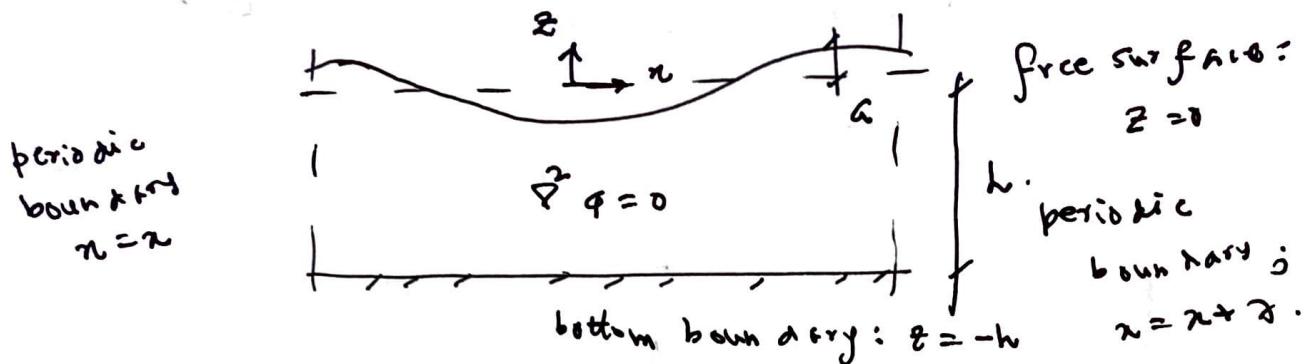


Linear theory of 2D progressive wave & cont wave dispersion



For inviscid, irrotational flow, velocity potential exists, $\phi = \phi(x, z, t)$. For incompressible flow, it satisfies, $\nabla^2 \phi = 0$ —①

- The velocity potential must conform to wave elevation of the form $\eta = \eta(x, z) = a \cos(kx - \omega t)$ at boundary conditions,

- ① periodic boundary conditions.
- ② bottom boundary condition, $z = -h$.
- ③ free surface boundary condition, $z = 0$.
- ④ Periodic boundary conditions.

$$\eta = a \cos(kx - \omega t) \quad \text{②}$$

$$\eta = \eta(x, t) \equiv \eta(x + \lambda, t)$$

$$\text{or, } a \cos(kx - \omega t) = a \cos(k(x + \lambda) - \omega t)$$

$$\text{or, } a \cos(kx \cos \omega t + \sin kx \sin \omega t)$$

$$= a (\cos kx \cos \omega t - \sin kx \sin \omega t)$$

$$= a (\cos(kx + \omega t)) \cdot \cos \omega t + \sin(kx + \omega t) \cdot \sin \omega t$$

$$\text{or, } \cos \omega t = \cos(kx + \omega t) \quad \text{③}$$

$$\sin \omega t = \sin(kx + \omega t). \quad \text{④}$$

for both ④ and ⑤ to be valid,

$$k\lambda = 2\pi \text{ or } \lambda = \frac{2\pi}{k}$$

$$k \rightarrow \infty$$

$$k = \frac{2\pi}{\lambda}$$

periodic boundary condition for time,

$$\eta(x, t) = \eta(x, t + T)$$

$$\alpha G_0(kx - \omega t) = \alpha G_0(kx - \omega(t + T))$$

$$\alpha G_0(kx \cos \omega t + e^{-i kx} \sin \omega t) = \alpha G_0(kx \cos(\omega t + \omega T) + e^{-i kx} \sin(\omega t + \omega T))$$

$$\text{or, } G_0(\omega t) = G_0(\omega t + \omega T) \quad \text{--- (4)}$$

$$\text{Or, } \sin(\omega t) = \sin(\omega t + \omega T) \quad \text{--- (5)}$$

both ④ and ⑤ to be valid, we must have

$$\omega T = 2\pi \text{ or } \omega T = \frac{2\pi}{T}$$

$$T = \frac{2\pi}{\omega}$$

Thus, the periodic boundary conditions do not give us anything related to the solution, rather than confirming that the 2D NURC iteration is periodic in both space and time with wave numbers and NURC period (T) respectively.

