

Multivibrators and Time base Generators.

A circuit which can oscillate at a number of frequencies is called a multivibrator. It has three types:

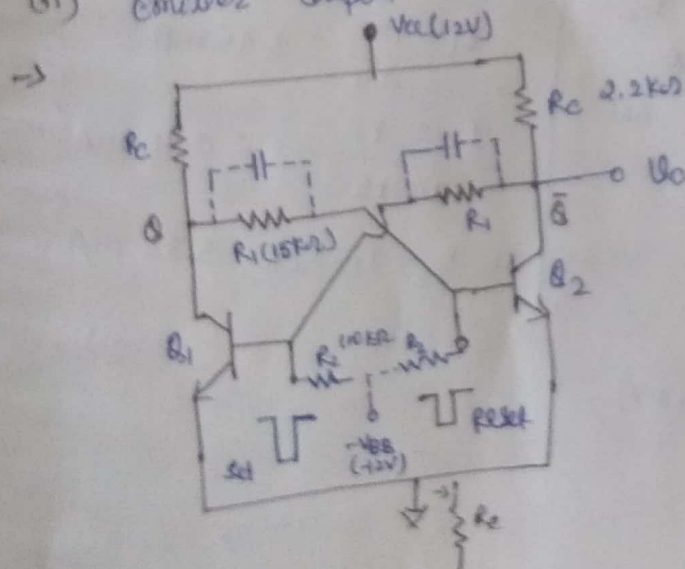
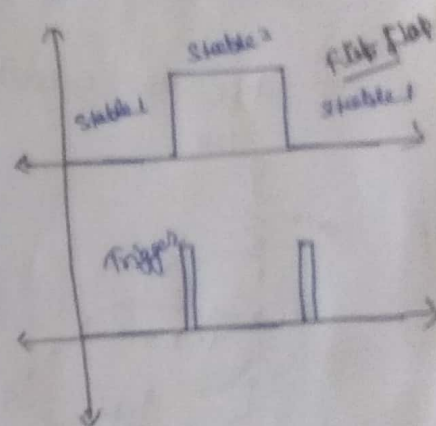
- (i) Bistable multivibrator
- (ii) Monostable "
- (iii) Astable "

* Bistable multivibrator:

It has two stable states and its make transition from one state to another state by external excitation. It is used as flip flop.

Types:

- (i) Collector coupled bistable multivibrator
 - (a) Fixed bias bistable multivibrator
 - (b) self-bias "
- (ii) Emitter coupled bistable multivibrator



Let consider that transistor Q_1 draws more current in compare to Q_2 . i.e. $Q_1 \rightarrow ON$ & $Q_2 \rightarrow OFF$. Transistor behave as inverter.

Operation:

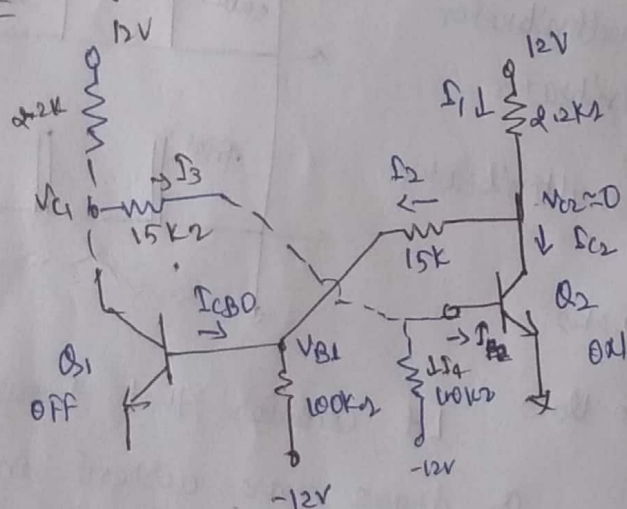
- when Q_1 is ON then collector vge is $V_{cc} - I_{C1}R_c$ i.e. less which is given to base of Q_2 and it is not sufficient to switch Q_2 ON. So, Q_2 collector vge is V_{cc} (high), which is given to base of Q_1 . i.e. Q_1 will be in saturation. output remains in same state.
- when small trigger pulse is given to base of Q_1 to set it into OFF, then Q_1 is OFF & Q_2 will be ON & \bar{Q} is $V_{cc} - I_{C2}R_c$. i.e. state has been changed. Same op is given to Q_1 , so, still it remains OFF.

→ To change the state again, small trigger pulse is given to base of Q_2 to reset. i.e. Q_2 will be OFF & Q is equal to V_{CC} , which is given to Q_1 . So, Q_1 will turn ON.

