# EEE-2103: Electronic Devices and Circuits

Dept. of Computer Science and Engineering University of Dhaka

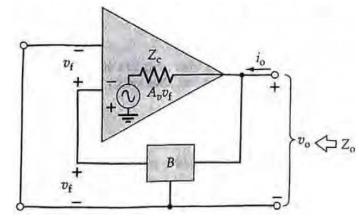
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## **Series Voltage Negative Feedback**

#### Output impedance:

Output voltage  $v_o$  produces feedback voltage  $v_f$   $v_f$  generates voltage  $A_v v_f$  in series with  $Z_c$   $Z_c$  = output impedance without feedback

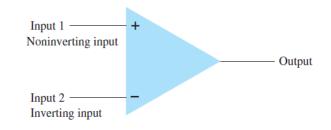
$$V_o = i_o Z_c - A_v V_f$$
  
 $i_o Z_c = V_o + A_v V_f = V_o + A_v B V_o = V_o (1 + A_v B)$   
 $Z_o = V_o / i_o = \frac{Z_c}{1 + A_v B}$ 



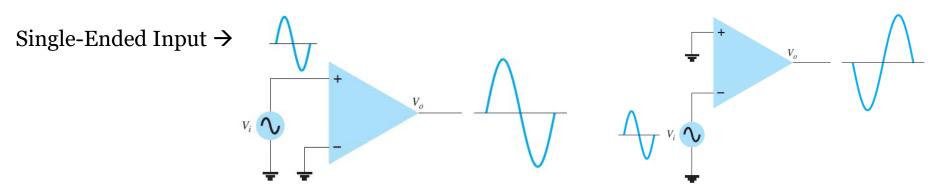
## **Operational Amplifiers (Op-Amps)**

Op-amp → very high gain differential amplifier, high input impedance, low output impedance.

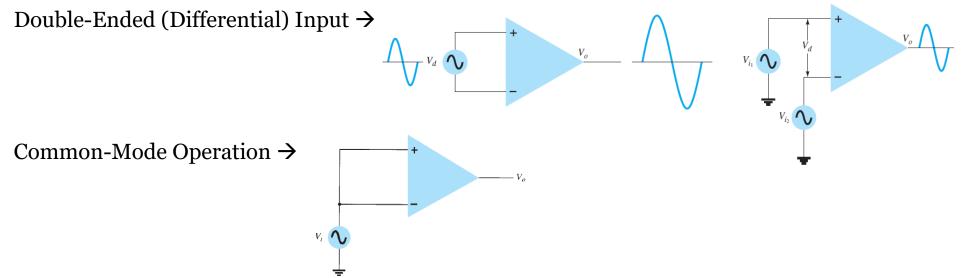
Uses → provide voltage amplitude changes, oscillators, filter circuits, instrumentation circuits.



Signal is applied to  $+ \rightarrow$  same polarity (or phase) output Signal is applied to  $- \rightarrow$  opposite polarity (or phase) output



#### **Operational Amplifiers (Op-Amps)**



#### Common-Mode Rejection $\rightarrow$

difference signal at inputs are highly amplified, common signals at inputs are slightly amplified = rejected. noise is common to both inputs.

differential connection provides → attenuation of unwanted input amplification of difference input.

#### **Voltage Follower Circuits**

Suppose,  $V_o > V_i \rightarrow$ 

 $V_{B2} = V_2 > V_{B1} = V_i$  $I_{C2}$  would be increased

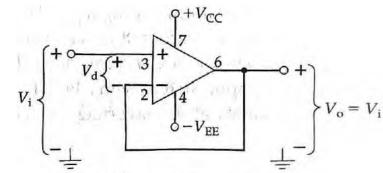
 $V_{RC}$  will be increased

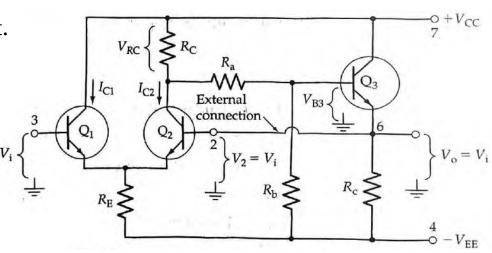
 $V_{B_3}$  will be reduced  $\rightarrow V_o = V_i$ 

Suppose,  $V_o < V_i \rightarrow$ 

 $V_o = V_i$  due to similar -ve feedback effect.

