

An aerial view of a city, likely King's Landing from Game of Thrones, in a state of complete ruin. A large, ornate building with a dark, ribbed dome is the central focus, its structure crumbling and debris falling. The surrounding city is a sea of rubble, with smoke rising from the wreckage. In the background, a body of water and distant mountains are visible under a cloudy sky.

# CSC417 Physics-Based Animation



# Rigid Body Simulation





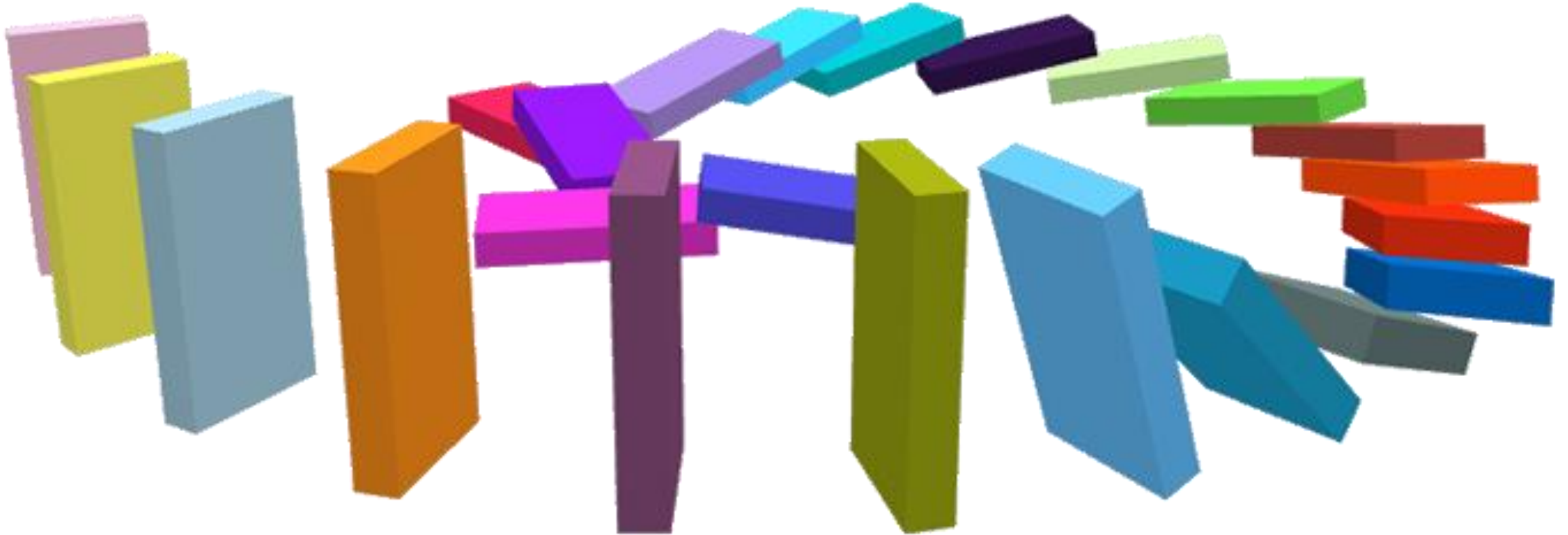


**Questions from Previous Lecture ?**

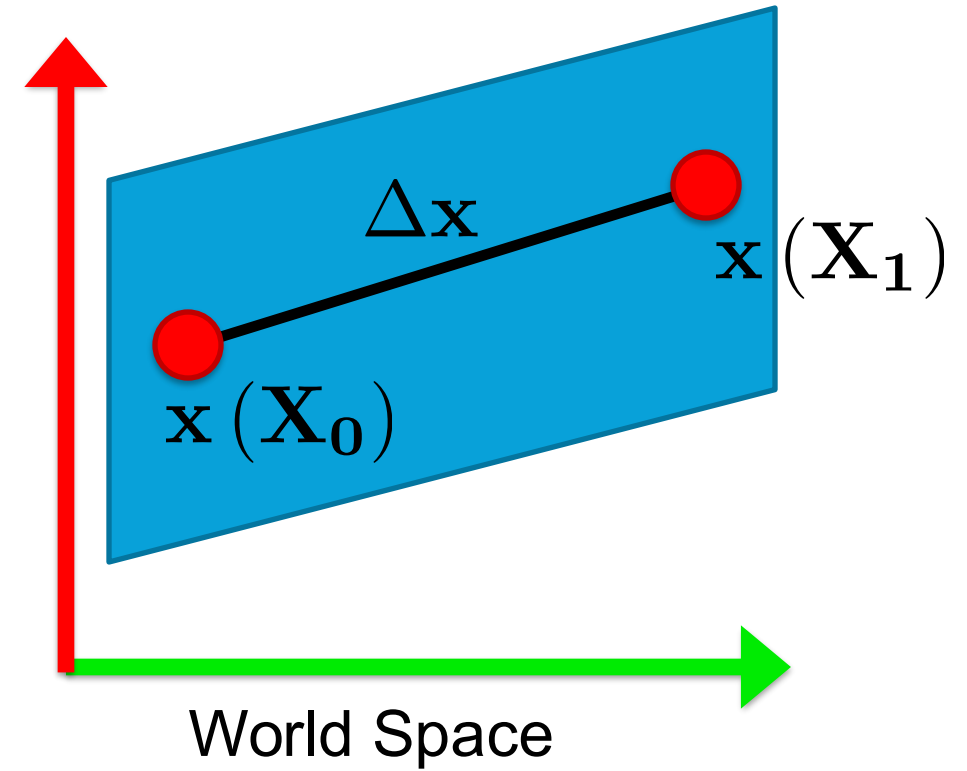
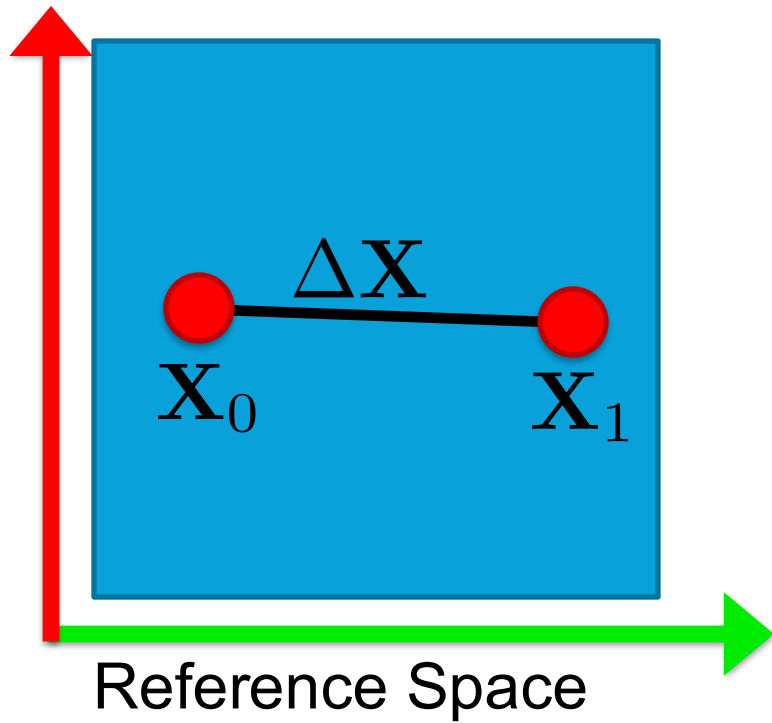




# What Makes an Object Rigid ?



# What Makes an Object Rigid ?



$$\Delta \mathbf{x} \approx \cancel{\mathbf{x}(\mathbf{Y})} + \underbrace{\frac{\partial \mathbf{x}}{\partial \mathbf{X}}}_{\text{deformation gradient } \mathbf{F}} \Delta \mathbf{X} - \cancel{\mathbf{x}(\mathbf{X}_0)}$$



# What Makes an Object Rigid ?

Strain  $\Delta \mathbf{x}^T \Delta \mathbf{x} - \Delta \mathbf{X}^T \Delta \mathbf{X}$

$$\Delta \mathbf{X}^T \mathbf{F}^T \mathbf{F} \Delta \mathbf{X} - \Delta \mathbf{X}^T \Delta \mathbf{X}$$

Right Cauchy Green Deformation

$$\Delta \mathbf{X}^T \underbrace{(\mathbf{F}^T \mathbf{F} - \mathbf{I})}_{\text{Green Lagrange Strain}} \Delta \mathbf{X} = \mathbf{0}$$

Green Lagrange Strain





# What Makes an Object Rigid ?

$$\Delta \mathbf{X}^T (\mathbf{F}^T \mathbf{F} - \mathbf{I}) \Delta \mathbf{X} = \mathbf{0}$$

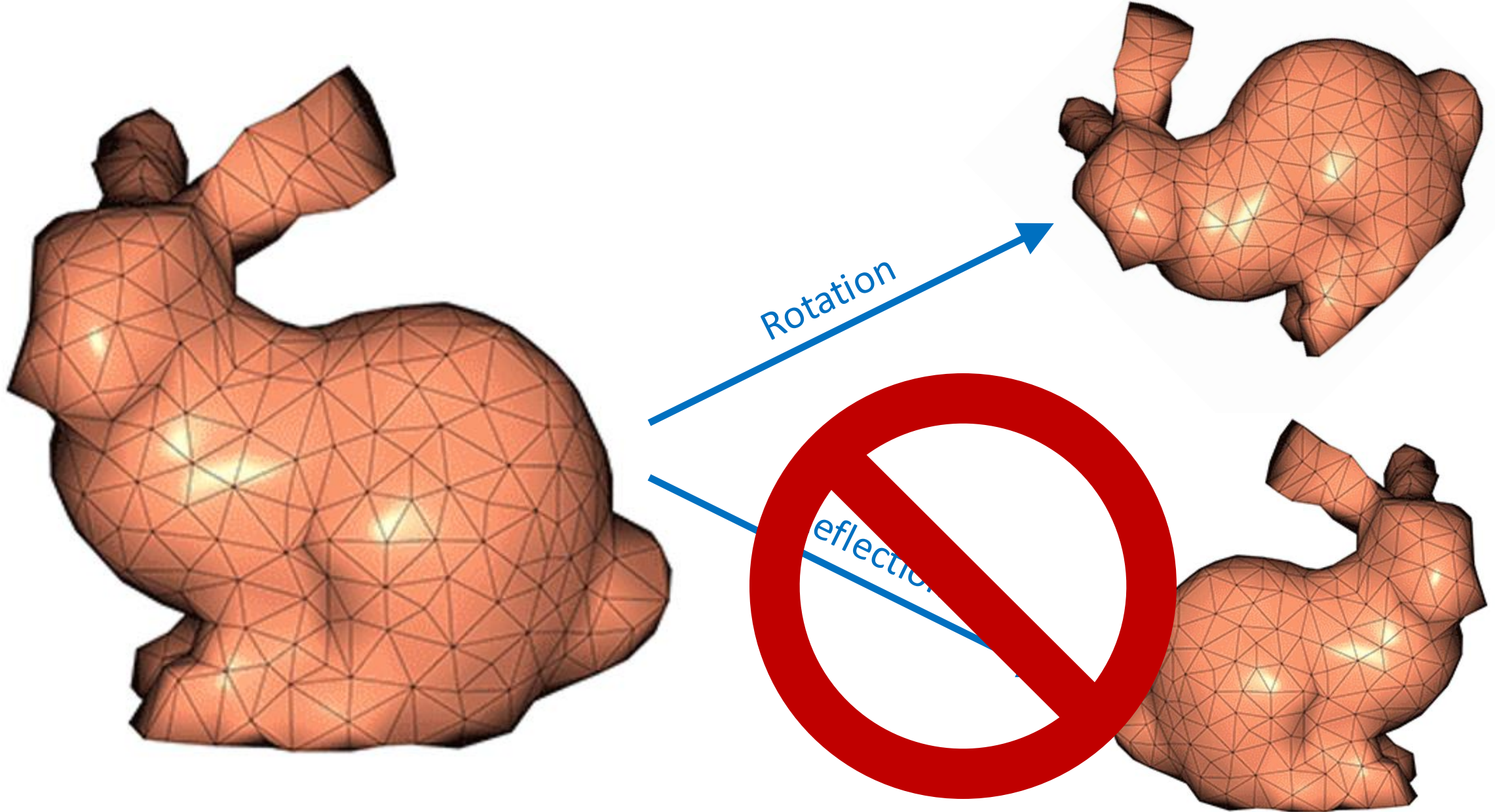
Implies

$$\mathbf{F}^T \mathbf{F} = \mathbf{I}$$

Orthogonal



# What Makes an Object Rigid ?



# What Makes an Object Rigid ?

$$\Delta \mathbf{X}^T (\mathbf{F}^T \mathbf{F} - \mathbf{I}) \Delta \mathbf{X} = \mathbf{0}$$

Implies

$$\mathbf{F}^T \mathbf{F} = \mathbf{I}$$

Orthogonal

**Rigid Bodies Rotate**

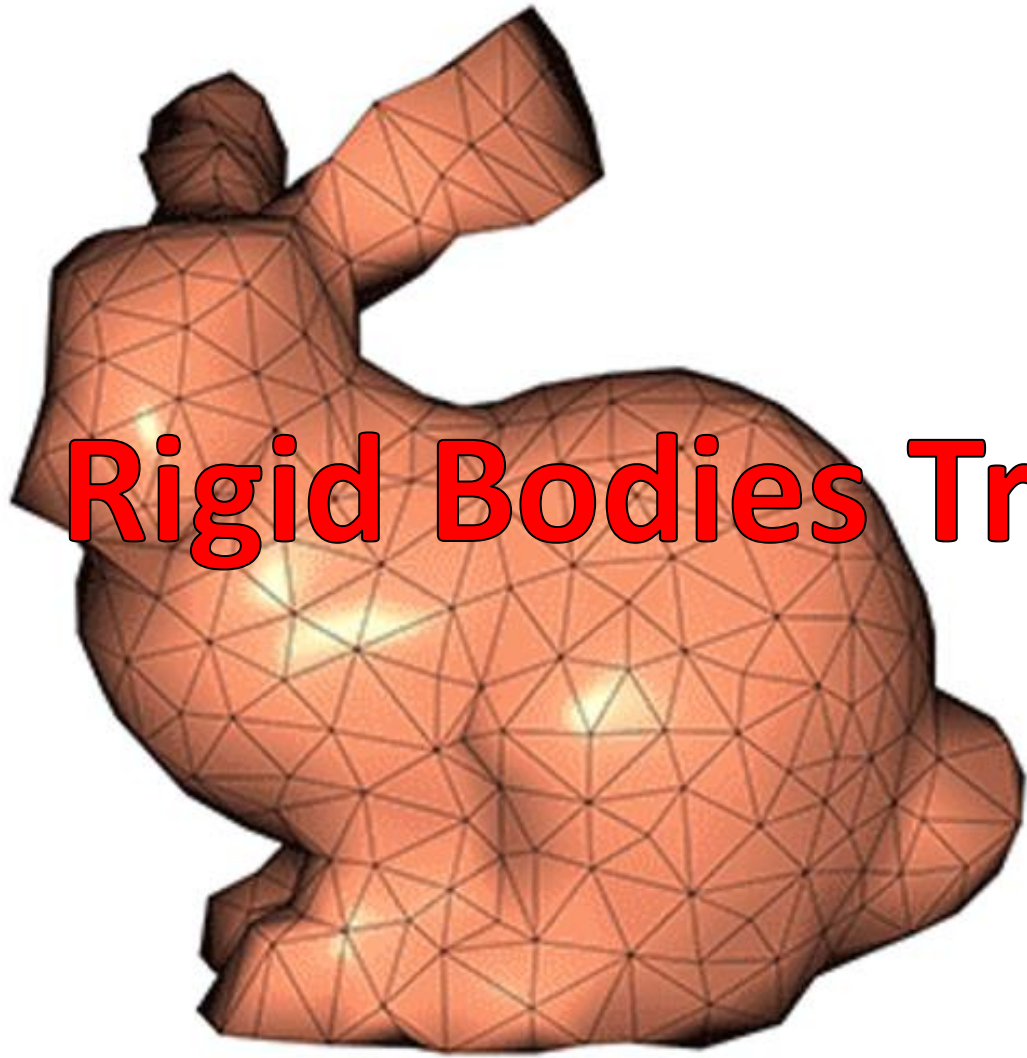
$$\mathbf{F} \in SO(3)$$

Special Orthogonal Group (Rotations) !





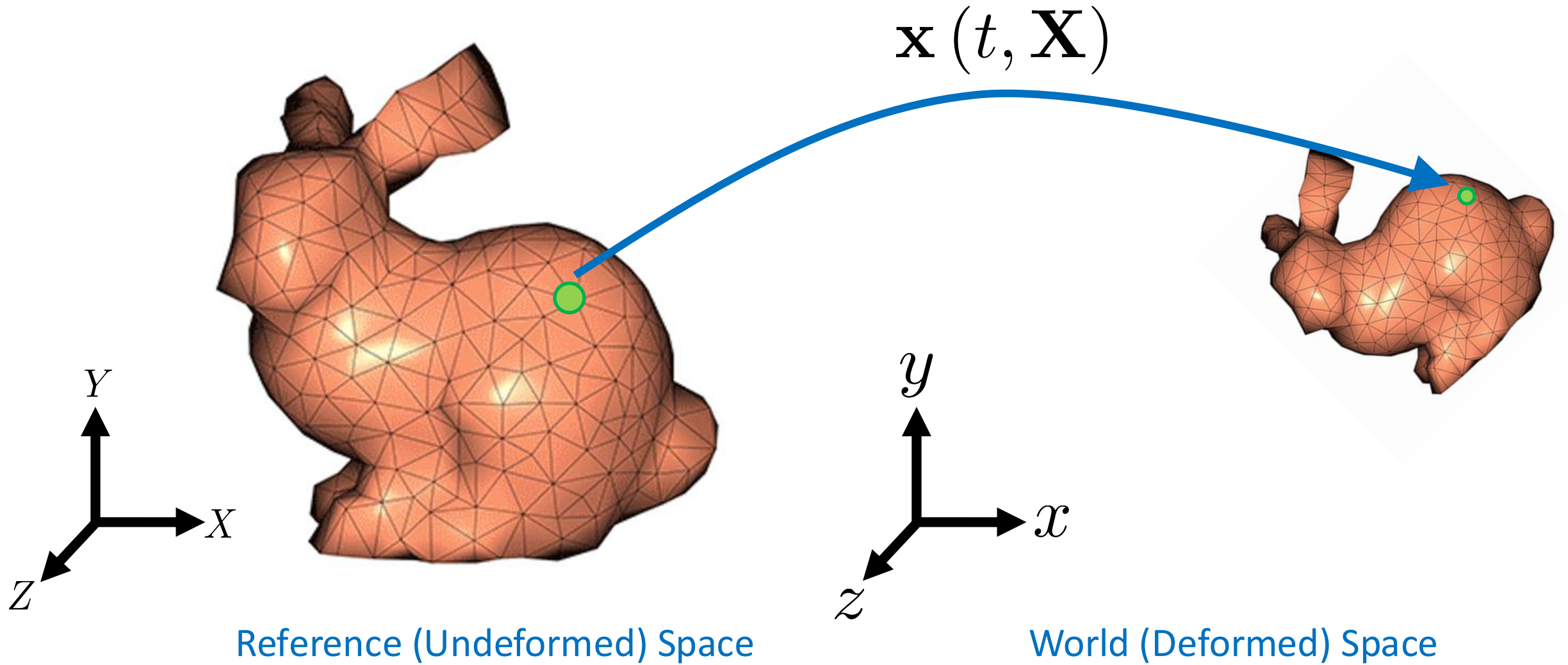
# What Makes an Object Rigid ?



**Rigid Bodies Translate**

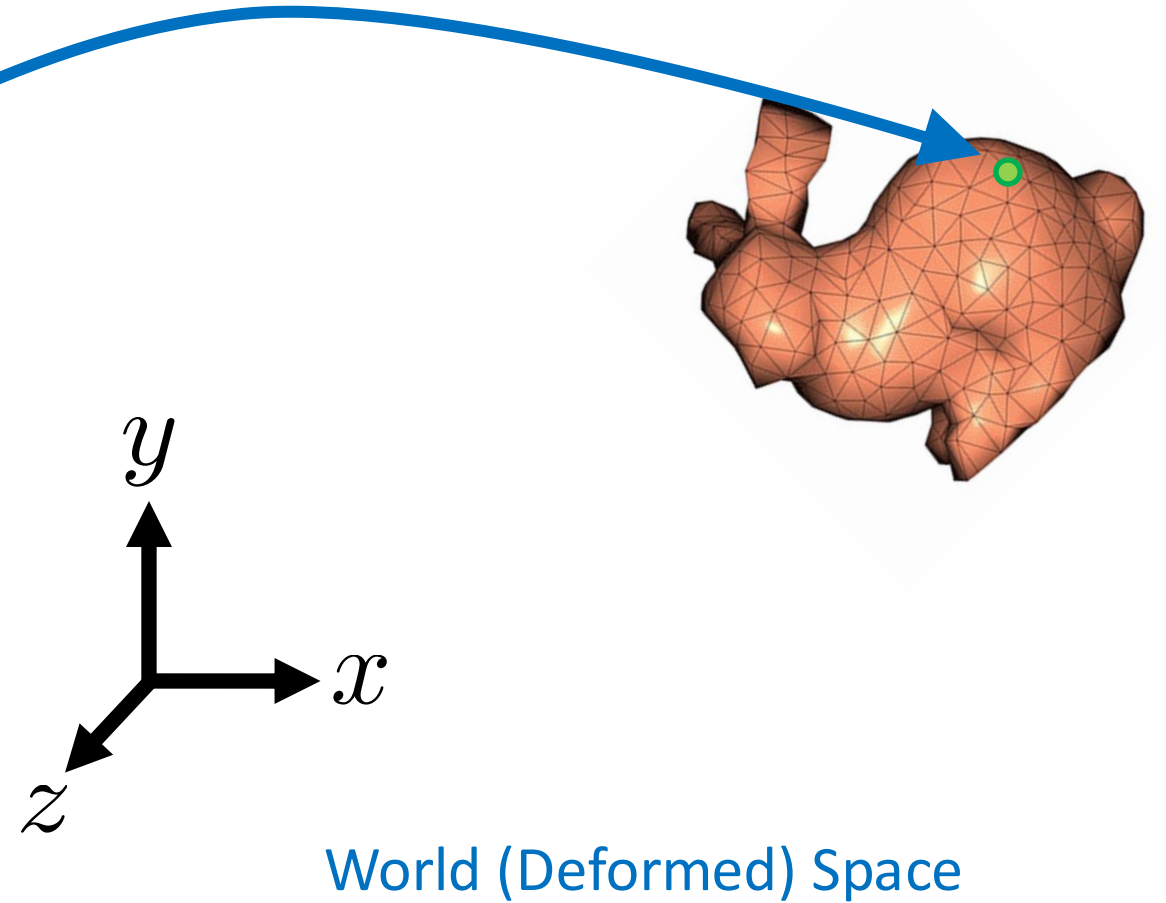
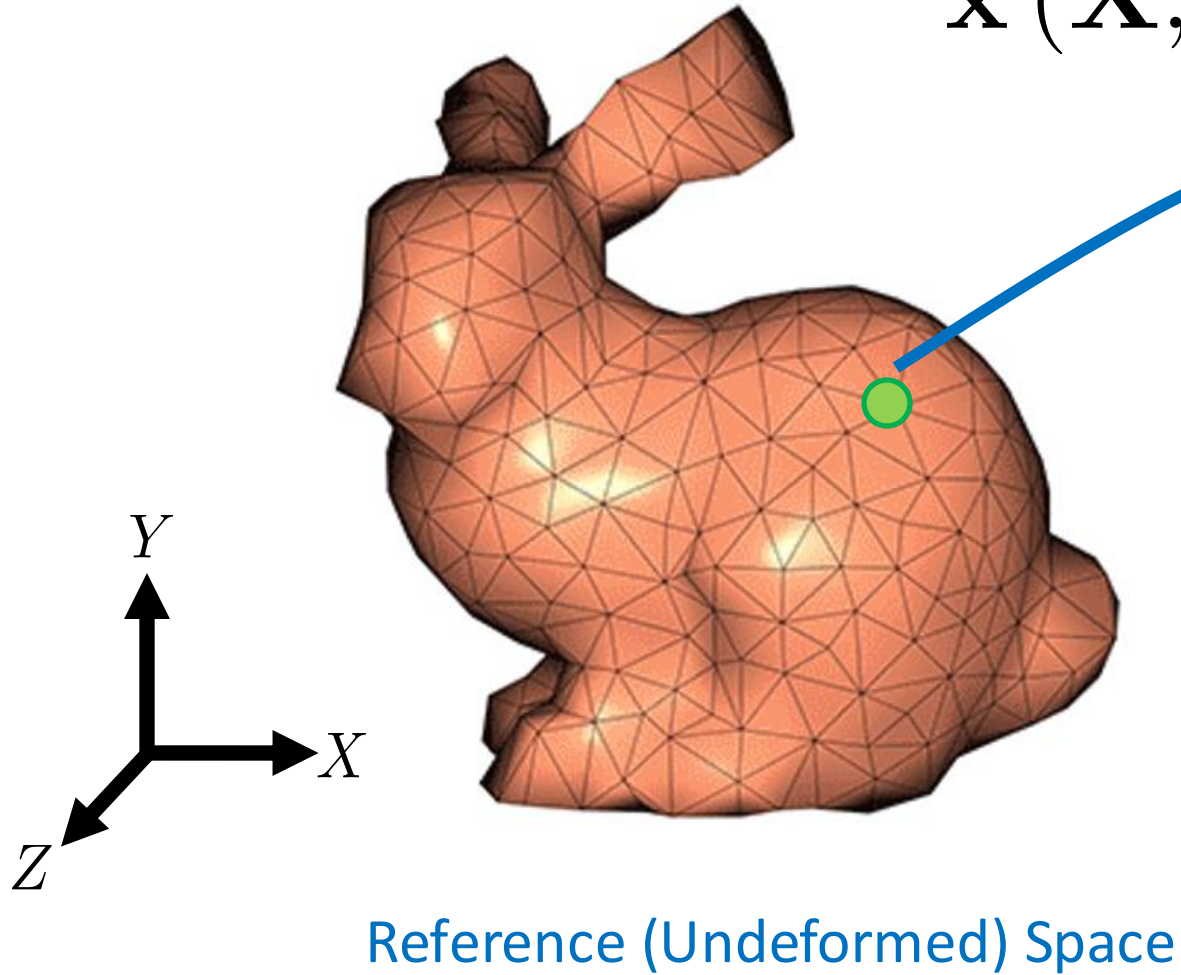


