

ANTENNA ARRAYS:Antenna Array:

The group of antenna elements which are similar is called as an Antenna Array.

To improve the radiation characteristics of antenna characteristics like Directivity the Antenna Arrays are designed.

The Antenna Array improvements radiations are improved and these are depend on

- (i) length of A Individual Antenna elements
- (ii) No. of Antenna elements in Antenna Array
- (iii) The current magnitude & phase provided with each element.
- (iv) Material used for each Antenna element
- (v) Separation b/w the individual Antenna elements in Antenna Array.

By, using the Antenna arrays, the concentration of radiations in particular direction ↑ and forms a beam of line radiation and this beam is used in point to point commⁿ bcz point to point

These are two types of Antenna Arrays.

Linear Antenna Array:

In this, each Antenna element is separated with the same distance in Antenna Array.

Uniform Antenna Array:

In this, each Antenna elements separation will be equal & has a uniform magnitude of current is provided for all the Antenna element and has a progressive phase shift.

Non-Uniform Antenna Array.

These are having unequal separation b/w Antenna elements & unequal magnitude of current for Antenna element

Based on construction & direction of main radiations Antenna Arrays are classified

as

- 1) Broad side Antenna Array (BSA)
- 2) Endfire " " " (CEFA)
- 3) Collinear " " " (CoR)
- Omnidirectional " " " (CAA)

$$\bar{E}_T = \bar{E}_1 + \bar{E}_2 + \bar{E}_3 + \dots + \bar{E}_m \text{ V/m}$$

BROADSIDE ANTENNA ARRAY:

Construction:

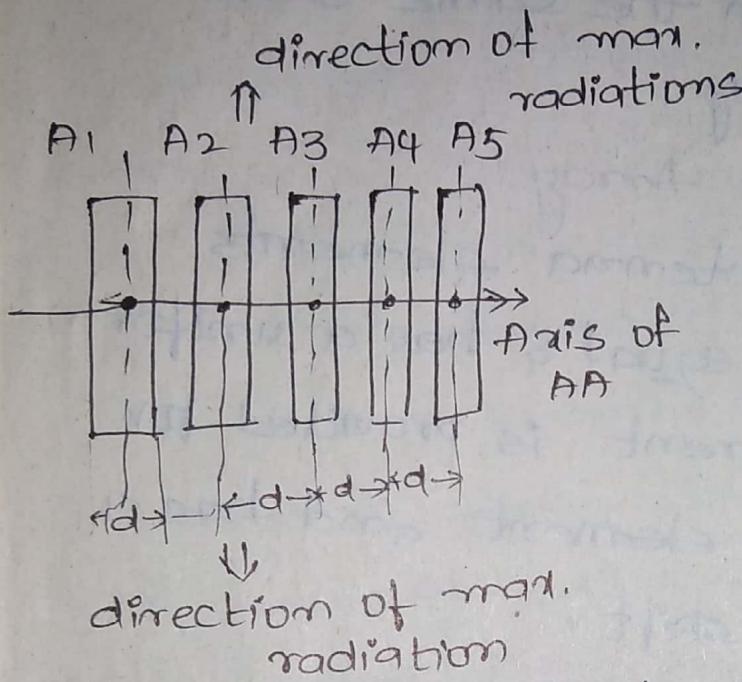
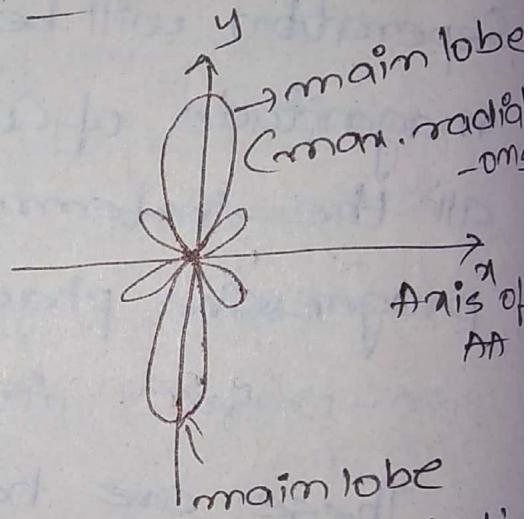


Fig (a) Broadside with 5 elements Equally Spaced

Radiation pattern
of AA



① All elements are parallel to each other.

② All elements are

Equally Spaced.

③ All elements are Equally arranged along the line of Antenna Array.

④ All elements are excited with uniform magnitude of current Space & phase

⑤ Radiation pattern is Bidirectional & wider than radiations \perp^{th} to Axis of AA.

fig: Bidirectional R.P of BSA .