Solution of the velocity potential from the Laplace equation

using separation of variables, we can get,

$$\phi = \phi(x, z, t) = R e^{[i k x + i \omega t]}$$

$$\therefore \frac{\partial \phi}{\partial x} = R e^{[-i k x + i \omega t]} \cdot e^{-i k x + i \omega t}$$

$$\therefore \frac{\partial^2 \phi}{\partial x^2} = R e^{[-i k x + i \omega t]} \cdot e^{-i k x + i \omega t}$$

$$\frac{\partial \sigma}{\partial z} = \text{Re} \left[\frac{\kappa^2}{\alpha z} \cdot e^{-ikx + i\omega t} \right]$$

$$\frac{\partial^2 \sigma}{\partial z^2} = \text{Re} \left[\frac{\kappa^2}{\alpha z^2} \cdot e^{-ikx + i\omega t} \right]$$

Now, from Laplace equation ① we get,

$$\frac{\partial^2 \sigma}{\partial z^2} - \kappa^2 \sigma = \text{Re} \left[\frac{\kappa^2}{\alpha z^2} \cdot e^{-ikx + i\omega t} \right] \quad ⑥$$

But this is general solution is of the form

$$Z = C_1 e^{kz} + C_2 e^{-kz} \quad ⑦$$

3. The bottom boundary condition

$$\text{At } z=0, \frac{\partial \sigma}{\partial z} = 0 \quad ⑧$$

$$\text{From term } \left. \frac{\partial \sigma}{\partial z} \right|_{z=-h} = 0 \quad ⑨$$

$$\text{or, } \text{Re} \left[\frac{\kappa^2}{\alpha z} \cdot e^{-ikz + i\omega t} \right] \Big|_{z=-h} = 0$$

$$\text{or, } \left. \frac{\kappa^2}{\alpha z} \right|_{z=-h} = 0 \quad ⑩$$

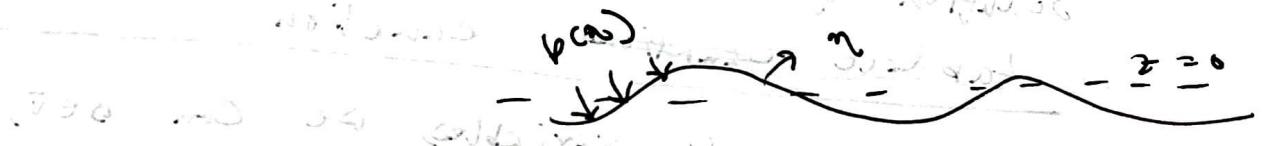
and this is true only if $\kappa^2 = 0$ or $\kappa = 0$. This is not possible.

So, the free surface boundary condition

4. Dyn amic free surface boundary condition

$$\text{at } z=0, \sigma(z) = 0$$

For water and air interface



$$\sigma(z) = \text{Re} [\sigma(z)] + z \frac{d}{dz} (\sigma(z)) \Big|_{z=0}$$

So,

for a Bernoulli's eqn. for

inviscid irrotational flow, valid throughout the fluid, we get,

$$\frac{\partial \alpha}{\partial t} + \frac{1}{2} (u^2 + w^2) + \frac{1}{g} + g z = 0$$

$$\text{or, } b = -g \left[\frac{\partial \alpha}{\partial t} + \frac{1}{2} (u^2 + w^2) + g z \right]$$

$$= -g \left[\frac{\partial \alpha}{\partial t} + \frac{1}{2} \left[\left(\frac{\partial u}{\partial x} \right)^2 + \left(\frac{\partial w}{\partial x} \right)^2 \right] + g z \right]$$

$$= -g \left[\frac{\partial \alpha}{\partial t} + \frac{1}{2} \left[\left(\frac{\partial u}{\partial x} \right)^2 + \left(\frac{\partial w}{\partial x} \right)^2 \right] + g z \right]$$