# The Rigid Body Mapping



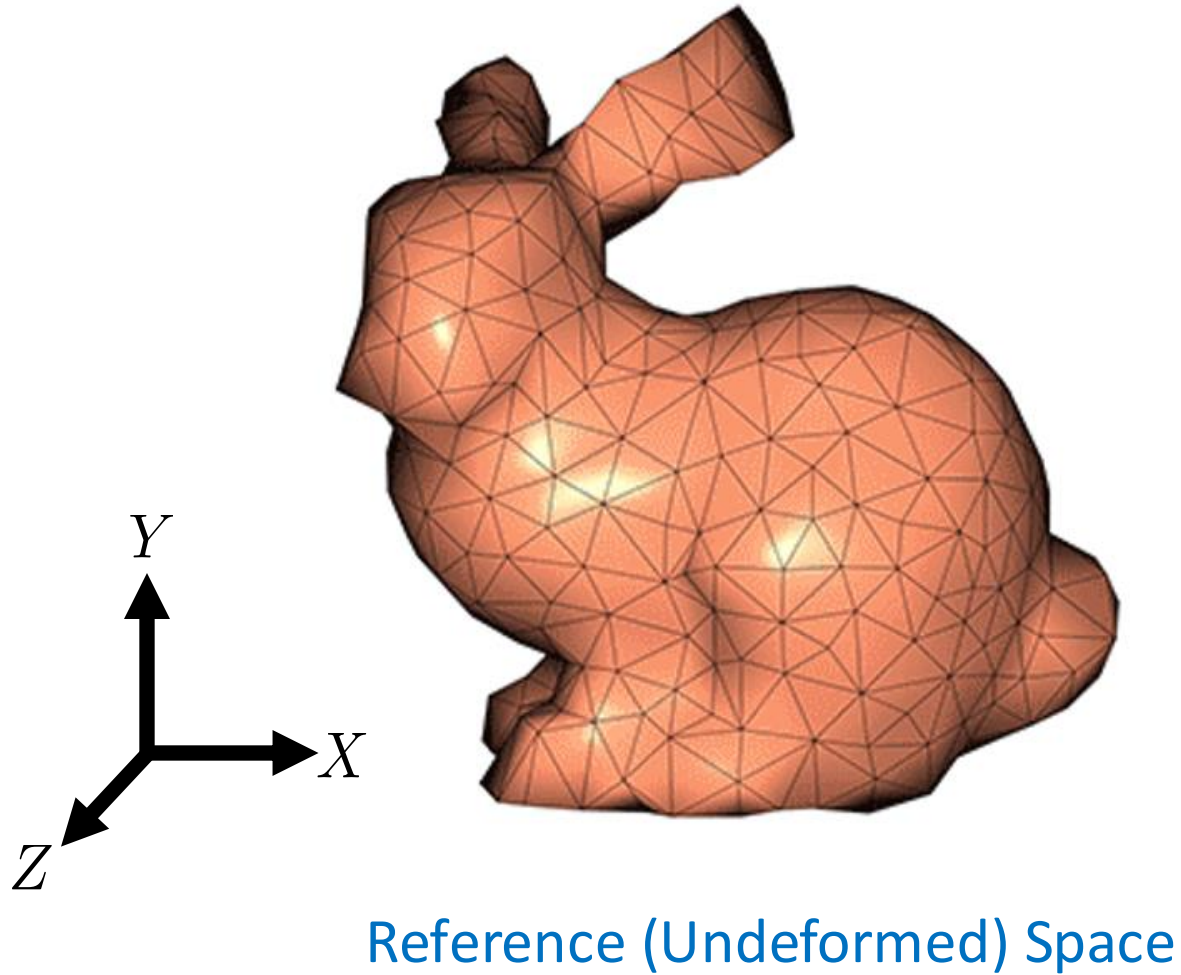
# The Rigid Body Mapping

$$\mathbf{x}(\mathbf{X}, t) = \mathbf{R}(t) \mathbf{X} + \mathbf{p}(t)$$





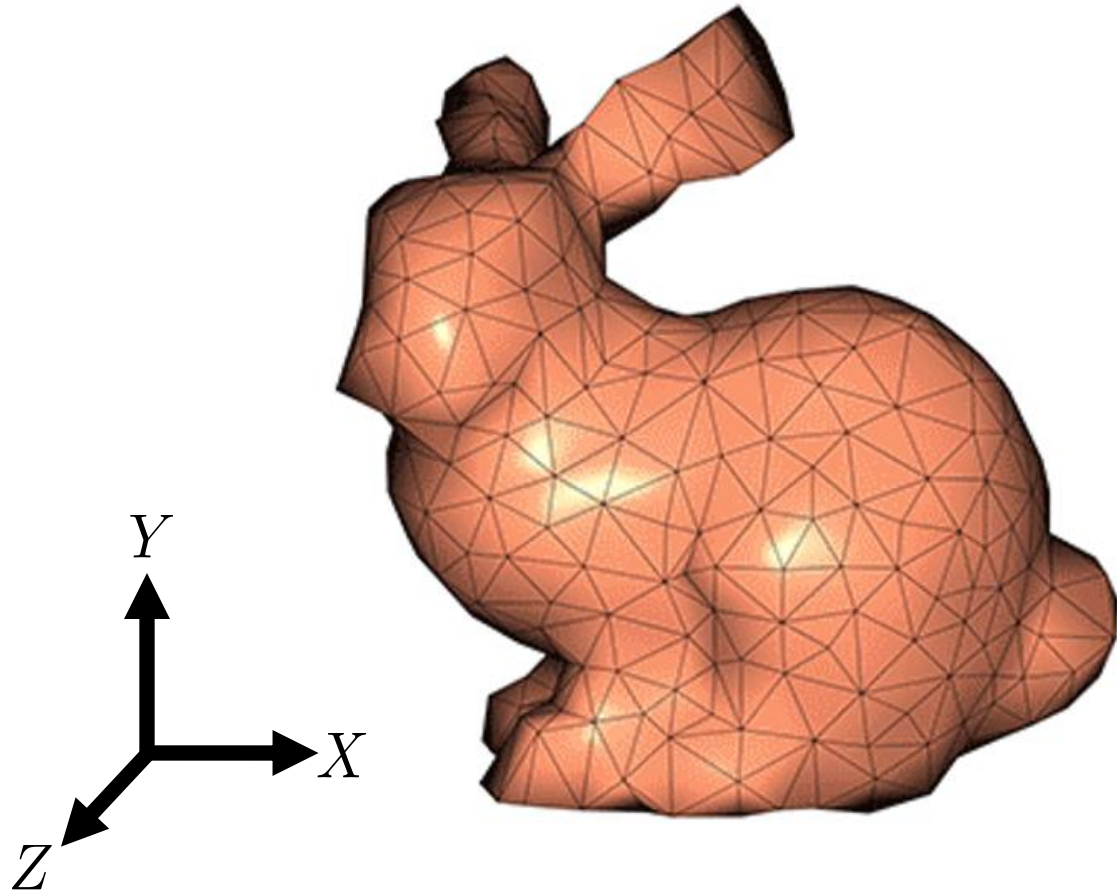
# Generalized Coordinates of a Rigid Body



$$\mathbf{x}(\mathbf{X}, t) = \underbrace{\mathbf{R}(t)}_{\text{Rotation Matrix} \in \mathbb{R}^{3 \times 3}} \mathbf{X} + \underbrace{\mathbf{p}(t)}_{\text{Translation} \in \mathbb{R}^{3 \times 1}}$$



# Generalized Coordinates of a Rigid Body



Reference (Undeformed) Space

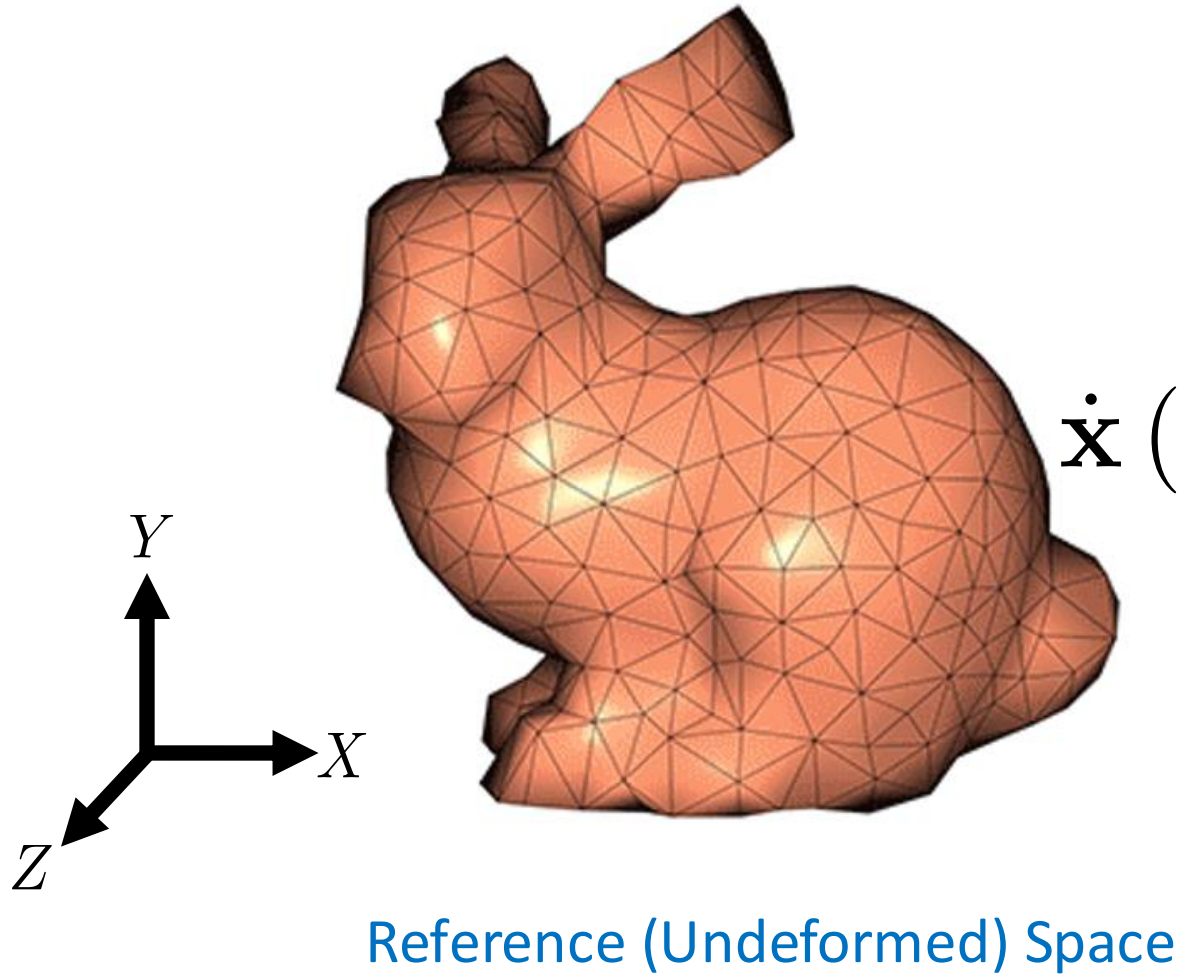
$$\mathbf{q} = \{\mathbf{R}, \mathbf{p}\}$$

└

Set with rotation and translation



# Generalized Velocity of a Rigid Body

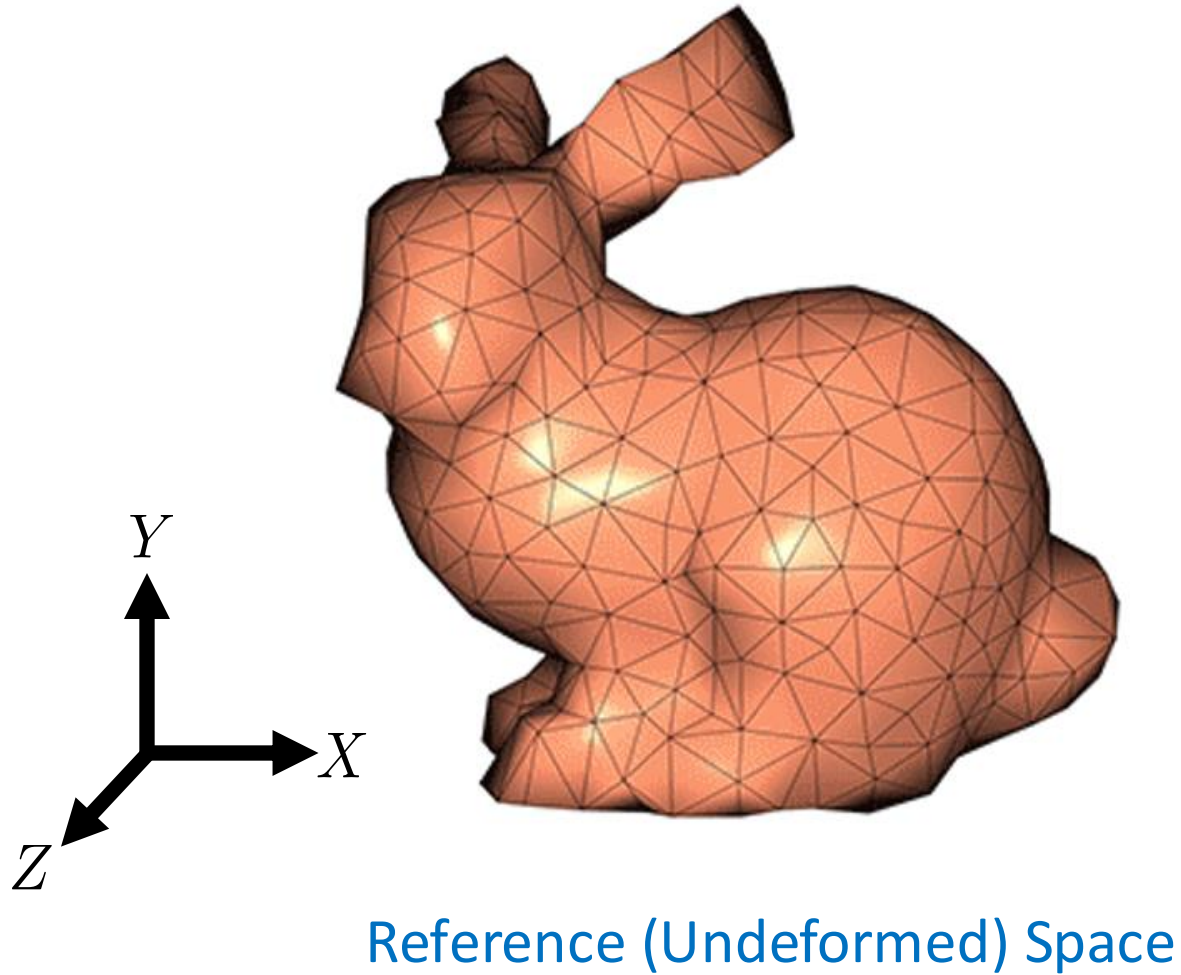


$$\dot{\mathbf{x}}(\mathbf{X}, t) = \frac{d}{dt} \left( \underbrace{\mathbf{R}(t)}_{\text{Rotation Matrix} \in \mathbb{R}^{3 \times 3}} \mathbf{X} + \underbrace{\mathbf{p}(t)}_{\text{Translation} \in \mathbb{R}^{3 \times 1}} \right)$$





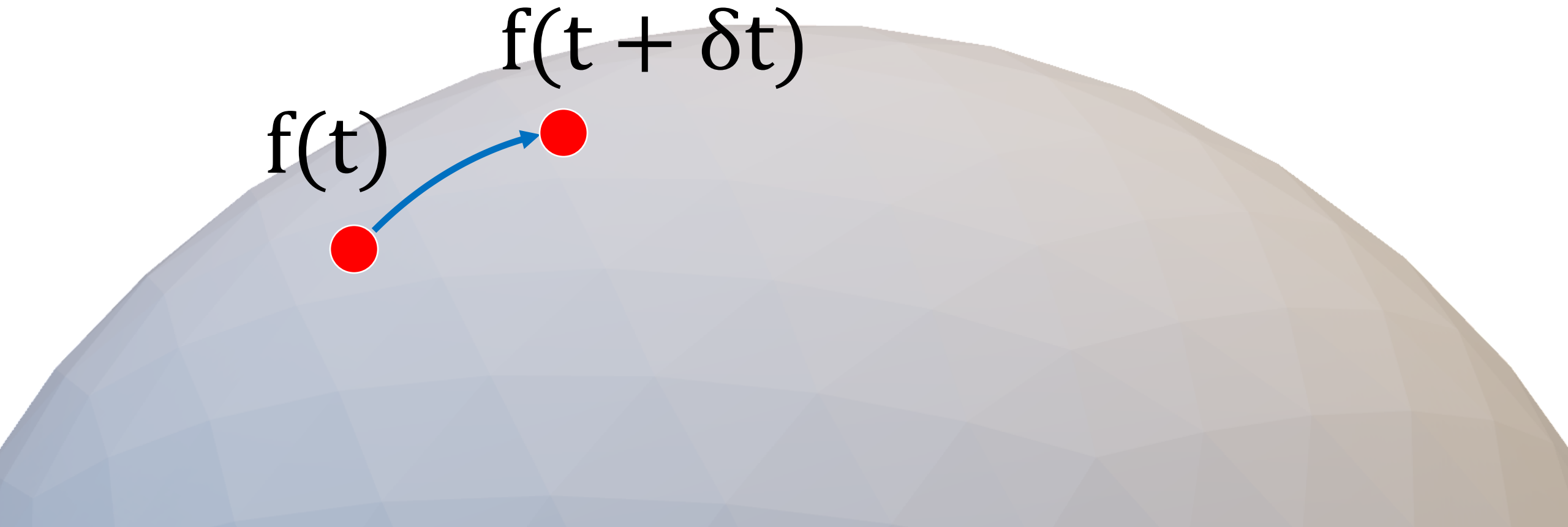
# Generalized Velocity of a Rigid Body



$$\dot{\mathbf{x}}(\mathbf{X}, t) = \underbrace{\dot{\mathbf{R}}(t)}_{\text{Time Derivative of Rotation Matrix}} \mathbf{X} + \underbrace{\dot{\mathbf{p}}(t)}_{\text{Linear Velocity}}$$



# Aside: Using Geometry to Compute Derivatives



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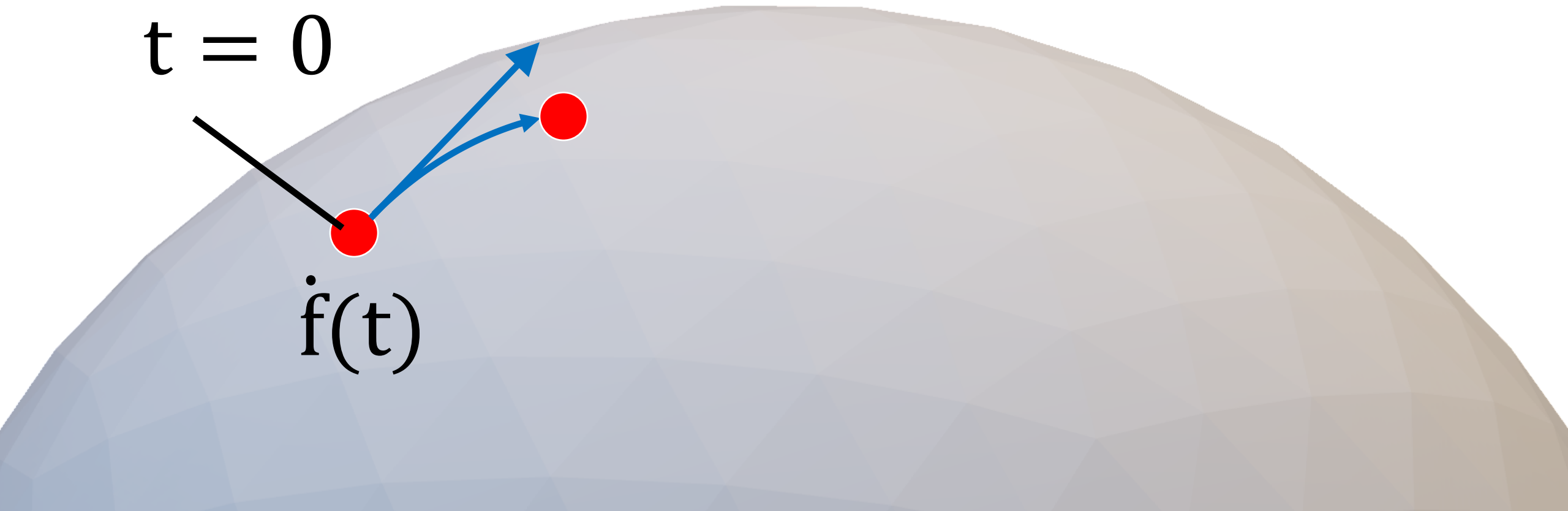




# Aside: Using Geometry to Compute Derivatives



# Aside: Using Geometry to Compute Derivatives



# Aside: Using Geometry to Compute Derivatives





# Time Derivatives of Rotation Matrices

$$R(t) \in SO(3)$$

$$R(t + \delta t) \quad \text{Next Rotation in } SO(3) \text{ (Yikes !)}$$

$$\exp([\omega]\delta t)R(t)$$

Angular velocity 3-dimensional vector

# Time Derivatives of Rotation Matrices

$$R(t) \in SO(3)$$

$$R(t + \delta t) \quad \text{Next Rotation in } SO(3) \text{ (Yikes !)}$$

$$\exp([\omega]\delta t)R(t)$$

 Square brackets = skew-symmetric matrix

# Time Derivatives of Rotation Matrices

$$R(t) \in SO(3)$$

$$R(t + \delta t) \quad \text{Next Rotation in } SO(3) \text{ (Yikes !)}$$

$$\exp([\omega]\delta t)R(t)$$

Matrix Exponential

**Step 1: d/dt**

$$\frac{d}{d\delta t} \exp([\omega]\delta t) R(t)$$

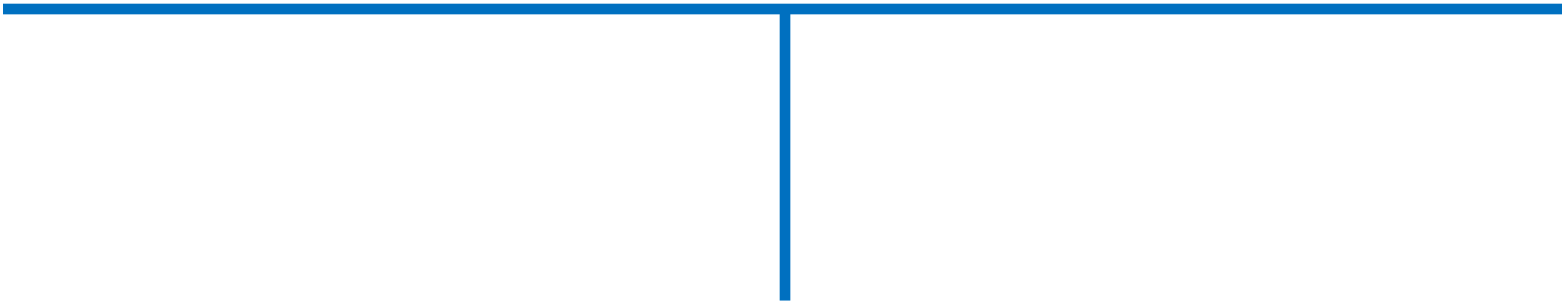
**Infinite Series for Exponential**

$$\frac{d}{d\delta t} (I + [\omega]\delta t + \frac{1}{2} [\omega][\omega]\delta t^2 \dots) R(t)$$



