Inverse Problems for Inertial Sensor Calibration

David L. Olson

$March\ 11,\ 2025$

Contents

1	\mathbf{Intr}	roduction	3
	1.1	IMU Calibration and Compensation	3
		1.1.1 Basic IMU Error Sources and Error Models	4
	1.2	IMU Temperature Compensation	5

Abstract

Inertial sensors are vital to navigation, guidance, and control (NGC) for a variety of vehicles. Inertial sensors such as accelerometers and gyroscopes measure specific and angular velocity respectively which are mechanized to produce a position, velocity, and attitude (PVA) solution [1]. All inertial sensors are subject to deterministic and stochastic error which require careful calibration and characterization before utilizing inertial sensors in a vehicle application. In industry, the current state of the art for inertial sensor calibration has made little advancement over the past couple decades, where calibration data is collected and post-processed using basic statistics to compute basic error model parameters. In the past, improved fidelity for calibration required purchasing higher and higher precision equipment, which eventually succumbs to the law of diminishing returns.

However, ongoing research addressing inertial sensor calibration seeks to break dependence on high-cost high-precision test equipment by introducing advanced estimation techniques and stochastic filtering to maintain high fidelity calibration performance [2, 3, 4, 5, 6]. While various papers only tackle small pieces of an entire calibration procedure, there is an opportunity to cast inertial sensor calibration as an inverse problem to provide a holistic methodology to the field. The forward problem is simply the process of transforming true dynamic inputs acting on the sensor to sensor outputs which is subject to error. Then, the inverse problem takes the form of calibration in which calibration parameters are estimated from collected sensor data. Using inverse problem techniques, calibration parameter estimation can advance beyond basic statistical techniques for higher fidelity performance to include covariance propagation to assign confidence to final calibration parameters. In addition, estimation may be performed in real-time during the collection of calibration data, alleviating logistical and programmatic troubles for an inertial test laboratory.

The author plans to build upon previous work [7] which homogenized multiple IEEE standards for varying accelerometer and gyroscope technologies [8, 9, 10, 11, 12, 13, 14] which provide highly detailed inertial sensor error models. Inertial sensor data will be simulated using [15] which can provide true inertial sensor measurements which can then be corrupted with error and noise. Then, inverse problem techniques may be demonstrated and contrasted with traditional methods to showcase improvements and possible limitations to using these new highly detailed models. Higher fidelity calibration yields increased sensor accuracy, which ultimately enhances inertial navigation capabilities for a wide range of vehicle applications.

Term Project 2 of 6

1 Introduction

A key challenge for self-driving cars is solving the navigation problem which requires determining the position, velocity, and attitude (PVA) of the vehicle. Navigation is an interdisciplinary field of engineering which seeks to fuse measurements of many different sensors such as inertial measurement units (IMUs), global positioning system (GPS) receivers, and a large variety of other sensors to form a PVA solution. It is crucial to not only formulate a navigation solution but also to track the uncertainty of that solution, which can play an important role in decision-making and risk-assessment for autonomous self-driving vehicle applications.

IMUs contain accelerometers and gyroscopes generally in all three Cartesian axes which measure specific force and angular velocity respectively. These measurements are integrated to provide a PVA solution, but an IMU-only solution will drift away from truth unbounded due to the integration of sensor noise and other errors. An inertial navigation system (INS) integrates the IMU measurements and then uses GPS to provide accurate measurements of position to fuse with the IMU solution typically via a Kalman filter thus combating any position error drift. This allows for long-term accurate navigation suitable for a self-driving car traveling across the country.

A driving need for navigation regarding self-driving cars is forming back-up modes of navigation when GPS signals are temporarily unavailable. This is especially important in urban environments where tall buildings and tunnels can cause signal blockages. Lack of GPS signals are problematic for an INS as its performance is dependent on receiving those signals, and the IMU-only solutions will drift away quickly from ground truth. Inertial-only navigation is suitable for short periods such as temporary GPS signal blockages, but the duration of a suitable inertial-only navigation is highly dependent on the quality of sensors contained within an IMU. This dilemma, among any others, motivates the need for rigorous IMU calibration and compensation.