By linearization, $\frac{\partial \alpha}{\partial t} = 0$

$$0 = -g \left[\frac{\partial \alpha}{\partial t} + g z \right] - g \cdot g \cdot g$$

$$\text{or, } g \cdot g = 0 = -\frac{\partial \alpha}{\partial t} (z + g) \quad \text{--- (10)}$$

$$\text{or, } \eta = -\frac{1}{g} \cdot \frac{\partial \alpha}{\partial t} \quad \text{--- (10)}$$

3. Kinematic free surface boundary condition

A point on the free surface remains on the free surface.

$$\frac{\partial}{\partial t} \eta = \frac{\partial}{\partial t} (u + j w) \frac{\partial \eta}{\partial x} + \frac{\partial}{\partial x} (u \frac{\partial \eta}{\partial x})$$

Now, $\frac{\partial \eta}{\partial x} = n(x, t)$ for 2D waves,

$u \cdot \frac{\partial \eta}{\partial x}$ neglected through linearization.

$$\text{thus, } \eta = \frac{\partial \eta}{\partial x} = \frac{\partial \eta}{\partial t} = \frac{\partial \eta}{\partial t}$$

$$\text{or, } \frac{\partial \eta}{\partial x} = \frac{\partial \eta}{\partial t} \quad \text{--- (11)}$$

Combining (10) and (11), we get

$$\frac{\partial \alpha}{\partial t} + g \frac{\partial \eta}{\partial t} = 0 \quad \text{--- (12)}$$

Equation (12) in brief is known as combined free surface boundary condition or CFSBC.

$\text{Fin. King} = \text{const} + \text{const}$

Applying (15) to (12), we get,

$$C \cdot e^{-kh} - D \cdot e^{kh} = 0 \quad \text{--- (13)}$$

Applying (13) into (10), we get,

$$C + D = \frac{i \omega g}{\omega} \quad \text{--- (14)}$$

by solving, we get,

$$C \cdot (e^{kh} + e^{-kh}) = \frac{i \omega g}{\omega} \cdot e^{kh} \quad \text{--- (15)}$$

$$D \cdot (e^{kh} + e^{-kh}) = \frac{i \omega g}{\omega} \cdot e^{-kh}$$

$$\text{thus, } \varphi(z) = \frac{i \omega g}{\omega} \cdot \frac{\operatorname{Gsh}(kh(z+h))}{\operatorname{Gsh}(kh)}$$

and also $\alpha = \omega c$ [from (12): $e^{inx+i\omega t}$]

$$= \frac{\alpha g}{\omega} \cdot \frac{\operatorname{Gsh}(kh(z+h))}{\operatorname{Gsh}(kh)} \cdot \sin(kh - \omega t) \quad \text{--- (15)}$$

Thus we get (wave) dispersion for finite depth

Applying (15) to (12) we get,

$$\omega^2 = gk \operatorname{tanh}(kh) \quad \text{--- (16)}$$

wave potential for infinite depth

$$\varphi(z) = C \cdot e^{-kh} \cdot C \cdot e^{kh} \cdot C \cdot e^{kz} \quad \text{--- (16)}$$

$D = 0$, since e^{-kh} more as z goes to $-\infty$

z decreases. Thus we have at $z = -\infty$

$$= C \cdot e^{kz} = 0.$$

$$\frac{1}{\omega} \quad H_b \quad C_g a \cdot \frac{b a}{\omega} \quad F$$

applying ⑩ into ⑫, we get,

$$C = \frac{i g a}{\omega}$$

$$\text{thus, } \varphi(x, z, t) = \frac{ab}{\omega} e^{kz} \sin(kx - \omega t) \quad \text{--- ⑬}$$

