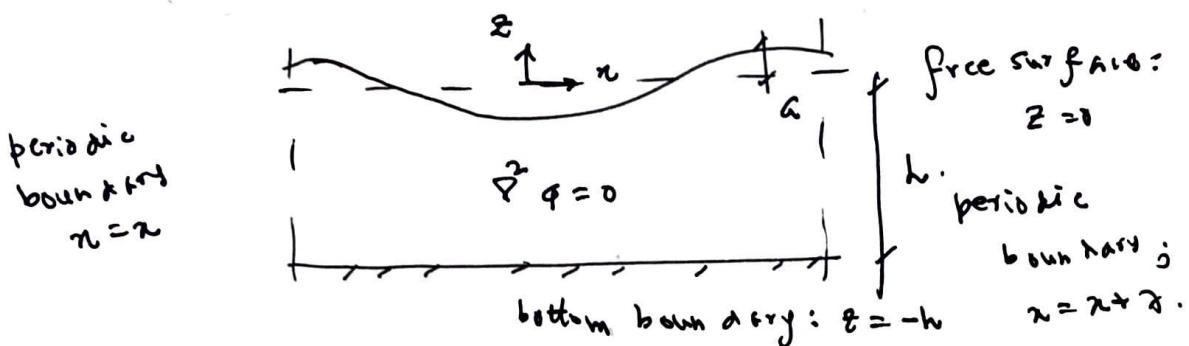


## Linear theory of 2D progressive wave & cut

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### Wave dispersion



For inviscid, irrotational flow, velocity potential exists,  $\phi = \psi(x, z, t)$ . For incompressible flow, it satisfies,  $\nabla^2 \phi = 0$  —①

- The velocity potential must conform to wave elevation of the form  $\eta = \eta(x, t) = a \cos(kx - \omega t)$  at boundary conditions,

- ① periodic boundary conditions.
- ② bottom boundary condition,  $z = -h$ .
- ③ free surface boundary condition,  $z = 0$ .

### ① Periodic boundary conditions.

$$\eta = a \cos(kx - \omega t) \quad .$$

$$\eta = \eta(x, t) \equiv \eta(x + \lambda, t)$$

$$\text{or, } a \cos(kx - \omega t) = a \cos(k(x + \lambda) - \omega t)$$

$$\text{or, } a (\cos kx \cos \omega t + \sin kx \sin \omega t)$$

$$= a (\cos(kx + k\lambda) \cos \omega t + \sin(kx + k\lambda) \sin \omega t)$$

$$= a (\cos(kx + k\lambda) \cos \omega t + \sin(kx + k\lambda) \cdot \sin \omega t)$$

$$\text{or, } \cos kx = \cos(kx + k\lambda) \quad \text{—②}$$

$$\text{or, } \sin kx = \sin(kx + k\lambda). \quad \text{—③}$$

For both ④ and ⑤ to be valid,

$$k\lambda = 2\pi \text{ or } \lambda = \frac{2\pi}{k}$$

~~Divide by k~~

$$k = \frac{2\pi}{\lambda}$$

periodic boundary condition for time,

$$\psi(x, t) = \psi(x, t + T)$$

$$\alpha G_3(kx - \omega t) = \alpha G_3(kx - \omega(t + T))$$

$$\alpha G_3(kx \cos \omega t + c \sin kx \sin \omega t) = \alpha G_3(kx \cos(\omega t + \omega T) + c \sin kx \sin(\omega t + \omega T))$$

$$\text{or, } G_3(\omega t) = G_3(\omega t + \omega T) \quad \text{--- (4)}$$

$$\text{Now, } \sin(\omega t) = \sin(\omega t + \omega T) \quad \text{--- (5)}$$

both ④ and ⑤ to be valid, we must have

$$\omega T = 2\pi \text{ or } T = \frac{2\pi}{\omega}$$

Thus, the periodic boundary conditions do not give us anything related to the solution, rather than confirming that the wave elevation is periodic in both space and time with wave number ( $k$ ) and wave period ( $T$ ) respectively.

Solution of the velocity potential from the Laplace ~~equation~~ equation

using separation of variables, we can get,

$$\psi = \psi(x, z, t) = R e [Z(z) e^{-ikx + i\omega t}]$$

$$\therefore \frac{\partial \psi}{\partial x} = R e [(-ik) Z(z) e^{-ikx + i\omega t}]$$

$$\text{and } \frac{\partial^2 \psi}{\partial x^2} = R e [(-ik)^2 Z(z) e^{-ikx + i\omega t}]$$

$$\frac{\partial \phi}{\partial z} = \operatorname{Re} \left[ \frac{\kappa^2}{\alpha z} \cdot e^{-ikx + i\omega t} \right]$$

$$\frac{\partial^2 \phi}{\partial z^2} = \operatorname{Re} \left[ \frac{\kappa^2}{\alpha z^2} \cdot e^{-ikx + i\omega t} \right]$$

Now, from Laplace equation ① we get,

$$\frac{\kappa^2}{\alpha z^2} - \kappa^2 \cdot 2 = 0. \quad \text{--- } ⑥$$

~~(Ansatz)~~ ~~But~~ general solution is of the form,  
~~(Ansatz)~~  $Z = C_1 e^{kz} + C_2 e^{-kz} \quad \text{--- } ⑦$