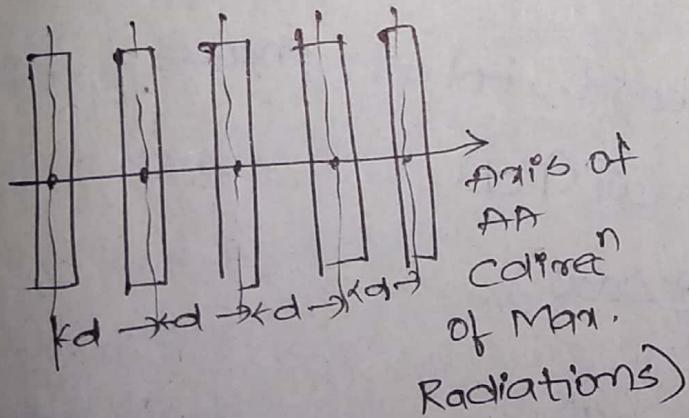
2) ENDFIRE ANTENNA ARRAY

construction of Endfire Antenna array
It is similar to Broadside Antenna Array.

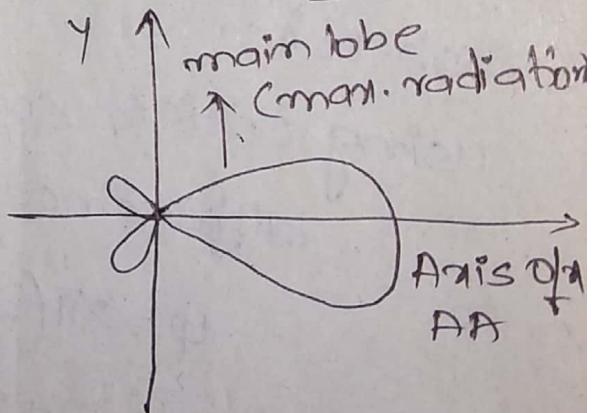
1, 2, 3, 4, points are same.

⑤ Radiation is Bi-directional. All elements are excited with uniform magnitude of current but variable phase.

so, the direction of Max. Radiations are along the axis. So, the Radiations are radial to the axis. ⇒ Radiation pattern is unidirectional.

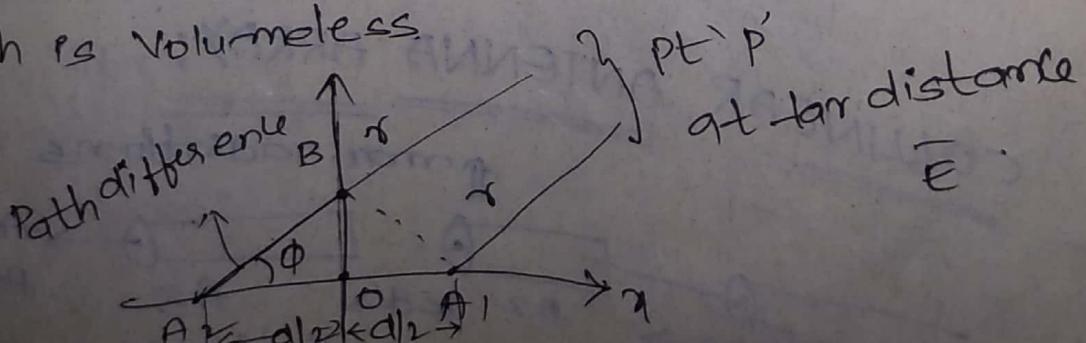


Radiation Pattern of AA



→ BSA WITH TWO ISOTROPIC POINT SOURCES

Point source is the part of Antenna which is volumeless.



Here, the A_2 radiations will reach last than A_2 radiations, this is bcz A_2 is having extra different distance than A_1 , and this distance is called Path difference.

From figure $\triangle ABA_2$, $\cos\phi = \frac{A_2B}{d} = \frac{A_2B}{A_1A_2}$

$$A_2B = d \cos\phi$$

Path difference expressed in terms of λ'

$$\rightarrow AB = \frac{d}{\lambda'} \cos\phi = Pd \text{ meters.}$$

Here, the two point sources are equally spaced & the two radiations are parallel to each other.