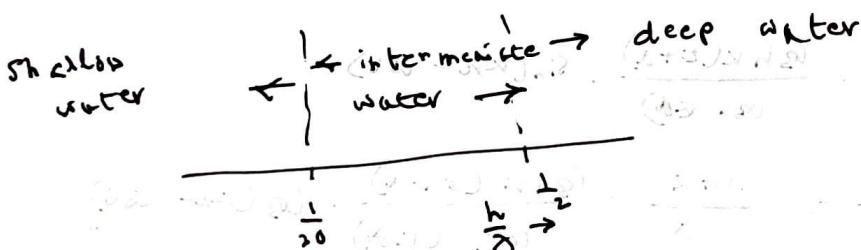
applying, applying ⑬ into ⑫, we get,

$$-\frac{k^2 a^2}{\omega} e^{2kz} \sin(kx/\omega t) + g \cdot \frac{a^2}{\omega} k \cdot e^{kz} \sin(kx - \omega t) = 0.$$

$$\omega = \frac{gk}{w} \quad \text{or, } \omega = gk \quad \text{--- ⑭}$$

Equation ⑭ is the wave dispersion relationship in infinite depth case. By using proper approximations for infinite depth for hyperbolic functions, it can also be shown that equation ⑬ reduced to equation ⑭.

Approximating linear wave dispersion for deep water and shallow water conditions.



$$\omega^2 = gk \cdot \tanh(kh)$$

$$= gk \cdot \frac{e^{kh} - e^{-kh}}{e^{kh} + e^{-kh}}$$

for deep water h is very large, or,
 $\frac{h}{\lambda} \gg 1$, thus $kh \gg 1$, since

$$kh = \frac{2\pi h}{\lambda}$$

$$\therefore \text{Thus, } \omega^2 = gk \cdot \frac{1 - e^{-2kh}}{1 + e^{-2kh}}$$

$$= gk \cdot \frac{1 - \frac{1}{e^{2kh}}}{1 + \frac{1}{e^{2kh}}} \approx gk. (1)$$

∴ $\omega^2 = gK^2 h$ — (1) and (2) gives
 Thus we can believe more simpler form for
 deep water condition by applying suitable
 transformation to $\tanh(Kh)$. (Q.E.D.)

~~On the other hand, for shallow~~
~~waters~~ $b \ll h$ ~~then~~, $\tanh(b/h) \approx 1 - b/h$.

Thus, $\omega^2 = gK \cdot \frac{1 - \frac{kh}{e^{kh}}}{e^{kh} + \frac{kh}{e^{kh}}}$

After simplification we get $\omega^2 = gK \cdot \frac{1 + kh - 1 + kh}{1 + kh + 1 - kh}$ which is
 comparison with $\omega^2 = gK \cdot (Kh) = 9.81 K^2 h$
 ∴ again, $\omega^2 = gK \cdot \frac{x^2}{T^2} = gK \cdot h$ or $\omega = \sqrt{gh}$

$\therefore \omega = 2\pi f = T \cdot \sqrt{gh}$. — (2)

velocity field under 2D progressive waves

$$\phi = \frac{\omega}{g} \cdot \frac{(gh \kappa(z+\alpha))}{(gh \kappa \alpha)} \cdot \sin(kx - \omega t)$$

$$u = \frac{\partial \phi}{\partial x} = \frac{\omega K}{\alpha} \cdot \frac{gh \kappa (z+\alpha)}{gh \kappa \alpha} \cdot \cos(kx - \omega t)$$

$$w = \frac{\partial \phi}{\partial z} = \frac{\omega K}{\alpha} \cdot \frac{\sinh \kappa (z+\alpha)}{\cosh \kappa \alpha} \cdot \sin(kx - \omega t)$$

→ u and w is in phase difference of $\frac{\pi}{2}$.

∴ Thus, when u is maximum, w is minimum
 and vice-versa.

Pressure field under a progressive wave in 2D

from Bernoulli's equation we get,

$$\left(\frac{\partial \Phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=0} = \left(\frac{\partial \Phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=n} \quad \text{--- (1)}$$