**Step 1: d/dt**

$$\frac{d}{d\delta t} \left( I + [\omega]\delta t + \frac{1}{2} [\omega][\omega]\delta t^2 \dots \right) R(t)$$

$$([\omega] + [\omega][\omega]\delta t \dots) R(t)$$


**Yuck, still an infinite series**

## Step 2: Limit !!!

$$([\omega] + [\omega][\omega]\delta t \dots) R(t)$$

---

**Yuck, still an infinite series**

$$\lim_{\delta t \rightarrow 0} ([\omega] + [\omega][\omega]\delta t \dots) R(t)$$

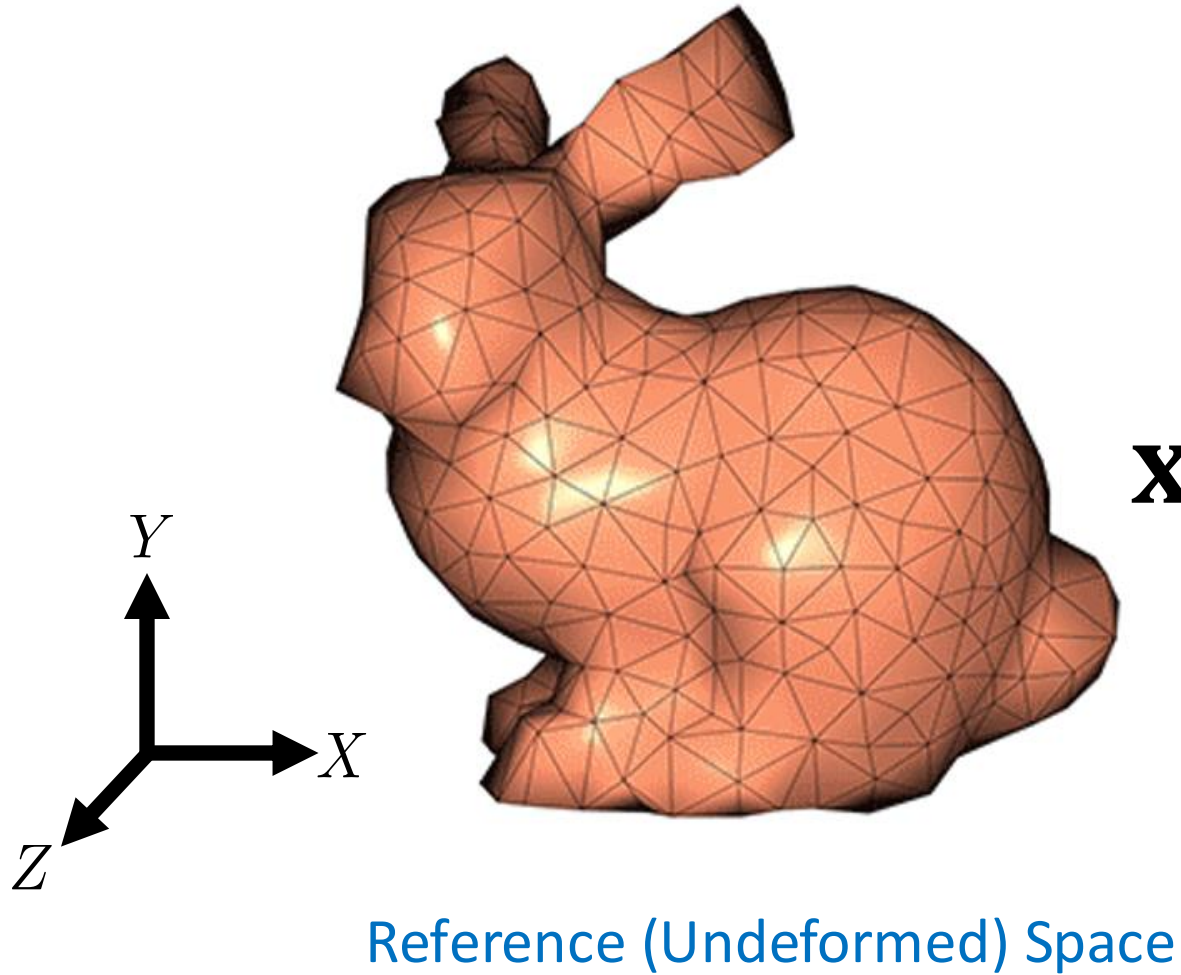
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**Only constant terms remain**

## Step 3: Finale

$$\dot{R}(t) = [\omega]R(t)$$

# Generalized Velocity of a Rigid Body

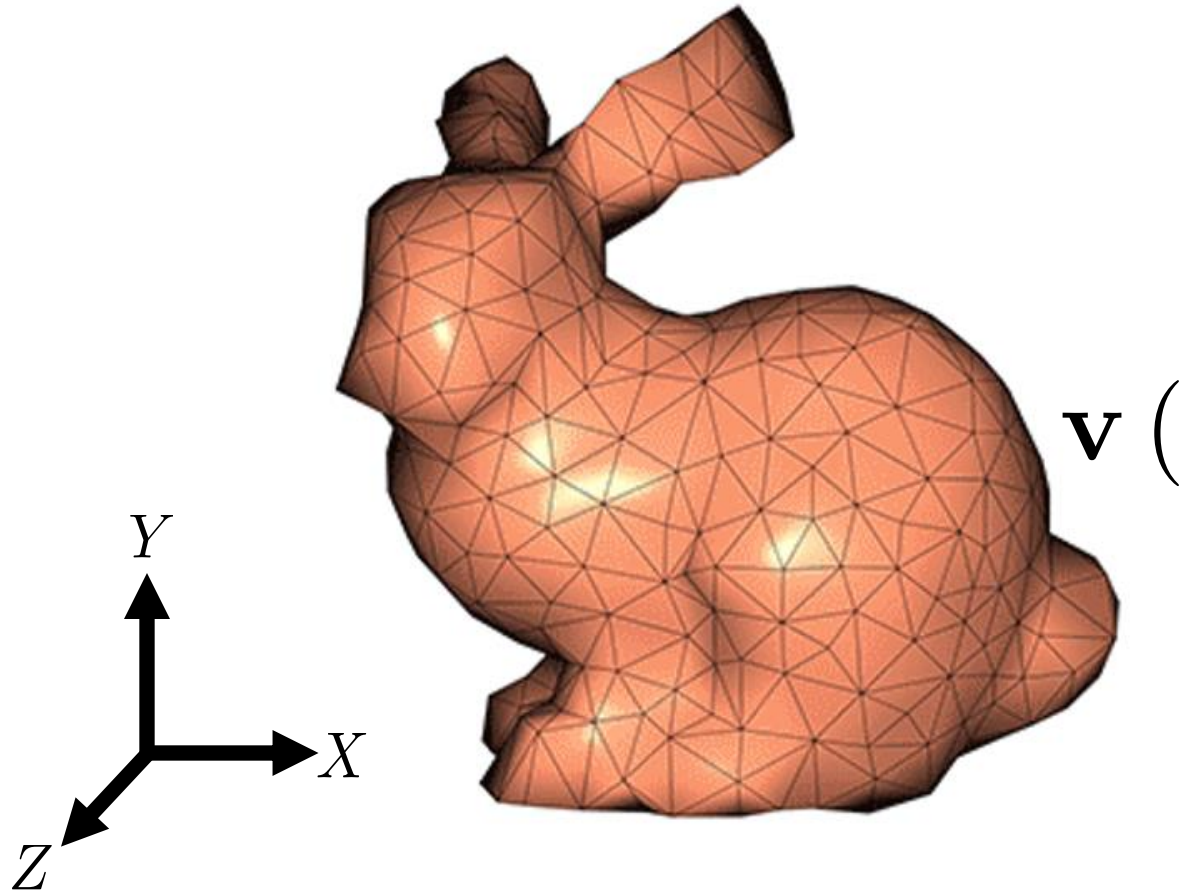


$$\mathbf{x}(\mathbf{X}, t) = \underbrace{[\omega]R(t)\mathbf{X}}_{\text{Can be understood as } \omega \times (R(t)\mathbf{X})} + \underbrace{\dot{\mathbf{p}}(t)}_{\text{Linear Velocity}}$$





# Generalized Velocity of a Rigid Body



Reference (Undeformed) Space

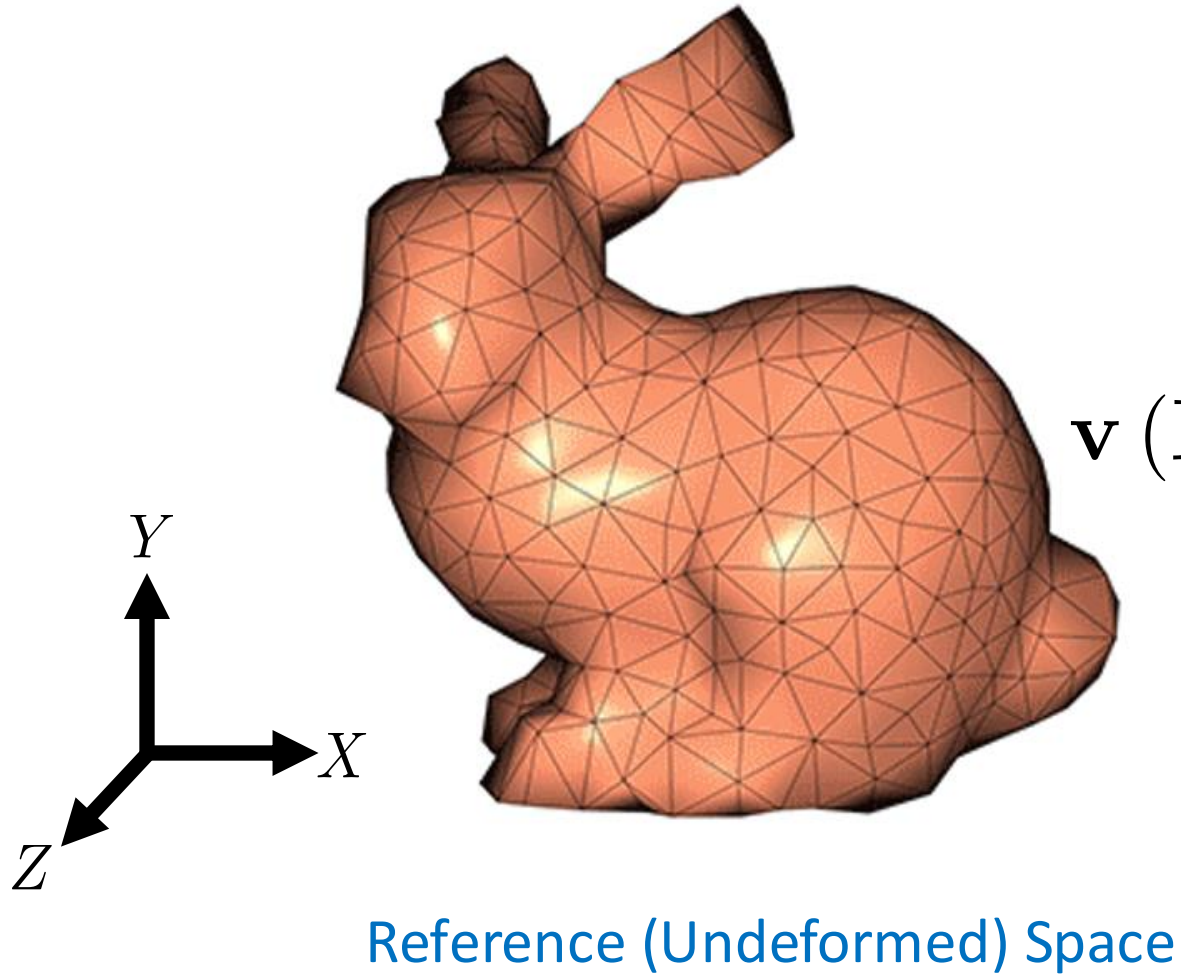
$$\mathbf{v}(\mathbf{X}, t) = \mathbf{R} \underbrace{[\mathbf{X}]^T}_{\text{Cross Product Matrix}} \mathbf{R}^T \underbrace{\boldsymbol{\omega}}_{\text{Angular Velocity} \in \mathbb{R}^3} + \underbrace{\dot{\mathbf{p}}(t)}_{\text{Linear Velocity}}$$

$$[\mathbf{X}] = \begin{pmatrix} 0 & -X_z & X_y \\ X_z & 0 & -X_x \\ -X_y & X_x & 0 \end{pmatrix}$$

Cross Product Matrix



# Generalized Velocity of a Rigid Body



$$\mathbf{v}(\mathbf{X}, t) = \mathbf{R} \begin{pmatrix} [\mathbf{X}]^T & \mathbf{I} \end{pmatrix} \begin{pmatrix} \mathbf{R}^T & 0 \\ 0 & \mathbf{I} \end{pmatrix} \begin{pmatrix} \omega \\ \dot{\mathbf{p}} \end{pmatrix}$$

$\dot{\mathbf{q}} \in \mathbb{R}^6$



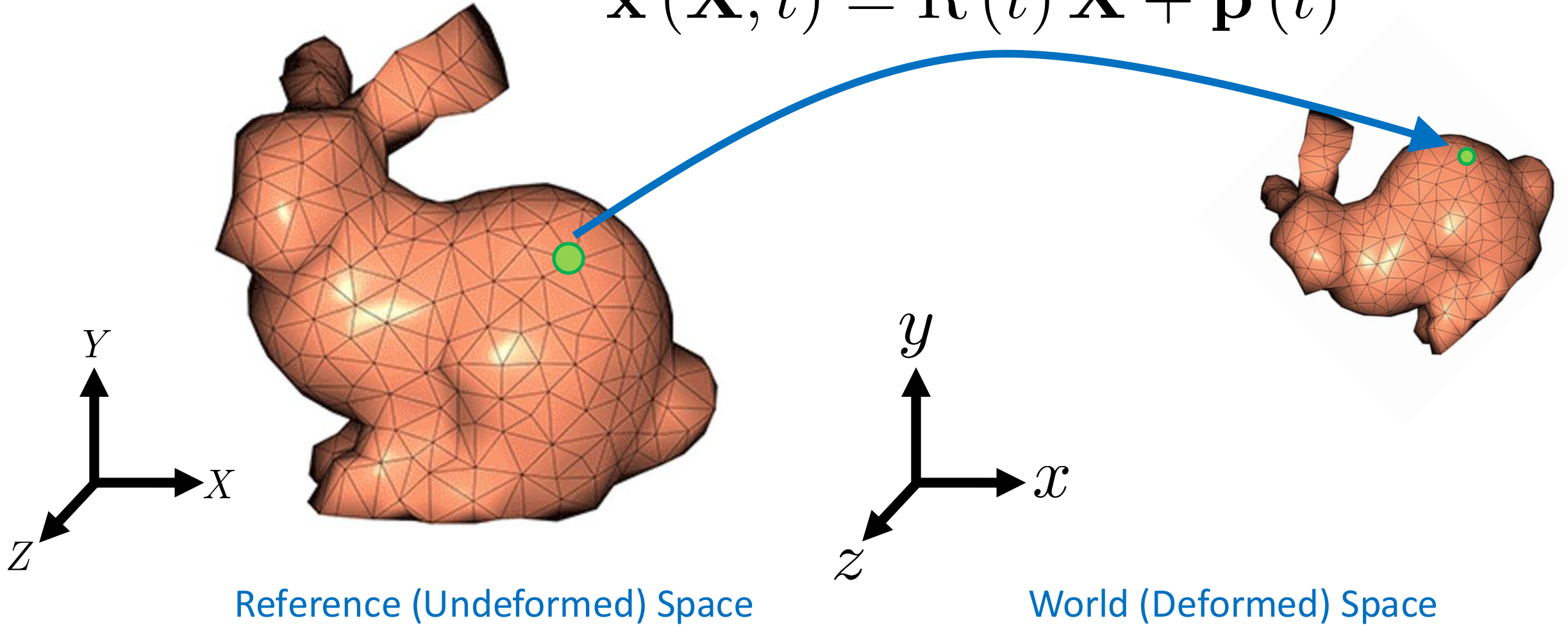
**Ok Who Wants to do the Second  
Derivates for Acceleration ?**

**Me Neither, Let's Do Something Else**



# The Rigid Body Mapping

$$\mathbf{x}(\mathbf{X}, t) = \mathbf{R}(t) \mathbf{X} + \mathbf{p}(t)$$



**Why did we use this mapping ?**



# What Makes an Object Rigid ?

$$\Delta \mathbf{X}^T (\mathbf{F}^T \mathbf{F} - \mathbf{I}) \Delta \mathbf{X} = \mathbf{0}$$

Implies

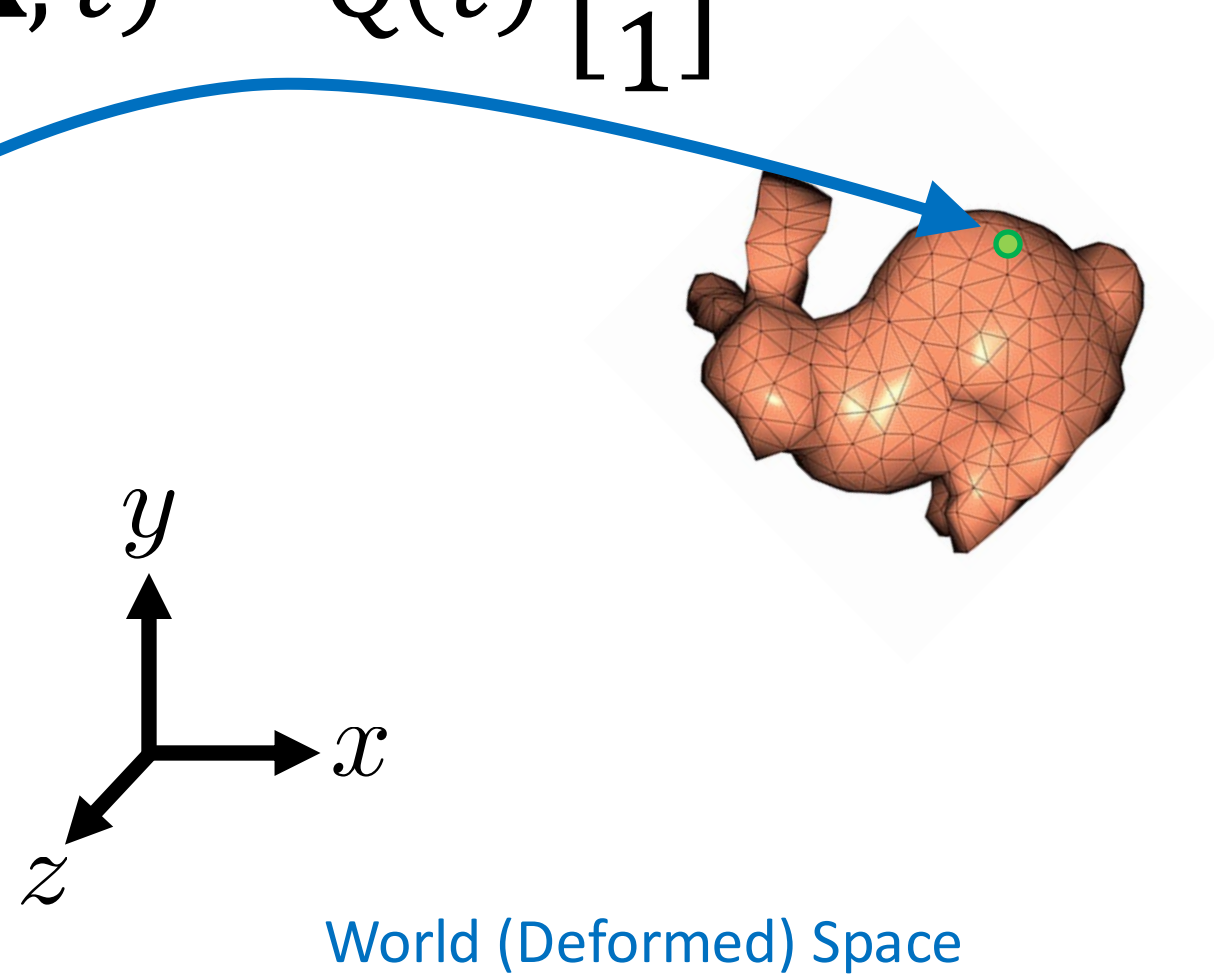
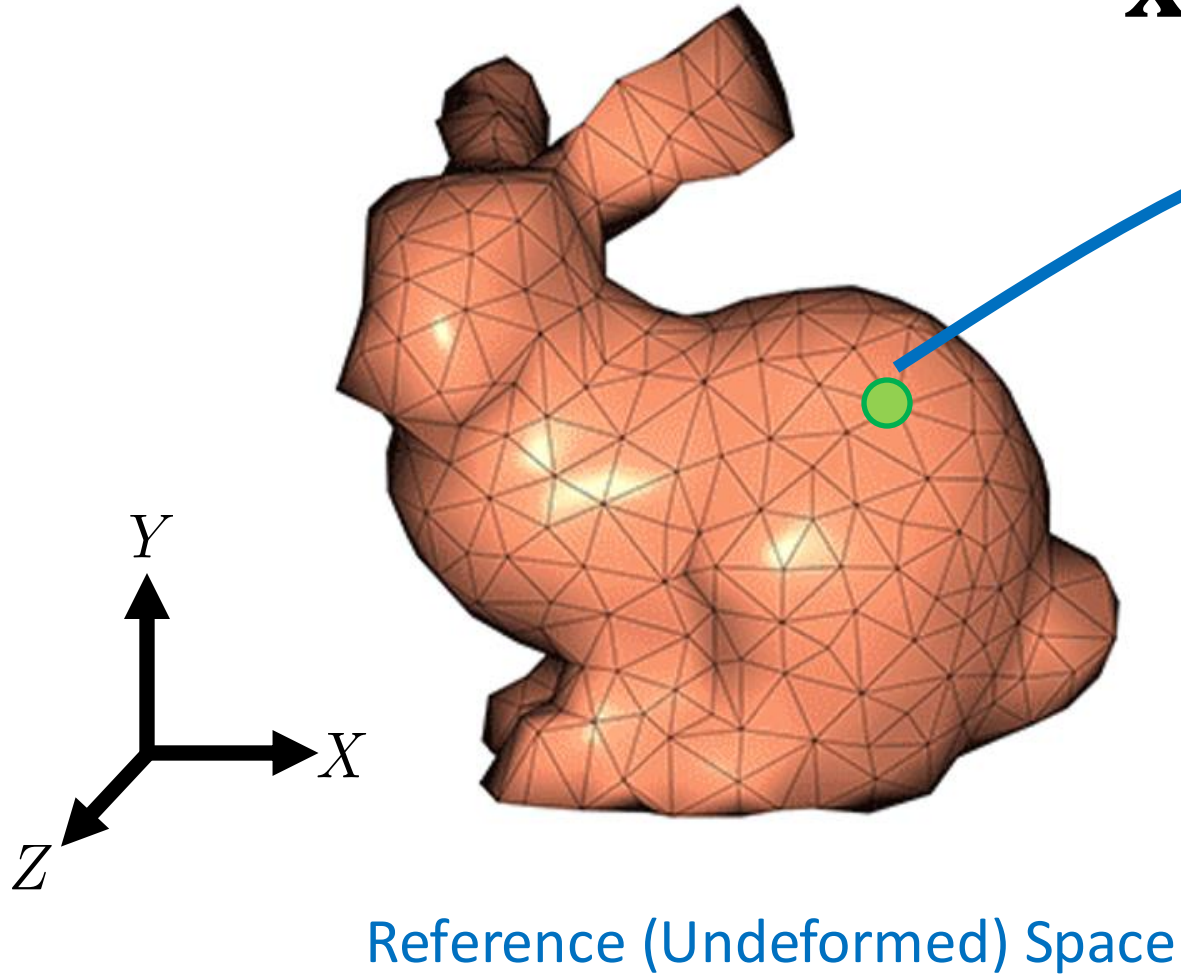
$$\mathbf{F}^T \mathbf{F} = \mathbf{I}$$