Using optics concept, total phase

$$\text{difference} = 2\pi(Pd)$$

$$\varphi = 2\pi \left(\frac{\lambda}{\lambda'} \cos\phi \right)$$

$$= \frac{2\pi}{\lambda'} \cdot d \cos\phi$$

$$\boxed{\varphi = \beta \cdot d \cos\phi}$$

③ COLLINEAR ANTENNA ARRAY:

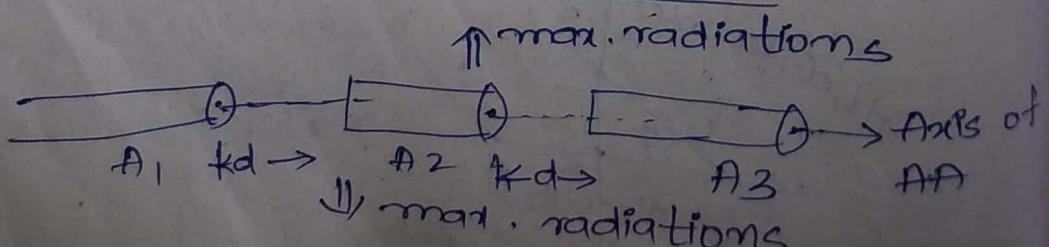


fig: Collinear AA with a ele
d should be 0.3λ to 0.5λ (practically)
The Antenna elements are connected
with Insulating material & these should
be finite, if it is not there, the Antenna
elements doesn't acts as an Antenna
array. The main radiations are in
 $\theta = 90^\circ \& 270^\circ$ (same as BSA). The drawback
is that a feeding problems ~~are taken~~ but in
place. In BSA, dipoles are used but in
collinear circular elements are used.

④ PARASITIC ANTENNA ARRAY

In all the BSA, EFA and collinear all the
Antennas are elements are excited by
the individual inputs & the ILP's are
by transmission line.

Parasitic Antenna array is having
two elements. They are:

① Parasitic element ② Driven element.

The ILP is given to the driven

element by the transmission

line. The Parasitic element is

without a taken any wire & due to
Electromagnetic Coupling b/w driven
element & parasitic element, radiation
takes place.

Parasitic elem

Driven elem

driven elem

driven elem

driven elem

The radiation pattern due to parasitic elements depends upon

- (i) length of driven element -
- (ii) length " " Parasitic element
- (iii) separation b/w " & Driven element

The direction of Antenna Array is unidirectional & the max. radiations takes place along the parasitic element when it satisfies the conditions below.

(i) When the separation b/w the Parasitic & driven element is $d = \lambda/4$. It is because of

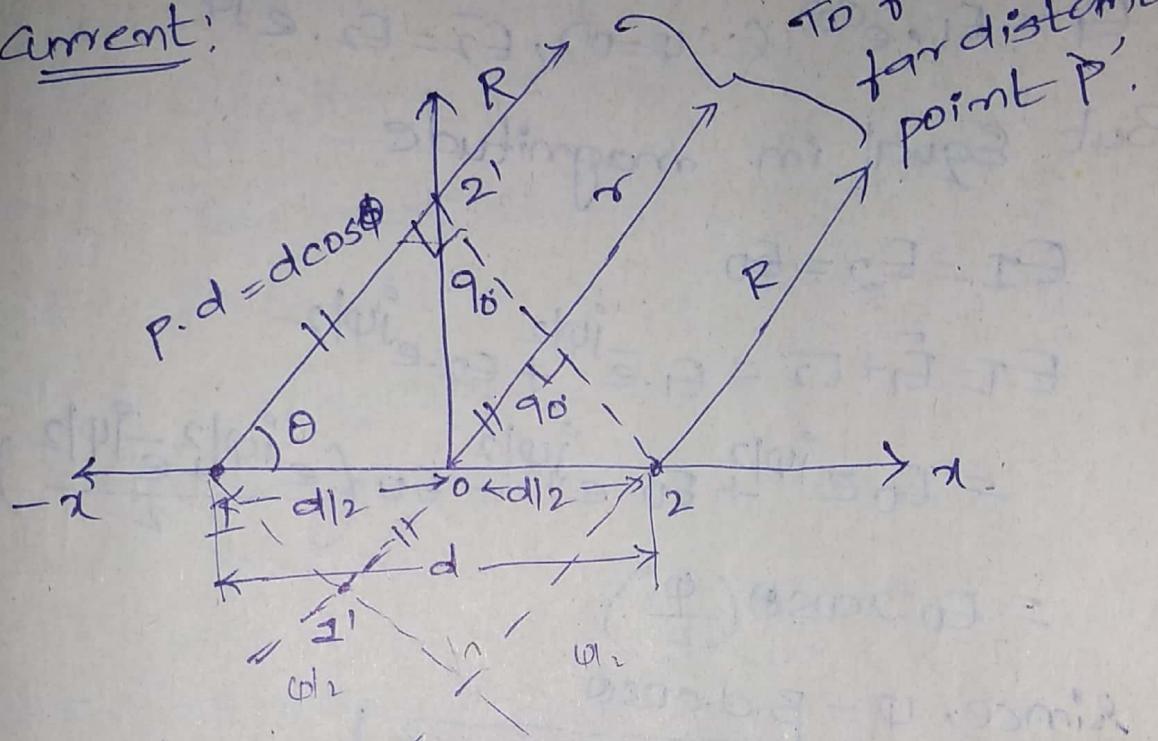
H Reason! when the ip is given to the driven element by the transmission line