→ So, when-when trigger pulse occur then there is transition in op. It is required that there should be change of state as soon as abrupt trigger pulse is applied.

The transition time can be reduced by connecting small capacitance in shunt with R_1 . It is known as commutating transistor or speed up capacitors.

e.g, $h_{fe} = 20$, calculate current & voltage:



→ we neglect T_{CO} .

$$V_{B1} = \frac{-12 \times 15}{(15+100)} = -1.56 \text{ V}$$

$$I_1 = \frac{12}{2.2} = 5.45 \text{ mA}$$

$$I_2 = \frac{12}{100+15} = 0.10 \text{ mA}$$

So, $I_{L2} = I_1 - I_2 = 5.35 \text{ mA}$

$$(I_{B2})_{min} = \frac{I_{C2}}{h_{fe}} = \frac{5.35}{20} = 0.27 \text{ mA}$$

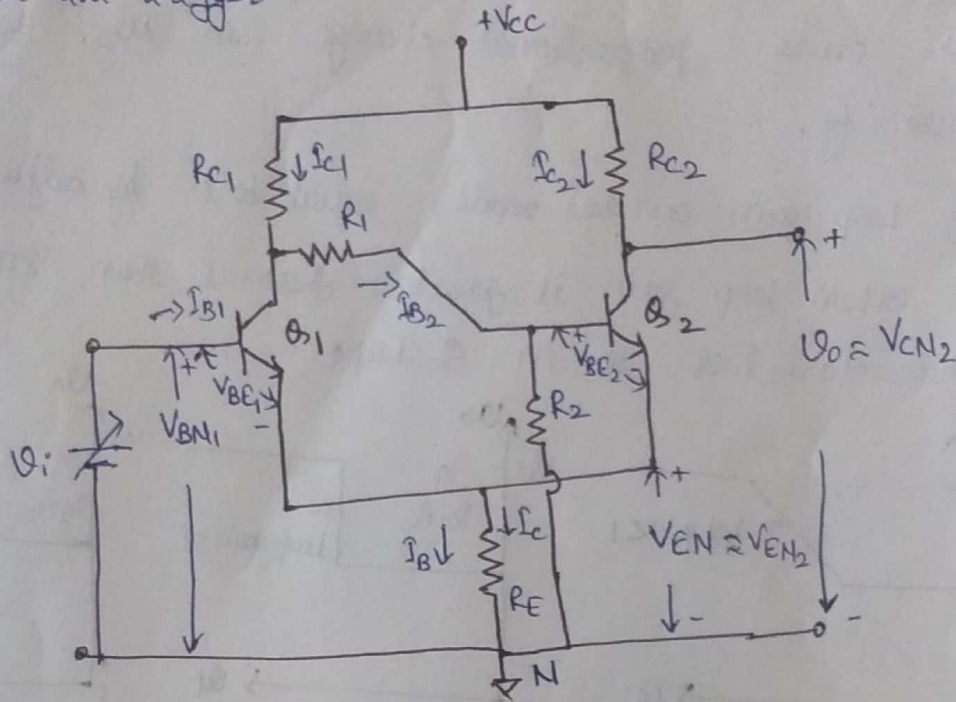
$$\rightarrow I_3 = \frac{12}{2.2 + 15} = 0.70 \text{ mA}$$

$$I_4 = \frac{12}{100} = 0.12 \text{ mA}$$

So, $I_{B3} = I_{B4} = 0.58 \text{ mA}$

* Schmitt Trigger:

An emitter-coupled bistable multivibrator is called as schmitt trigger.



→ The I/P voltage V_i is variable. R_{C1} , R_1 & R_2 are voltage dividers.

Case-I:

when $V_i < (V_{BE1} \text{ i.e. } V_{BE1} + V_{EN})$ then transistor Q_1 is off.

The O/P at collector of Q_1 is high, which is given to I/P to Q_2 . The voltage at base of Q_2 is given as,

$$V_{BN2} = \frac{V_{CC} \cdot R_2}{R_{C1} + R_1 + R_2}$$

Due to this Q_2 turns ON & O/P voltage V_O is equal to $V_{CC} - I_{C2} R_{C2}$. The current I_{B2} & I_{C2} flow through the resistance R_E . Let assume that Q_2 is in active region.

Case-II:

when V_i is increased, then at $V_i = V_{EN2} + V_{Y1}$, Q_1 begins to conduct. So, voltage at base of Q_2 decreases.