Through the process of linearization, we get,

$$\left(\frac{\partial \Phi}{\partial t} \right) \approx \left(\frac{\partial \Phi}{\partial t} \right)_{z=0}$$

$$\left(\frac{\partial \Phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=n} \approx \left(\frac{\partial \Phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=0} + \eta \cdot \frac{\partial}{\partial z} \left(\frac{\partial \Phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=0}$$

from Dynamic free surface boundary condition

$$p(z=n) = 0$$

From dynamic free surface boundary condition, we get,

$$p(z=n) = 0 \quad \text{and, } \eta = -\frac{1}{g} \cdot \frac{\partial \Phi}{\partial t} \Big|_{z=0}$$

$$\text{and also, } \frac{\partial \Phi}{\partial t} \Big|_{z=n} \approx \frac{\partial \Phi}{\partial t} \Big|_{z=0}, \text{ since } n \text{ is very small.}$$

Thus, from equation (1), we get,

$$\left(\frac{\partial \Phi}{\partial t} + \frac{p}{\rho} + gz \right) \Big|_{z=n} = \left(\frac{\partial \Phi}{\partial t} \right)_{z=0} - g \cdot \frac{1}{g} \cdot \frac{\partial \Phi}{\partial t} \Big|_{z=0}$$

$$\text{with } \therefore \partial \Phi / \partial t = 0$$

$$\text{or, } \frac{p}{\rho} = -gz - \frac{\partial \Phi}{\partial t}$$

$$\text{or, } \frac{p}{\rho} = -gz + \underbrace{g \alpha g \cdot K_p(z)}_{\text{Dynamic part}} \cdot A_3 (K_n - w_t)$$