Orthogonal

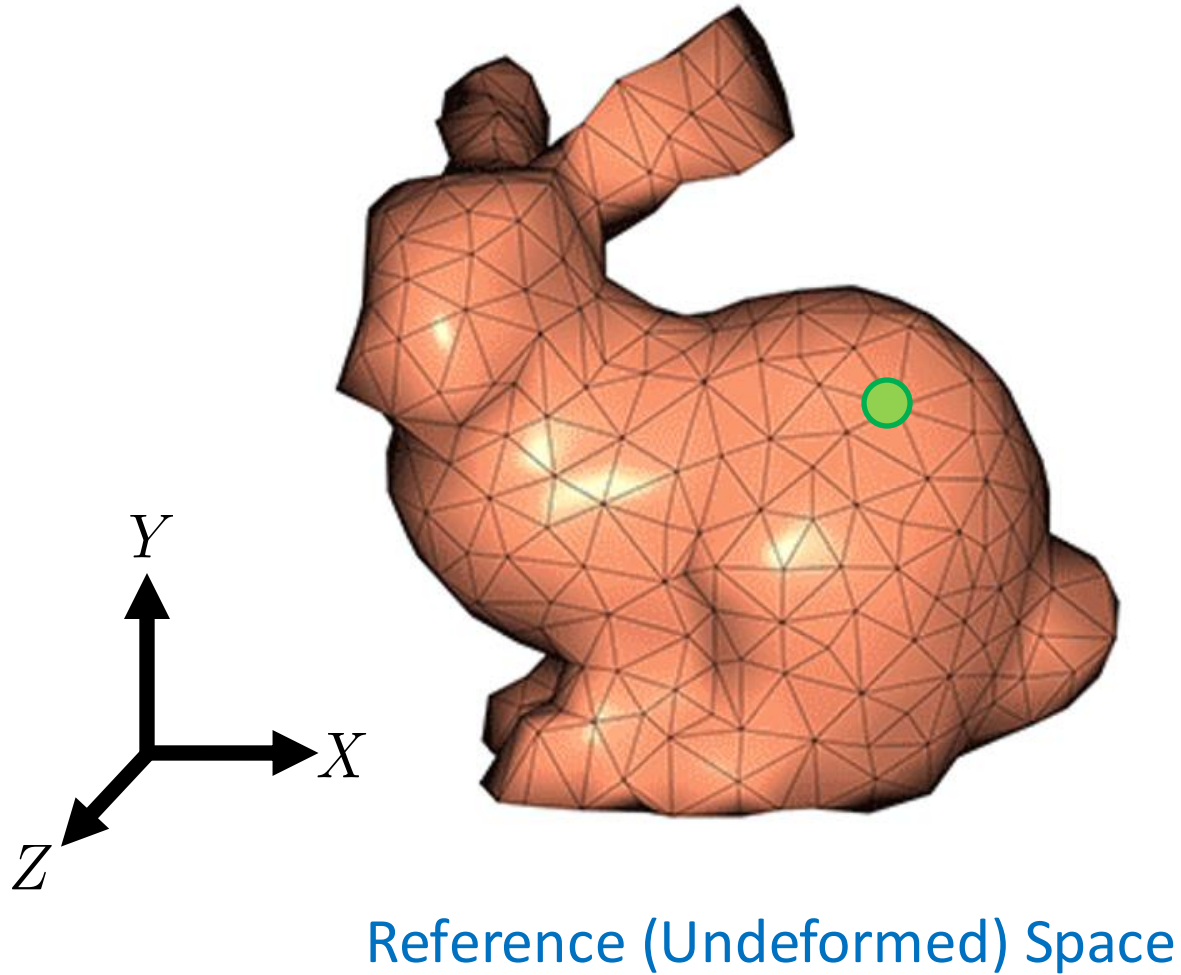


# The Affine Body Mapping

$$\mathbf{x}(\mathbf{X}, t) = \mathbf{Q}(t) \begin{bmatrix} \mathbf{X} \\ 1 \end{bmatrix}$$



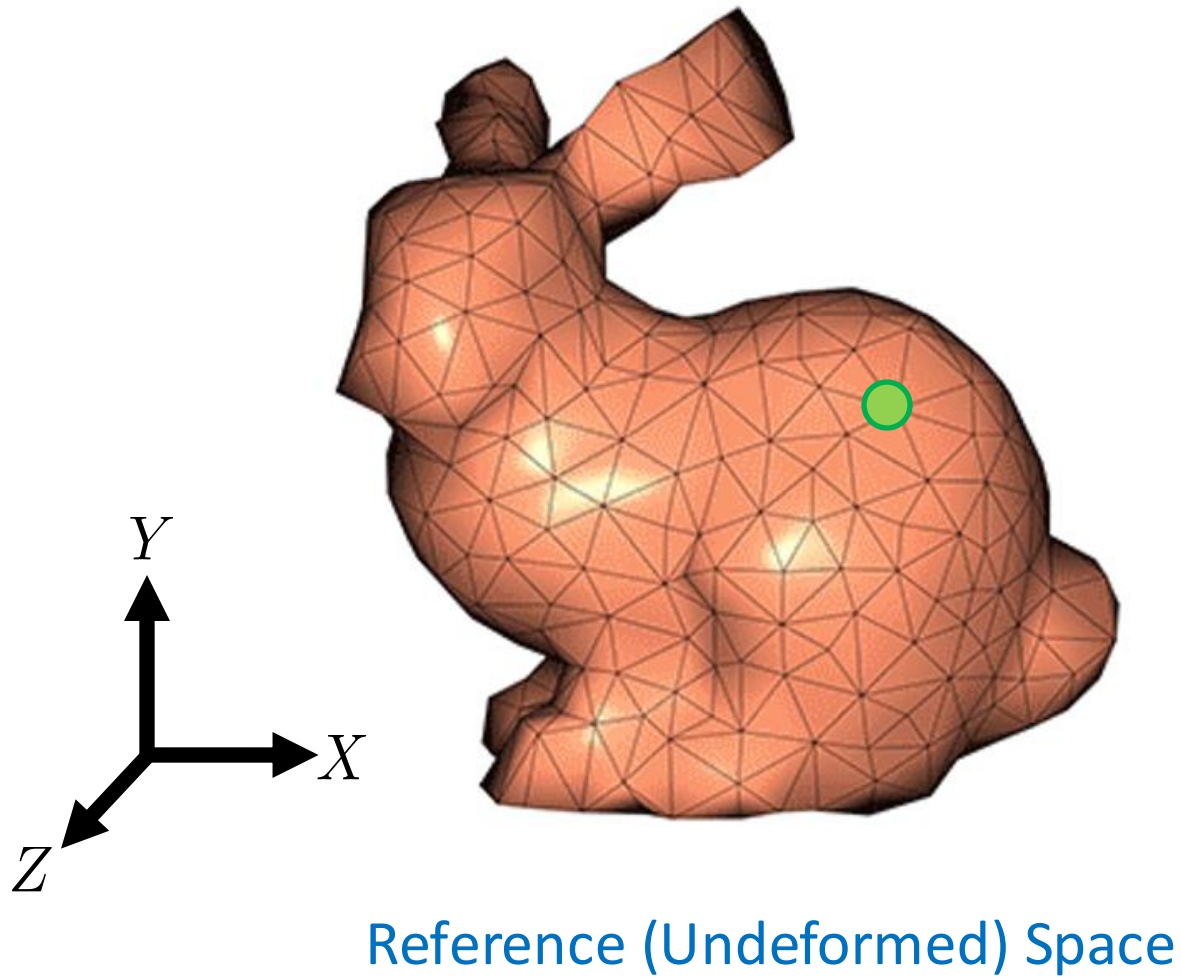
# The Affine Body Mapping



$$\mathbf{x}(\mathbf{X}, t) = \underbrace{Q(t)}_{\text{Affine Transform}} \begin{bmatrix} \mathbf{X} \\ 1 \end{bmatrix}$$



# The Affine Body Mapping

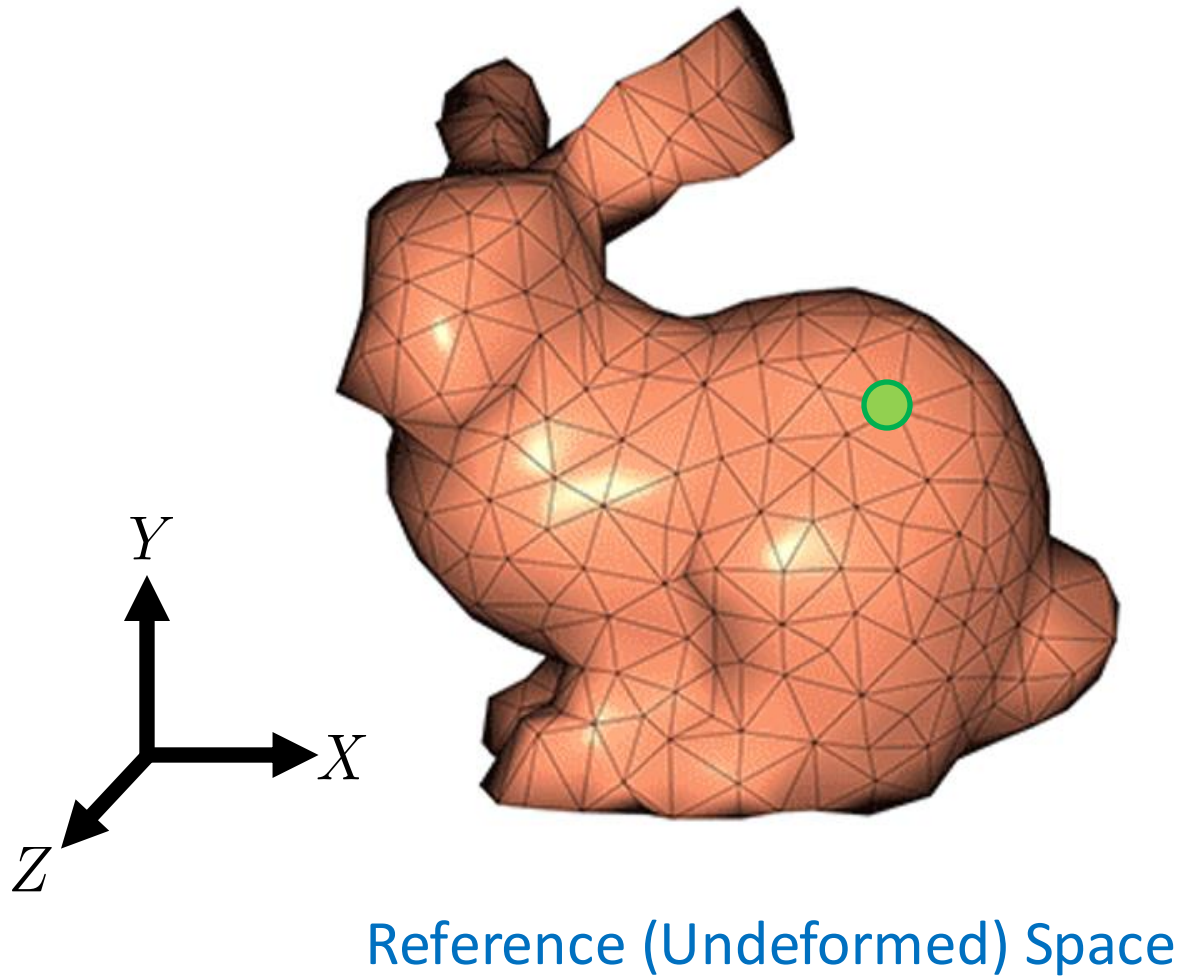


$$\mathbf{x}(\mathbf{X}, t) = \underbrace{Q(t)}_{\begin{pmatrix} q_0 & q_1 & q_2 & q_3 \\ q_4 & q_5 & q_6 & q_7 \\ q_8 & q_9 & q_{10} & q_{11} \end{pmatrix}} \begin{bmatrix} \mathbf{X} \\ 1 \end{bmatrix}$$





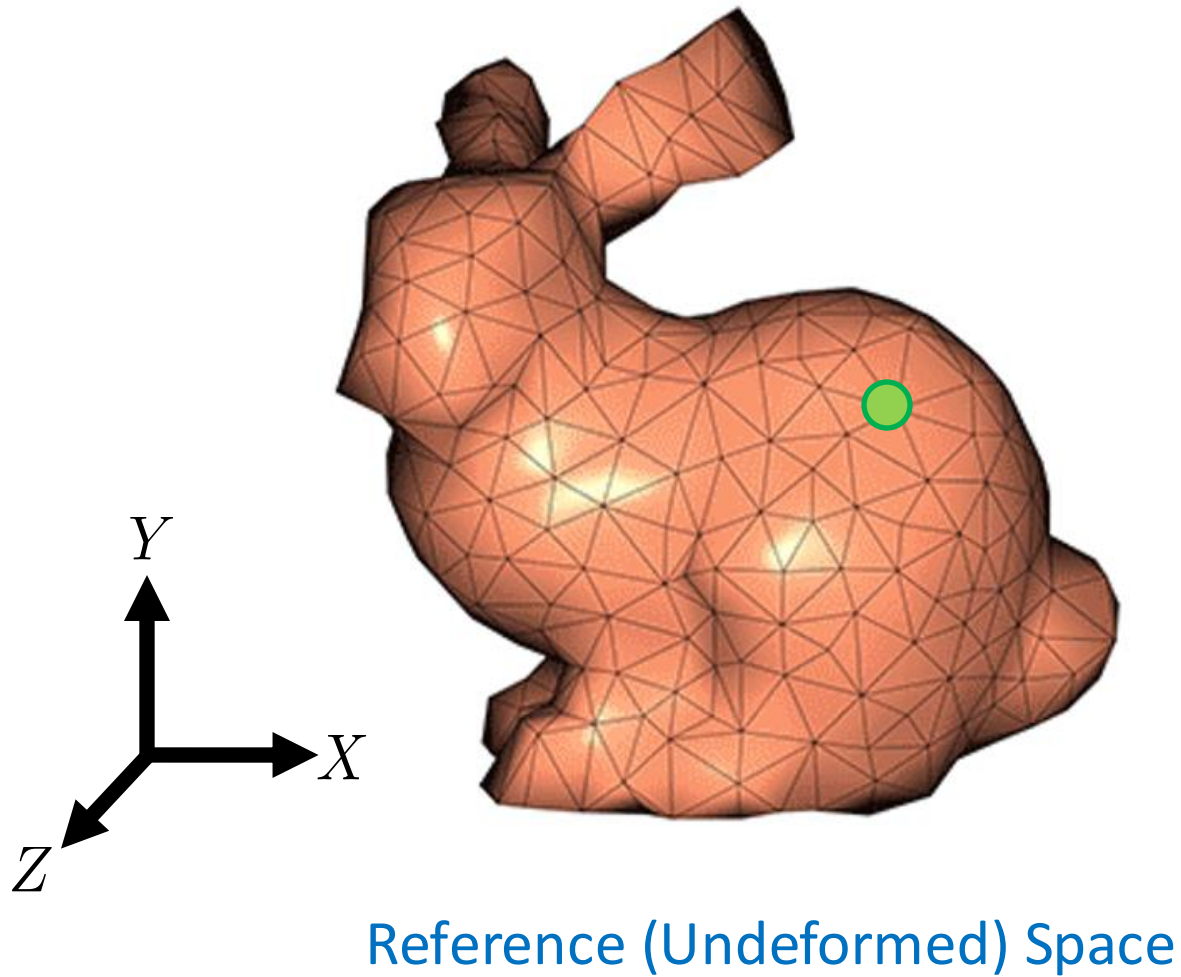
# The Affine Body Mapping



$$\mathbf{x}(\mathbf{X}, t) = \underbrace{Q(t)}_{\substack{\text{Linear Transform} \\ \text{Linear Transform}}} \begin{bmatrix} \mathbf{X} \\ 1 \end{bmatrix}$$

The diagram illustrates the affine body mapping equation. The transformation matrix  $Q(t)$  is shown as a 4x4 matrix of parameters  $q_0$  through  $q_{11}$ , arranged in three rows and four columns. A green box highlights the first three rows, and a blue line points from the text "Linear Transform" below to this box. A green dot on the right side of the matrix indicates the mapping of a point from the reference space to the current configuration.

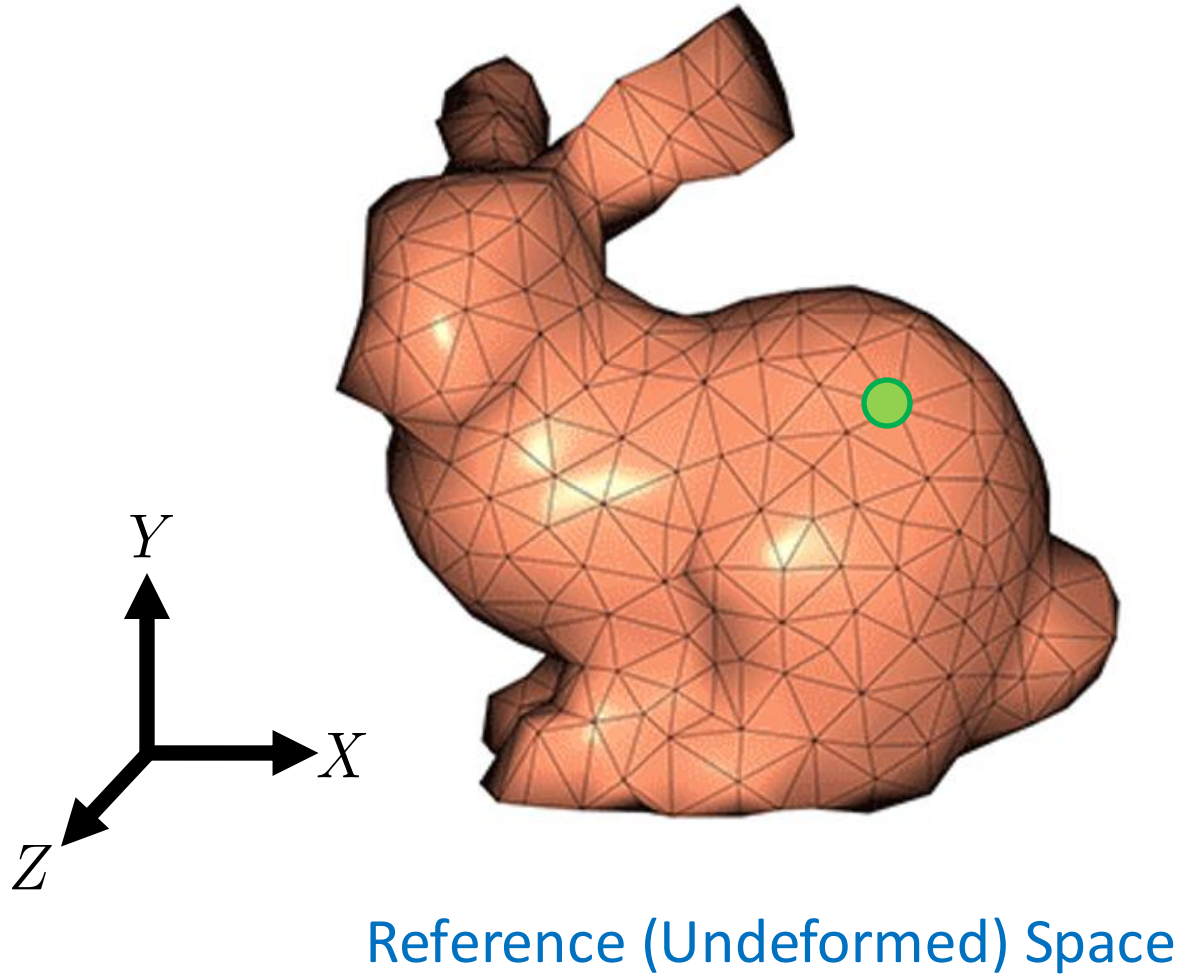
# The Affine Body Mapping



$$\mathbf{x}(\mathbf{X}, t) = \underbrace{Q(t)}_{\substack{\begin{pmatrix} q_0 & q_1 & q_2 & q_3 \\ q_4 & q_5 & q_6 & q_7 \\ q_8 & q_9 & q_{10} & q_{11} \end{pmatrix} \\ \text{Translation}}} \begin{bmatrix} \mathbf{X} \\ 1 \end{bmatrix}$$

The diagram illustrates the affine body mapping equation. The transformation matrix  $Q(t)$  is shown as a 4x4 matrix of parameters  $q_0$  through  $q_{11}$ . A blue line connects the underbrace under  $Q(t)$  to the matrix. A green dot is placed above the matrix, and a blue line connects it to the word "Translation" below the matrix.

# Vectorized Generalized Coordinates

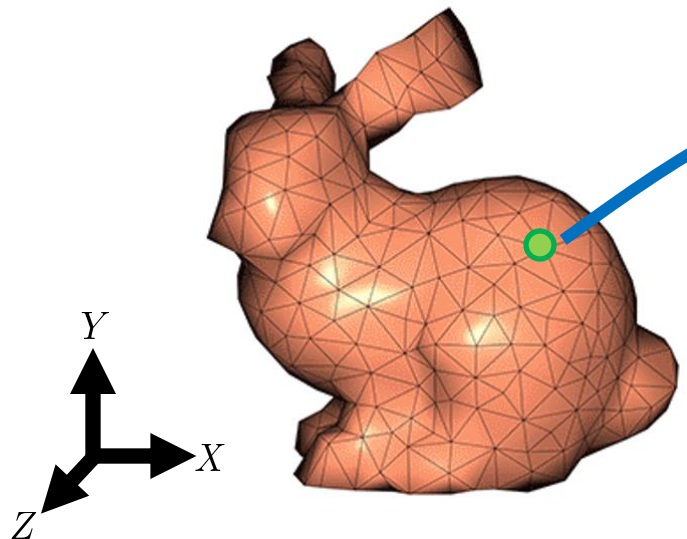


J is ?? x ??

$$\mathbf{x}(\mathbf{X}, t) = \text{mat} \left( \begin{bmatrix} \mathbf{X} \\ 1 \end{bmatrix} \right) \underset{\text{Row-wise Flatten}}{\mathbf{q}(t)}$$



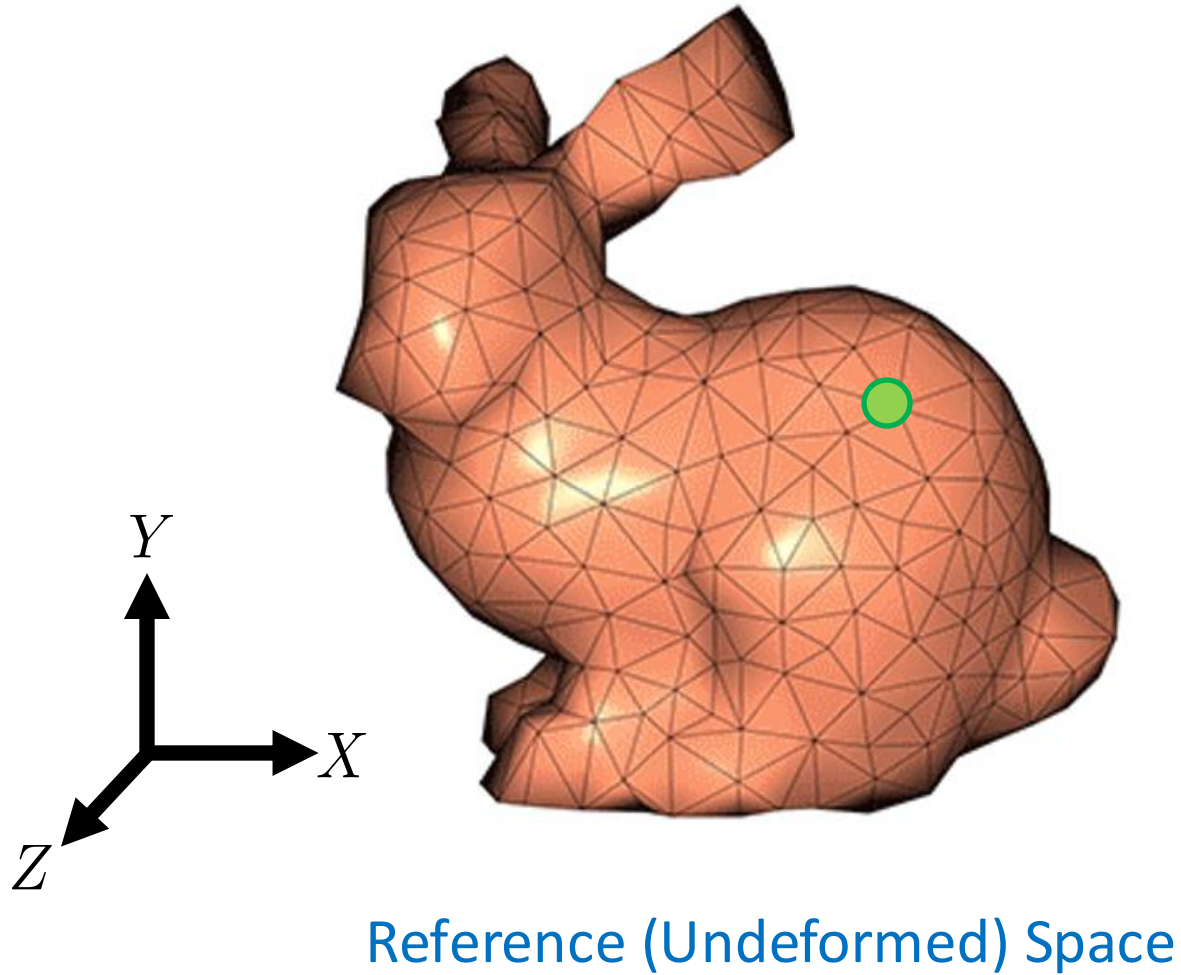
# The Kinematic Jacobian



$$\begin{bmatrix} X & Y & Z & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \boxed{X} & \boxed{Y} & \boxed{Z} & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & X & Y & Z & 1 \end{bmatrix}$$