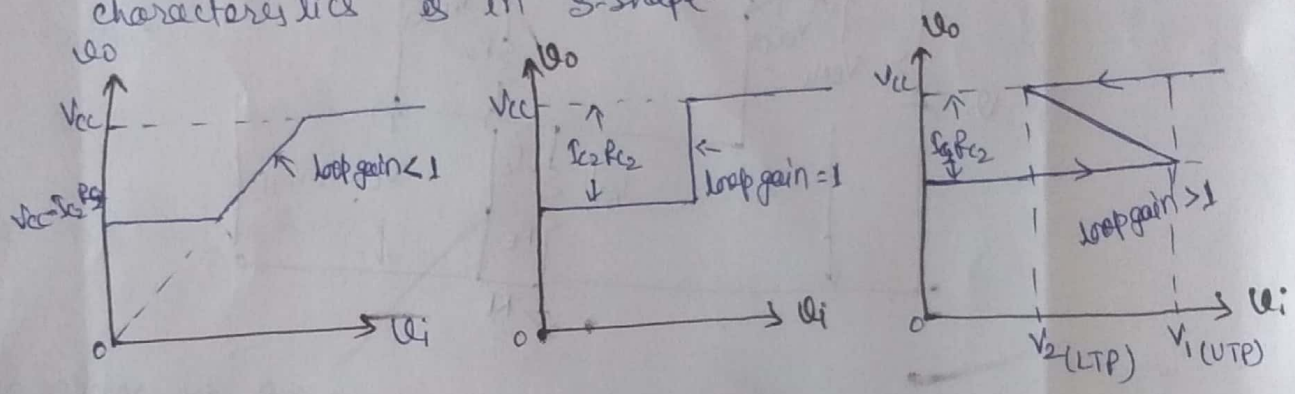
→ If V_i increased further, then Q_1 is ON & Q_2 is OFF.

The O/P voltage is equal to V_{CC} .

→ If loop gain is less than unity then incremental change ΔV_i cause proportional change in ΔV_o . i.e. it has linearity.

→ Loop gain can be made equal to 1 by adjusting R_{C1} & R_{C2} .

→ when loop gain is greater than 1 then transfer characteristics is in S-shape.



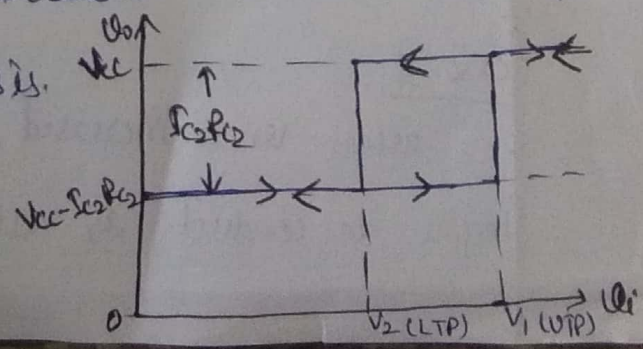
→ The voltage (at which) $V_i = V_1$, when O/P voltage changes suddenly from $V_{CC} - I_{C2}R_{C2}$ to V_{CC} is known as upper trip point (UTP).

Case-III:

when I/P voltage V_i is decreased & at voltage $V_i = V_2$, O/P voltage falls from V_{CC} to $V_{CC} - I_{C2}R_{C2}$ is known as lower trip point (LTP). The hysteresis voltage is given as, $V_H = V_1 - V_2$.

when V_i is increased to V_1 , it has to pass the pt. V_2 . Similarly when V_i is decreased to V_2 , it has to pass the pt. V_1 .

This is called hysteresis.



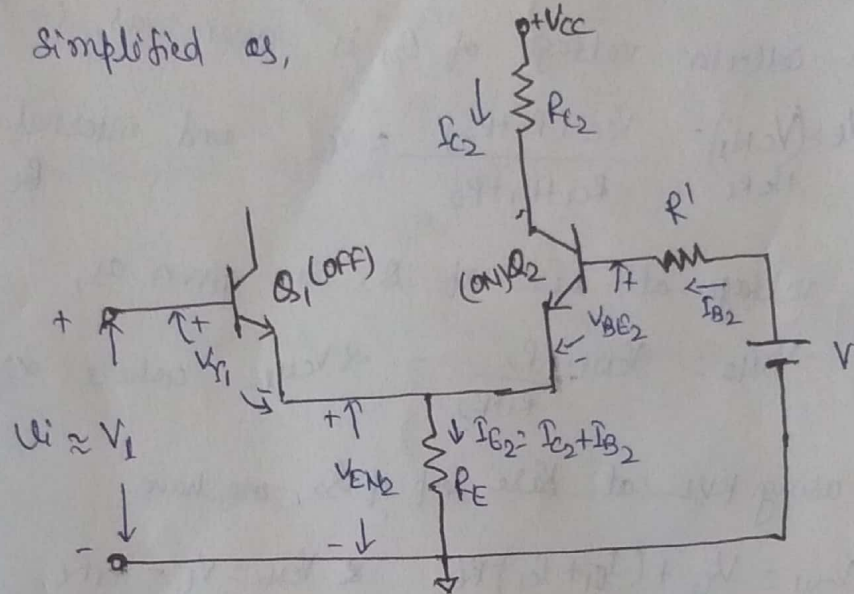
→ Calculation of UTP & LTP i.e. V_1 & V_2 :