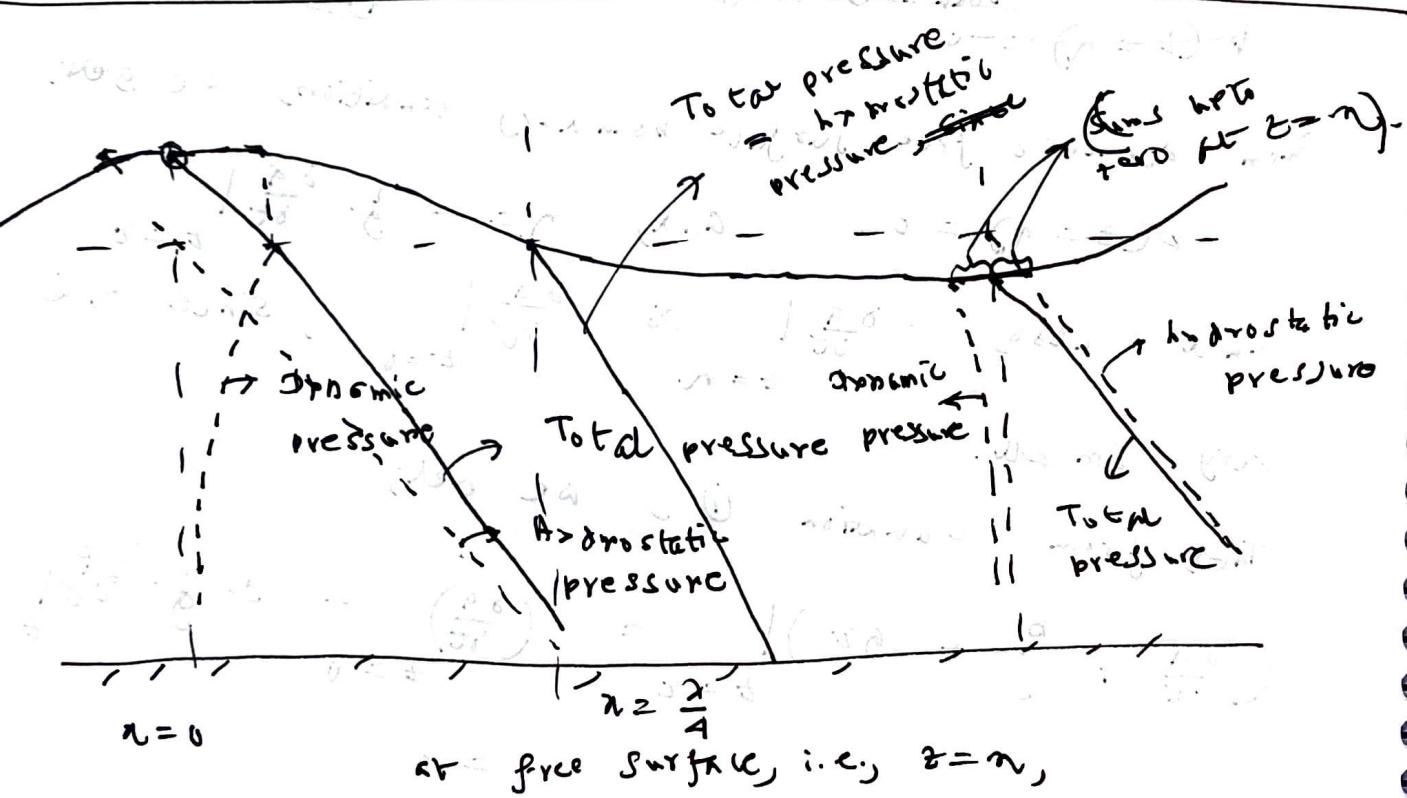
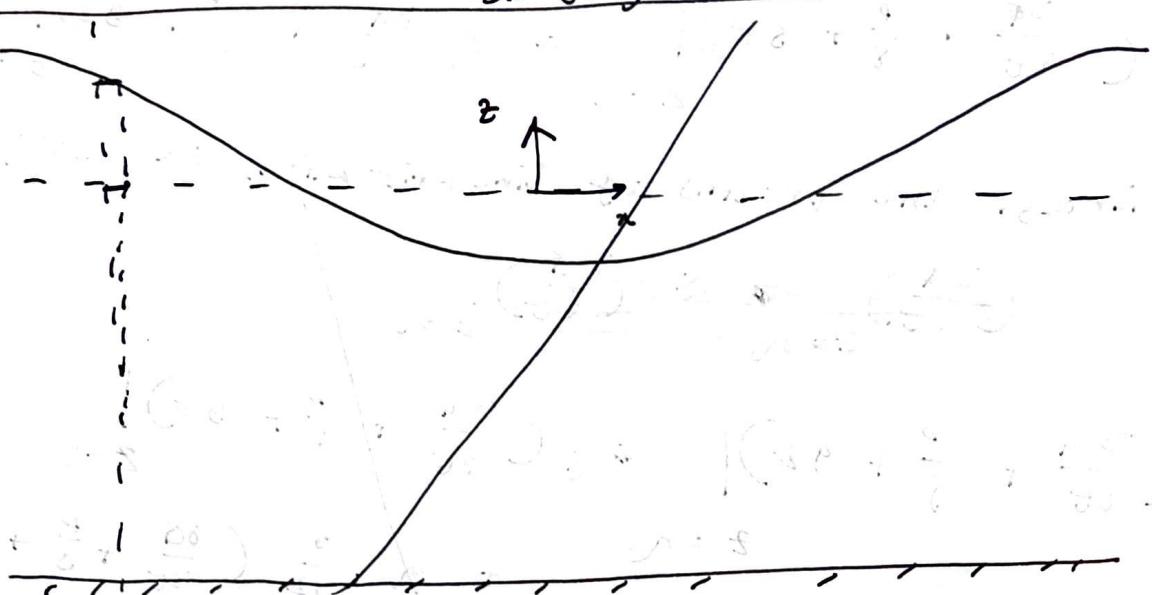
hydrostatic (using full solution of part)

part $\Phi(x, z, t)$ defined earlier

where, $K_p(z)$ is pressure response factor.

For define as,

$$k_p(z) = \frac{BhK(h+z)}{Bh(Kh)}$$



$$\underline{k_p(z=n) = -300}$$

$$\underline{k_p(z=n) = -300 + g \cdot \frac{\partial \sigma}{\partial z} \Big|_{z=0}} = 0$$

$$\underline{k_p(z=n) = -300 - 300 - g \cdot \frac{\partial \sigma}{\partial z} \Big|_{z=0}} = 0$$

- At $z = n$, the hydrostatic part is ~~cancelle~~ by the dynamic part and thus we have $b(z=n) = 0$.