When  $V_i$  at 3 is increased or decreased  $\rightarrow$  $V_o$  follows  $V_i$  perfectly.





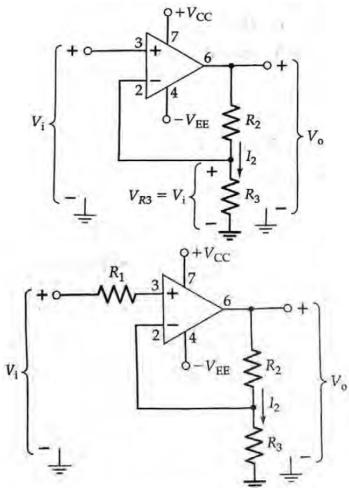
## **Non-Inverting Amplifiers**

Portion of  $V_o$  is fed back to inverting input.  $V_o$  changes as necessary  $\rightarrow V_{R_3} = V_i = I_2 R_3$   $I_2 >> \text{op-amp input bias current}$ 

$$I_2 = \frac{V_o}{R_2 + R_3}$$
 Circuit voltage gain,  $A_{CL} = \frac{V_o}{V_i} = \frac{I_2(R_2 + R_3)}{I_2 R_3} = \frac{R_2 + R_3}{R_3}$ 

 $V_{R_1}$  is produced by input bias current.

$$R_1 = R_2 | | R_3$$



## **Non-Inverting Amplifiers**

#### Problem-45:

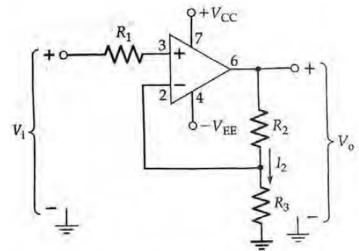
Design a direct-coupled non-inverting amplifier using 741 op-amp. The output voltage is to be 2 V when the input is 50 mV. Also, calculate typical input and output impedances for the amplifier. Assume  $I_{B(max)}$  = 500 nA,  $A_v$  = 200000,  $r_i$  = 2 M $\Omega$ ,  $r_o$  = 75  $\Omega$ .

$$\begin{split} I_{2(min)} &= 100 I_{B(max)} = 100 \times (500 \times 10^{-9}) = 50 \; \text{µA} \\ R_3 &= V_i / I_2 = (50 \times 10^{-3}) / (50 \times 10^{-6}) = 1 \; \text{k}\Omega \\ R_2 &+ R_3 = V_o / I_2 = 2 / (50 \times 10^{-6}) = 40 \; \text{k}\Omega \\ R_2 &= (R_2 + R_3) - R_3 = 40 - 1 = 39 \; \text{k}\Omega \\ R_1 &= R_2 |\, |R_3 = 39|\, |1 \approx 1 \; \text{k}\Omega \end{split}$$

$$B = \frac{R_3}{R_2 + R_3} = \frac{1}{39 + 1} = \frac{1}{40}$$

$$Z_i = (1 + A_v B) r_i = \left[ 1 + 200000 \frac{1}{40} \right] \times 2 \times 10^6 \approx 10000 \text{ M}\Omega$$

$$Z_o = \frac{r_0}{1 + A_v B} = \frac{75}{1 + (200000/40)} \approx 0.015 \Omega$$



# **Inverting Amplifiers**

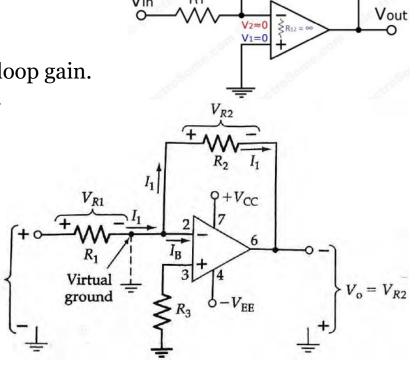
Non-inverting input terminal is grounded via  $R_3$ Inverting input terminal  $\rightarrow$  voltage  $\approx$  ground. virtual ground.