J

# Vectorized Generalized Coordinates

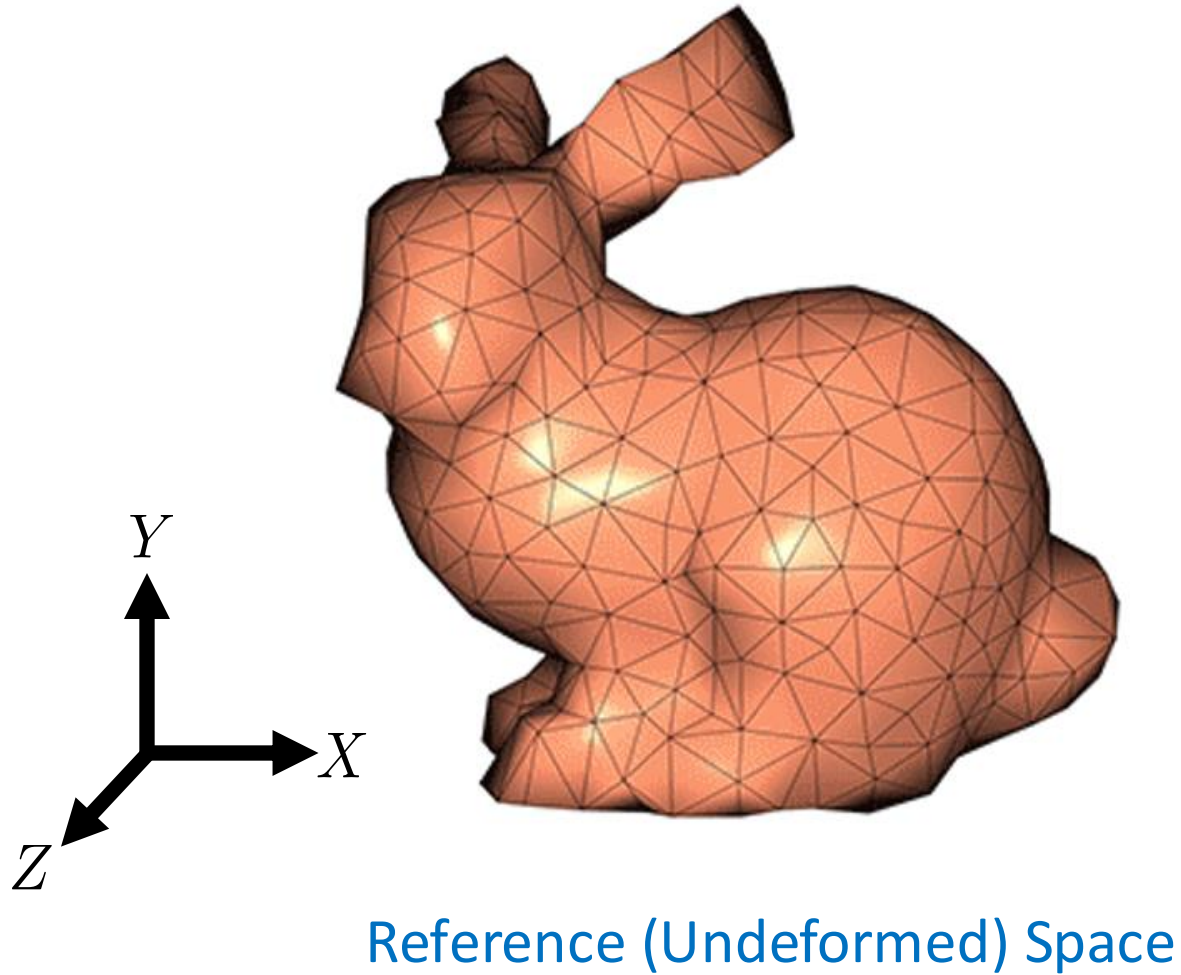


$$\mathbf{x}(\mathbf{X}, t) = \mathbf{J}(\mathbf{X})\mathbf{q}(t)$$





# Generalized Velocity of an Affine Body



$$\mathbf{v}(\mathbf{X}, t) = \mathbf{J}(\mathbf{X})\dot{\mathbf{q}}(t)$$

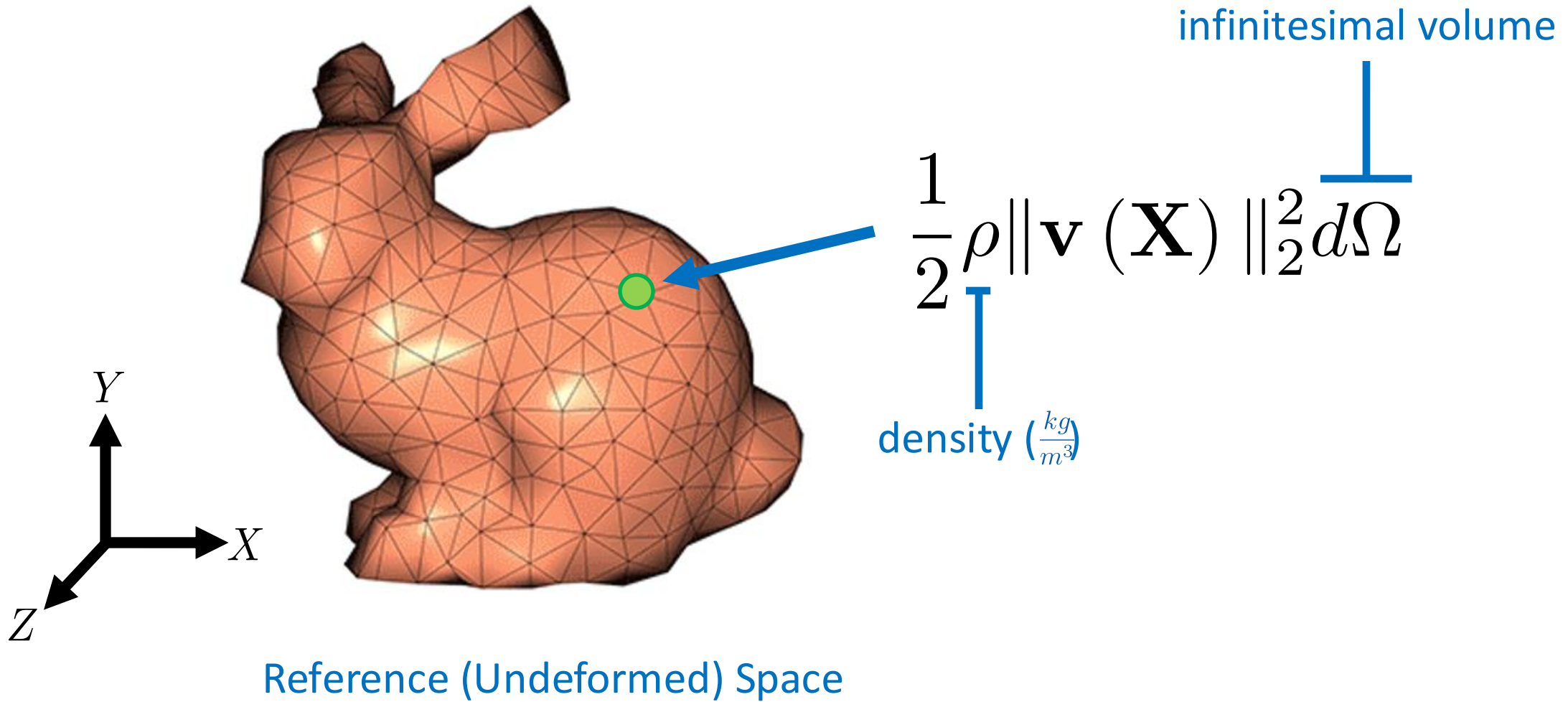




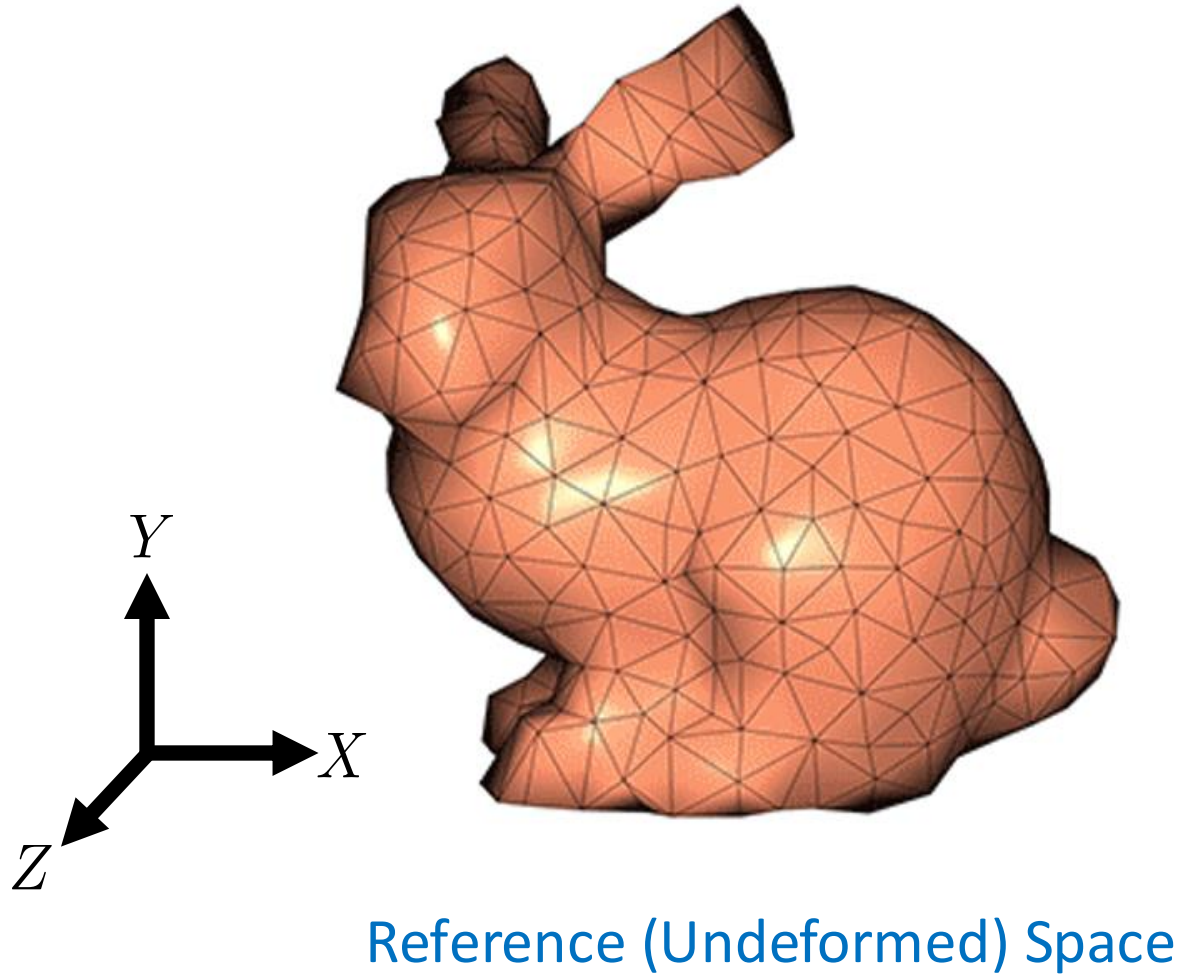
# Equations of Motion

$$M\ddot{\mathbf{q}} = - \frac{\partial V}{\partial \mathbf{q}}$$

# Kinetic Energy of an Affine Body



# Kinetic Energy of an Affine Body



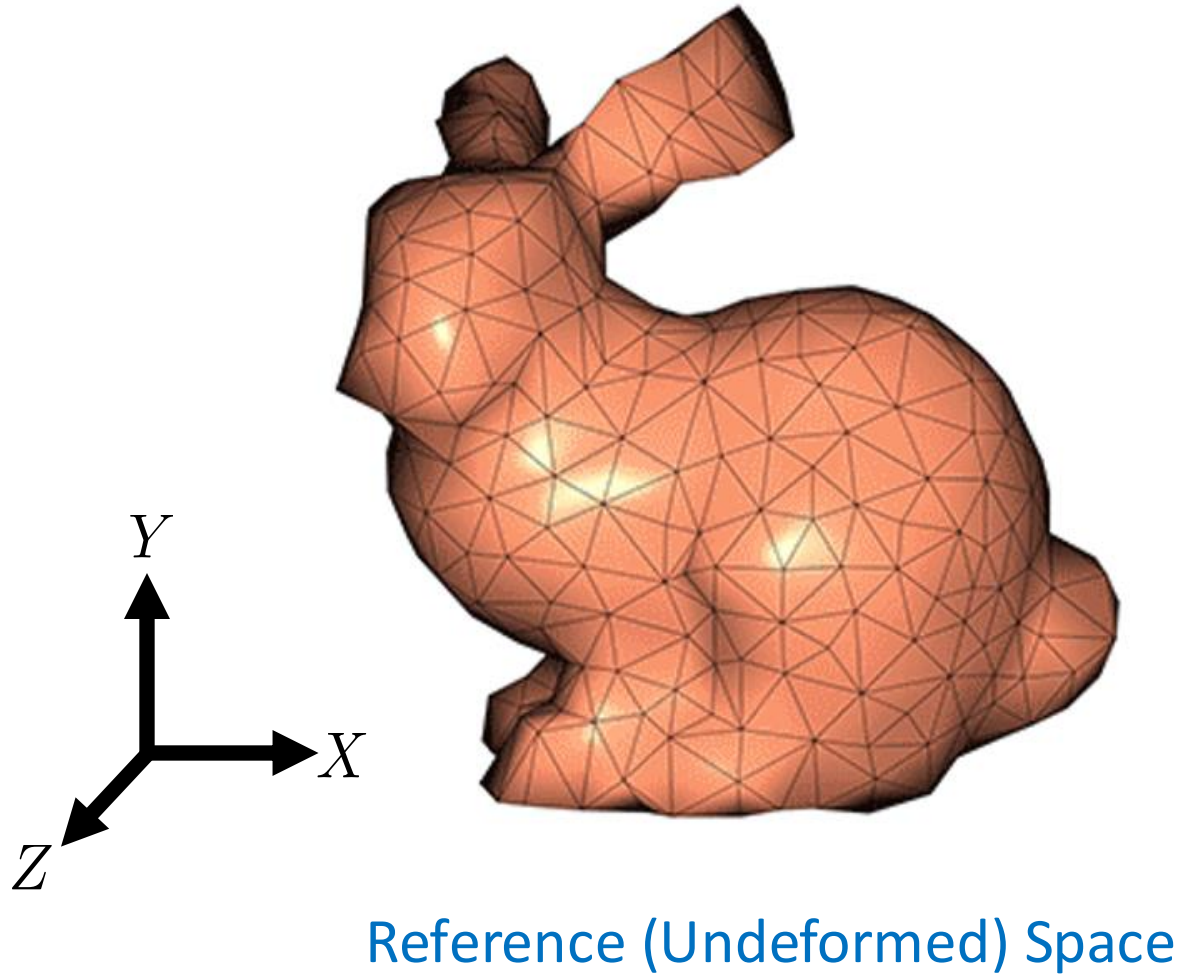
$$\frac{1}{2} \int_{\Omega} \rho \| \mathbf{v}(\mathbf{X}) \|^2 d\Omega$$

entire rigid body

infinitesimal volume



# Kinetic Energy of an Affine Body

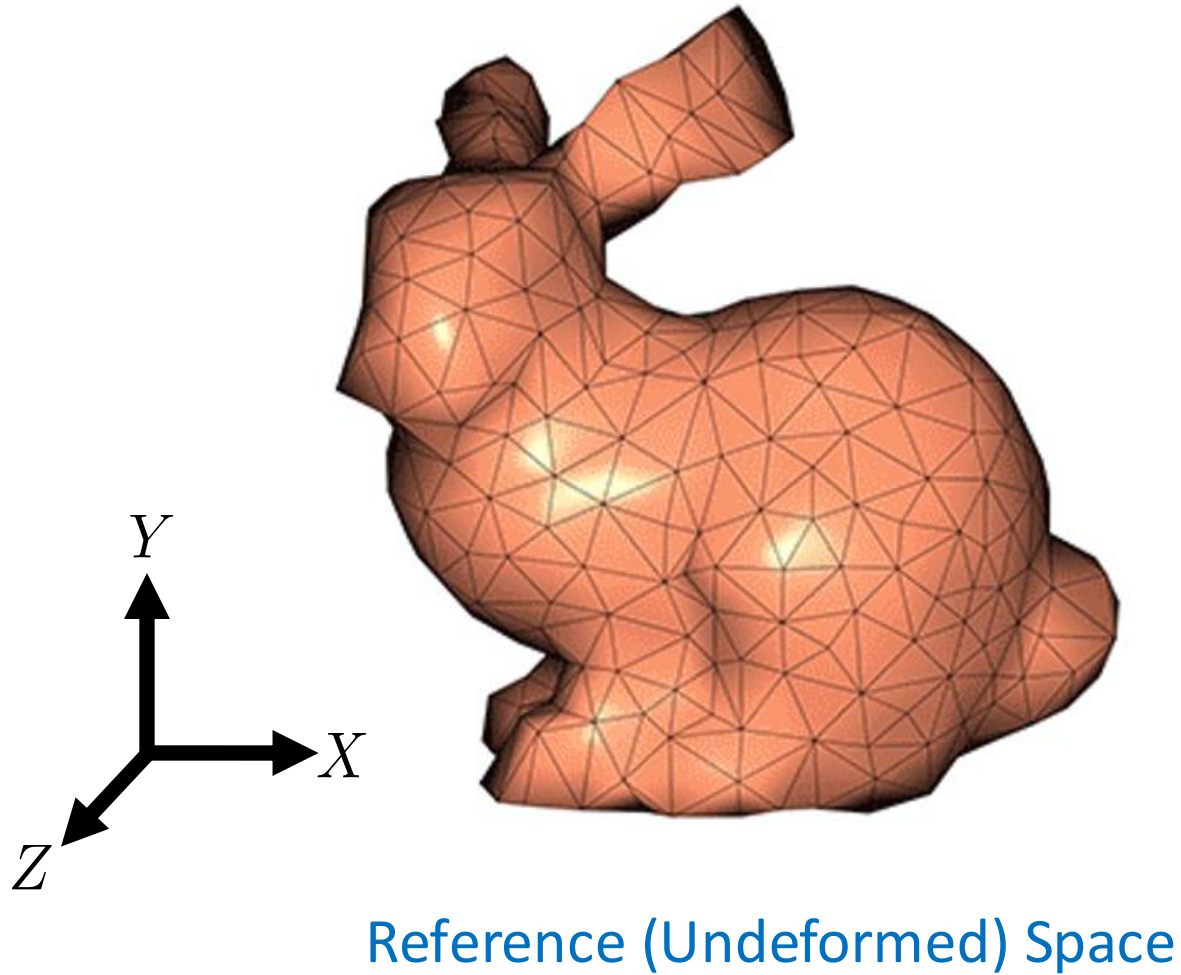


$$\frac{1}{2} \int_{\Omega} \rho \mathbf{v}^T \mathbf{v} d\Omega$$

entire rigid body



# Kinetic Energy of an Affine Body

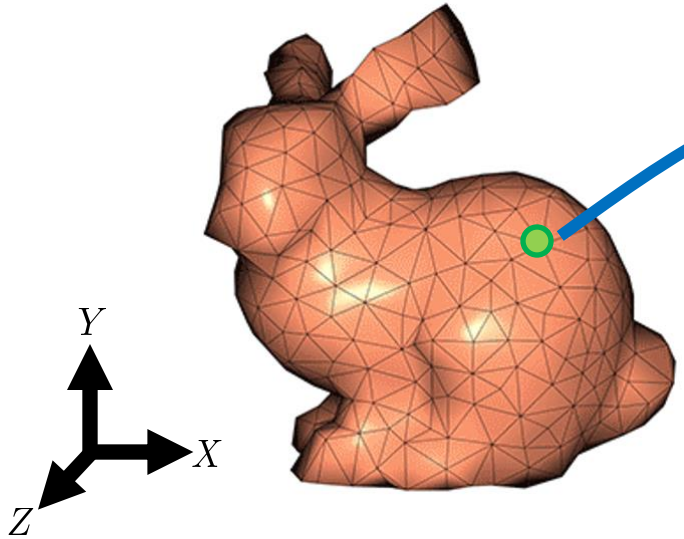


$$\frac{1}{2} \dot{\mathbf{q}}^T \left( \underbrace{\rho \int_{\Omega} \mathbf{J}(\mathbf{X})^T \mathbf{J}(\mathbf{X}) d\Omega}_{\mathbf{M}_0} \right) \dot{\mathbf{q}}$$

Mass Matrix  $\mathbf{M}$



Recall  $J$  ... What does this tell us about  $M_0$  ?



$$\begin{bmatrix} X & Y & Z & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \boxed{X} & \boxed{Y} & \boxed{Z} & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & X & Y & Z & 1 \end{bmatrix}$$

$J$



$$M_0 =$$

$$\begin{pmatrix} X^2 & XY & XZ & X & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ XY & Y^2 & YZ & Y & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ XZ & YZ & Z^2 & Z & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ X & Y & Z & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & X^2 & XY & XZ & X & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & XY & Y^2 & YZ & Y & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & XZ & YZ & Z^2 & Z & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & X & Y & Z & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & X^2 & XY & XZ & X \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & XY & Y^2 & YZ & Y \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & XZ & YZ & Z^2 & Z \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & X & Y & Z & 1 \end{pmatrix}$$