→ UTP (V_1): The Q_1 switches into ON and Q_2 switches into OFF

The voltage at the base of Q_2 is given as,

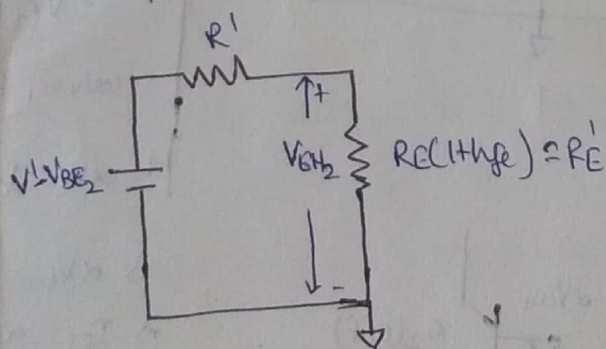
$$V' = V_{B2} = \frac{V_{CC} \times R_2}{R_1 + R_1 + R_2}$$

& internal resistance $R' = R_2 \parallel (R_1 + R_1)$. So, circuit can be simplified as,



The emitter current $I_{E2} = I_{B2} + I_{C2} = I_{B2} \left(1 + \frac{I_{C2}}{I_{B2}} \right) = I_{B2} (1 + \beta_{FE})$.

The net voltage in base loop is $V' - V_{BE2}$. This base loop is simplified as,



$$V_{EN2} = \frac{(V' - V_{BE2}) \times R_E'}{R' + R_E'}$$

$$\text{As } R' \ll R_E'$$

$$\text{So, } V_{EN2} = V' - V_{BE2}.$$

$$\text{And we have, } V_1 = V_{T1} + V_{EN2}.$$

We assume that Q_1 is in active region.

We have,

$$V_{CB2} = V_{CE2} - V_{BE2} \quad \& \quad V_{CE2} + V_{EN2} = V_{CC} - I_{C2} R_{C2}$$

$$\text{So, } V_{CB2} = V_{CC} - I_{C2} R_{C2} - V_{EN2} - V_{BE2}$$

$$\text{and } V_{EN2} = (I_{B2} + I_{E2}) R_E = I_{C2} \left(1 + \frac{I_{B2}}{I_{C2}} \right) R_E = I_{C2} \left(1 + \frac{1}{h_{FE}} \right) R_E$$

$$\Rightarrow V_{EN2} = I_{C2} \cdot R_E'' \quad , \text{ where } R_E'' = \left(1 + \frac{1}{h_{FE}} \right) R_E$$

$$\text{Hence, } \boxed{V_1 = I_{C2} R_E'' + V_{CE1}}$$

→ LTP(V₂): Q₁ switches in to OFF & Q₂ switches in to ON.

The collector voltage of Q₁ is given as, (i.e. Thevenin's voltage source)

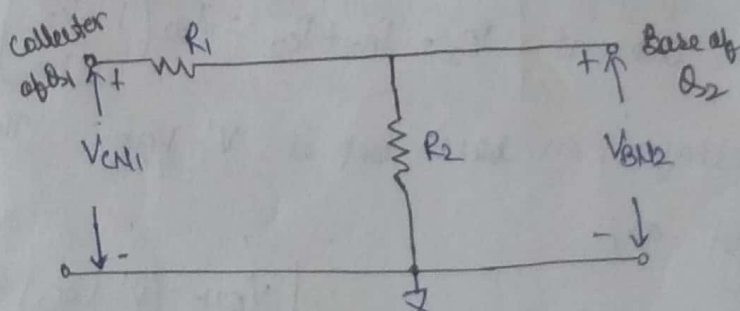
$$V_t = \frac{V_{CE1}}{1 + I_{C1} R_t} = \frac{V_{CC} (R_1 + R_2)}{R_{C1} + R_1 + R_2} \approx V_t \quad \text{and internal resistance } R_t = R_{C1} \parallel (R_1 + R_2)$$

The voltage at base of Q₂ is given as,

$$V_{BE2} = V_{CE1} \cdot \frac{R_2}{R_1 + R_2} = \alpha V_{CE1} \quad \text{where } \alpha = \frac{R_2}{R_1 + R_2}$$