3. The bottom boundary condition

③ ~~(Ansatz)~~ ~~From~~ ~~bottom~~ ~~boundary~~ ~~condition~~

$$\text{From bottom } \frac{\partial \phi}{\partial z} \Big|_{z=-h} = 0 \quad \text{--- } ⑧$$

$$\text{or, } \operatorname{Re} \left[ \frac{\kappa^2}{\alpha z} \cdot e^{-ikz + i\omega t} \Big|_{z=-h} \right] = 0$$

$$\text{or, } \frac{\kappa^2}{\alpha z} \Big|_{z=-h} = 0 \quad \text{--- } ⑨$$

~~(Ansatz)~~ ~~from~~ ~~bottom~~ ~~boundary~~ ~~condition~~

4. Dynamic free surface boundary condition

$$\text{At free surface } \beta(n) = 0$$



$$\beta(n) := \beta(n, \beta(z)) + n \frac{d}{dz} (\beta(z)) \Big|_{z=0}$$

~~(Ansatz)~~

for boundary condition we get,

inviscid irrotational flow, vertical throughout the fluid, we get,

$$\frac{\partial \alpha}{\partial t} + \frac{1}{2} (u^2 + v^2) + \frac{b}{g} + g z = 0.$$

$$\text{or, } b = -g \left[ \frac{\partial \alpha}{\partial t} + \frac{1}{2} (u^2 + v^2) + g z \right]$$

$$= -g \left[ \frac{\partial \alpha}{\partial t} + \frac{1}{2} \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) + g z \right]$$

$$= -g \left[ \frac{\partial \alpha}{\partial t} + \frac{1}{2} \left[ \left( \frac{\partial u}{\partial x} \right)^2 + \left( \frac{\partial v}{\partial x} \right)^2 \right] + g z \right]$$

By ~~linearization~~ linearization,

$$0 = -g \left[ \frac{\partial \alpha}{\partial t} + g z \right] \quad \text{at } z=0$$

$$\text{or, } n \cdot g = - \frac{\partial \alpha}{\partial t} \quad \text{at } z=0$$

$$\text{or, } n = - \frac{1}{g} \cdot \frac{\partial \alpha}{\partial t} \quad \text{at } z=0 \quad \text{--- (10)}$$

### 3. Kinematic free surface boundary condition

A point on the free surface remains on the free surface.

$$\frac{D}{Dt} n = \frac{\partial}{\partial t} n + u \frac{\partial n}{\partial x} + v \frac{\partial n}{\partial y}$$

$\Rightarrow n = n(x, t)$  for 2D waves,

$$\therefore \frac{\partial n}{\partial z} = 0.$$

$n \cdot \frac{\partial n}{\partial z}$  neglected through linearization.

$$\text{thus, } n = \frac{\partial \alpha}{\partial t} = \frac{\partial \alpha}{\partial x} = \frac{\partial \alpha}{\partial t}$$

$$\text{or, } \frac{\partial \alpha}{\partial z} = \frac{\partial \alpha}{\partial t} \quad \text{--- (11)}$$

Combining (10) and (11), we get,

$$\frac{\partial \alpha}{\partial t} + g \frac{\partial \alpha}{\partial x} = 0 \quad \text{--- (12)}$$

Equation (12) in brief is known as kinematic free surface boundary condition or CFBC.

### Finding constants (contd)

applying ⑦ into ⑨, we get,

$$C \cdot e^{-kh} - D \cdot e^{kh} = 0 \quad \text{--- (13)}$$

applying ⑦ into ⑩, we get,

$$C + D = \frac{i \alpha g}{\omega} \quad \text{--- (14)}$$

by solving, we get,

$$C \cdot (e^{kh} + e^{-kh}) = \frac{i \alpha g}{\omega} \cdot e^{kh}$$

$$D \cdot (e^{kh} + e^{-kh}) = \frac{i \alpha g}{\omega} \cdot e^{-kh}$$

$$\text{thus, } Z(z) = \frac{i \alpha g}{\omega} \cdot \frac{(g_b h k (z+h))}{(g_b h k h)} \cdot e^{izx + i\omega t}$$

$$\text{or, } \eta = \eta_0 [Z(z) \cdot e^{izx + i\omega t}]$$

$$= \frac{\alpha g}{\omega} \cdot \frac{(g_b h k (z+h))}{(g_b h k h)} \cdot \sin(kx - \omega t) \quad \text{--- (15)}$$

### wave dispersion for finite depth

applying ⑮ to ⑫ we get,

$$\omega = g_b \tanh(kh) \quad \text{--- (16)}$$

### wave potential for infinite depth

$$Z(z) = \cos(kh) \cdot \cancel{e^{izx}} \cdot C \cdot e^{izx} \quad \text{--- (16)}$$

$D = 0$ , since  $e^{-izx}$  increases as  $z \rightarrow -\infty$   
 $B$  decreases. Thus we have at  $Z(x)$

$$= C \cdot e^{izx} = 0.$$

$$\text{Applying } (1) \text{ into } (10), \text{ we get,}$$

$$C = \frac{i g a}{\omega}.$$

thus,  $\varphi(x, z, t) = \frac{g a}{\omega} e^{kz} \sin(kx - \omega t) \quad - (12)$

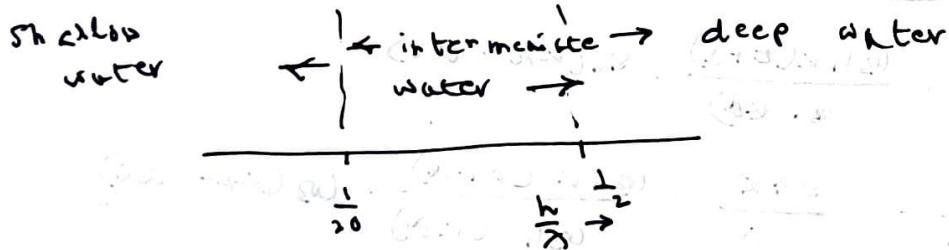
$$\text{Applying, we get, Applying } (2) \text{ into } (12), \text{ we get,}$$

$$-\frac{k^2 a^2}{\omega} \cdot e^{kz} \sin(kx/\omega t) + g \cdot \frac{a^2}{\omega} \cdot k \cdot e^{kz} \sin(kx - \omega t) = 0.$$

$$\omega = \frac{g k}{\omega} \text{ or, } \omega = g k \quad - (13)$$

Equation (13) is the wave dispersion relationship in infinite depth case. By using proper approximations for infinite depth for hyperbolic functions, it can also be shown that equation (1) is reduced to equation (13).