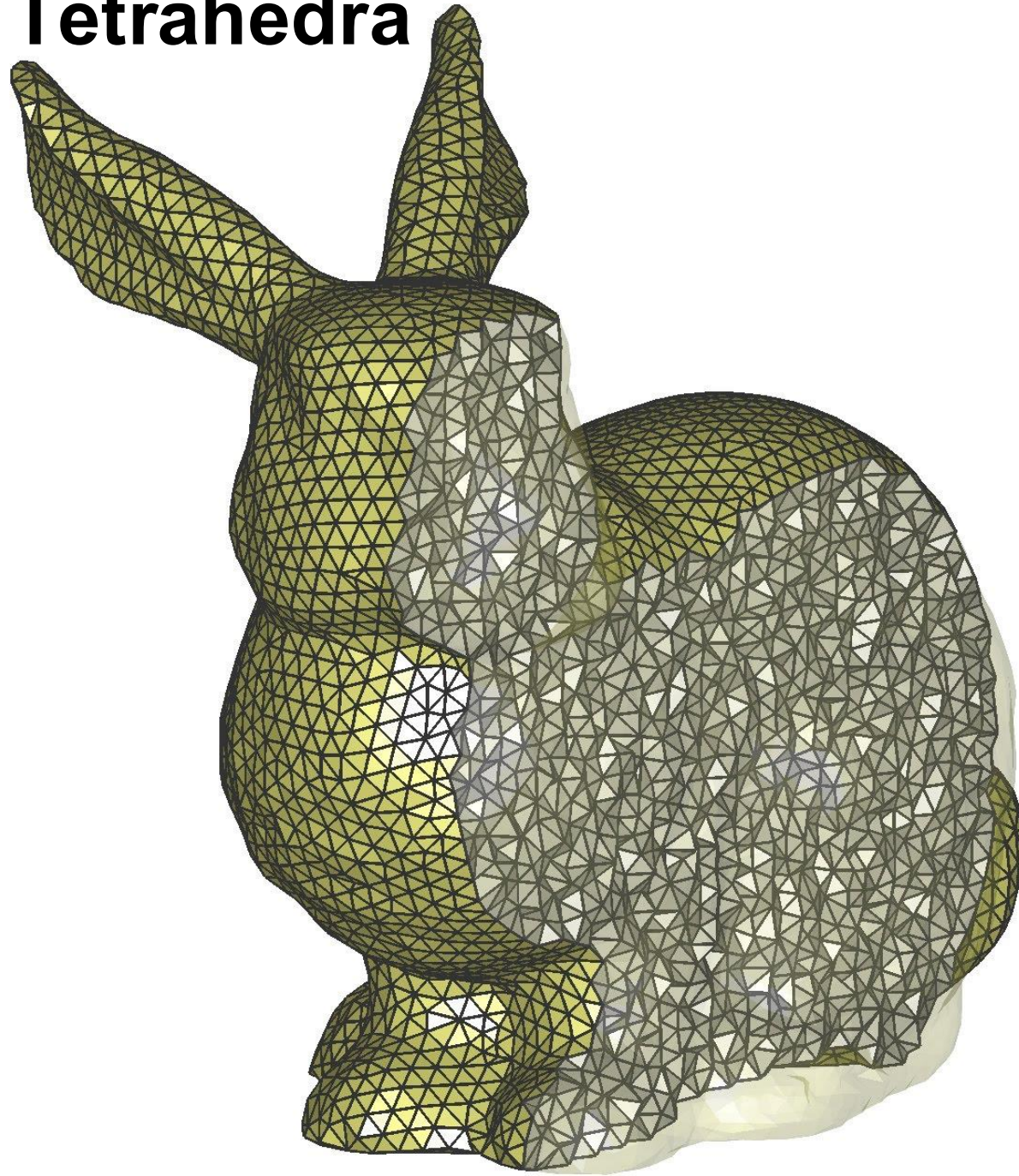
$$M_0 =$$

$$\begin{pmatrix} X^2 & XY & XZ & X & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ XY & Y^2 & YZ & Y & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ XZ & YZ & Z^2 & Z & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ X & Y & Z & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & X^2 & XY & XZ & X & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & XY & Y^2 & YZ & Y & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & XZ & YZ & Z^2 & Z & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & X & Y & Z & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & X^2 & XY & XZ & X \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & XY & Y^2 & YZ & Y \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & XZ & YZ & Z^2 & Z \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & X & Y & Z & 1 \end{pmatrix}$$

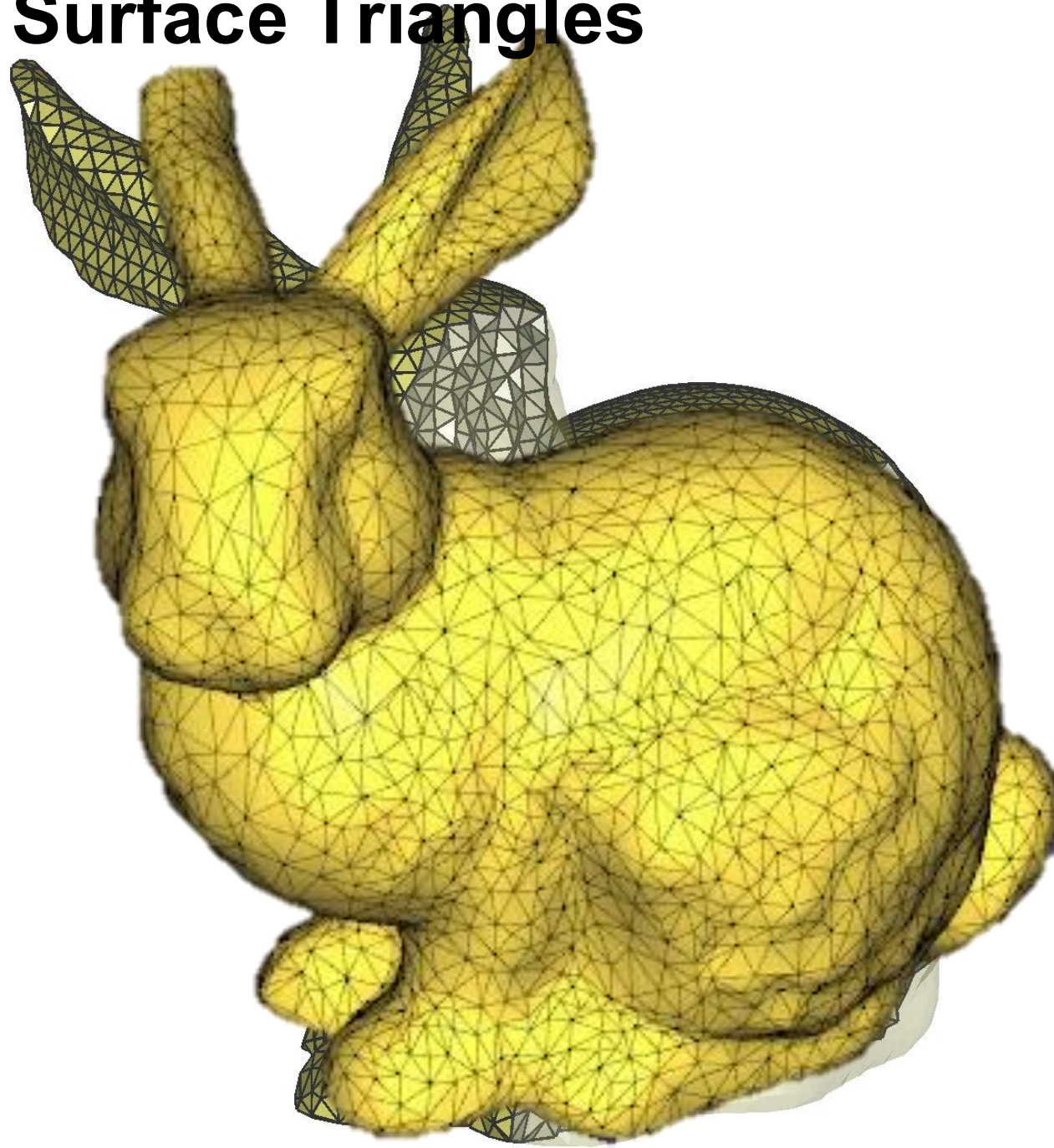
$$\int_{\Omega} X^2 d\Omega$$

Volume

# Integrate over Tetrahedra

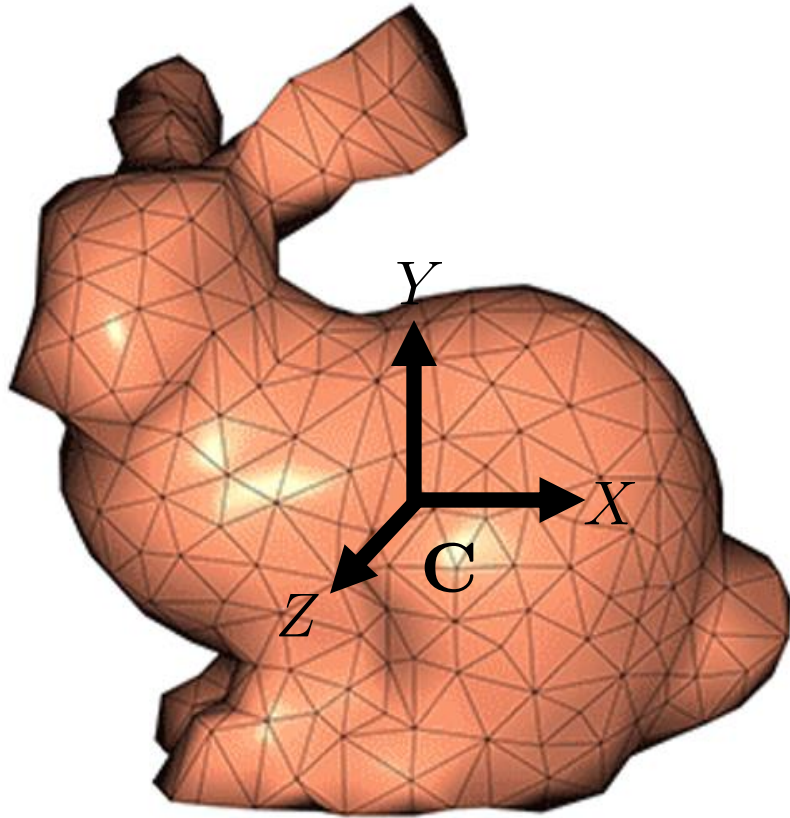


# Integrate over Surface Triangles





# Aside: Divergence Theorem

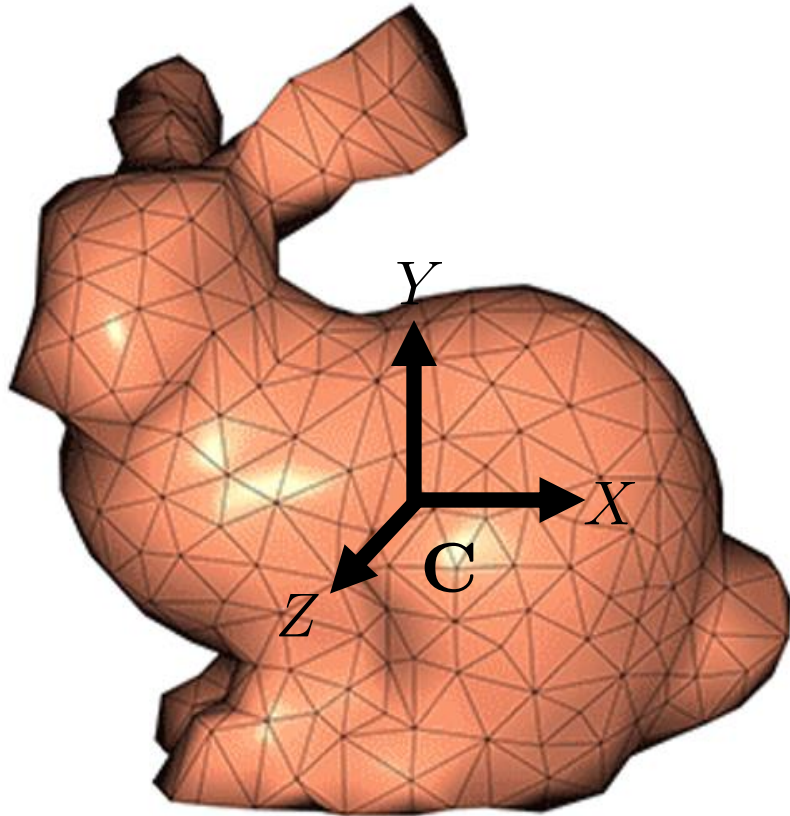


Reference (Undeformed) Space

$$\underbrace{\int_{\Omega} \nabla \cdot \overbrace{\mathbf{f}(\bar{\mathbf{X}})}^{\in \mathbb{R}^3} d\Omega}_{\text{volume integral}} = \underbrace{\int_{\Gamma} f(\bar{\mathbf{X}}) \cdot \overbrace{\mathbf{n}}^{\text{surface normal}} d\Gamma}_{\text{surface integral}}$$



# Integrate over Volume



Express using divergence

$$\int_{\Omega} x^2 d\Omega = \int_{\Omega} \nabla \cdot \begin{bmatrix} ? \\ ? \\ ? \end{bmatrix} d\Omega$$

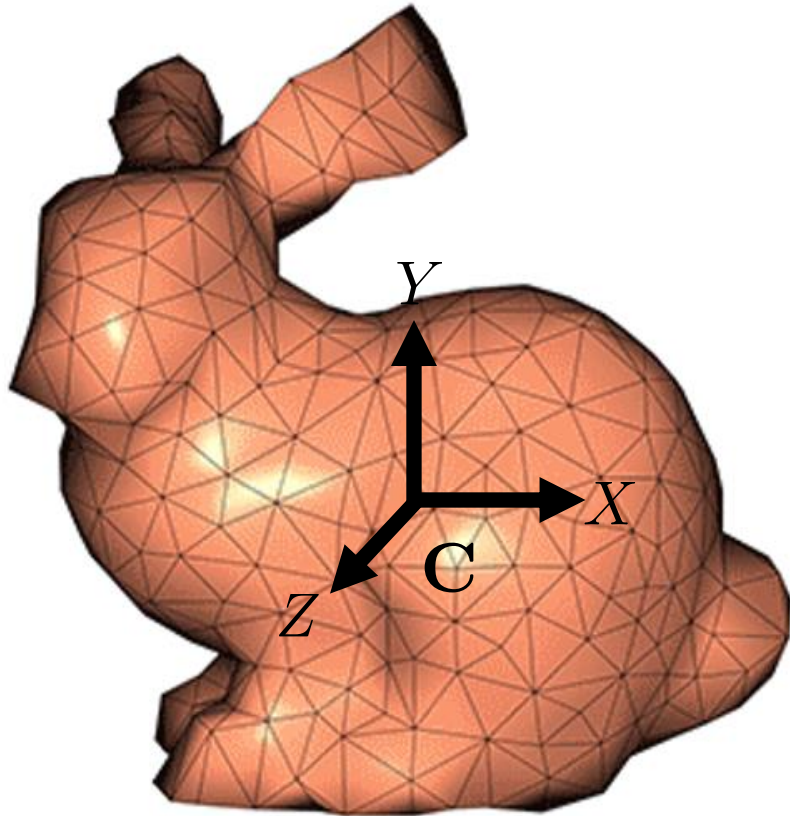
Reference (Undeformed) Space

**Reminder**  $\nabla \cdot \begin{bmatrix} a \\ b \\ c \end{bmatrix} = \frac{\partial a}{\partial x} + \frac{\partial b}{\partial y} + \frac{\partial c}{\partial z}$





# Integrate over Volume



Express using divergence

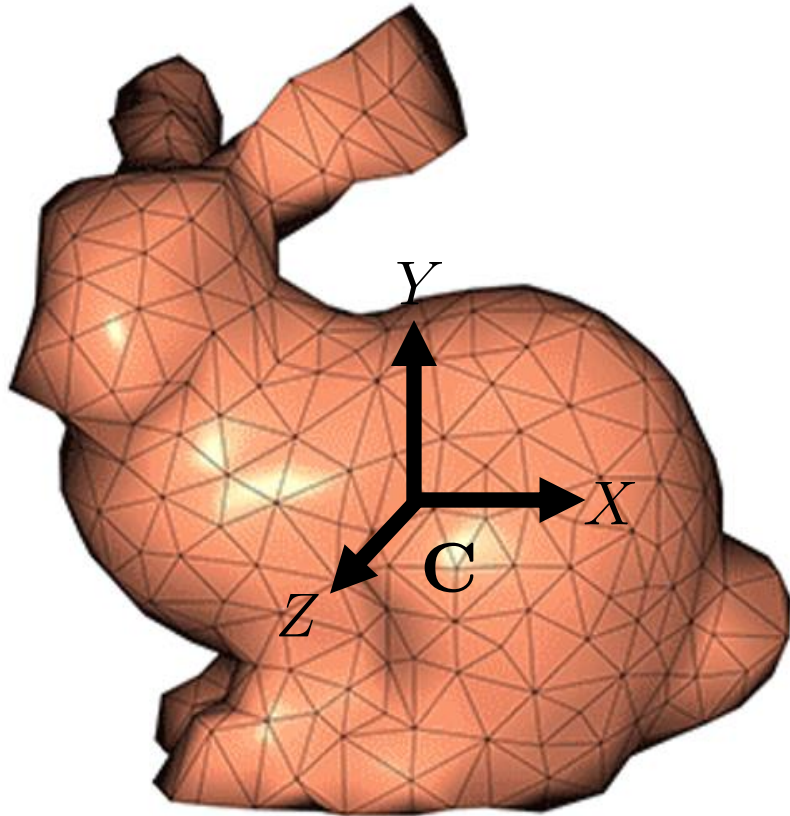
$$\int_{\Omega} X^2 d\Omega = \int_{\Omega} \nabla \cdot \begin{bmatrix} \frac{1}{3} X^3 \\ 0 \\ 0 \end{bmatrix} d\Omega$$

Reference (Undeformed) Space

**Reminder**  $\nabla \cdot \begin{bmatrix} a \\ b \\ c \end{bmatrix} = \frac{\partial a}{\partial x} + \frac{\partial b}{\partial y} + \frac{\partial c}{\partial z}$



# Integrate over Surface



Reference (Undeformed) Space

Convert to Surface Integral

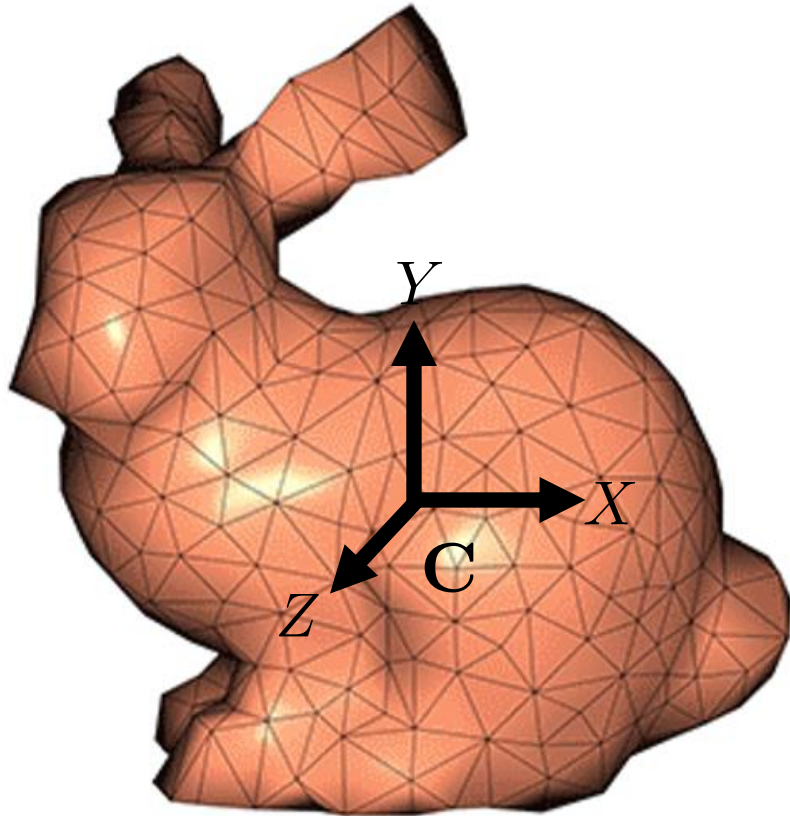
$$\int_{\Gamma} \frac{1}{3} X^3 n_x d\Gamma$$

A blue vertical line points from the  $d\Gamma$  term in the integral to the text 'Little surface area' below.

Little surface area



# Integrate over Triangles !!!!



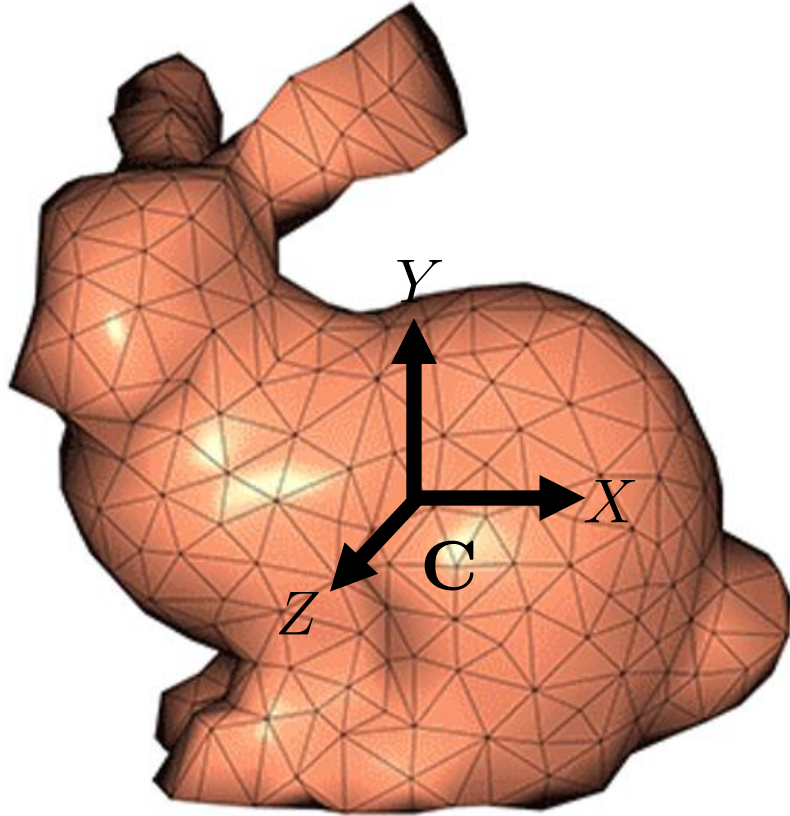
Reference (Undeformed) Space

Convert to Surface Integral

$$\sum_{i=0}^{|T|} \int_{T_i} \frac{1}{3} X^3 \underset{\substack{\text{Triangle Area}}}{n_x} dT$$