One particular challenge with the use of commercial-grade or automotive-grade micro-electrical mechanical system (MEMS) inertial sensors is their sensitivity to temperature. Characterizing how common error sources such as bias, scale factors, and misalignments shift in response to temperature is a tough problem which requires hours of testing per unit and is often too burdensome for applications using automotive-grade devices.

1.1 IMU Calibration and Compensation

Accelerometers and gyroscopes are subject to a variety of error sources such as biases, scale factor imperfections, axis misalignments, noise, and many others. IMU calibration is the process of characterizing these error sources, while compensation is the process of correcting measurements in real-time to provide the most accurate and precise measurements possible. The better these error sources are characterized, the slower that the IMU-only navigation solution will drift away from truth

Inertial sensor calibration can be treated as an inverse problem. Consider an accelerometer as an example where the ideal forward model is quite straight forward; specific force in equals specific force out. Unfortunately in practice, we are not quite so lucky. Any error in the forward model is defined as

$$\Delta f := \tilde{f} - f$$

where Δf is the measurement error, \tilde{f} is the specific force measured by the sensor which is

Term Project 3 of 6

subject to error, and f is the true specific force acting on the accelerometer. The same applies to gyroscope measurements.

$$\Delta\omega := \tilde{\omega} - \omega$$

Inertial sensor errors Δf and $\Delta \omega$ are subject to both deterministic and stochastic error and any number of contributing factors can make up these terms.

1.1.1 Basic IMU Error Sources and Error Models

Consider an IMU which contains three accelerometers and three gyroscopes arranged to point in a standard Cartesian right-handed coordinate frame. A basic forward model framework appropriate for commercial- and automotive-grade inertial sensors is provided in [1].

$$\tilde{\boldsymbol{f}} = [I + M_a] \, \boldsymbol{f} + \boldsymbol{b}_a + \boldsymbol{w}_a, \quad \boldsymbol{w}_a \sim N \left(0, \, \sigma^2 \right)$$

$$\tilde{\boldsymbol{\omega}} = [I + M_q] \, \boldsymbol{\omega} + \boldsymbol{b}_q + \boldsymbol{w}_q \quad \boldsymbol{w}_q \sim N \left(0, \, \sigma^2 \right)$$
(1)

In these models are bias terms b_a , $b_g \in \mathbb{R}^3$ for the accelerometers and gyroscopes respectively. In addition are the misalignment matrices M_a , $M_g \in \mathbb{R}^{3 \times 3}$, whose diagonal elements are scale factor error terms. The off-diagonal elements are misalignment terms which account for imperfections in the alignment of the sensing axes. All inertial sensors are also subject to noise, which is captured by terms w_a , w_g which are additive zero-mean white Gaussian noise. Equation 2 restates equation 1 in terms of all its various elements.

$$\begin{bmatrix} \tilde{f}_x \\ \tilde{f}_y \\ \tilde{f}_z \end{bmatrix} = \begin{bmatrix} 1 + s_{a,x} & m_{a,xy} & m_{a,xz} \\ m_{a,yx} & 1 + s_{a,y} & m_{a,yz} \\ m_{a,zx} & m_{a,zy} & 1 + s_{a,z} \end{bmatrix} \begin{bmatrix} f_x \\ f_y \\ f_z \end{bmatrix} + \begin{bmatrix} b_{a,x} \\ b_{a,y} \\ b_{a,z} \end{bmatrix} + \begin{bmatrix} w_{a,x} \\ w_{a,y} \\ w_{a,z} \end{bmatrix}$$

$$\begin{bmatrix} \tilde{\omega}_x \\ \tilde{\omega}_y \\ \tilde{\omega}_z \end{bmatrix} = \begin{bmatrix} 1 + s_{g,x} & m_{g,xy} & m_{g,xz} \\ m_{g,yx} & 1 + s_{g,y} & m_{g,yz} \\ m_{g,zx} & m_{g,zy} & 1 + s_{g,z} \end{bmatrix} \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix} + \begin{bmatrix} b_{g,x} \\ b_{g,y} \\ b_{g,z} \end{bmatrix} + \begin{bmatrix} w_{g,x} \\ w_{g,y} \\ w_{g,z} \end{bmatrix}$$

$$(2)$$

The goal of IMU calibration is characterize to these IMU error sources, resulting in estimates $\hat{\boldsymbol{b}}_a$, \hat{M}_a , $\hat{\boldsymbol{b}}_g$, \hat{M}_g which then allows for the correction of inertial sensor measurements in real-time, which is referred to as compensation. In essence, this can be treated as the inverse model with estimated parameters. Using the estimated model parameters, inertial sensor measurements $\tilde{\boldsymbol{f}}$, $\tilde{\boldsymbol{\omega}}$ are compensated to provide new measurements $\hat{\boldsymbol{f}}$, $\hat{\boldsymbol{\omega}}$ per equation 3.