Approximating linear wave dispersion for deep water and shallow water conditions.



$$\omega^r = g k \cdot \tanh(h k)$$

$$= g k \cdot \frac{e^{kh} - e^{-kh}}{e^{kh} + e^{-kh}}$$

for deep water  $h$  is very large, or,  
 $\frac{h}{k} \gg 1$ , thus  $kh \gg 1$ , since

$$kh = \frac{2\pi k}{\lambda}.$$

$$\therefore \text{Thus, } \omega^r = g k \cdot \frac{1 - e^{-2kh}}{1 + e^{-2kh}}$$

$$= g k \cdot \frac{1 - \frac{1}{e^{2kh}}}{1 + \frac{1}{e^{2kh}}} \approx \approx g k. (1)$$

$$\text{or, } \omega^2 = gk - \dots \quad (1)$$

Thus we can resolve wave dispersion for deep water condition by applying suitable transformation to  $\tanh(kh)$ .

~~On the other hand, for shallow water,  $b \ll h$  or,  $kh \gg 1$ .~~

$$\text{Thus, } \omega^2 = gk \cdot \frac{e^{kh} - e^{-kh}}{e^{kh} + e^{-kh}}$$

$$\approx gk \cdot \frac{1 + kh - 1 + kh}{1 + kh + 1 - kh}$$

$$= gk \cdot (kh) = gk^2 h$$

$$\text{or, } c = \frac{x^2}{T^2} = gh \text{ or, } c = \sqrt{gh}$$

$$\text{or, } \lambda = T \cdot \sqrt{gh}. \quad (2)$$

velocity field under 2D progressive wave

$$\varphi = \frac{a_0}{\omega} \cdot \frac{\cosh k(z+\alpha)}{\cosh k\alpha} \cdot \sin(kx - \omega t)$$

$$u = \frac{\partial \varphi}{\partial x} = \frac{\partial a_0 k}{\partial x} \cdot \frac{\cosh k(z+\alpha)}{\cosh k\alpha} \cdot \cos(kz - \omega t)$$

$$w = \frac{\partial \varphi}{\partial z} = \frac{\partial a_0 k}{\partial z} \cdot \frac{\sinh k(z+\alpha)}{\cosh k\alpha} \cdot \sin(kx - \omega t)$$

$\rightarrow u$  and  $w$  is in phase difference of  $\frac{\pi}{2}$ .

Thus, when  $u$  is maximum,  $w$  is minimum and vice versa.

$$\frac{dt}{dx} = \frac{H_b}{C_{gA}} - \frac{b_a}{C_{gA}}$$

## Pressure field under a progressive wave in 2D

From Bernoulli's equation we get,

$$\left( \frac{\partial \phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=0} = \left( \frac{\partial \phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=n} \quad \text{--- (1)}$$

Through the process of linearization, we get,

$$\left( \frac{\partial \phi}{\partial t} \right) \approx \left( \frac{\partial \phi}{\partial t} \right)_{z=0}$$

$$\left( \frac{\partial \phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=n} \approx \left( \frac{\partial \phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=0} + \frac{\partial}{\partial z} \left( \frac{\partial \phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=0}$$

From Dynamic free surface

$$p(z=0) = 0 \quad \text{boundary condition}$$

From dynamic free surface boundary condition, we get,

$$p(z=0) = 0. \quad \text{And, } \eta = - \frac{1}{g} \cdot \frac{\partial \phi}{\partial t} \Big|_{z=0}$$

~~$$\text{And also, } \frac{\partial \phi}{\partial t} \Big|_{z=n} \approx \frac{\partial \phi}{\partial t} \Big|_{z=0}, \text{ since } n \text{ is very small.}$$~~

Thus, from equation (1), we get,

$$\left( \frac{\partial \phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=n} = \left( \frac{\partial \phi}{\partial t} \right) \Big|_{z=0} - g \cdot \frac{1}{g} \cdot \frac{\partial \phi}{\partial t} \Big|_{z=0}$$

$$\text{or, } \frac{p}{\rho} = - gz - \frac{\partial \phi}{\partial t}$$

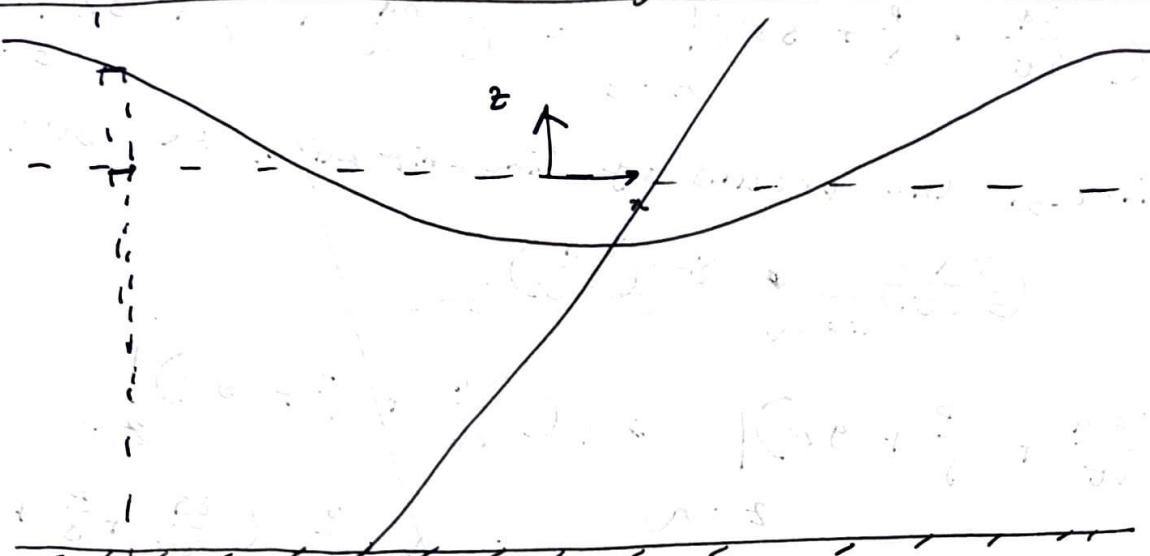
$$\text{or, } \frac{p}{\rho} = - gz + \underbrace{g \alpha g \cdot K_p(z)}_{\text{hydrostatic dynamic part}} \cdot \underbrace{(K_n - w_t)}_{\text{using free surface of part}}$$