By using KVL at base loop of Q₂, we have

$$\alpha V_{CE1} = V_{BE2} + (I_{B1} + I_{C1}) R_E \quad \& \quad V_{CE1} = V_t - I_{C1} R_t$$



$$\begin{aligned} \text{so, } \alpha (V_t - I_{C1} R_t) &= V_{BE2} + I_{C1} \left(1 + \frac{I_{B1}}{I_{C1}} \right) R_E \\ &= V_{BE2} + I_{C1} \left(1 + \frac{1}{h_{FE}} \right) R_E \\ &= V_{BE2} + I_{C1} \cdot R_E'' \end{aligned}$$

where, $R_E'' = \left(1 + \frac{1}{h_{FE}} \right) R_E$

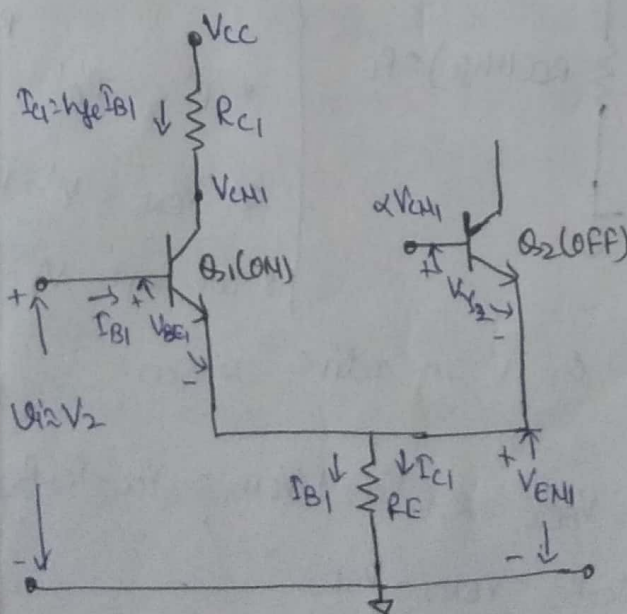
$$\begin{aligned} \text{So } \alpha V_t - I_{C1} \alpha R_t &= V_{BE2} + I_{C1} R_E'' \\ \Rightarrow \alpha V_t &= I_{C1} (\alpha R_t + R_E'') + V_{BE2} \\ \Rightarrow I_{C1} &= \frac{\alpha V_t - V_{BE2}}{\alpha R_t + R_E''} \end{aligned}$$

we have,

$$\alpha V_t = \frac{V_{CC} (R_1 + R_2)}{R_{C1} + R_1 + R_2} \times \frac{R_2}{R_1 + R_2} = V'$$

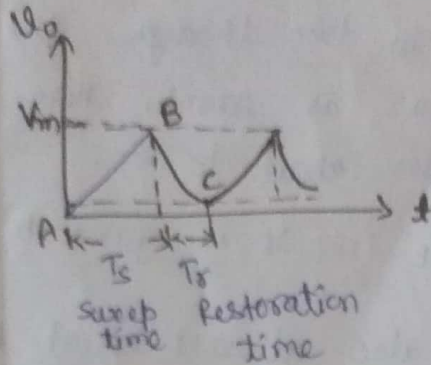
$$\text{So } I_{C1} = \frac{V' - V_{BE2}}{(\alpha R_t + R_E'')}$$

$$\text{Hence } \boxed{V_2 = V_{BE1} + I_{C1} R_E''}$$



* Timebase generator or sweep generator:

- It is basically a function generator that generate waveform.
- It produce o/p voltage / current which is linear w.r.t time.
- It is used in CRO to sweep electron beam & in T.V etc.



→ Types:

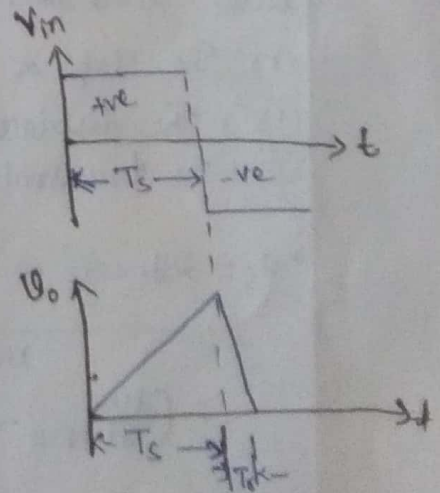
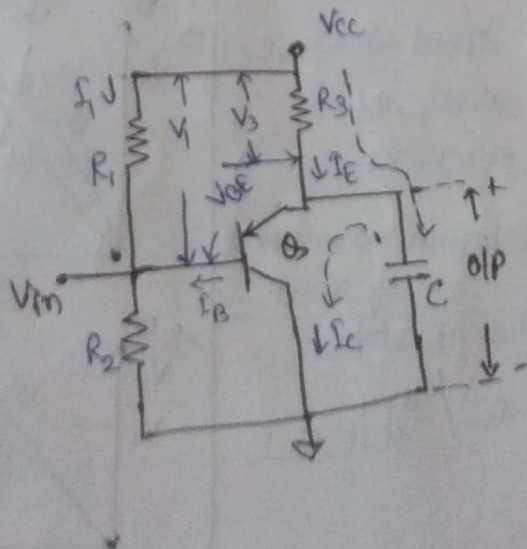
- Free running Time base generator: without trigger
- Triggered Time base generator: required trigger signal