Under the notes, i.e., at $z = \frac{\lambda}{4}$ the total pressure is purely hydrostatic since,

~~$$G_3(kx - \omega t) \Big|_{z=\frac{\lambda}{4}} = G_3\left(\frac{\pi}{2} - \omega t\right)$$~~

~~$$\text{and this state is normal if } G_3 \text{ is zero.}$$~~

$$\text{and } G_3 \text{ is zero if } \sin \omega t + \cancel{G_3 \sin \frac{\pi}{2}} = G_3 \omega t \cdot \sin \frac{\pi}{2}$$

$$= 0 \text{ (cosine)}.$$

Under the notes, i.e., at $z = \frac{3\lambda}{4}$ the total pressure is purely hydrostatic since,

~~$$(G_3(kx - \omega t)) \Big|_{z=\frac{3\lambda}{4}}$$~~

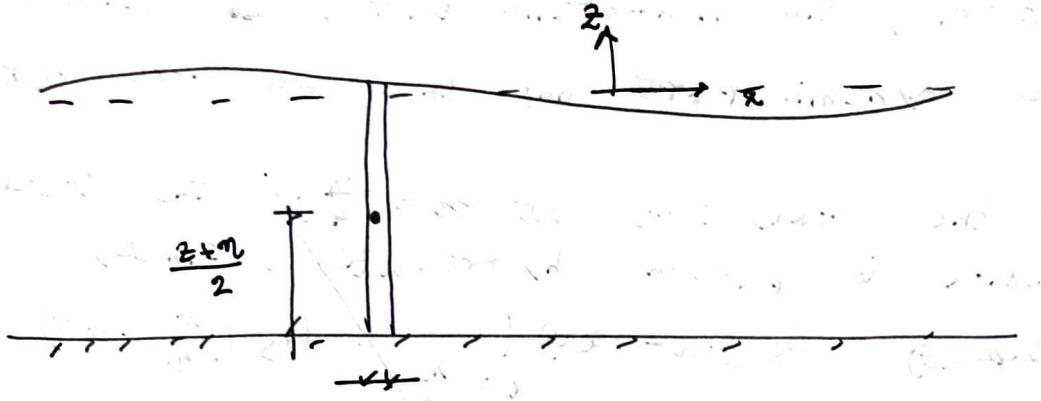
~~$$z = \frac{3\lambda}{4}, \omega t = 0$$~~

thus for the dynamic pressure is zero and the depth.

Wave Energy is defined as

for a progressive periodic wave, there is a movement of the free surface. Thus there is a potential energy. On the other hand, as the wave propagates, there is a movement of a fluid element due to the existence of a velocity field. Thus there is a ~~potent~~ kinetic energy.

Estimation of wave energy is required for ~~assessing~~ assessing power required to drive a wave maker in a flume for dry experiments and for estimating ~~as~~ availability of wave power while planning a device for ~~transforming~~ transforming wave energy into other forms of energy.



for ~~const~~ a water column of ~~width~~ width Δx and thickness along x axis Δz , the potential energy is

$$\begin{aligned} d(P_E) &= \text{Density} \cdot g \cdot \frac{z+n}{2} \Delta z \quad \text{(from mean level)} \\ &\approx dm = g \cdot (z+n) \cdot \Delta z \quad \text{(from mean level)} \\ \therefore d(P_E) &= g g \frac{(z+n)^2}{2} \Delta z \\ &= \frac{1}{2} g g (z^2 + 2zn + n^2) \Delta z \end{aligned}$$

The average potential energy over a wave length

$$\begin{aligned} (\overline{P_E})_a &= \frac{1}{\lambda} \int_{-\lambda/2}^{\lambda/2} \left(\frac{1}{2} g g (z^2 + 2zn + n^2) \right) dx \\ &= \left(\frac{1}{2} \right) \cdot \left(\frac{g g}{2} \right) \cdot \int_{-\lambda/2}^{\lambda/2} (k^2 + 2ka \cos(kx - \omega t) + a^2) dx \\ &\quad + a^2 g g^2 (kx - \omega t) dx \end{aligned}$$