where,  $\phi(x, z, t)$  defined earlier

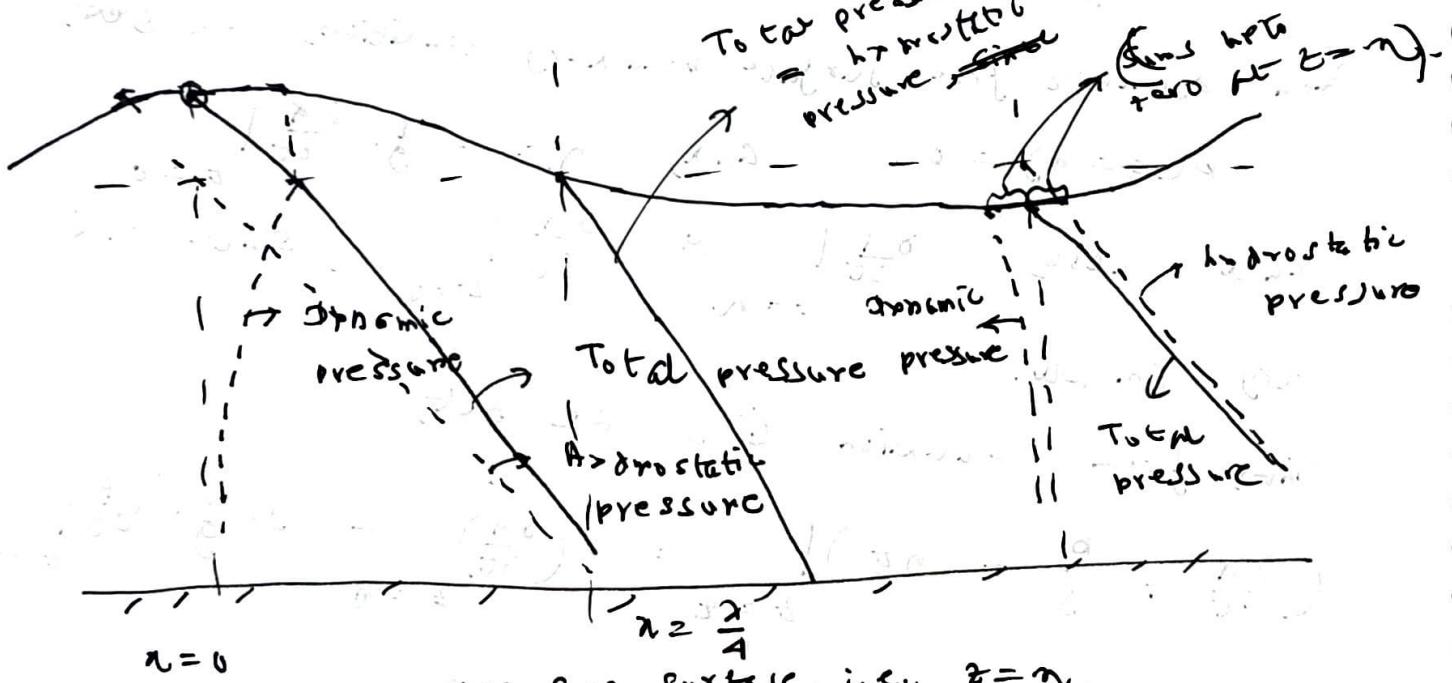
where,  $K_p(z)$  pressure response factor.

Friction coefficient is defined as,

$$k_p(z) = \frac{B h K (h+z)}{B h (K h)}$$



Total pressure = hydrostatic pressure + friction pressure



at free surface, i.e.,  $z=n$ ,

$$p(z=n) = -\rho g n + \rho g \frac{\partial \eta}{\partial t} \quad (1)$$

$$\underline{p(z=n) = -\rho g n}$$

$$\underline{p(z=n) = -\rho g n + g \cdot \frac{\partial \eta}{\partial t}} \Big|_{z=0} = 0$$

$$\underline{p(z=n) = -\rho g n - g \cdot \frac{\partial \eta}{\partial t}} \Big|_{z=0} = 0$$

$$\frac{1}{x} \quad \frac{H_b}{x} - \frac{C_{g_a}}{x} \cdot b_a$$

- At  $z = \infty$ , the hydrostatic part is cancelled by the dynamic part and thus we have  $b(z=\infty) = 0$ .

Under the waves, i.e., at  $x = \frac{\lambda}{4}$  if the total pressure is purely hydrostatic, since,

$$\cancel{(b)} \cdot b_3 (kx - wt) \Big|_{x=\frac{\lambda}{4}} \neq b_3 \left( \frac{\pi}{2} - wt \right)$$

$$\begin{aligned} \text{and dynamic pressure } &= b_3 \frac{\pi}{2} \sin wt + \cancel{\sin wt} b_3 \\ \text{but } & \sin \pi/2 = 1 \\ & \therefore \sin wt \neq \cancel{\sin wt} b_3 \\ &= 0 \text{ (zero dynamic pressure)} \end{aligned}$$

Under the waves, i.e., at  $x = \frac{\lambda}{4}$ , the total pressure is purely hydrostatic, since,

$$(b (kx - wt)) \Big|_{x=\frac{\lambda}{4}, k=0} = 0$$

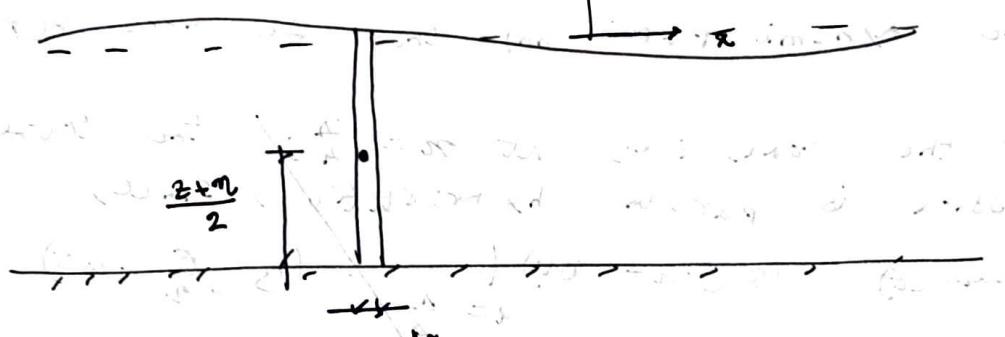
$$x = \frac{\lambda}{4}, k = 0$$

~~thus~~ for the dynamic pressure is zero and the depth.

