

# DC to AC converters

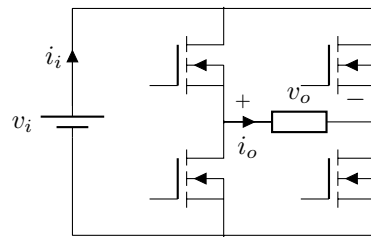
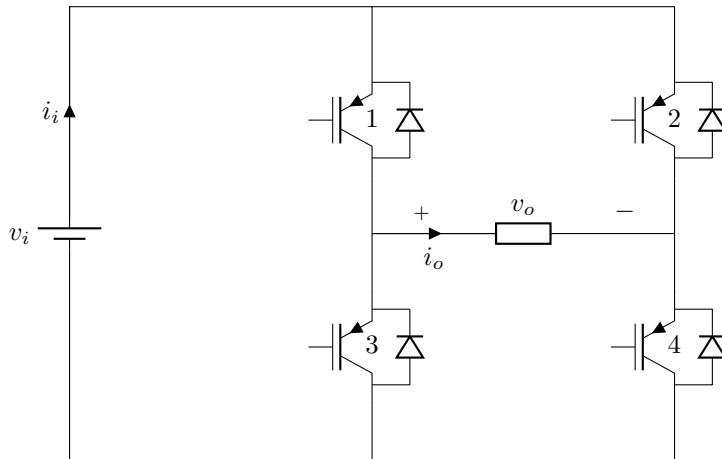
Diego Trapero

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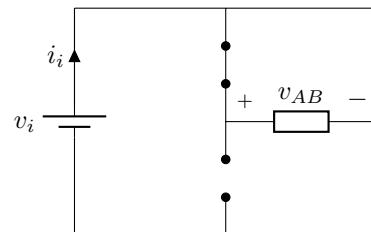
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# 1 DC to AC converters

## 1.1 Full bridge circuit

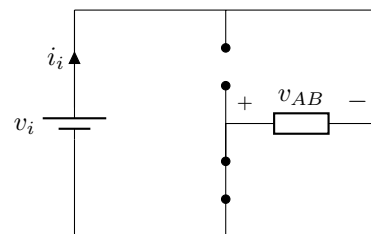


**Direct polarization of the load. S1 and S4**



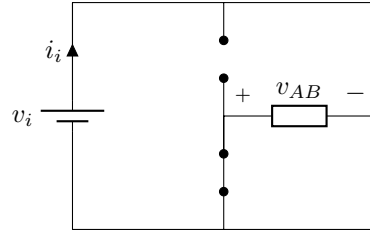
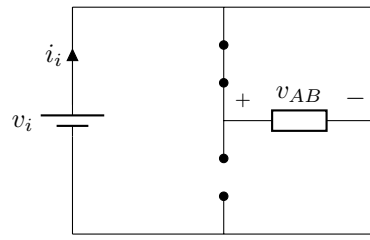
$$v_{AB} = V_i$$

**Inverse polarization of the load. S2 and S3**



$$v_{AB} = -V_i$$

**Grounding. S1 and S3 OR S2 and S4**



$$v_{AB} = 0$$

**Shorting the source.** The two switches of a branch cannot be closed at the same time because it would short the source. That's the reason why same-branch switch control signals have to be complementary:

$$S1 = \bar{S}3$$

$$S2 = \bar{S}4$$

**$i_o$  and  $v_o$  phase shift** If a phase shift  $\varphi$  exists between output voltage and current, the diodes in the bridge start conducting the current in some moments of the period.

**RLC/RL Load** If an RLC or RL load is connected to the inverter

- $i_o$  can be considered perfectly sinusoidal as an analysis hypothesis.
- A phase-shift  $\varphi$  may appear and the diodes would conduct current.

## 2 Non modulated control

### 2.1 Square wave control

**Control signals**

**Conducting devices** When  $i_o$  is shifted  $\varphi$  from the voltage  $v_o$ :

- if  $v_o$  and  $i_o$  have the same sign, the IGBT are conducting the current.
- if  $v_o$  and  $i_o$  have the different sign, the diodes are conducting the current.

The 4 regions are

1. D4, D1

2. S1, S4
3. D1, D3
4. S1, S4

### Output current

- when the IGBTs are conducting, current is leaving the source,  $i_i > 0$ .
- when the diodes are conducting, current is entering the source,  $i_i < 0$ .

The output current mean value can be calculated with the following integral:

$$\begin{aligned}
 \bar{i}_i &= \frac{1}{T} \int_t^{t+T} A \sin(\omega t) d\omega t \\
 &= \frac{A}{\pi} \left[ -\cos(\omega t) \right]_{\pi-\varphi}^{-\varphi} \\
 &= \frac{A}{\pi} \left[ -\cos(\pi - \varphi) + \cos(-\varphi) \right] \\
 &= \frac{A}{\pi} \left[ -(\cos(\pi) \cos(\varphi) + \sin(\pi) \sin(\varphi)) + \cos(-\varphi) \right] \\
 &= \frac{A}{\pi} \left[ \cos(\varphi) + \cos(-\varphi) \right] \\
 &= \frac{2A}{\pi} \cos(\varphi)
 \end{aligned}$$

## 2.2 Phase shift control

### Control signals

**Conducting devices** When  $i_o$  is shifted  $\varphi$  from the voltage  $v_o$ :

- if  $v_o \neq 0$ ,  $v_o$  and  $i_o$  have the same sign, the IGBT are conducting the current.
- if  $v_o \neq 0$ ,  $v_o$  and  $i_o$  have the different sign, the diodes are conducting the current.
- if  $v_o = 0$ , a pair diode-IGBT is conducting the current.

