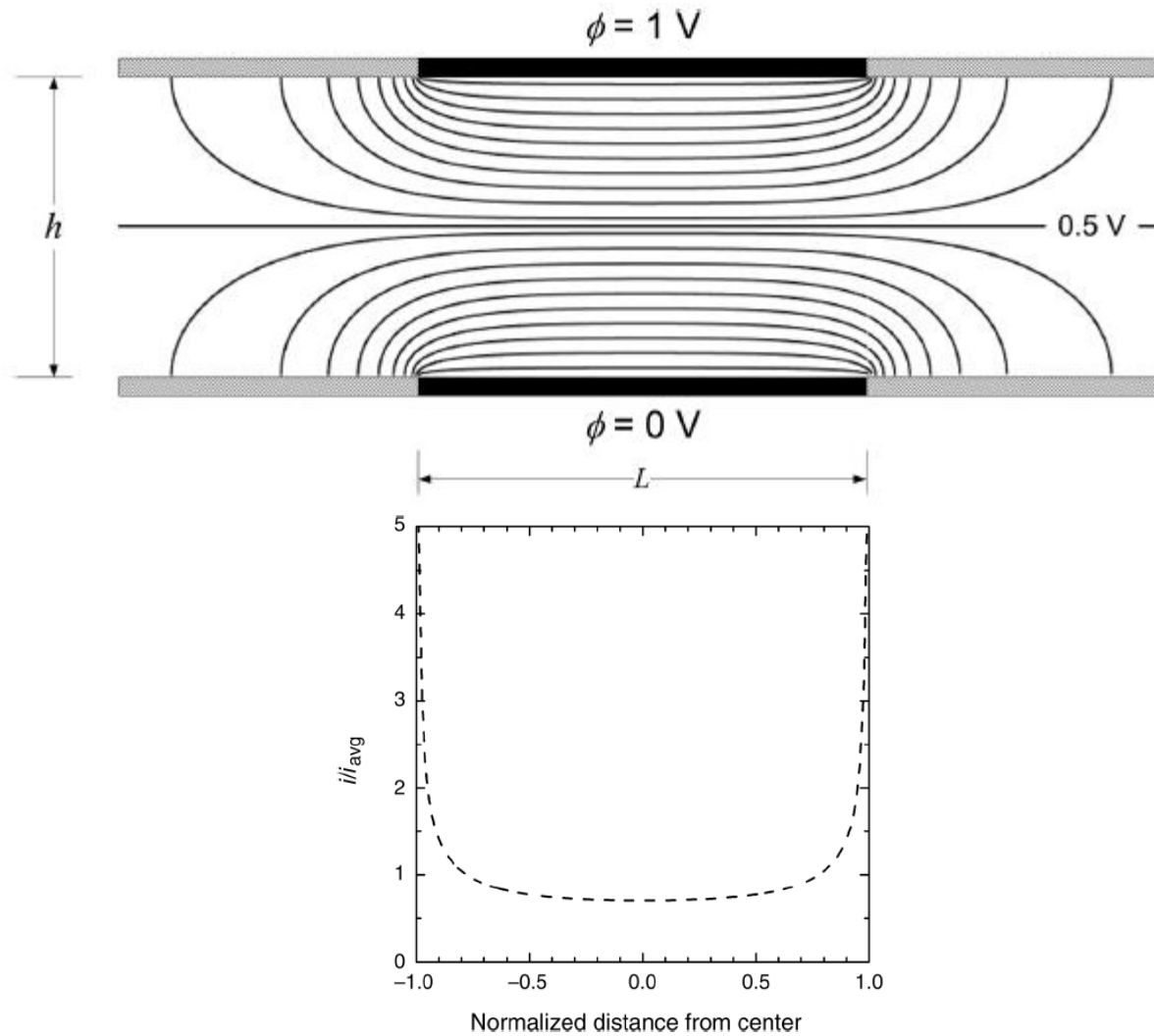
How to change/influence the  $Wa$ ?

Conductivity, Length scale, Exchange current density, Overall current?