### Wave Energy

for a progressive periodic wave, there is a movement of the free surface. Thus there is a potential energy. On the other hand, as the wave propagates, there is a movement of a fluid element due to the existence of a velocity field. Thus there is a ~~potent~~ kinetic energy.

Estimation of wave energy is required for assessing power required to drive a wave maker in a flume for drag experiments and for estimating availability of wave power while designing a device for transforming ~~transforming~~ transforming wave energy into other forms of energy.



for ~~across~~ a water column of ~~width~~ width  $\Delta x$  and thickness along  $z$  axis  $\Delta z$ , the potential energy is

$$\Delta PE = \text{Volume} \cdot \frac{\rho + n}{2}$$

$$\Delta m = g \cdot (\rho + n) \cdot \Delta z$$

$$\therefore \Delta PE = g g \frac{(\rho + n)^2}{2} \Delta z$$

$$= \frac{1}{2} g g (\rho^2 + 2\rho n + n^2) \Delta z$$

The average potential energy over a wave length

$$(\overline{PE}) = \frac{1}{\lambda} \int_{-\lambda/2}^{\lambda/2} \left( \frac{1}{2} g g \right) (\rho^2 + 2\rho n + n^2) \Delta x$$

$$= \left( \frac{1}{2} \right) \cdot \left( \frac{g g}{\lambda} \right) \int_{-\lambda/2}^{\lambda/2} (\rho^2 + 2\rho n + n^2) \cos(kx - \omega t) dx$$

$$+ \frac{a^2 \rho^2}{\lambda} \cos^2(kx - \omega t) dx$$

$$\int_{-\lambda/2}^{\lambda/2} \rho^2 dx = 0 \quad \text{because } \rho \text{ is constant}$$

$$\int_{-\lambda/2}^{\lambda/2} 2\rho n \cos(kx - \omega t) dx = 0 \quad \text{because } \cos(kx - \omega t) \text{ is odd}$$

$$\int_{-\lambda/2}^{\lambda/2} n^2 dx = \frac{a^2 \rho^2}{\lambda} \int_{-\lambda/2}^{\lambda/2} \cos^2(kx - \omega t) dx$$

$$H_a \quad H_b \quad C_{ga} \cdot b_a$$

$$\therefore \frac{8g}{3} \cdot \frac{1}{2} \cdot \frac{\dot{a}^2}{K} = \frac{8g}{2\pi} \cdot \frac{\dot{a}^2}{2\pi} = \frac{8g a^2}{4}$$

Similarly, • kinetic energy of a small fluid element of size  $dx dz$  at a depth  $z$  and at a distance  $x$  is

$$d(KE) = dm \cdot \frac{u^2 + w^2}{2} \cdot dx dz = g \frac{\dot{u}^2 + \dot{w}^2}{2} \cdot dx dz$$

per unit thickness across

y axis

Thus average kinetic energy is

$$(\bar{KE}) = \frac{1}{3} \int_{x=0}^{x=3} \int_{z=-h}^{z=0} g \frac{\dot{u}^2 + \dot{w}^2}{2} \cdot dx dz$$

Substitution for  $u$  and  $w$  given,

$$(\bar{KE}) = \frac{1}{3} \int_{x=0}^{x=3} \int_{z=-h}^{z=0} g \left( \frac{1}{2} \right) \left( \frac{a^2 \dot{a}^2 k^2}{\omega^2} \cdot \frac{\sinh^2(kz+h)}{\cosh^2(kz+h)} \right)$$

$$= \frac{1}{3} \left[ g \frac{a^2 \dot{a}^2 k^2}{\omega^2} \cdot \frac{\sinh^2(k(z+h))}{\cosh^2(k(z+h))} \right]$$

$$= \frac{1}{3} \left[ \int_{x=0}^{x=3} \int_{z=-h}^{z=0} \frac{g^2 \dot{a}^2 k^2}{\omega^2} \cdot \frac{\sinh^2(kx - \omega t)}{\cosh^2(kx - \omega t)} \cdot dx dz \right]$$

$$+ \left[ \int_{x=0}^{x=3} \int_{z=-h}^{z=0} g^2 a^2 k^2 \cdot \frac{\sinh^2(k(x+z)) \cdot \sinh^2(k(x-\omega t))}{\cosh^2(k(x+z)) \cdot \cosh^2(k(x-\omega t))} \right]$$

$$= \frac{1}{3} \cdot 3 \cdot \frac{8g a^2}{4} \int_{x=0}^{x=3} \int_{z=-h}^{z=0} \frac{1}{\cosh^2(k(x+z))} \cdot \frac{1}{\cosh^2(k(x-\omega t))} \cdot dx dz$$