Since $\int_{-\lambda/2}^{\lambda/2} k^2 dx = 0$ because area of sinusoidal function is zero in a symmetric interval. Also $\int_{-\lambda/2}^{\lambda/2} \cos(kx - \omega t) dx = 0$ as it is zero over one complete cycle. So

$$\int_{-\lambda/2}^{\lambda/2} 2ka \cos(kx - \omega t) dx = 0$$

$$\int_{-\lambda/2}^{\lambda/2} a^2 g g^2 (kx - \omega t) dx = \frac{a^2 g g^2}{2} \lambda$$

$$\therefore \frac{g g a^2}{\lambda} \cdot \frac{\partial x}{K} = \frac{g g}{2\lambda}, \frac{\partial^2 x}{\partial z^2} = \frac{g g a^2}{4}$$

Similarly, • kinetic energy of a small fluid element of size $\Delta x \Delta z$ at a depth z and at a distance x is

$$\Delta KE = \text{mass} \cdot \frac{u^2 + v^2}{2} \cdot \Delta x \Delta z = g \frac{u^2 + v^2}{2} \cdot \Delta x \Delta z$$

per unit thickness across
y axis.

Thus average kinetic energy is

$$(\bar{KE}) = \frac{1}{\lambda} \int_{x=0}^{x=\lambda} \int_{z=-h}^{z=0} g \frac{u^2 + v^2}{2} \cdot \Delta x \Delta z$$

Now substitution for u and v given,

$$(\bar{KE}) = \frac{1}{\lambda} \int_{x=0}^{x=\lambda} \int_{z=-h}^{z=0} g \left(\frac{1}{2} \right) \left(\frac{g^2 a^2 K^2}{\omega^2} \cdot \frac{\cosh^2 K(z+h)}{\cosh^2(Kh)} \right)$$

$$= \frac{g^2 a^2 K^2}{\omega^2} \cdot \frac{\cosh^2 K(z+h)}{\cosh^2(Kh)}$$

$$+ \frac{g^2 a^2 K^2}{\omega^2} \cdot \frac{\sinh^2 K(z+h)}{\cosh^2(Kh)}$$

$$= \frac{1}{\lambda} \int_{x=0}^{x=\lambda} \int_{z=-h}^{z=0} \frac{g^2 a^2 K^2}{\cosh^2(Kh)} \cdot \frac{1}{\cosh^2(Kh)} \cdot \left[\cosh^2 K(h+z) \cdot \sin^2(Kx - \omega t) + \sinh^2 K(h+z) \cdot \sinh^2(Kx - \omega t) \right] \Delta x \Delta z$$

$$= \frac{g g a^2}{4}$$

Thus, the total wave energy per wave length and per unit thickness across y axis is

$$E = \frac{g g a^2}{A} + \frac{g g a^2}{4} = \frac{g g a^2}{2}, = \frac{g g H^2}{8}$$

This ~~is also~~ may also be defined as wave energy per unit surface area (i.e., ~~per~~ ~~A~~)

where b may be any measure of separation
is between identical wave trains.

monats-Sonntagsmahl am 13. Februar 1933

and it is at the top of the body along the direction of

\rightarrow propagation

b k

A hand-drawn diagram showing a cross-section of a river bend. The river flows from the bottom right towards the top left. The left bank is labeled '6' and the right bank is labeled '1'. The water surface is represented by a wavy line. A vertical dashed line extends from the river bed at the bottom to the water surface at the top.

~~Weg zur Sibirienfahrt~~

~~shab in 2 w 0.2 m 6.700 L = (5)~~

$$1 - \left[M^{-2} \right] = \left[M^{-2} \right]$$

$$[E] = 2 \cdot \frac{1}{2} S g a^2 = [M L^{-3}] \cdot [L T^{-2}] \cdot [L^2] = [M T^{-2}]$$

$[ET]$ we know is $[MLT^{-2}] \cdot [L] = [L^2 T^{-2}]$

$$[G][L^{-2}] = [M^2 T^{-2}][L^{-2}] = M T^{-2}$$