Very small input voltage difference is amplified by open-loop gain. Portion of  $V_o$  is fed back via  $R_2$  and  $R_1$  to correct changes.

Circuit input current,  $I_1 = V_{R1}/R_1 = V_i/R_1$  [ $V_{R1} = V_i$ ]  $I_1 >>$  input bias current  $I_B$   $V_{R2} = I_1R_2$   $V_o = -I_1R_2$ 

Circuit voltage gain,  $A_{CL} = V_o/V_i = -I_1R_2/I_1R_1 = -R_2/R_1$ 

Input impedance,  $Z_i = R_1$ 



## **Inverting Amplifiers**

#### Problem-47:

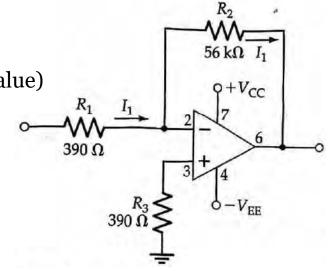
Design a direct-coupled inverting amplifier using a 741 op-amp. The input voltage amplitude is 20 mV and the voltage gain is to be 144. Assume  $I_{B(max)}$  = 500 nA.

$$I_{1(min)} = 100I_{B(max)} = 100 \times (500 \times 10^{-9}) = 50 \,\mu\text{A}$$

$$R_1 = V_i/I_1 = (20 \times 10^{-3})/(50 \times 10^{-6}) = 400 \Omega$$
 (use 390  $\Omega$  standard value)

$$R_2 = A_{CL}R_1 = 144 \times 390 = 56.2 \text{ k}\Omega \text{ (use 56 k}\Omega \text{ standard value)}$$

$$R_3 = R_1 | | R_2 = 390 | | (56 \times 10^3) \approx 390 \Omega$$

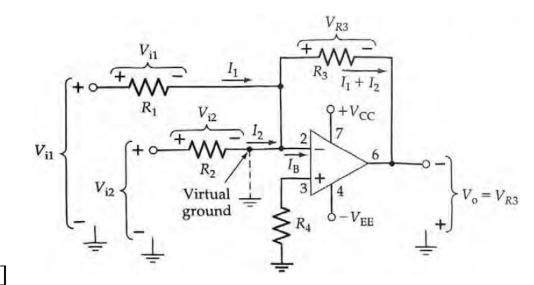


## **Summing Amplifiers**

- 2 inputs applied to  $R_1$  and  $R_2$
- 2 input voltages,  $V_{i1}$  and  $V_{i2}$
- 2 input currents  $\rightarrow$   $I_1 = V_{i1}/R_1$  $I_2 = V_{i2}/R_2$

Output voltage,

$$\begin{split} V_o &= -(I_1 + I_2)R_3 \\ &= -\left[\frac{V_{i1}}{R_1} + \frac{V_{i2}}{R_2}\right]R_3 \\ &= -\frac{R_3}{R_1}[V_{i1} + V_{i2}] \qquad [R_1 = R_2] \\ &= -[V_{i1} + V_{i2}] \qquad [R_1 = R_2 = R_3] \end{split}$$



#### **Summing Amplifiers**

#### Problem-48:

Design a three-input summing amplifier using an op-amp and to have a voltage gain of 3. Calculate the resistor currents and the output voltage when all three inputs are 1 V.

Select 
$$R_4$$
 = 1 M $\Omega$   
Let,  $R_1$  =  $R_2$  =  $R_3$  =  $R_4/A_{CL}$  = 1×10<sup>6</sup>/3 = 333 k $\Omega$  (use 330 k $\Omega$  standard value)

$$\begin{split} I_1 &= I_2 = I_3 = V_i/R_1 = 1/(330\times10^3) = 3.03~\mu\text{A} \\ I_4 &= I_1 + I_2 + I_3 = 3.03 + 3.03 + 3.03 = 9.09~\mu\text{A} \\ V_o &= -I_4 R_4 = -9.09\times10^{-6}\times1\times10^6 = -9.09~\text{V} \end{split}$$

