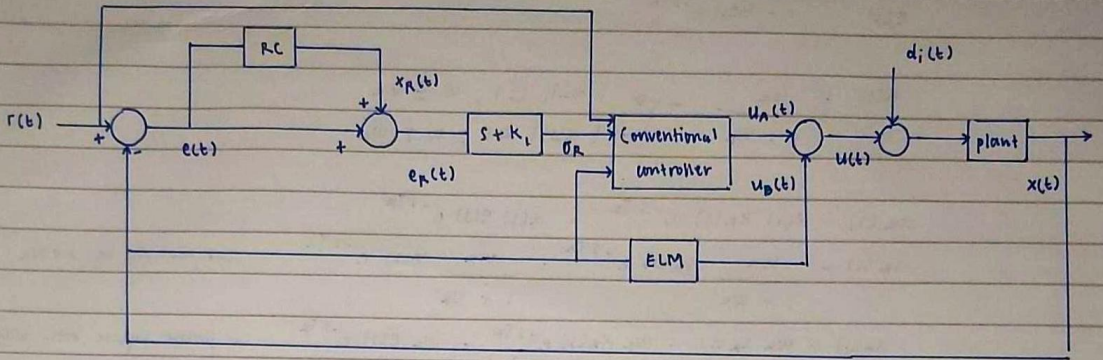


* Block diagram



* Open loop plant

$$P(s) = \frac{\theta(s)}{V(s)} = \frac{K}{s(Ts + 1)}$$

$u(t)$: control input

$x(t)$: position output

$\dot{x}(t)$: velocity output

$\ddot{x}(t)$: acceleration output

$d_i(t)$: input disturbance

Let $v(t) = u(t)$, and $\theta(t) = x(t)$, then

$$\frac{x(s)}{u(s)} = \frac{K}{Ts^2 + s}$$

$$Ts^2 x(s) + s x(s) = K u(s) \rightarrow \text{inverse laplace}$$

We have

$$T \ddot{x}(t) + \dot{x}(t) = K u(t)$$

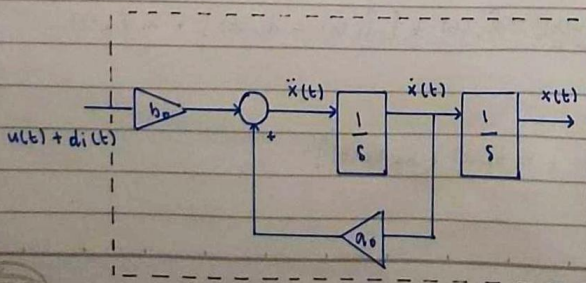
$$\ddot{x}(t) = -\frac{1}{T} \dot{x}(t) + \frac{K}{T} u(t)$$

Let write $a_0 = -\frac{1}{T}$, $b_0 = \frac{K}{T}$, and $d_i(t)$ appears at the input

$$\ddot{x}(t) = -a_0 \dot{x}(t) + b_0 [u(t) + d_i(t)]$$

$$\ddot{x}(t) = -a_0 \dot{x}(t) + b_0 u(t) + b_0 d_i(t)$$

* Open-loop realization



* Consider general modified RC with low-pass filter $\alpha(s)$

$$X_R(s) = \frac{\alpha(s) e^{-sT_d}}{1 - \alpha(s) e^{-sT_d}} E(s), \text{ where } \alpha(s) \text{ is first order low-pass filter given by:}$$

$$\alpha(s) = \frac{W_R}{s + W_R} \rightarrow \begin{cases} |\alpha(s)| \approx 1, & \omega \leq W_R \\ |\alpha(s)| < 1, & \omega > W_R \end{cases}$$

$$X_R(s) - \alpha(s) X_R(s) e^{-sT_d} = \alpha(s) E(s) e^{-sT_d}$$

$$X_R(s) - \frac{W_R}{s + W_R} X_R(s) e^{-sT_d} = \frac{W_R}{s + W_R} E(s) e^{-sT_d} \rightarrow \text{multiply by } s + W_R$$

$$s X_R(s) + W_R X_R(s) - W_R X_R(s) e^{-sT_d} = W_R E(s) e^{-sT_d} \rightarrow \text{inverse laplace both side}$$

$$\dot{x}_R(t) = -W_R x_R(t) + W_R x_R(t - T_d) + W_R e(t - T_d)$$

(state space model of modified RC)

* consider no saturation at the output of RC

* we define $e_R(t) = e(t) + x_R(t)$

* Tracking error dynamics:

$$e(t) = r(t) - x(t)$$

$$\ddot{e}(t) = \ddot{r}(t) - \ddot{x}(t) = \ddot{r}(t) - (-a_0 \dot{x}(t) + b_0 u(t) + b_0 d(t))$$

$$= \ddot{r}(t) + a_0 \dot{x}(t) - b_0 u(t) - b_0 d(t)$$

$$\ddot{e}_R(t) = \ddot{e}(t) + \ddot{x}_R$$

$$= \ddot{r}(t) + a_0 \dot{x}(t) - b_0 u(t) - b_0 d(t) + \ddot{x}_R$$

consider

$$d_L(t) = b_0 d(t) + \ddot{x}_R \rightarrow \ddot{e}_R(t) = \ddot{r} + a_0 \dot{x} - b_0 u - d_L$$