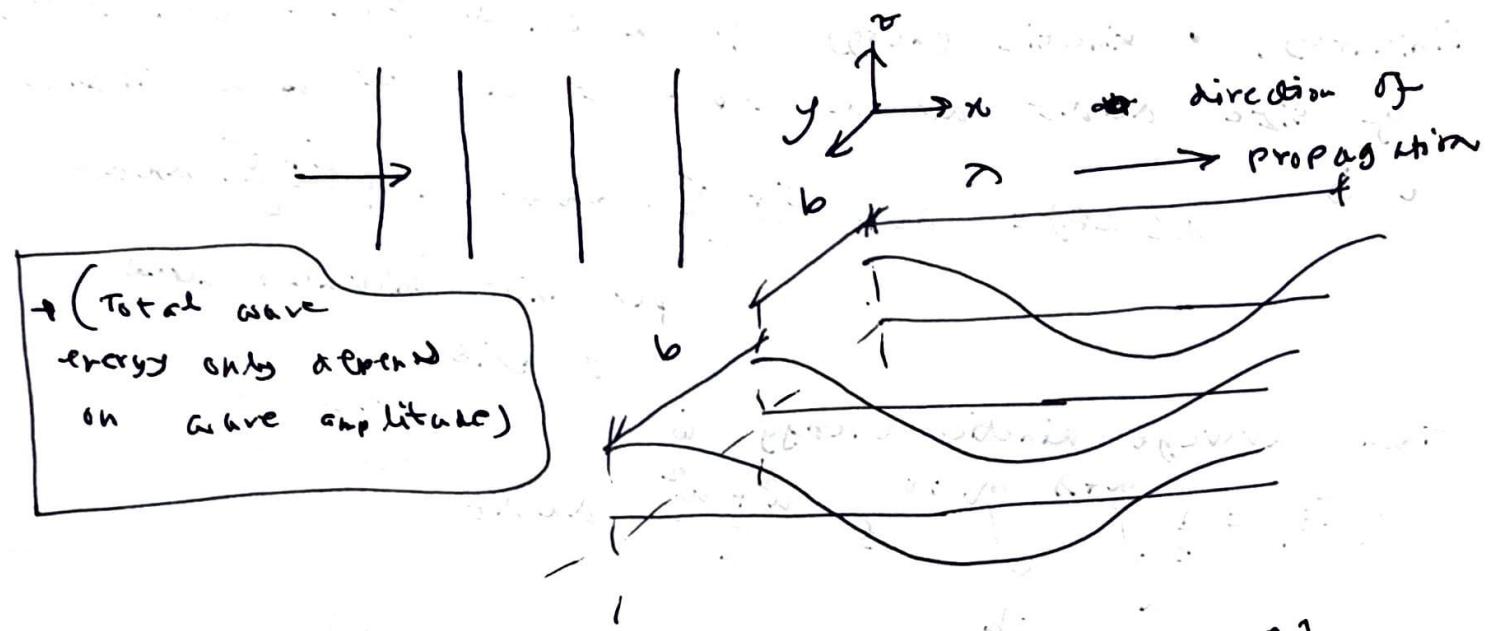
Thus, the total wave energy per wave length

and per unit thickness across y axis is

$$E = \frac{8g a^2}{4} + \frac{8g a^2}{4} = \frac{8g a^2}{2} = \frac{8g H^2}{8}$$

This ~~may also~~ may also be defined as wave energy per unit surface area (i.e., ~~area~~  $b_a$ )

where  $b$  may be ~~any~~ a measure of separation  
between identical wave trains.



$$[E] = ? \frac{1}{2} S g a^2 \equiv [ML^{-3}] \cdot [LT^{-2}] \cdot [L^2] \equiv [M T^{-2}]$$

$$[E] \text{ we know is } [MLT^{-2}] \cdot [L] \equiv [ML^2 T^{-2}]$$

$$\therefore [B] [L^{-2}] \equiv [ML^2 T^{-2}] [L^2] \equiv [M T^{-2}]$$

Some details about the kinetic energy derivation

$$(KE) = \frac{1}{2} \int_{-h}^{n+h} \int_{-\infty}^{\infty} \left( \frac{g}{2} \right) \cdot \left[ \frac{\partial^2 \tilde{z}^2 u^2}{\omega^2} \cdot \frac{\cosh^2 k(h+z)}{\cosh^2(kh)} \cdot \cos^2(kx - \omega t) \right]$$

$$+ \left( \frac{g^2 a^2 k^2}{\omega^2} \cdot \frac{\sinh^2 k(h+z)}{\cosh^2(kh)} \cdot \sin^2(kx - \omega t) \right) \frac{\partial^2 \tilde{z}^2}{\partial x \partial z}$$

$$= \left( \frac{g}{2\pi} \right) \cdot \frac{g^2 a^2 k^2}{\omega^2} \cdot \frac{1}{\cosh^2(kh)} \cdot \int_{-h}^{n+h} \int_{-\infty}^{\infty} \left[ \cosh^2 k(h+z) \cdot \cos^2(kx - \omega t) + \sin^2 k(h+z) \cdot \sin^2(kx - \omega t) \right]$$

We observe,

$$\cosh^2 \alpha \cdot \cos^2 \theta + \sinh^2 \alpha \cdot \sin^2 \theta$$

$$= \left( \frac{e^\alpha + e^{-\alpha}}{2} \right)^2 \cdot \cos^2 \theta + \left( \frac{e^\alpha - e^{-\alpha}}{2} \right)^2 \cdot \sin^2 \theta$$

$$\begin{aligned}
 &= \frac{e^{2\alpha} + 2 + e^{-2\alpha}}{4} \cdot \cos^2 \theta + \frac{e^{2\alpha} - 2 + e^{-2\alpha}}{4} \cdot \sin^2 \theta \\
 &= \frac{e^{2\alpha} + e^{-2\alpha}}{4} \cdot \cos^2 \theta + \frac{e^{2\alpha} + e^{-2\alpha}}{4} \cdot \sin^2 \theta + \frac{2}{4} \cdot (\cos^2 \theta - \sin^2 \theta)
 \end{aligned}$$

$$= \frac{1}{2} \cdot \cos b(2\alpha) + \frac{1}{2} \cdot (\cos 2\theta)$$

$$\text{thus, } (\bar{k}\theta) = \left(\frac{3}{2}\right) \cdot \frac{\partial^2 \theta^2 k^2}{\partial x^2} \cdot \int_{-h}^{x+h} \frac{1}{2} (\cos b(2\alpha) + \cos 2(x - h)) dx$$