# Barycentric Integration for Each Triangle



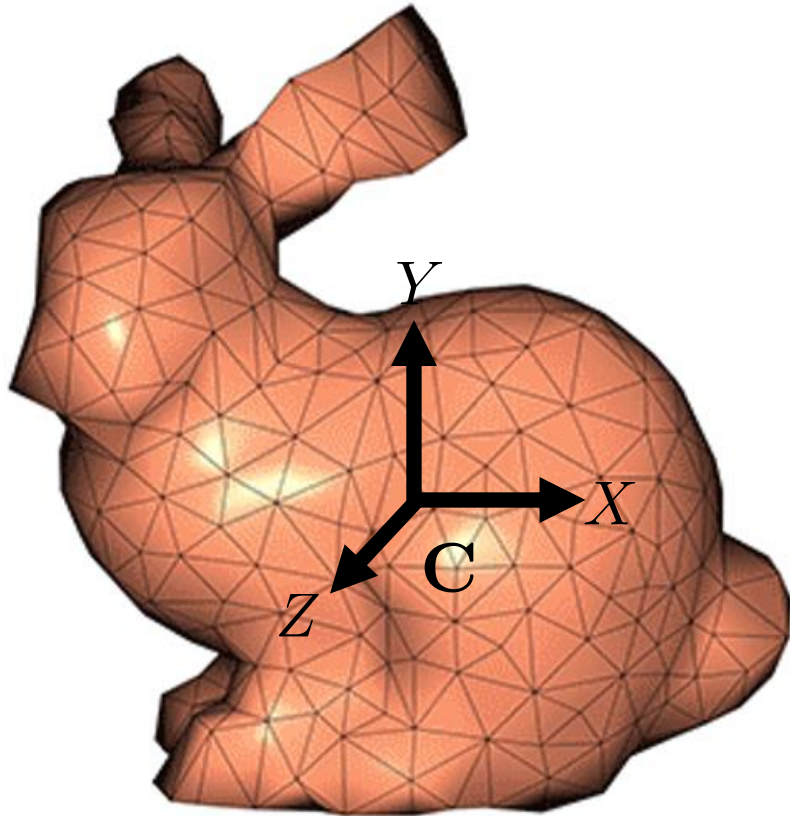
Reference (Undeformed) Space

Convert to Surface Integral

$$\int_{T_i} \frac{1}{3} X^3 n_x dT$$



# Barycentric Integration for Each Triangle



Reference (Undeformed) Space

Replace  $X$  (resp  $Y, Z$ ) with:

$$X = \sum_{i=0}^2 X_i \phi_i(\mathbf{X})$$

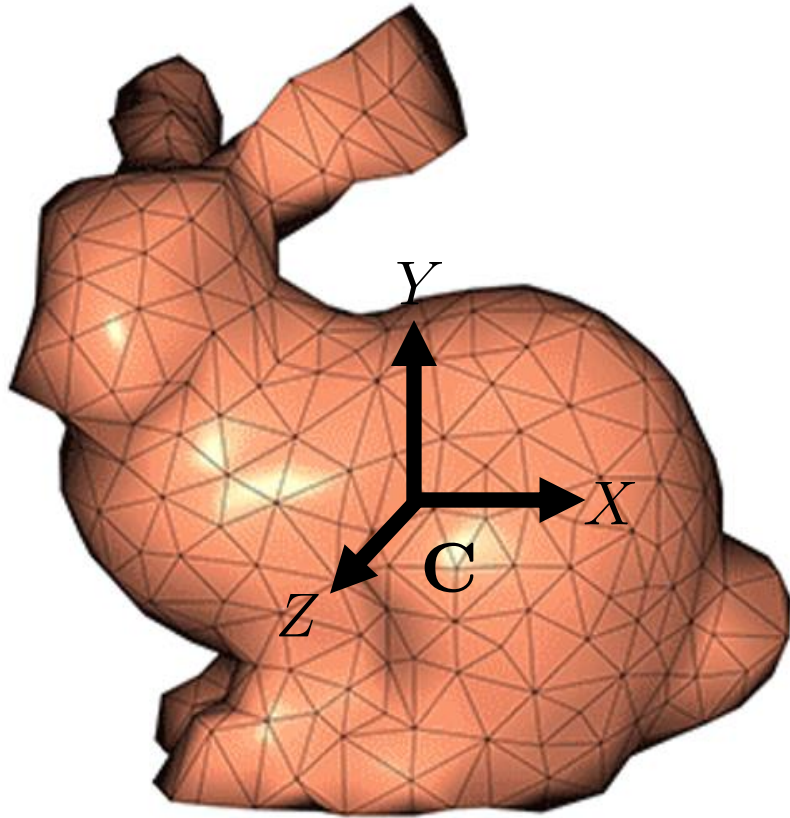
$\mathbf{T}$

Barycentric Coordinates





# Barycentric Integration for Each Triangle



Integrate using Barycentric Coordinates

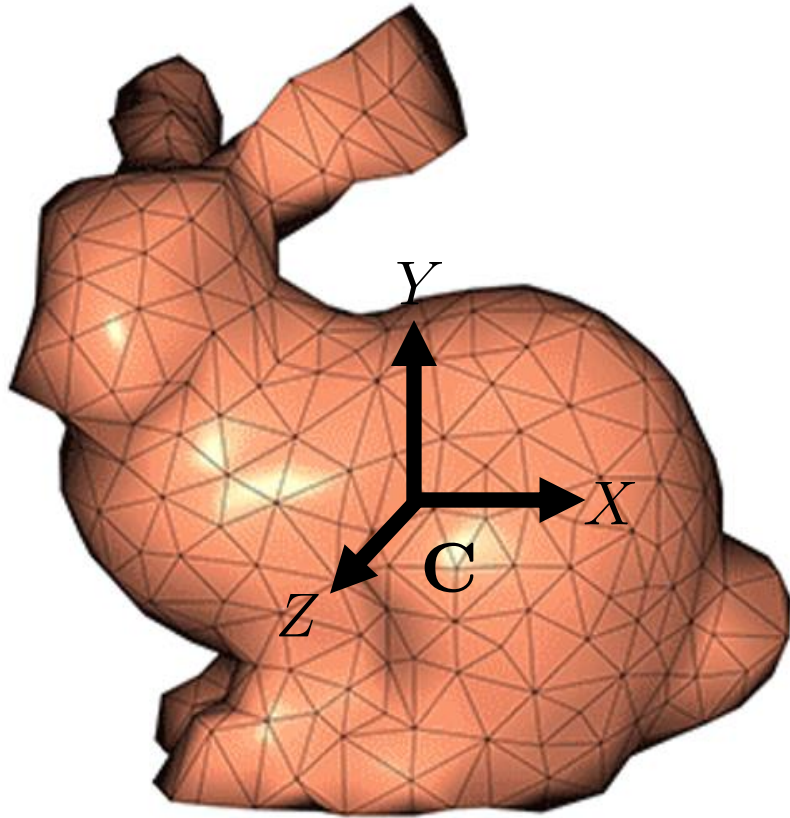
$$\int_0^1 \int_0^{1-\phi_1} \frac{1}{3} X(\phi_1, \phi_2))^3 n_x d\phi_1 d\phi_2$$

Reference (Undeformed) Space





# Add up to form full Mass Matrix



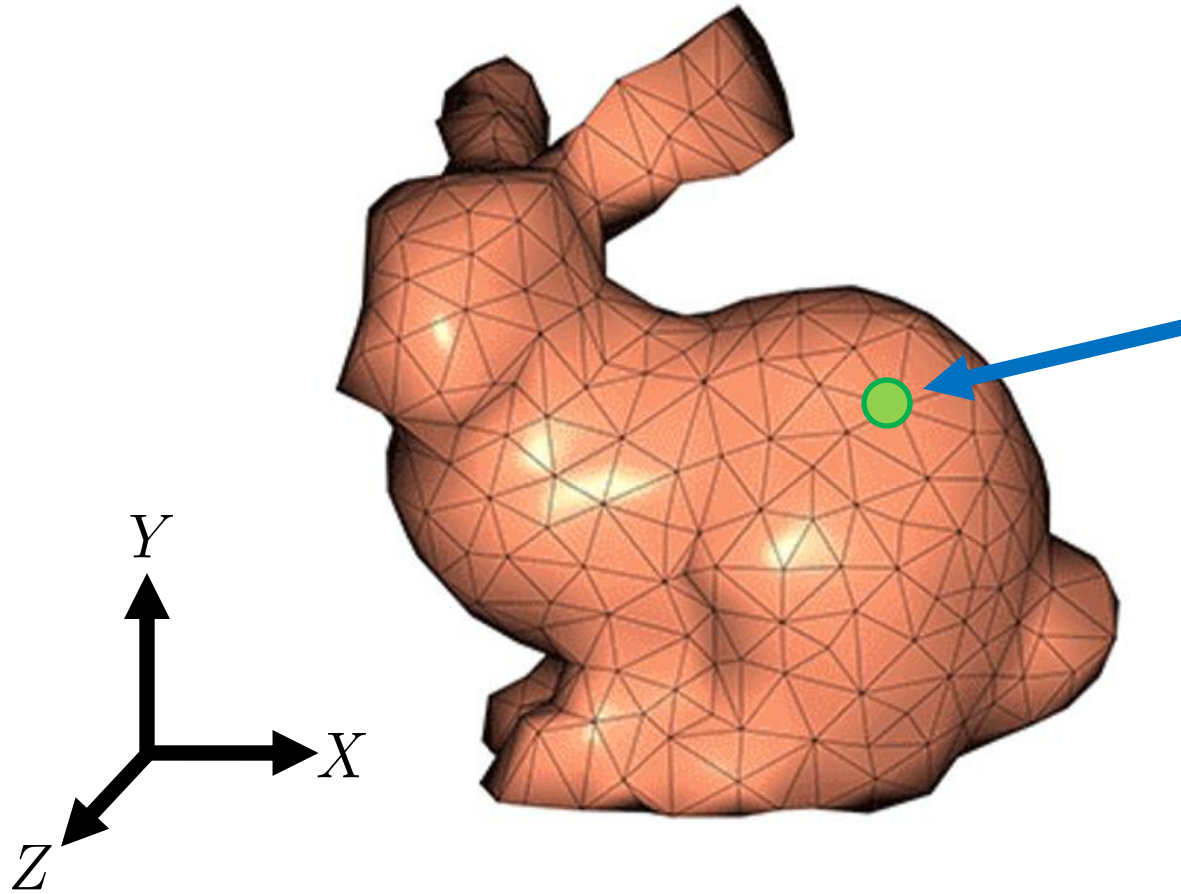
Reference (Undeformed) Space

Convert to Surface Integral

$$\sum_{i=0}^{|T|} \int_{T_i} \frac{1}{3} X^3 \underset{\substack{\text{Triangle Area}}}{T} n_x dT$$



# Potential Energy of Affine Body



Reference (Undeformed) Space

$$\psi(q) = \text{????}$$

How do we keep the object rigid ?



# What Makes an Object Rigid ?

$$\Delta \mathbf{X}^T (\mathbf{F}^T \mathbf{F} - \mathbf{I}) \Delta \mathbf{X} = \mathbf{0}$$

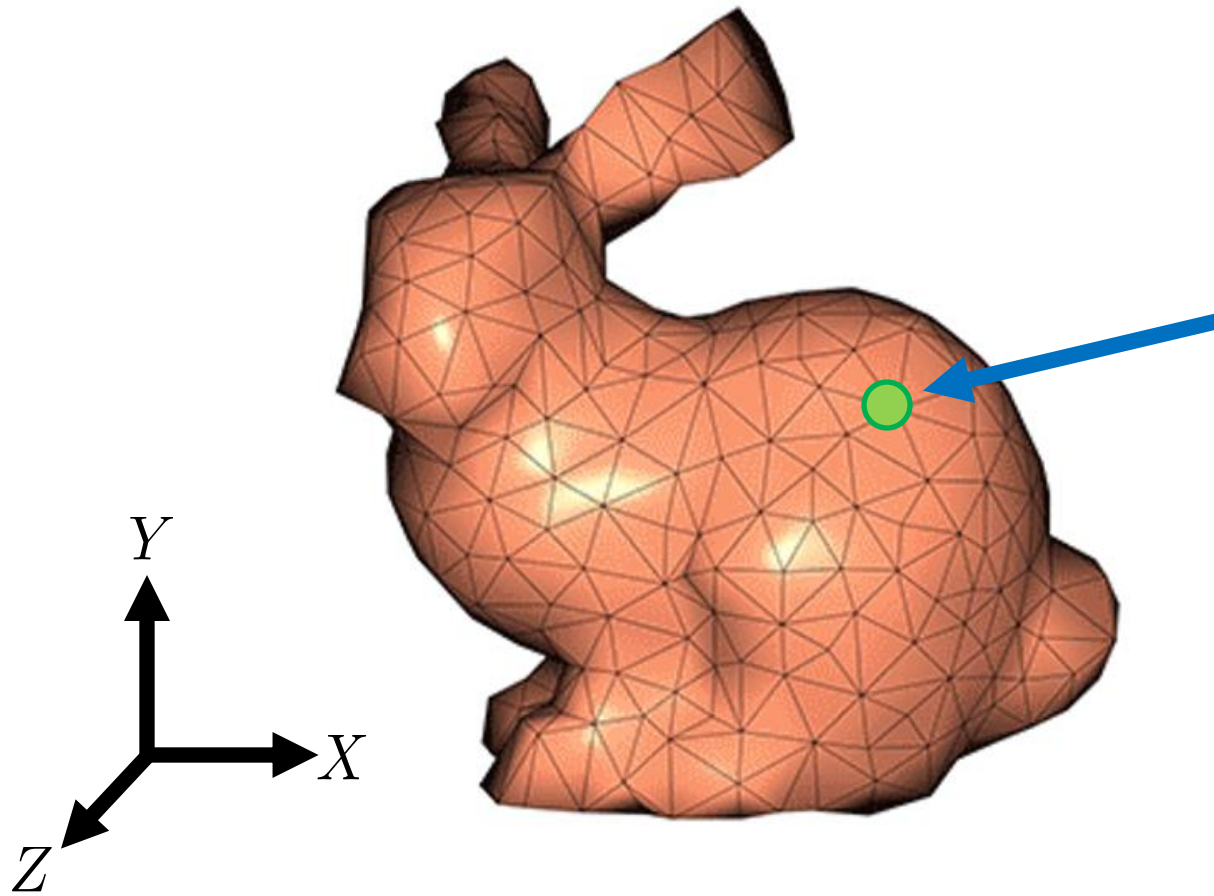
Implies

$$\mathbf{F}^T \mathbf{F} = \mathbf{I}$$

Orthogonal



# Potential Energy of Affine Body



Reference (Undeformed) Space

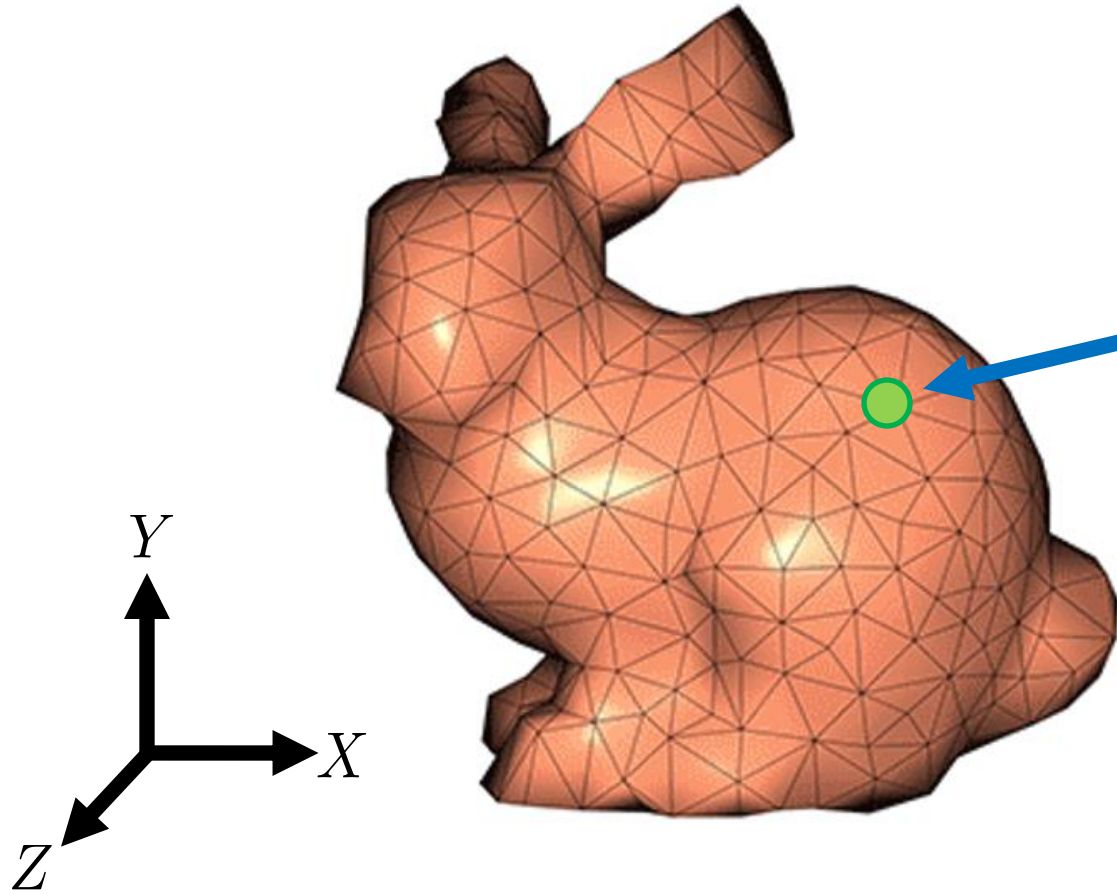
Set this to a big value

$$\psi = \kappa \left\| F^T F - I \right\|_F^2 d\Omega$$

How do we keep the object rigid ?