→ Methods to generate Time base generator:

- Exponential charging: VDT relaxation osc.
- Miller integration: Miller sweep ckt
- Bootstrap: Bootstrap time base generator
- Constant current charging: current time base generator

* Constant current Ramp generator:

eg Inductor ckt, Transistor ckt, sweep ckt



→ Resistance R_1 & R_2 provide voltage V_1 to the base of transistor. The voltage across R_3 is equal to $V_1 - V_{BE}$.

→ Case-I:

→ Initially when V_{IC} is given then pnp transistor is off due to reverse biasing of EP junction. During this time capacitor C charges up to V_{IC} through the resistance R_3 , linearly. So, output appear as ramp. Here, current is constant. The o/p increases about to V_{IC} .

The current across ' R_E ' i.e. I_E is given by $\frac{V_1 - V_{BE}}{R_E}$.

The collector current I_C is also almost equal to I_E .

→ Case-II:

When transistor's base has negative supply voltage then it will turn it into ON condition. So, capacitor C , which was charged. Now, it will discharge through the path emitter & collector of transistor. So, o/p decreases.

Application:

It is used in TV, RADAR & computers to provide magnetic deflection.

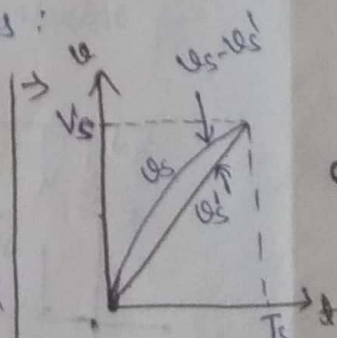
* Deviation from linearity:

It is difficult to generate linear sweep signal by time base generator. It is expressed as:

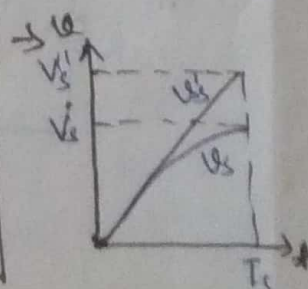
- (i) The slope or sweep speed error, e_s
- (ii) The displacement error, e_d
- (iii) The transmission error, e_t

→ e_s = difference in slope at beginning and end of sweep

$$= \frac{\text{initial value of slope}}{\left(\frac{dV_o}{dt} \Big|_{t=0} - \frac{dV_o}{dt} \Big|_{t=T_s} \right) / \frac{dV_o}{dt} \Big|_{t=0}}$$