The 6 regions are

1. diodes
2. igbts
3. S1 and D2
4. diodes

5. igbts
6. D4 and S3

### Output current

- when the IGBTs are conducting, current is leaving the source,  $i_i > 0$ .
- when the diodes are conducting, current is entering the source,  $i_i < 0$ .
- when a IGBT-diode pair is conducting, no current leaves or enter the source,  $i_i = 0$ .

## 3 PWM control

Modulation parameters:

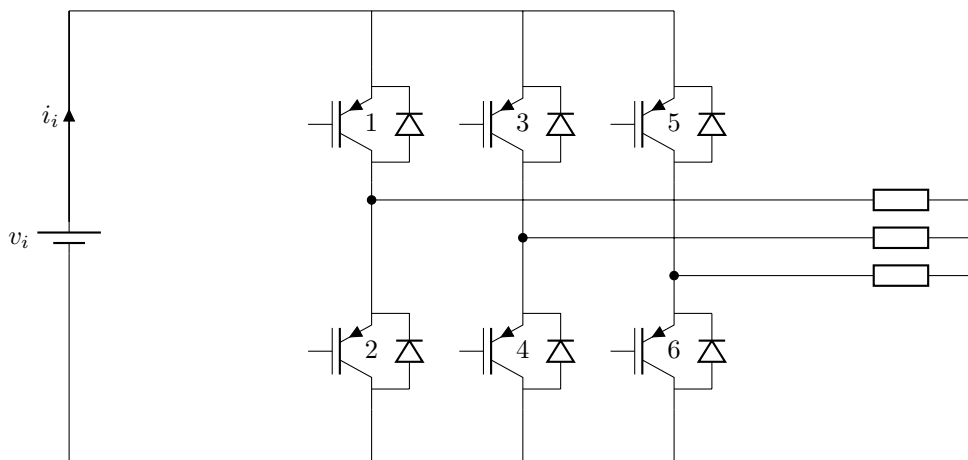
$$m_a = \frac{V_{sin}}{V_{tri}} < 1$$

$$m_f = \frac{T_{sin}}{T_{tri}} = \frac{f_{tri}}{f_{sin}} > 1$$

### 3.1 Unipolar PWM

### 3.2 Bipolar PWM

## 4 Triphasic inverters



### 4.1 Non modulated control

Control

- Same-branch switches are complementary.
- Each switch conducts for 180 degrees and then opens for other 180 degrees.
- Branches are phase-shifted 120 degrees between them.

### 4.2 PWM control

Control

## 5 Inverter amplitudes tables

**PWM Sinusoidal Unipolar. Normalized amplitudes,  $V_n/V_{DC}$**

$m_a$	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
$n = 1$	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
$n = 2mf + -1$	0.10	0.19	0.27	0.33	0.36	0.37	0.35	0.31	0.25	0.18
$n = 2mf + -3$	0.00	0.00	0.01	0.02	0.04	0.07	0.10	0.14	0.18	0.21

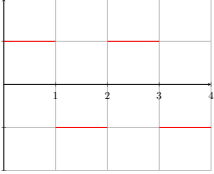
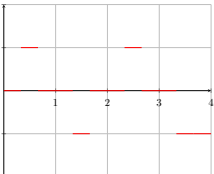
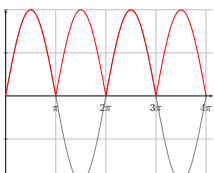
**PWM Sinusoidal Bipolar. Normalized amplitudes,  $V_n/V_{max}$**

$m_a$	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
$n = 1$	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
$n = mf$	1.27	1.24	1.20	1.15	1.08	1.01	0.92	0.82	0.71	0.60
$n = mf + -2$	0.00	0.02	0.03	0.06	0.09	0.13	0.17	0.22	0.27	0.32

**PWM Sinusoidal Triphasic. Normalized amplitudes,  $V_n/V_{DC}$  (line tension)**

$m_a$	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
$n = 1$	0.087	0.173	0.260	0.346	0.433	0.520	0.606	0.693	0.779	0.866
$n = mf + -2$	0.003	0.013	0.030	0.053	0.801	0.114	0.150	0.190	0.232	0.275
$n = 2mf + -1$	0.086	0.165	0.232	0.282	0.313	0.321	0.307	0.272	0.221	0.157

**Fourier series table**

Function	Fourier Series
	$\frac{4}{\pi} \left( \frac{\sin(t)}{1} + \frac{\sin(3t)}{3} + \frac{\sin(5t)}{5} + \dots \right)$
	$\frac{4}{\pi} \left( \frac{\sin(t) \cos(\beta)}{1} + \frac{\sin(3t) \cos(3\beta)}{3} + \frac{\sin(5t) \cos(5\beta)}{5} + \dots \right)$
	$\frac{2}{\pi} - \frac{4}{\pi} \left( \frac{\sin(t)}{1 \cdot 3} + \frac{\sin(2t)}{3 \cdot 5} + \frac{\sin(3t)}{5 \cdot 7} + \dots \right)$