# Potential Energy of Affine Body

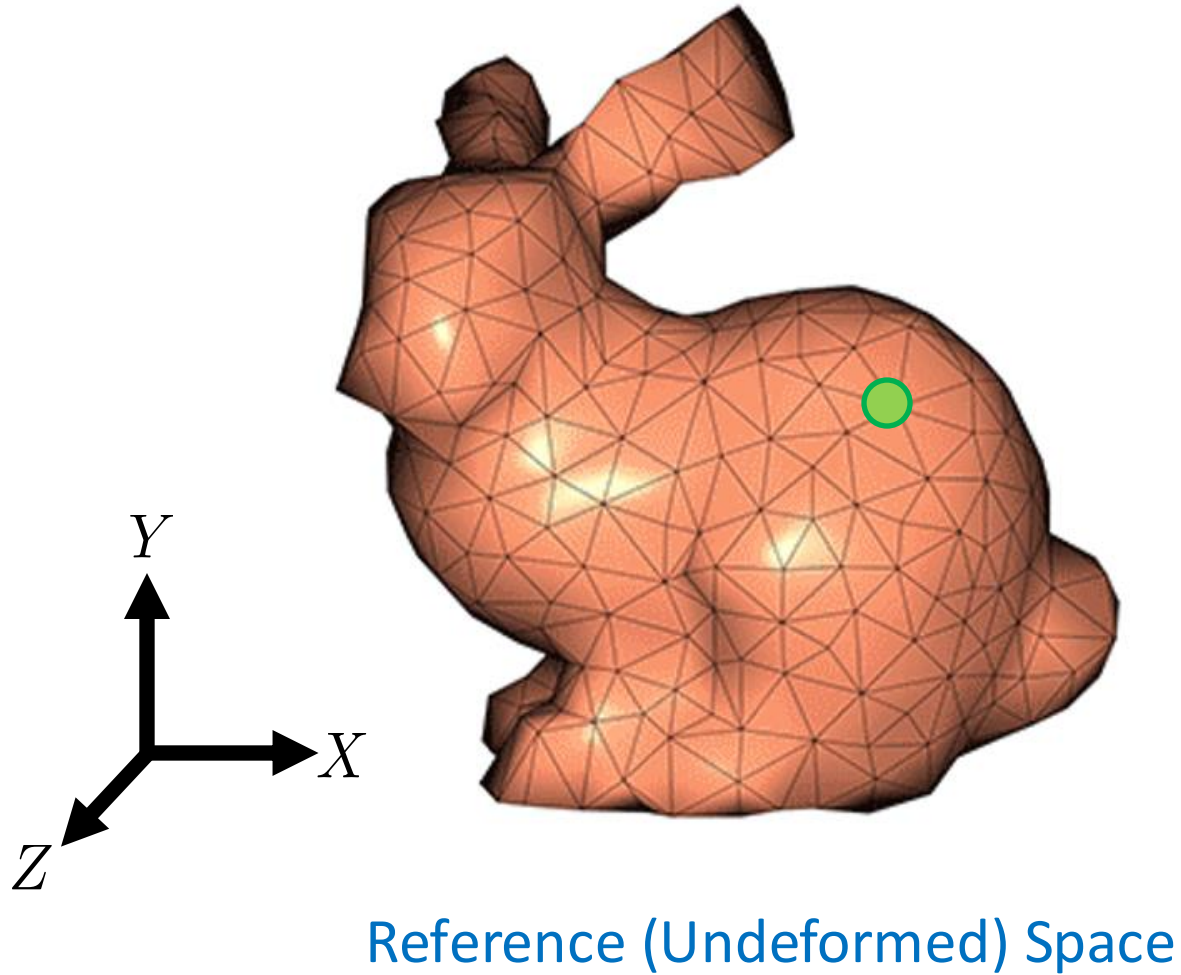


$$V = \int \kappa ||F^T F - I||_F^2 d\Omega$$

Reference (Undeformed) Space



# But what is the Deformation Gradient ?

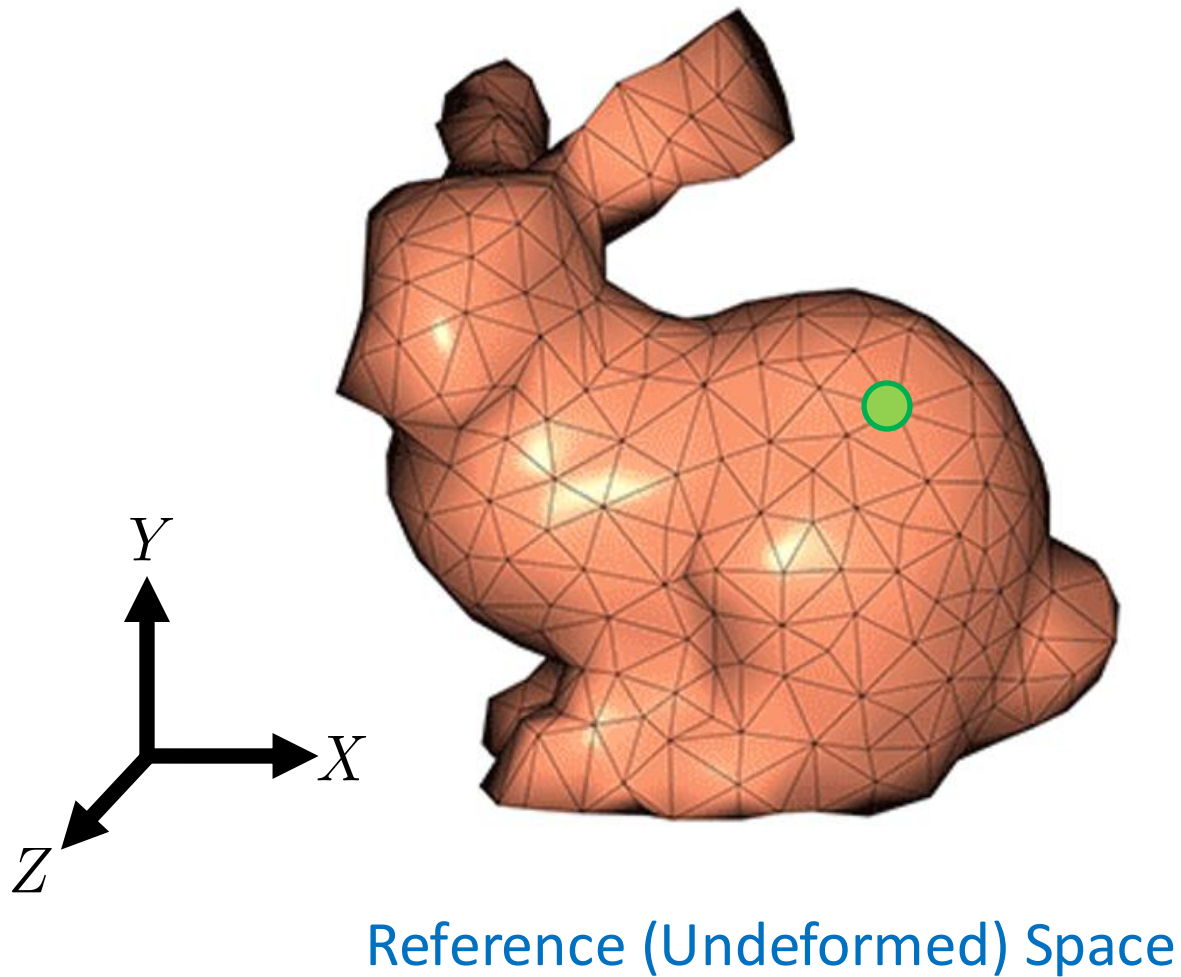


$$\mathbf{x}(\mathbf{X}, t) = \mathbf{J}(\mathbf{X})\mathbf{q}(t)$$



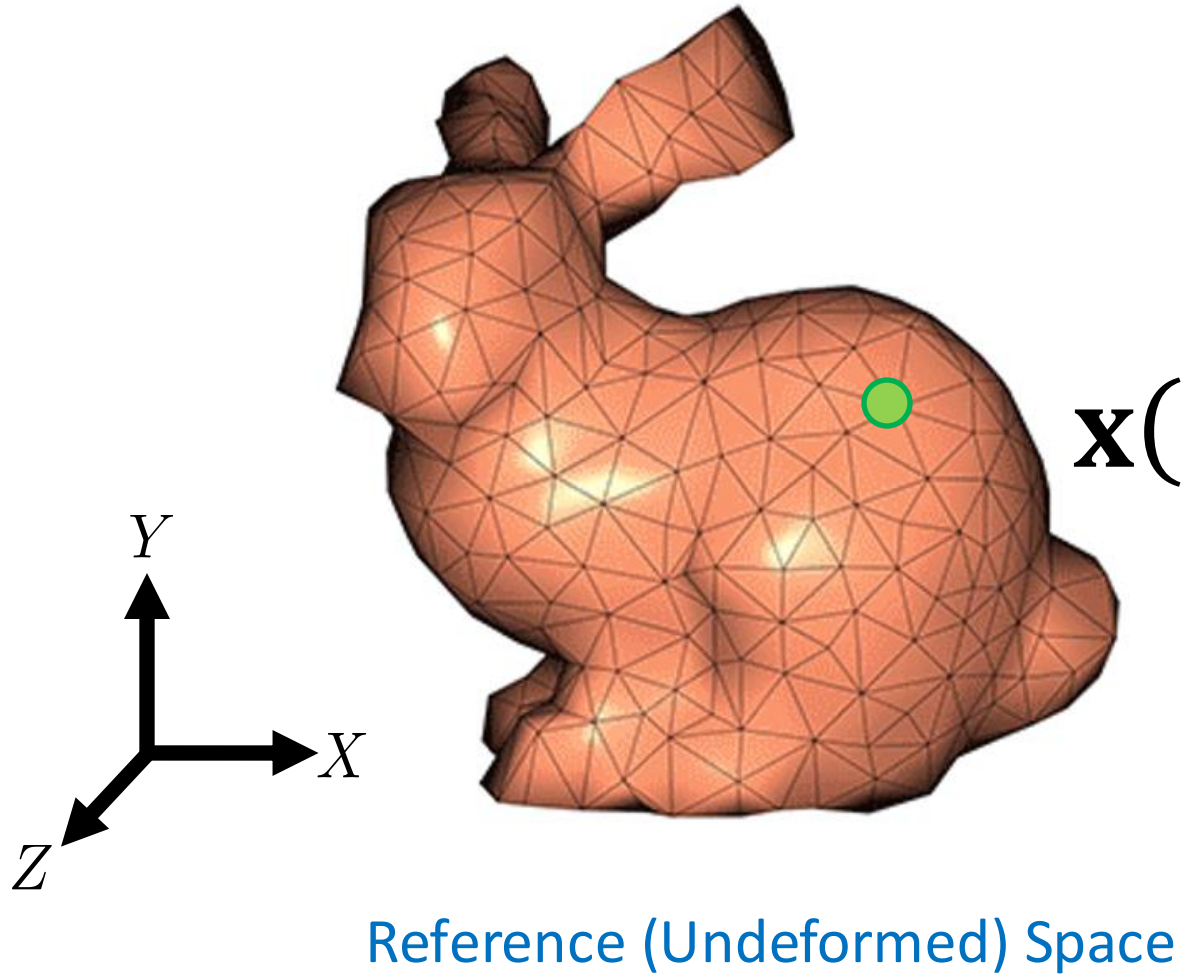


# But what is the Deformation Gradient ?



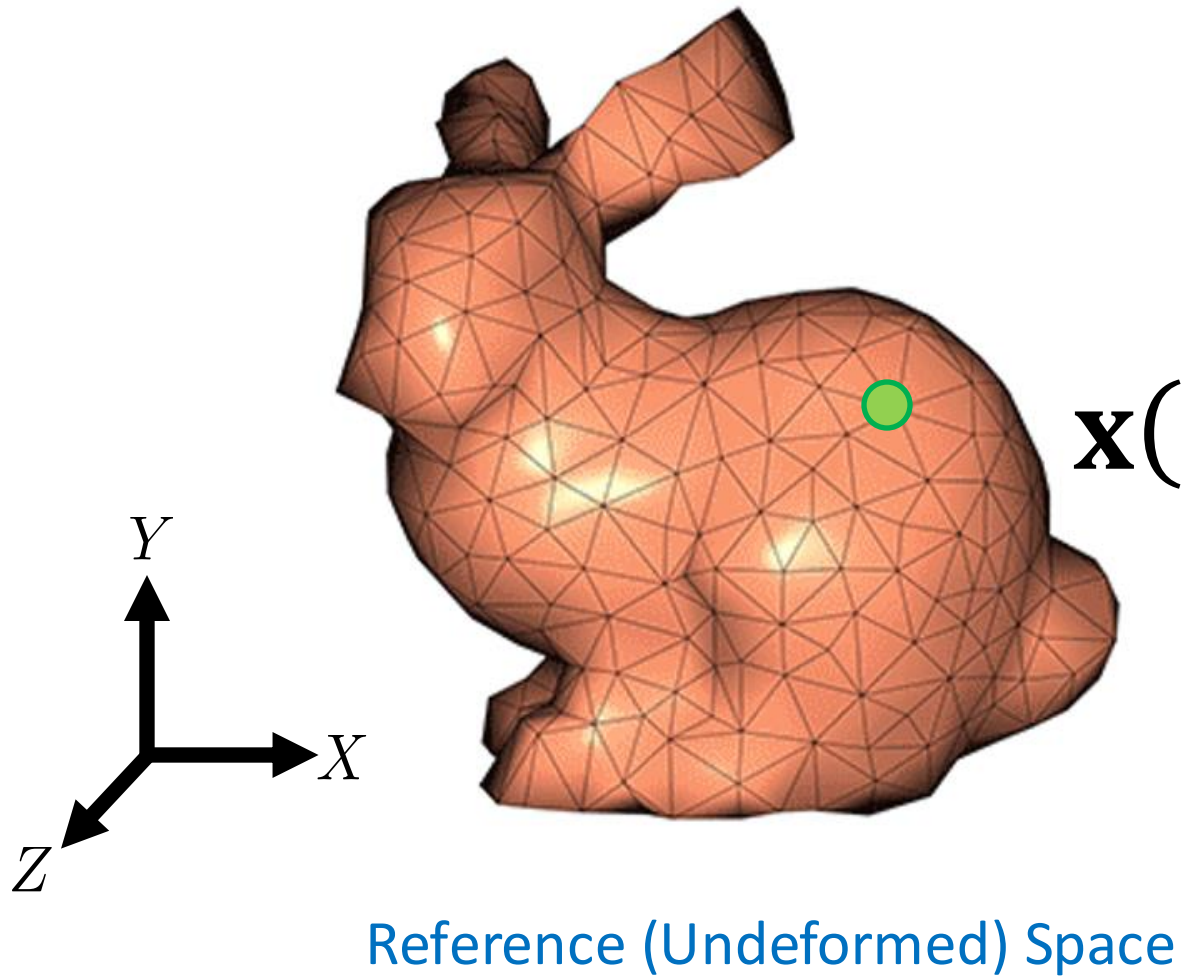
$$\mathbf{x}(\mathbf{X}, t) = \underbrace{Q(t)}_{\substack{\begin{pmatrix} q_0 & q_1 & q_2 & q_3 \\ q_4 & q_5 & q_6 & q_7 \\ q_8 & q_9 & q_{10} & q_{11} \end{pmatrix} \\ \text{Linear Transform} \quad \text{Translation}}} \begin{bmatrix} \mathbf{X} \\ 1 \end{bmatrix}$$

# But what is the Deformation Gradient ?



$$\mathbf{x}(\mathbf{X}, t) = \begin{bmatrix} q_0 & q_1 & q_2 \\ q_4 & q_5 & q_6 \\ q_8 & q_9 & q_{10} \end{bmatrix} \mathbf{X} + \begin{bmatrix} q_3 \\ q_7 \\ q_{11} \end{bmatrix}$$

# But what is the Deformation Gradient ?

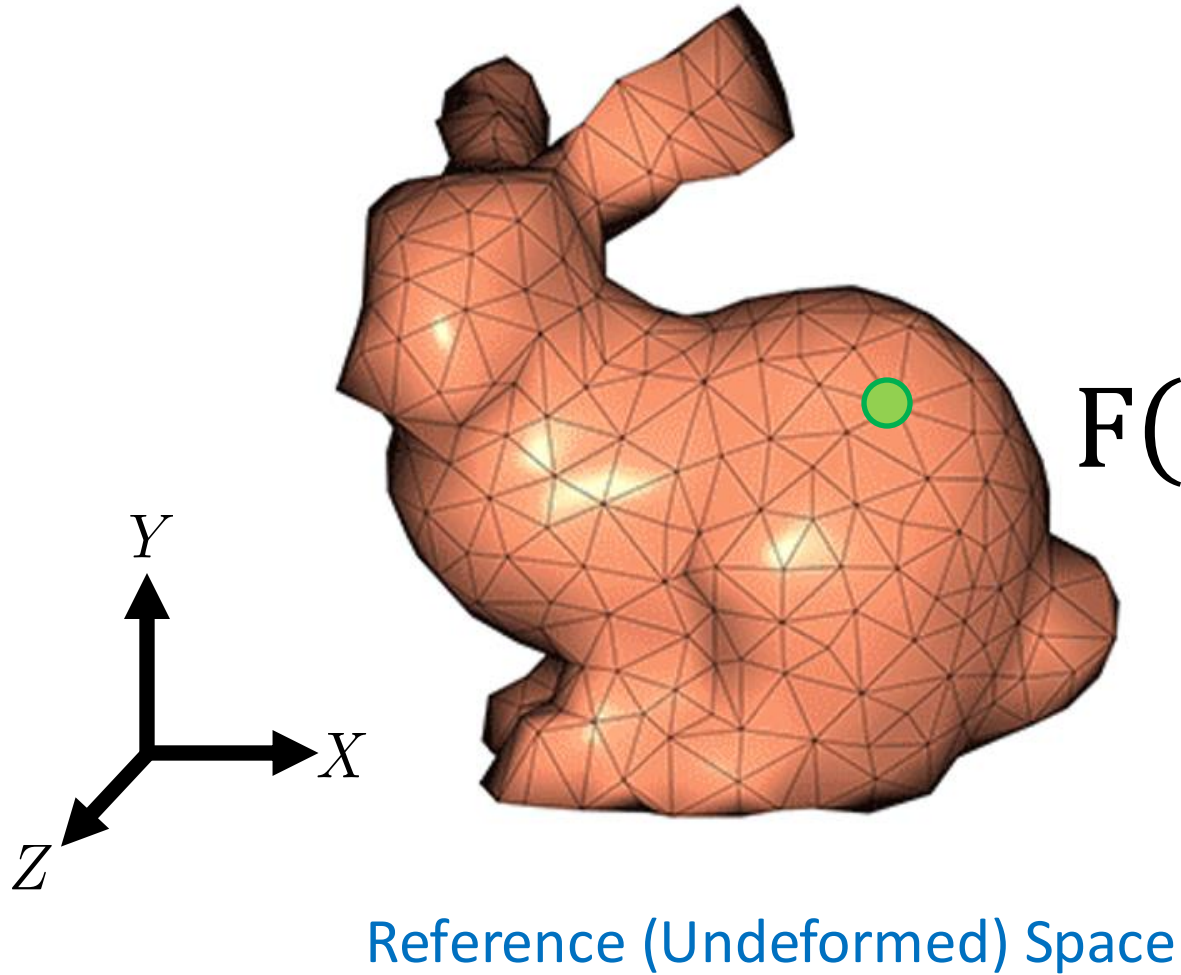


$$\mathbf{x}(\mathbf{X}, t) = \begin{bmatrix} q_0 & q_1 & q_2 \\ q_4 & q_5 & q_6 \\ q_8 & q_9 & q_{10} \end{bmatrix} \mathbf{X} + \begin{bmatrix} q_3 \\ q_7 \\ q_{11} \end{bmatrix}$$

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$$F = \frac{\partial \mathbf{x}}{\partial \mathbf{X}}$$

# But what is the Deformation Gradient ?

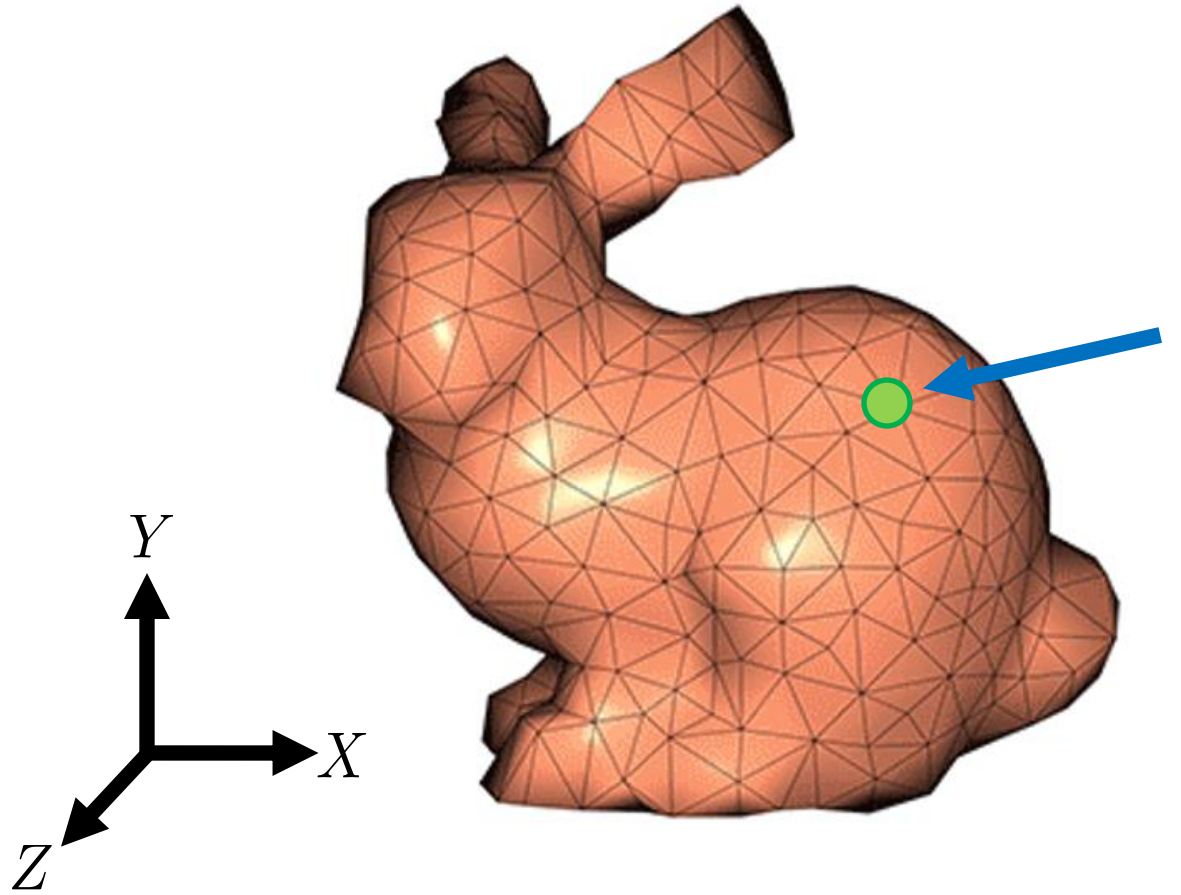


$$\mathbf{F}(\mathbf{X}, t) =$$

$$\begin{bmatrix} q_0 & q_1 & q_2 \\ q_4 & q_5 & q_6 \\ q_8 & q_9 & q_{10} \end{bmatrix}$$

$$\mathbf{F} = \frac{\partial \mathbf{x}}{\partial \mathbf{X}}$$

# Potential Energy of Affine Body



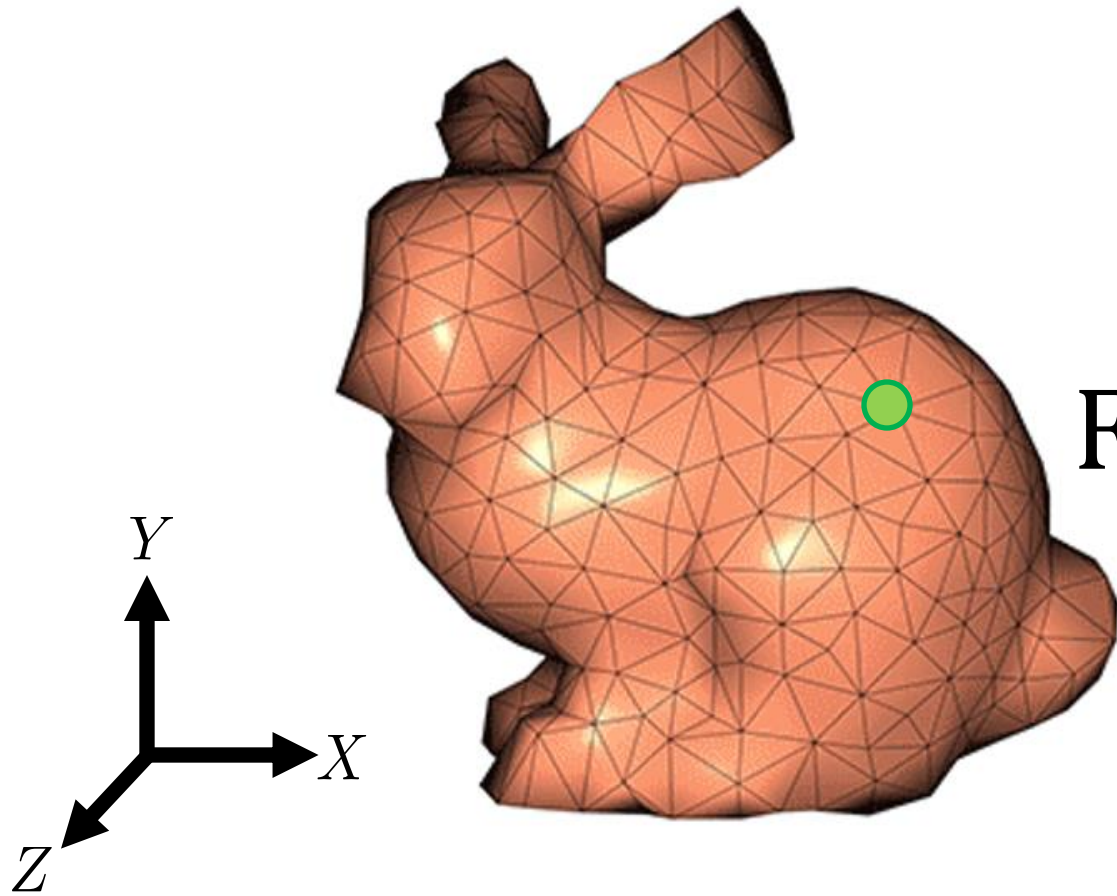
$$V(\mathbf{q}) = \int \kappa ||F^T F - I||_F^2 d\Omega$$

Reference (Undeformed) Space





# But what is the Deformation Gradient ?



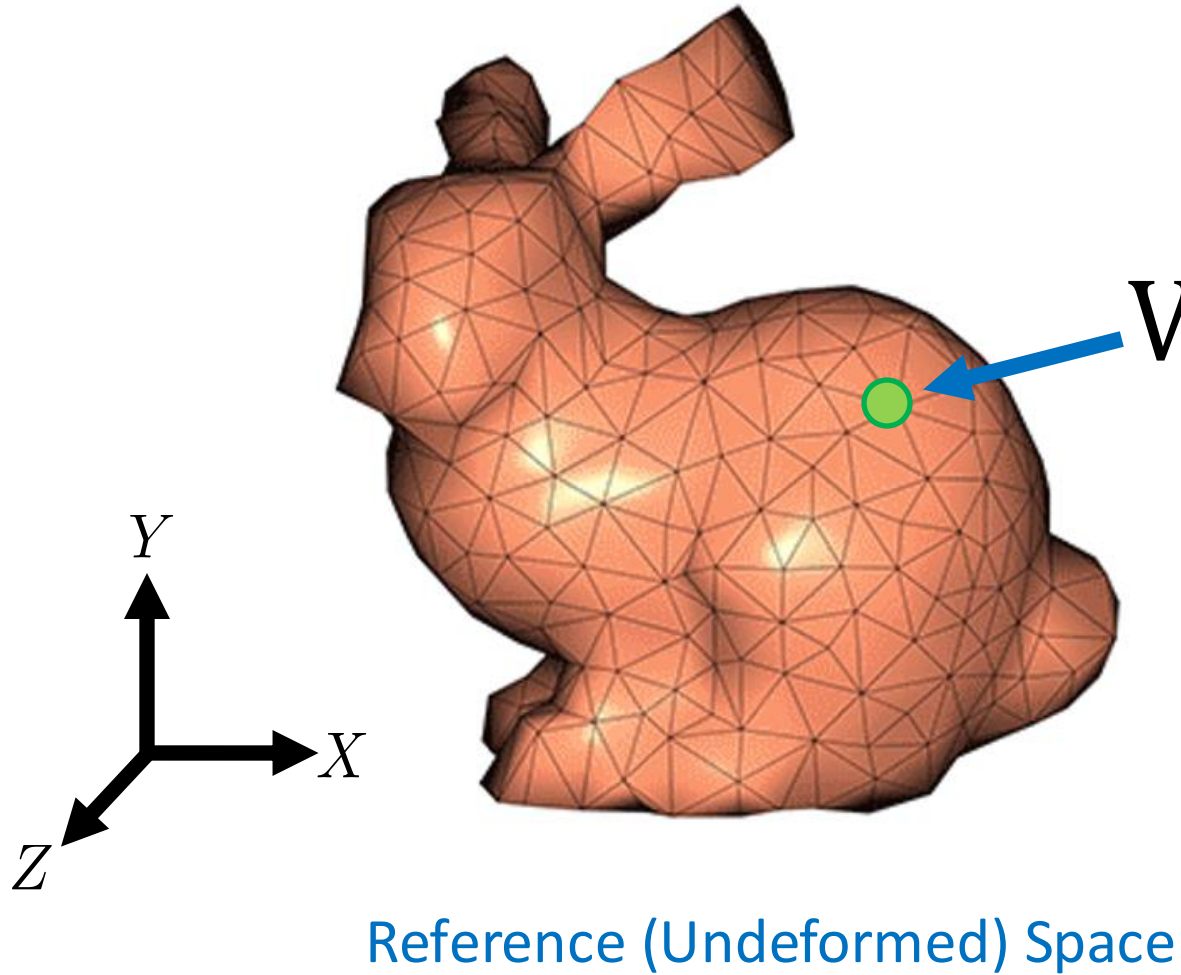
$$\mathbf{F}(\mathbf{X}, t) = \begin{bmatrix} q_0 & q_1 & q_2 \\ q_4 & q_5 & q_6 \\ q_8 & q_9 & q_{10} \end{bmatrix}$$

Reference (Undeformed) Space

How does this change as a function of  $\mathbf{X}$ ?



# Potential Energy of Affine Body

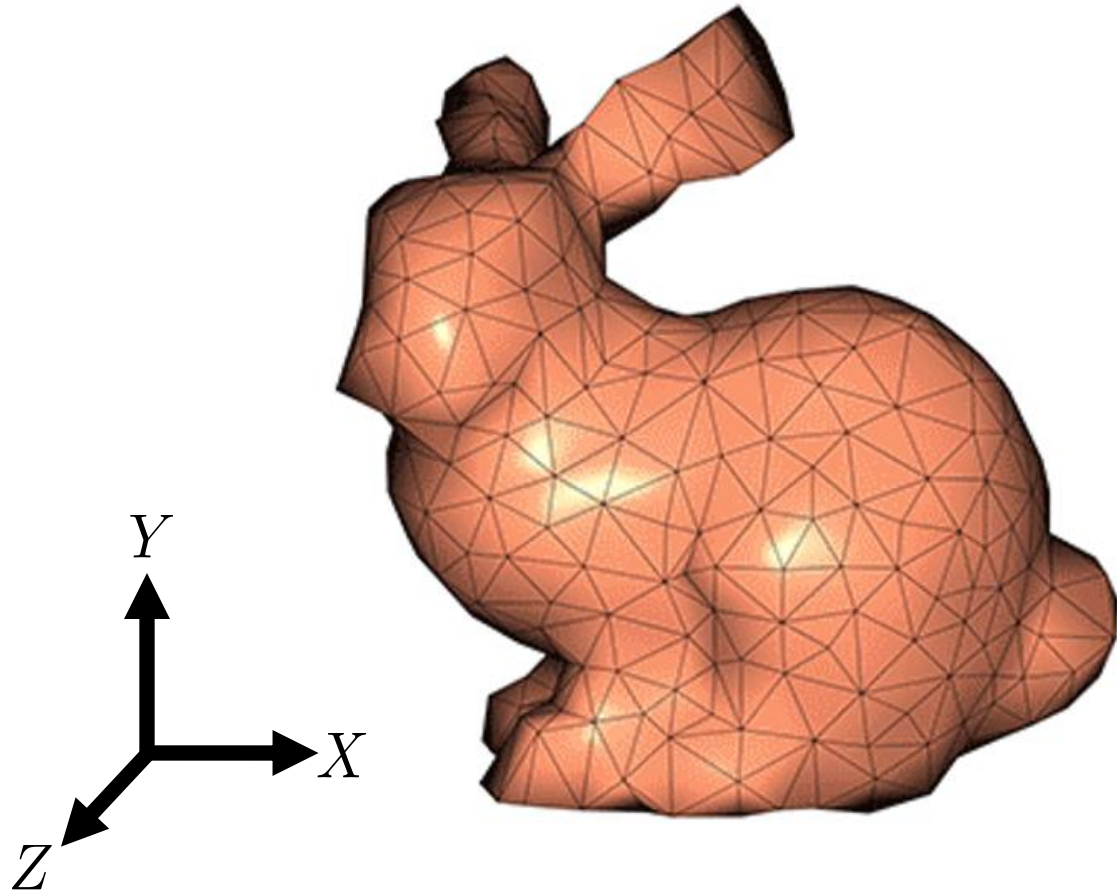


$$V(\mathbf{q}) = \kappa \cdot \text{vol} \cdot \left\| F^T F - I \right\|_F^2$$

Volume of Rigid Body



# Kinetic Energy of an Affine Body



Reference (Undeformed) Space

$$\text{vol} = \int_{\Omega} 1 d\Omega$$

**We computed this when we computed the mass matrix**



# Equations of Motion

$$M\ddot{\mathbf{q}} = - \frac{\partial V}{\partial \mathbf{q}}$$

# Solve using Optimization via Newton's Method

$$E(\mathbf{q}^{i+1}) = \frac{1}{2} (\mathbf{q}^{i+1} - \tilde{\mathbf{q}}^i)^T M(\mathbf{q}^{i+1} - \tilde{\mathbf{q}}^i) + h^2 V(\mathbf{q}^{i+1})$$