$$\hat{\boldsymbol{f}} = \left[I + \hat{M}_a \right]^{-1} \left(\tilde{\boldsymbol{f}} - \hat{\boldsymbol{b}}_a \right)$$

$$\hat{\boldsymbol{\omega}} = \left[I + \hat{M}_g \right]^{-1} \left(\tilde{\boldsymbol{\omega}} - \hat{\boldsymbol{b}}_g \right)$$
(3)

Term Project 4 of 6

(4)

There are many more error models which are often applied to higher grade devices [7] but these error models are out of scope for this work due to their difficulty to simulate.

1.2 IMU Temperature Compensation

In IMU applications there is a common saying that floats around industry, "MEMS sensors are almost more useful thermometers than inertial sensing themselves!". This rings true in practice, and temperature compensation becomes a key

Term Project 5 of 6

References

[1] P. Groves, Principles of GNSS, Inertial, and Multisensor Integrated Navigation Systems, Second Edition. GNSS/GPS, Artech House, 2013.

- [2] P. G. Savage, "Improved strapdown inertial measurement unit calibration procedures," in 2018 IEEE/ION Position, Location and Navigation Symposium (PLANS), pp. 522–533, 2018.
- [3] H. Rahimi and A. A. Nikkhah, "Improving the calibration process of inertial measurement unit for marine applications," *NAVIGATION: Journal of the Institute of Navigation*, vol. 67, no. 4, pp. 763–774, 2020.
- [4] A. Kozlov and F. Kapralov, "Millimeter-level calibration of imu size effect and its compensation in navigation grade systems," in 2019 DGON Inertial Sensors and Systems (ISS), pp. 1–12, 2019.
- [5] X. Li, W. Huang, X. Zhu, and Z. Zhao, "Mems-imu error modelling and compensation by 3d turntable with temperature chamber," in 2022 International Symposium on Networks, Computers and Communications (ISNCC), pp. 1–5, 2022.
- [6] C.-Y. Hung and S.-C. Lee, "A calibration method for six-accelerometer ins," *International Journal of Control Automation and Systems*, vol. 4, 10 2006.
- [7] D. L. Olson, J. Bingham, and M. R. Walker, "A generalized imu modeling framework for varying inertial sensing technologies and performance grades," 06 2023.
- [8] "Ieee standard specification format guide and test procedure for linear single-axis, nongyroscopic accelerometers," *IEEE Std 1293-2018 (Revision of IEEE Std 1293-1998)*, pp. 1–271, 2019.
- [9] "Ieee standard specification format guide and test procedure for coriolis vibratory gyros," *IEEE Std 1431-2004*, pp. 1–78, 2004.
- [10] "Ieee standard for specifying and testing single-axis interferometric fiber optic gyros," *IEEE Std 952-2020 (Revision of IEEE Std 952-1997)*, pp. 1–93, 2021.
- [11] "Ieee specification format for single-degree-of-freedom spring-restrained rate gyros," ANSI/IEEE Std 292-1969, pp. 1–16, 1968.
- [12] "Ieee standard specification format guide and test procedure for single-degree-of-freedom rate-integrating gyros," *IEEE Std 517-1974*, pp. 1–60, 1974.
- [13] "Ieee standard specification format guide and test procedure for single-axis laser gyros," *IEEE Std 647-2006 (Revision of IEEE Std 647-1995)*, pp. 1–96, 2006.
- [14] "Ieee specification format guide and test procedure for two-degree-of-freedom dynamically tuned gyros," ANSI/IEEE Std 813-1988, pp. 1–68, 1989.
- [15] J. K. Bingham, "Rotational testbed simulator." https://github.com/sandialabs/RTSim, 2024.

Term Project 6 of 6