" " produces electromagnetic field. So, when the Parasitic element (Antenna, i.e. Conductor) is not placed near the field, the current produces. As according to the Faradays law, when the conductor ~~rod~~ is placed in magnetic field it produces a current. So, that the Parasitic elements will radiate.

(ii) The relative phased phase difference b/w relative currents produced by driven element & parasitic element is $\pi/2$.

ARRAY OF POINT SOURCES

Case : I, Array of two point sources fed with equal amplitude and same phase of current.



Path difference = $d \cos \theta$
In terms of Wavelengths

$$Pd = \frac{d}{\lambda} \cos \theta$$

using optics concept,
total phase difference b/w 2 element

$$= 2\pi (\text{path difference}) = 2\pi \left(\frac{d}{\lambda}\right) \cdot \cos \theta$$

$$\psi = \beta d \cos \theta \quad (1)$$

According to superposition concept.

$$E_T = \bar{E}_1 + \bar{E}_2$$

$$\text{Since, } \bar{E}_1 = E_1 \cdot e^{-j\phi/2} \quad (\bar{r} = |r|, \phi)$$

$$\bar{E}_2 = E_2 \cdot e^{j\phi/2}$$

Note: Origin of system is taken as reference for phase calculation

Vector magnitude
unit

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$$\text{Error} = \cos(\pi l_2 \cos \theta) \quad \text{(B)}$$

Since, $d = \lambda/2$, $B = 2\pi/l\lambda$.

Let us find the direction of max. radiations, min. radiations using above equation.

Case i) Direction of Maxima:

When $\text{Error}_{\text{normalised}} = \text{maximum}$ in the direction of θ , there will be max. radiations.

$$\text{Error} = \cos(\pi l_2 \cos \theta) = \pm 1 (\text{max})$$

$$\pi l_2 \cos \theta_{\text{max}} = n\pi$$

where $n = 0, 1, 2, \dots$

If $n = 0$,

$$\pi l_2 \cos \theta_{\text{max}} = 0$$

$$\boxed{\theta_{\text{max}} = 90^\circ \text{ & } 270^\circ}$$

Case ii) Direction of Minima:

When $\text{Error}_{\text{normalised}} = \text{min.}$ in the direction of θ , there will be min. radiations.

$$\text{Error} = \cos(\pi l_2 \cos \theta) = 0$$

$$(\pi l_2 \cos \theta_{\text{min}}) = \pm (2m+1)\pi/2$$

where $m = 0, 1, 2, 3, \dots$

$$\pi l_2 \cos \theta_{\text{min}} = \pm \frac{\pi}{2}$$

$$\cos \theta_{\text{min}} = \pm 1 \Rightarrow \theta_{\text{min}} = \cos^{-1}(\pm 1)$$

$$\boxed{\theta_{\text{min}} = 0^\circ \text{ & } 180^\circ}$$

iii) Half Power Point:

At Half Power point, $E_{\text{noi}} = \pm \frac{1}{\sqrt{2}}$

$$\cos(\pi/2 \cos \theta) = \pm (2n+1)\pi/4$$

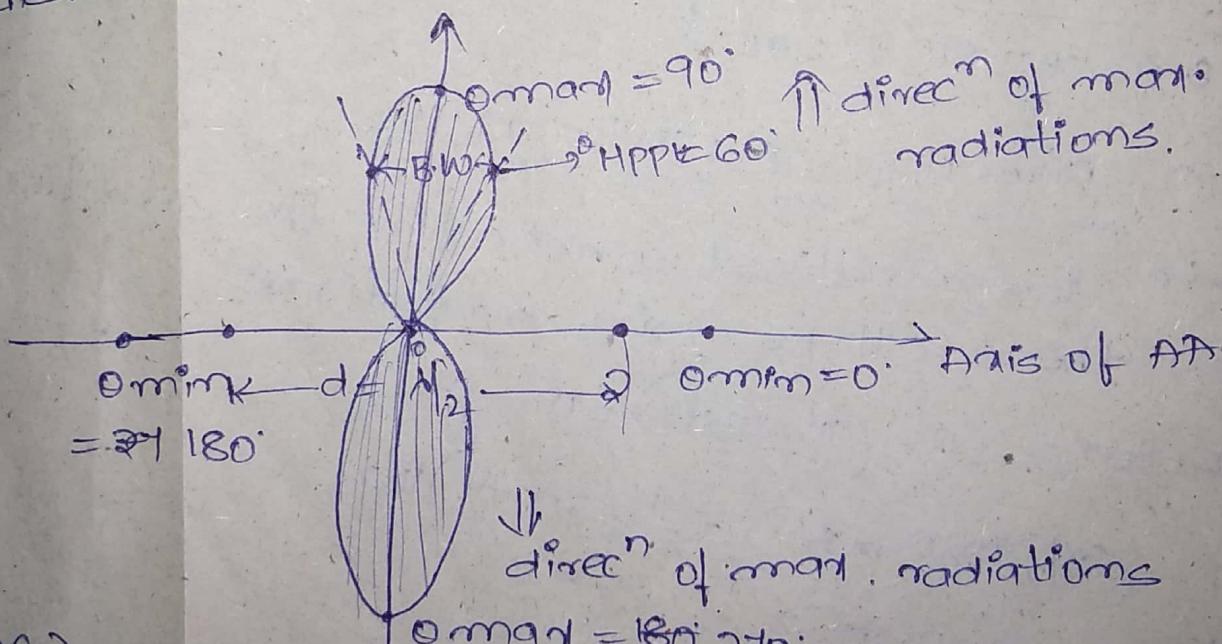
when $n=0$.

$$\cos(\pi/2 \cos \theta) = \pm \frac{\pi}{4}$$

$$\cos \theta = \pm \frac{1}{2}$$

$$\boxed{0^\circ \text{ HPP} = 60^\circ \text{ & } 120^\circ}$$

Using above data Radiation Pattern will be,
Radiations in minimum direction is 0. Therefore
there is no lobe.



fig(6) 2-Isotropic point source spaced by $\lambda/2$ apart.
The three-dimensional vertical pattern is
Donut shape

The above is the two isotropic point
source with equal Amplitude & op same phase.

Case ii): 2-isotropic point sources with equal Amplitude, unequal phase.

Consider fig(a) of case ii)

$$\Phi = \beta d \cos \theta \rightarrow (i)$$

Opposite phase means if $\theta=0^\circ$ max. radiations occurs, then at 180° , min. radiations occur.

should occur. The max. radiations should be unidirectional

According to superposition $\bar{E} = \bar{E}_1 + \bar{E}_2$

$$E_1 = -E_0 e^{j\psi/2}, E_2 = E_0 e^{j\psi/2}, \text{ Since, equal Amp'}$$

E_1 is taken as -ve bcz opposite phase mean at left side, Amplitude is $-E_0$ (as at this $\angle \theta$ is 180°)

$$\text{Since, } E_1 = E_2 = E_0$$

$$\bar{E} = -E_0 e^{j\psi/2} + E_0 e^{j\psi/2} = -E_0 e^{-j\psi/2} + E_0 e^{j\psi/2} = E_0 (e^{j\psi/2} - e^{-j\psi/2})$$

$$= E_0 \cdot 2 \cdot \left(\frac{e^{j\psi/2} - e^{-j\psi/2}}{2} \right) = 2E_0 \cdot j \sin\left(\frac{\psi}{2}\right)$$

$$\Phi = \beta d \cos \theta$$

$$\bar{E} = 2E_0 \cdot j \sin\left(\frac{\beta d \cos \theta}{2}\right)$$

j indicates the 2 point sources are opposite phase

$\bar{E}_{\text{max}} @ (i)$ considering the max radiations occurs, $2jE_0 = 1$, if $d = \lambda/2$, $\beta = 2\pi/\lambda$

$$E_{\text{max}} = \frac{1}{2} \sin\left(\frac{\pi}{2} \cos \theta\right)$$

$$\sin\left(\frac{\pi}{2} \cos \theta\right) = \pm 1$$

$$\Rightarrow \frac{\pi}{2} \cos \theta_{\text{max}} = \frac{\pi}{2} (2m+1)$$

$$\cos \theta_{\text{max}} = (2m+1)$$

$$\text{X } \sin\theta_{\max} = \pm (m+1) \frac{\pi}{2}$$

When $\theta = m=0$

$$\sin\theta_{\max} = \pm \frac{\pi}{2} \rightarrow \sin\theta_{\max} = \pm \frac{\pi}{2}$$