$$e_d = \frac{(V_s - V'_s)_{\text{max}}}{V_s}$$

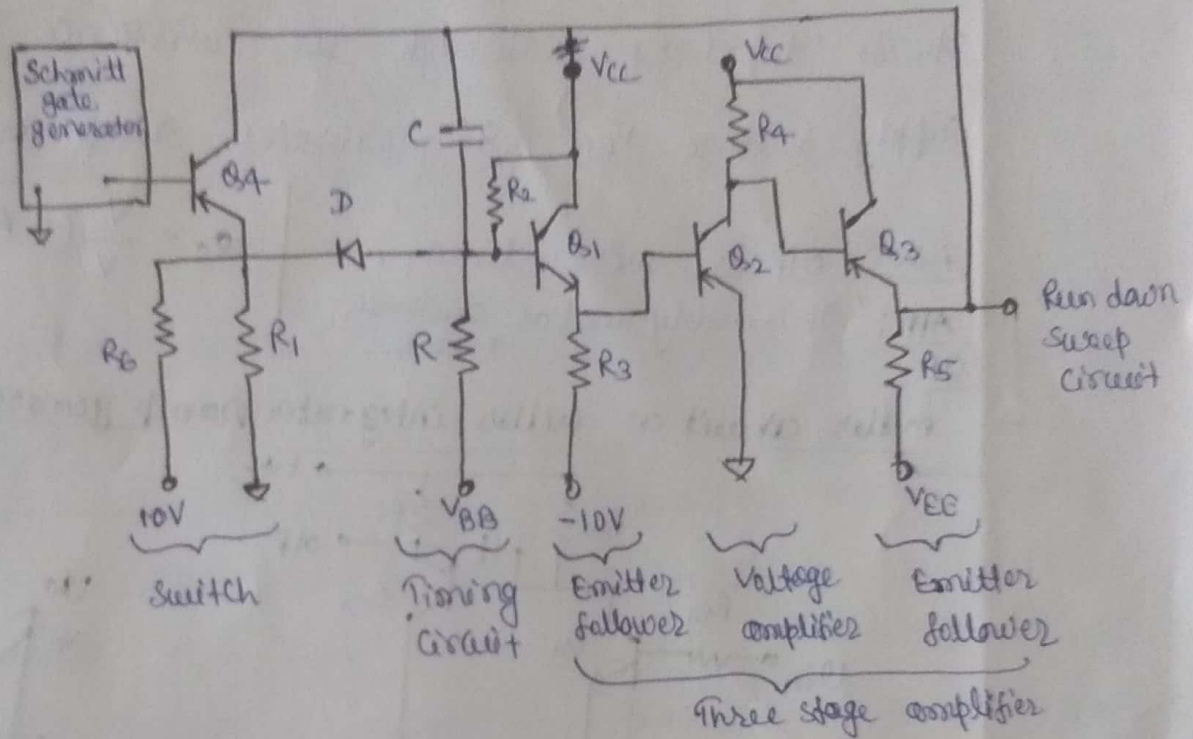


$$e_t = \frac{V_s - V'_s}{V'_s}$$

→ By reducing these errors, we can improve nonlinearity.

* Miller sweep generator:

The transistor Miller time base generator circuit is popular miller integrator circuit, that produces sweep waveform. It is mostly used in horizontal deflection circuit.



Construction:

It consists of transistor Q_4 as switch. It has three stage amplifier. In which Q_1 acts as emitter follower, Q_2 acts as voltage amplifier & Q_3 acts as emitter follower. The capacitor C is connected b/w base of Q_1 & emitter of Q_2 . The combination of C & R acts as timing circuit. The Q_1 provides high I/P impedance.

Operation:

Case I: when there is negative pulse at base of Q_4 then Q_4 turns ON and current flows through the resistance R_1 . It makes diode D in forward bias. The capacitor C appears in parallel with Q_4 . So it doesn't charge during this period. i.e. voltage across capacitor is zero.

case-II

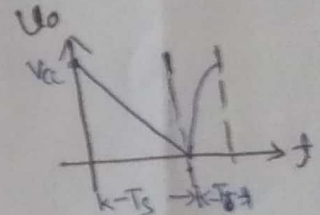
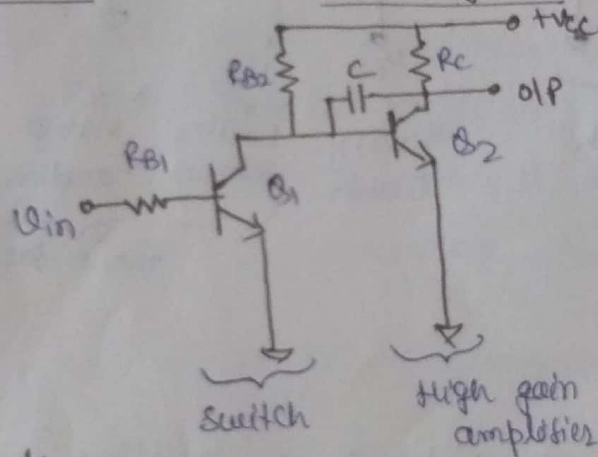
when positive pulse is available at the base of Q_1 , then it turns OFF. So, positive voltage appears across the resistance R_1 due to 10V supply voltage. Due to this diode gets reverse bias and capacitor C starts to charge through the resistance R due to supply voltage V_{BB} . It generates sweep voltage at O/P.

Adv: O/P is more linear.

App: It is widely used as sawtooth generator.