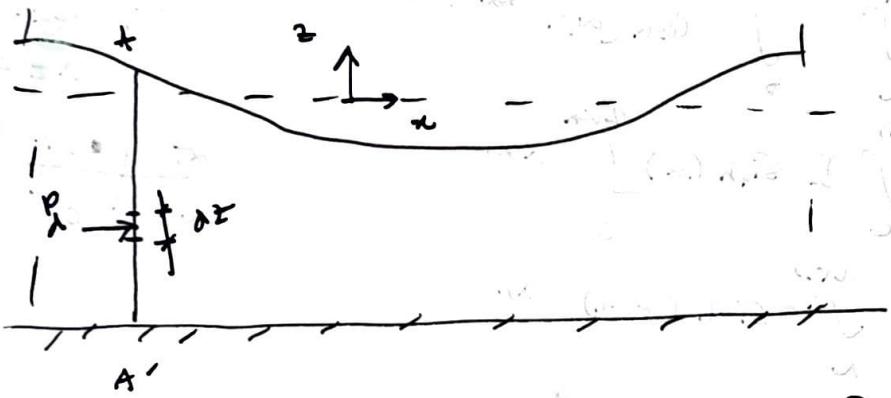
$$\begin{aligned}
 &\text{Now, } \int_{-h}^{x+h} \int_0^\infty (\cos b(2\alpha) + \cos 2(x - h)) d\alpha d\theta \\
 &= \frac{1}{2} \int_x^{x+h} \int_0^\infty \cosh(\alpha) \cdot \cos b(2\alpha) d\alpha d\theta, \quad 2k(b+2) = \infty. \\
 &= \frac{1}{2k} \int_x^{x+h} \left[ \sinh(\alpha) \right]_0^{2kh} d\theta \\
 &= \frac{1}{2k} \int_x^{x+h} \sinh(2kh) d\theta \\
 &= \frac{1}{2k} \cdot \sinh(2kh) \cdot x
 \end{aligned}$$

$$\text{and, } \int_{-h}^{x+h} \int_0^\infty \cos 2(kx - \omega t) d\alpha d\theta$$

$$\begin{aligned}
 &= \int_{-h}^0 \int_x^{x+h} \cos 2(kx - \omega t) d\alpha d\theta, \quad 2(kx - \omega t) = \theta. \\
 &= \int_{-h}^0 \int_x^{x+h} \cos 2(kx + \omega t - \omega t) d\alpha d\theta, \quad 2k d\alpha = \lambda \theta \\
 &= \int_{-h}^0 \int_x^{x+h} \cos 2(kx + \omega t) d\alpha d\theta, \quad d\alpha = \frac{d\theta}{2k} \\
 &= \int_{-h}^0 \int_x^{x+h} [\sin \theta] \cdot \frac{d\theta}{2k} d\theta, \quad \frac{x}{2k} \int_x^{x+h} \frac{d\theta}{2k} = \frac{(kx - \omega t)}{2k} + \frac{\omega t}{2k} \\
 &= 0
 \end{aligned}$$

$$\begin{aligned}
 \text{Thus, } (\bar{K}_B) &= \left(\frac{3}{2\pi}\right) \cdot \frac{g^2 \bar{a}^2 k}{\omega^2} \cdot \frac{1}{(G_B h)^2 (K_B)} \cdot \frac{1}{4\pi} \cdot \text{Sinh}(2Kh) \cdot \pi \\
 &= \left(\frac{3}{\pi}\right) \cdot \frac{g^2 \bar{a}^2 k}{G_B h \text{tanh}(Kh) \cdot G_B h^2 (Kh)} \cdot \frac{1}{4} \cdot \pi \text{Sinh}(Kh) \text{tanh}(Kh) \\
 &= \frac{\frac{3}{4} g^2 \bar{a}^2}{\text{Sinh}(Kh) \cdot \text{tanh}(Kh)} \cdot \frac{\text{Sinh}(Kh) \cdot (G_B h)^2 (Kh)}{\text{Sinh}(Kh) \cdot \text{tanh}(Kh)} \\
 &= \frac{\frac{3}{4} g^2 \bar{a}^2}{1}
 \end{aligned}$$

Idea about wave energy flux



Rate at which work is done by fluid on one side of section A-A' is the other side is

$\alpha(\omega) = p_a(z) \cdot u \Delta z$  per unit width across y-axis.

Thus, the time average rate of work done is defined as energy flux and given as,

$$\begin{aligned}
 E &= \frac{1}{T} \int_{t-h}^{t+T} \int_{-\infty}^{\infty} p_a(z) \cdot u \Delta z dt \\
 &= \frac{1}{T} \int_{t-h}^{t+T} \int_{-\infty}^{\infty} 88 g K_p(z) \cdot u \cdot \frac{\partial a k}{\omega} \cdot \frac{(G_B h k(h+\omega))}{(G_B h k(h))} dz dt \\
 &= \frac{1}{T} \cdot \frac{8 \bar{a}^2 \bar{g}^2 k}{\omega} \int_{t-h}^{t+T} \int_{-\infty}^{\infty} \frac{(G_B h^2 k(h+\omega))}{(G_B h^2 (Kh))} \cdot (a^2 (kx - \omega t)) dz dt
 \end{aligned}$$

$$= \frac{3\bar{g}^2 k}{e \omega T} \quad \text{for } \frac{1}{\cosh^2(kh)} \cdot \int_{-h}^{h+T} \int_{-\infty}^{\infty} (\cos^2 k(h+z) \cdot \cos^2(kx - \omega t)) dz dt$$

$$\text{we find} \int_{-h}^{h+T} \int_{-\infty}^{\infty} \cos^2 k(h+z) \cos^2(kx - \omega t) dz dt$$

$$= \int_{kx - \omega t = 0}^{\infty} \int_0^{kh} \cosh^2(\omega) \cdot \frac{\partial \theta^2(0)}{k} \left( \frac{\partial \theta}{\omega} \right)$$

det,  $k(h+t) = \alpha$ .  
or,  $k\Delta t = \partial \theta$ .  
 $\Delta t = \frac{\partial \theta}{k}$ .