$\theta_{\max} = 90^\circ \text{ or } 180^\circ$

$$\boxed{\text{Error} = \sin\left(\frac{\pi \cos\theta}{2}\right)}$$

Max. radiations

$$\pi/2 \cos(0) \sin(\pi/2 \cos\theta) = \pm 1$$

$$\Rightarrow \sin(\pi/2 \cos\theta) = \pm (m+1) \pi/2$$

$$\pi/2 \cos\theta = \pm (2m+1) \frac{\pi}{2}$$

$$\cos\theta_{\max} = (m+1)$$

When $m=0$

$$\Rightarrow \cos\theta_{\max} = 1$$

$$\theta_{\max} = \cos^{-1}(1) = \cos^{-1}(1)$$

$$\boxed{\theta_{\max} = 0^\circ \text{ or } 180^\circ}$$

Min. radiations

$$\sin(\pi/2 \cos\theta) = 0$$

$$\sin(\pi/2 \cos\theta) = \pm m\pi$$

$$\pi/2 \cos\theta_{\min} = m\pi$$

$$\cos\theta_{\min} = 2m$$

$$\text{if } m=0, \cos\theta_{\min} = 0 \Rightarrow \theta_{\min} = \cos^{-1}(0)$$

$$\theta_{\min} = \cos^{-1}(0)$$

$$\boxed{\theta_{\min} = 0^\circ \text{ or } 90^\circ \text{ or } 270^\circ}$$

Half Power Point

$$\sin(\pi n \cos\theta) = \pm \sin(\pi n + \frac{\pi}{4})$$

$$\pi/2 \cos\theta_{HPP} = (2n+1)\frac{\pi}{4}$$

$$\cos\theta_{HPP} = (2n+1)\frac{1}{2}$$

When $n=0$

$$\cos\theta_{HPP} = \frac{1}{2} \rightarrow \theta_{HPP} = 60^\circ \text{ (or) } 120^\circ$$

Radiation Pattern

Consider the main radiations are

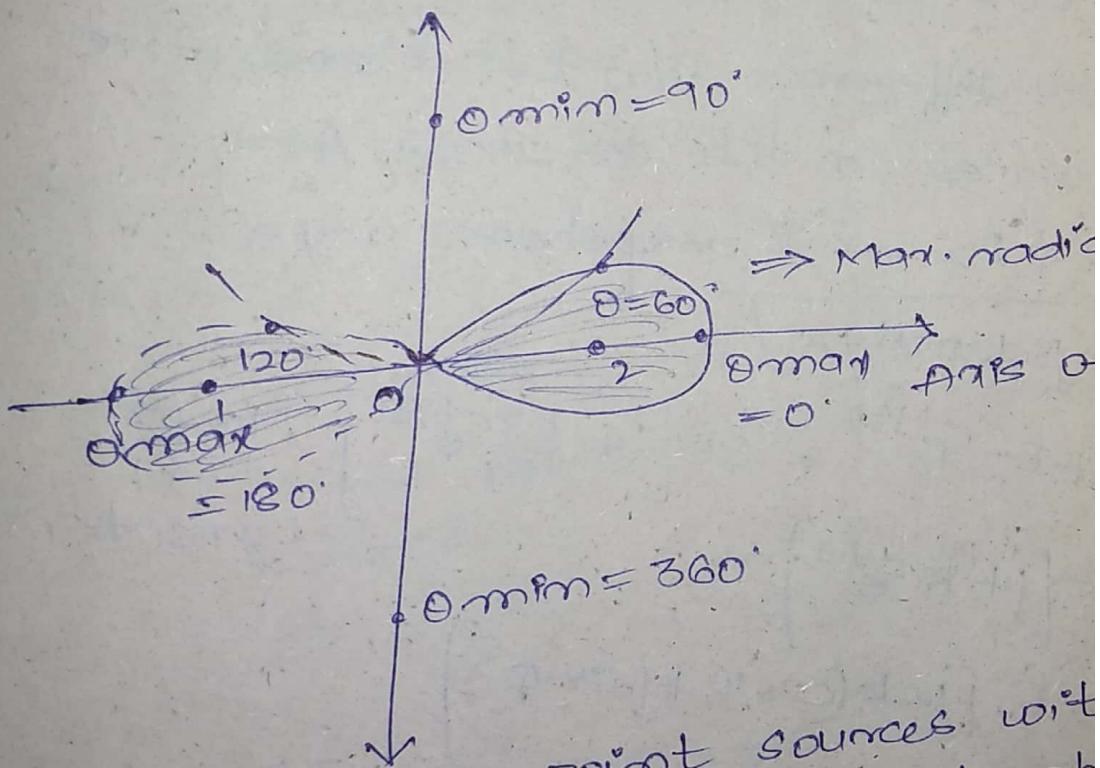


Fig (2) 2-Isotropic point sources with spaced with $d = \lambda/2$ and opposite ph. This Radiation Pattern is Endfire And Array bcz the main. radiations are unidirectional.