OR

→ Miller circuit or Miller integrator ramp generator:

Construction:

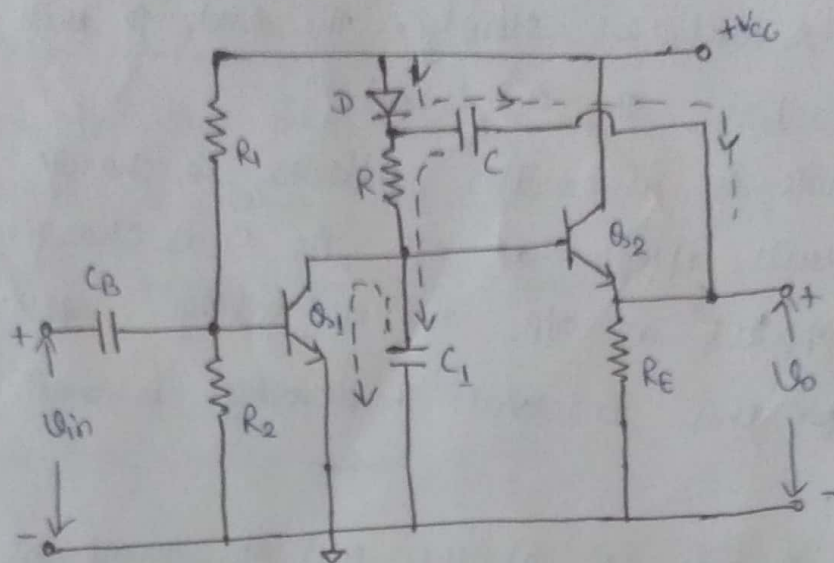
It consists of transistor Q_1 as switch & Q_2 as high gain amplifier. The capacitor 'C' is connected b/w J_n of collector of Q_1 & base of Q_2 and collector terminal of Q_2 .

operation:

→ When the voltage appears at base of Q_1 due to V_{in} then it turns ON. So, Q_2 is OFF and O/P voltage is equal to V_{CC} . During this capacitor C charges through the R_C . So, charging time constant is equal to $C \cdot R_C$.

→ When V_{in} is removed then Q_1 turns OFF. So, Q_2 is ON. The O/P voltage decreases, which depends on discharging of capacitor 'C' through R_{B2} . If discharging time constant $C \cdot R_{B2}$ is large then it provides constant discharge current. The O/P voltage decreases linearly. It has excellent ramp linearity.

* Bootstrap (Circuit) Time base generator:



Construction:

It consists of two transistors Q_1 & Q_2 . The Q_1 acts as a switch & Q_2 acts as an emitter follower. The capacitor C_B is a blocking capacitor. The capacitor C is connected b/w the cathode of the diode & the emitter terminal of Q_2 . The capacitor C_1 is connected to the collector of Q_1 & the base of Q_2 and ground. The capacitance of $C \gg C_1$.

Operation:

Case-I:

Before applying the gating waveform V_{in} at $t=0$, the Q_1 is ON due to the biasing voltage at its base terminal, which is obtained from $+V_{cc}$ & a combination of R_1 & R_2 . Since Q_1 is ON, there is no sufficient voltage at the base of Q_2 to switch it on to ON. i.e. Q_2 is OFF.

So, capacitor C will charge up to $+V_{cc}$ through the diode D . The O/P voltage V_o is zero.

Case-II:

Now a negative trigger pulse from the gating waveform of a monostable multivibrator is applied to the base of Q_1 .

So, Q_1 turn OFF. The capacitor C discharge and capacitor C_1 charge through R . Since capacitance of $C \gg C_1$, so, C charges & discharges slowly. The diode D will be in reverse bias. The Q_2 is ON.

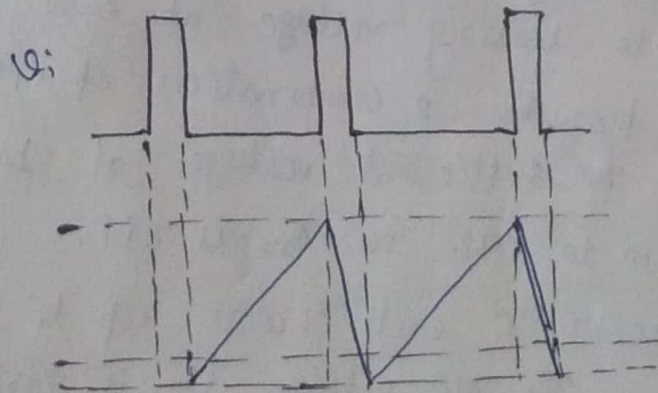
Since Q_2 is emitter follower, so, change at the base of Q_2 will appear at O/P. As C_1 is charging that voltage appears as O/P. The O/P voltage appears as ramp signal for this interval. The O/P voltage is max^m about V_{cc} .

Case - III:

When Q_1 gets ON at the end of ramp signal then capacitor C_1 discharges rapidly to its initial value through Q_1 . The diode again become forward bias and capacitor C will start to charge again. Again circuit produce next ramp signal.

The capacitor ' C ' provides feedback current to C_1 , it is known as boot strapping capacitor.

Output waveform:



Adv:

The O/P voltage ramp is very linear and amplitude reaches to supply voltage.