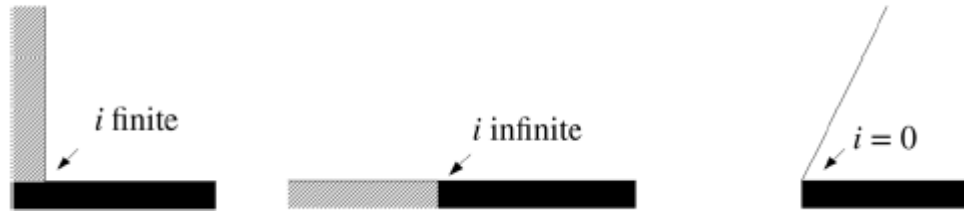
**Figure 4.12** Characteristic length.

# Primary Current Distribution: $Wa=0$

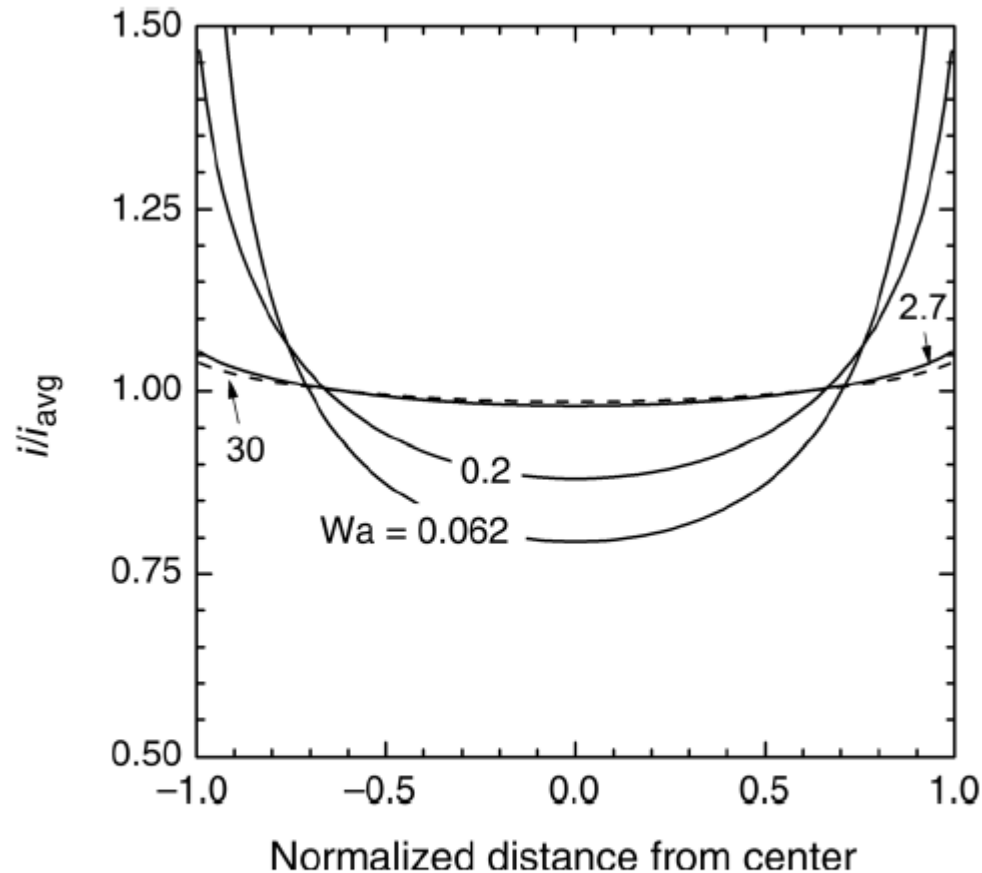




# Primary Current Distribution



# Wa vs current density distribution



**Figure 4.16** Primary current distribution between two parallel plate electrodes. The distance between the electrodes ( $h$ ) is 1.25 times the electrode width ( $L$ ). Geometry and conductivity.

# Reference:



- ☐ Fuller and Harb
- ☐ Newman and xxx
- ☐ Bockris and Reddy