* The actuated lump disturbance is $d_L(t) = H\beta^*$

* The estimated lump disturbance is $\hat{d}_L(t) = H\hat{\beta}$, where $\hat{\beta}$ is the estimated output weight matrix.

$$\ddot{\sigma}_R(t) = (s + k_1) e_R(t) = \dot{e}_R(t) + k_1 e_R(t)$$

$$\ddot{\sigma}_R(t) = \ddot{e}_R(t) + k_1 \dot{e}_R(t)$$

$$= \ddot{r}(t) + a_0 \dot{x}(t) - b_0 u(t) - d_L(t) + k_1 \dot{e}_R(t)$$

can be rewritten

$$\ddot{\sigma}_R(t) = \ddot{r}(t) + a_0 \dot{x}(t) - b_0 u(t) - \hat{d}_L(t) + [\hat{d}_L(t) - d_L(t)] + k_1 \dot{e}_R(t)$$

* control law: $u(t) = u_A + u_b$

$$u_A(t) = \frac{1}{b_0} [a_0 \dot{x}(t) + \ddot{r}(t) + k_1 \dot{e}_R(t) + k_2 \sigma_R(t)]$$

$$u_b(t) = \frac{1}{b_0} [-\hat{d}_L(t)]$$

* estimated output weight matrix $\hat{\beta}$ is updated by :

$$\dot{\hat{\beta}}^T = -\eta \sigma_R H \rightarrow \eta > 0 \text{ positive constant}$$

* substituting the control law $u(t) = u_A + u_B$

$$\begin{aligned} \sigma_R(t) &= \ddot{r}(t) + a_0 \dot{x}(t) - b_0 [u_A + u_B] - \hat{d}_L + \hat{\dot{d}}_L - d_L + k_1 \dot{e}_R(t) \\ &= \ddot{r}(t) + a_0 \dot{x}(t) - b_0 \left[\frac{1}{b_0} (+ a_0 \dot{x}(t) + \ddot{r}(t) + k_1 \dot{e}_R(t) + k_2 \sigma_R(t)) + \right. \\ &\quad \left. \frac{1}{b_0} (-\hat{\dot{d}}_L(t)) \right] - \hat{d}_L(t) + \hat{\dot{d}}_L(t) - d_L + k_1 \dot{e}_R(t) \\ &= \ddot{r}(t) + a_0 \dot{x}(t) + a_0 \dot{x}(t) - \ddot{r}(t) - k_1 \dot{e}_R(t) - k_2 \sigma_R(t) + \hat{\dot{d}}_L(t) - \hat{d}_L(t) \\ &\quad + \hat{d}_L(t) - d_L + k_1 \dot{e}_R(t) \\ &= -k_2 \sigma_R(t) + \hat{\dot{d}}_L(t) - d_L \\ &= -k_2 \sigma_R(t) + H \tilde{\beta} \end{aligned}$$

$$\begin{aligned} d_L - \hat{d}_L &= H \beta^* - H \hat{\beta} \\ &= H [\beta^* - \hat{\beta}] \\ &= H \tilde{\beta} \end{aligned}$$

$$-d_L + \hat{d}_L = -H \tilde{\beta}$$

$$\begin{aligned} \tilde{\beta}^T &= \dot{\beta}^{*T} - \dot{\hat{\beta}}^T \\ &= 0 - \dot{\hat{\beta}}^T \\ &= -\eta \sigma_R H \end{aligned}$$

* Define Lyapunov function as

$$V = \frac{1}{2} \sigma_R^2(t) + \frac{1}{\eta} \tilde{\beta}^T \tilde{\beta}$$

* ~~Take~~ Taking derivative

$$\begin{aligned} \dot{V} &= \sigma_R \dot{\sigma}_R + \frac{1}{\eta} \tilde{\beta}^T \dot{\tilde{\beta}} \\ &= \sigma_R [-k_2 \sigma_R(t) + H \tilde{\beta}] + \frac{1}{\eta} \tilde{\beta}^T \tilde{\beta} \\ &= -k_2 \sigma_R^2(t) + \sigma_R H \tilde{\beta} + \frac{1}{\eta} \tilde{\beta}^T \tilde{\beta} \\ &= -k_2 \sigma_R^2(t) + \sigma_R H \tilde{\beta} + \frac{1}{\eta} (-\eta \sigma_R H) \tilde{\beta} \\ &= -k_2 \sigma_R^2(t) + \sigma_R H \tilde{\beta} + (-\sigma_R H \tilde{\beta}) \\ &= -k_2 \sigma_R^2(t) \\ &\quad (k_2 \text{ positive gain}) \end{aligned}$$