$$= - \frac{1}{\omega k} \cdot \left( \frac{1}{2} \right) \cdot \int_{kx - \omega t}^{kx - \omega t - 2\pi} \int_0^{kh} (1 + \cosh(2\alpha)) \cos^2 \theta d\alpha d\theta$$

$$= - \frac{1}{2\omega k} \cdot \int_{kx - \omega t}^{kx - \omega t - 2\pi} \left[ \alpha + \frac{\sinh(2\alpha)}{2} \right]_0^{kh}$$

$\alpha = \frac{kh}{\omega} - \frac{\partial \theta}{\omega}$

$$= - \frac{1}{2\omega k} \cdot \left( kh + \frac{\sinh(2kh)}{2} \right) \cdot \left( \frac{1}{2} \right) \int_{kx - \omega t - 2\pi}^{kx - \omega t} (1 + \cos 2\theta) d\theta$$

$$= - \frac{1}{2\omega k} \cdot \frac{1}{2} \cdot \left( kh + \frac{\sinh(2kh)}{2} \right) \cdot \left[ \theta + \frac{\sin 2\theta}{2} \right]_{kx - \omega t}^{kx - \omega t - 2\pi}$$

$$= - \frac{1}{4\omega k} \cdot \left( kh + \frac{\sinh(2kh)}{2} \right) (kx - \omega t - 2\pi + \frac{\sin 2(kx - \omega t - 2\pi)}{2} - kh - \omega t - \frac{\sin 2(kx - \omega t)}{2})$$

$$= \frac{1}{4\omega k} \cdot \left( kh + \frac{\sinh(2kh)}{2} \right) \cdot (2\pi)$$

$$\text{thus, } E = \frac{8\bar{g}^2 k}{4\omega^2} \cdot \frac{1}{\cosh^2(kh)} \cdot \frac{1}{4\omega k} \cdot \left( kh + \frac{\sinh(2kh)}{2} \right)$$

$$\geq \frac{8\bar{g}^2 k^2}{4\omega^2 \cosh^2(kh)} \cdot kh \left( 1 + \frac{\sinh(2kh)}{2kh} \right)$$

$$= \frac{8\bar{g}^2 k^2 \omega}{4\omega^2 \cosh^2(kh)} \cdot kh \cdot \frac{\sinh(2kh)}{2kh} \left( 1 + \frac{2kh}{\sinh(2kh)} \right)$$

$$\begin{aligned}
 &= \frac{g \tilde{a}^2 \tilde{\omega}}{1 - \omega^2 \tanh^2(kh)} \cdot \sinh(2kh) \cdot \frac{1}{2} \left( 1 + \frac{2kh}{\sinh(2kh)} \right) \\
 &= \frac{g \tilde{a}^2 \tilde{\omega} \cdot n \sinh(kh) \cosh(kh)}{4 \cdot g \cdot k \cdot t \tanh(kh) \cdot \cosh^2(kh)} \cdot \frac{1}{2} \left( 1 + \frac{2kh}{\sinh(2kh)} \right) \\
 &= \left( \frac{\tilde{\omega}}{n} \right) \cdot \left( \frac{g \tilde{a}^2}{2} \right) \cdot \frac{1}{2} \frac{\sinh(kh) \cosh(kh)}{\sinh(kh) \cosh(kh)} \cdot \frac{1}{2} \left( 1 + \frac{2kh}{\sinh(2kh)} \right) \\
 &= c \cdot \left( \frac{g \tilde{a}^2}{2} \right) \cdot \frac{1}{2} \left( 1 + \frac{2kh}{\sinh(2kh)} \right) \\
 &= \textcircled{a}. E. c_g,
 \end{aligned}$$

where,  $c_g = \frac{1}{2} \left( 1 + \frac{2kh}{\sinh(2kh)} \right) \cdot L = n \cdot c$ .

$c_g$  is known as the group velocity. This is the velocity at which energy travels through the free surface due to wave propagation.

in shallow water,  $n$  asymptotes to 1,  
 since,  $\frac{1}{2} \left( 1 + \frac{2kh}{\sinh(2kh)} \right) \approx \frac{1}{2} \left( 1 + \frac{2kh}{1 + 2kh - \frac{1+2kh}{2}} \right)$

$$= 1, \quad \text{if } kh \ll 1 \text{ or } h < \infty.$$

On the other hand,  $n$  in deep water  $n$  asymptotes toward  $\frac{1}{2}$ , since,  $\frac{1}{2} \left( 1 + \frac{2kh}{\sinh(2kh)} \right)$ .

$$\textcircled{a} = \frac{1}{2} \left( 1 + \frac{2kh}{\frac{1 - e^{-4kh}}{2}, e^{2kh}} \right)$$

$$\approx \frac{1}{2} \quad \text{if } h \gg \infty \text{ in deep water.}$$

thus the wave ~~as~~ energy travels much slower in deep water than in shallow water.

$$\frac{1}{\omega} \frac{d\omega}{dk} = C_g a$$

why this velocity is called as group velocity?

because, we have,  $\omega = \omega(k)$  for water wave and for wave dispersion this is accounted to,  
 $\omega = gk + \alpha k^2 \tanh(kh)$ . —①

from ① it can be shown that,  $\frac{d\omega}{dk} = c_g$ .

and now, if we have two wave systems with frequency and <sup>wave number</sup> being very close to  $\omega$  and  $k$  as,  $\omega_1 = \omega - \frac{d\omega}{2}$  and,  $\omega_2 = \omega + \frac{d\omega}{2}$ , then we can define the two wave systems as,  
 $\eta_1 = A \cos(\omega_1 x - \omega_1 t)$  and,  
 $\eta_2 = A \cos(\omega_2 x - \omega_2 t)$ .

The superposition of  $\eta_1$  and  $\eta_2$  will lead to modulated wave profile over space. ~~with~~ The envelope of this modulated wave profile travels at the speed of  $c_g$  and carried the energy of the main wave of frequency  $\omega$  and wave number  $k$  or wave length  $\lambda$ .