Case III) 2 point sources fed with unequal amplitude & any phase:

I_2 leads the current I_1

Now, taking I_1 as reference, then

$$E_1 = E_1 \cdot e^{j\psi \cos \theta}$$

$$E_2 = E_2 \cdot e^{j\psi}$$

$$\bar{E} = E_1 + E_2$$

$$= E_1 \cdot e^0 + E_2 \cdot e^{j\psi} = E_1 + E_2 e^{j\psi}$$

α = phase difference b/w two consecutive point sources in the Antenna Array

Say $E_1 \neq E_2$, & anywhere say α .

$$\Phi = \beta d \cos \theta + \alpha$$

$$\bar{E}_T = E_1 + E_2 \cdot e^{j\psi} = E_1 \left[1 + \frac{E_2}{E_1} e^{j\psi} \right], k = \frac{E_2}{E_1}$$

$$\bar{E}_T = E_1 \left[1 + k \cdot e^{j\psi} \right]$$

$$= E_1 \left[1 + k (\cos \psi + j \sin \psi) \right]$$

$$|\bar{E}_T| = |E_1 [1 + k \cos \psi + j \sin \psi]|$$

$$|\bar{E}_T| = E_1 \sqrt{(1+k \cos \psi)^2 + \sin^2 \psi k^2 \alpha^2}$$

$$|\bar{E}_T| \text{ where } \alpha = \tan^{-1} \left(\frac{k \sin \psi}{1 + k \cos \psi} \right)$$

Note: If $\alpha = 0^\circ$ or 180° , $E_1 = E_2$, we can obtain radiation patterns of first two earlier cases.

N-element uniform Linear Array:-

→ If the individual elements of the array are equally spaced along a line is called as Linear array

→ If the elements are fed with currents of equal amplitude and having an uniform progressive phase shift along the line is called as uniform linear array.

→ consider a linear array

of 'n' isotropic point

sources in which point sources are spaced equally and are fed with in-phase currents

of equal amplitude 'E₀'.

→ The total far-field value at a distance point 'p' is obtained by adding the fields of individual sources.

$$E_t = E_0 e^{j\psi} + E_0 e^{j\psi} + E_0 e^{j\psi} + \dots + E_0 e^{j(n-1)\psi}$$

$$E_t = E_0 + E_0 e^{j\psi} + E_0 e^{j2\psi} + \dots + E_0 e^{j(n-1)\psi}$$

$$E_t = E_0 [1 + e^{j\psi} + e^{j2\psi} + \dots + e^{j(n-1)\psi}] \quad (1)$$

where $\psi = \beta d \cos\theta + \alpha$.

ψ → Total phase difference of the fields at point 'p'.

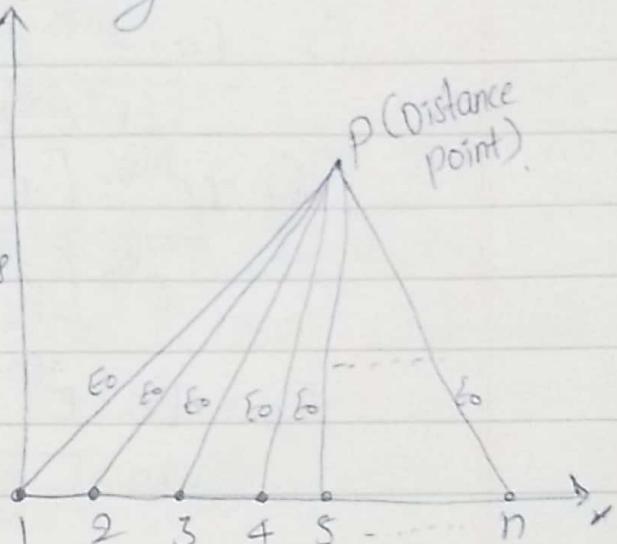
β → phase shift constant.

α → phase difference b/w adjacent elements.

eqn(1) multiplied by $e^{j\psi}$.

$$E_t e^{j\psi} = E_0 [e^{j\psi} + e^{j2\psi} + e^{j3\psi} + \dots + e^{jn\psi}] \quad (2)$$

Subtracting eq(2) from (1)



$$E_t - E_0 e^{j\psi} = E_0 [1 + e^{j\psi} + e^{j2\psi} + e^{j3\psi} + \dots + e^{j(n-1)\psi}] \cdot E_0 [e^{j\psi} + e^{j2\psi} + e^{j3\psi} + \dots + e^{jn\psi}]$$

$$= E_0 [1 - e^{jn\psi}] = E_0 [1 - e^{jn\psi}]$$

$$E_t = E_0 \frac{[1 - e^{jn\psi}]}{[1 - e^{j\psi}]}$$

$$E_t = E_0 \frac{[e^{jn\psi/2} \cdot e^{-jn\psi/2} - e^{jn\psi/2} \cdot e^{jn\psi/2}]}{[1 - e^{j\psi/2} \cdot e^{j\psi/2}]}$$

$$E_t = E_0 \frac{e^{jn\psi/2} [e^{-jn\psi/2} - e^{jn\psi/2}]}{e^{j\psi/2} [e^{-j\psi/2} - e^{j\psi/2}]}$$

$$E_t = E_0 \cdot \frac{e^{j(n-1)\psi/2} [e^{jn\psi/2} - e^{-jn\psi/2}]}{[e^{j\psi/2} - e^{-j\psi/2}]}$$

$$E_t = E_0 \cdot e^{j(n-1)\psi/2} \cdot S_{\text{SA}}(n\psi/2)$$

$$2j S_{\text{SA}}(\psi/2)$$

$$E_t = E_0 \cdot e^{j(n-1)\psi/2} \cdot \frac{\sin(n\psi/2)}{\sin(\psi/2)}$$

$$E_t = E_0 \frac{\sin(n\psi/2)}{\sin(\psi/2)} \angle e^{j\phi} \quad \phi = (n-1)\psi/2$$

$$E_t = E_0 \cdot \frac{\sin(n\psi/2)}{\sin(\psi/2)} [\cos\phi + j\sin\phi]$$

The total field pattern of linear array of n-isotropic point source is given as,

$$E_t = E_0 \frac{\sin(n\psi/2)}{\sin(\psi/2)} \angle \phi$$

Array factor

$$\frac{E_t}{E_0} = \frac{\sin(n\psi/2)}{\sin(\psi/2)}$$

Maximum Electric field:-

→ In the total field vector, if $\psi = 0$ the equation becomes indeterminate. Hence L' hospital rule must be applied to evaluate the function.

$$\lim_{\psi \rightarrow 0} E_t = E_0 \frac{\lim_{\psi \rightarrow 0} \frac{d}{d\psi} (\sin(n\psi/2))}{\lim_{\psi \rightarrow 0} \frac{d}{d\psi} (\sin(\psi/2))}$$

$$E_{t\max} \Rightarrow E_0 \lim_{\psi=0} \frac{\frac{n}{2} \cos(n\psi/2)}{\frac{1}{2} \cos(\psi/2)}$$

$$= E_0 \cdot \frac{\frac{n}{2} \cdot \cos 0^\circ}{\frac{1}{2} \cos 0^\circ}$$

$$= E_0 \cdot n$$

$$\boxed{E_{t\max} = E_0 \cdot n}$$

The maximum value of E_t is n' times the field from a single source.

Normalized field:-

$$E_{\text{norm}} = \frac{E_t}{E_{t\max}}$$

$$E_{\text{norm}} = \frac{E_0 \left(\sin(n\psi_2) \right)}{\sin(\psi_2)} \cdot E_0 \cdot n$$

$$E_{\text{norm}} = \frac{\sin(n\psi_2)}{n \sin(\psi_2)} = (\text{Array factor})_n$$

Characteristics of Broadside Array:-

→ In broadside array, the maximum radiation is in perpendicular to array axis i.e. 90° & 270°

→ sources are in-phase. i.e. $\alpha=0$ & $\phi=0$

Ψ = Total phase difference at point P

the field at point P:

\rightarrow phase difference in adjacent point sources.

$$\Psi = \beta d \cos \theta + \alpha \quad (\because \Psi = \alpha)$$

$$\beta d \cos \theta = 0$$

Maximum Radiation:-

$$\beta d \cos \theta_{\max} = 0$$

$$\cos \theta_{\max} = 0$$

$$\theta_{\max} = \cos^{-1}(0)$$

$$\theta_{\max} = 90^\circ \text{ & } 270^\circ$$

