

## Abstract

- Recent increase in use of fibre reinforced composite materials in **aerospace, automotive** and other industries.
- Composite materials offer attractive properties like **high strength-to-weight ratio, flexibility of shaping, corrosion resistance**.

## Automated Tape Winding

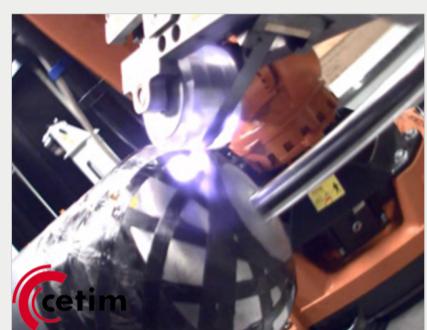


Figure: Tape winding process.

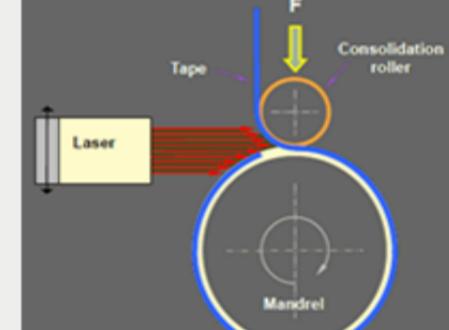


Figure: Winding head schematic.

- Automated Tape Winding (ATW) is a fabrication technique for composite components.
- Workpiece liner is mounted onto a rotating mandrel.
- Heated fibre tows are consolidated over the liner in desired paths using a compaction roller.

## SPIDE-TP Platform

- ATW system installed at **CETIM**.
- KUKA KR210 R3100 ultra robot (Payload: **210kg**, Reach: **3095mm**).
- KUKA KL-2000 linear axes (Range: **4500mm**).
- 2 external AFPT winding axis (Workpiece diameters from **25mm** to **2500mm** and lengths up to **3500mm**).
- AFPT laser-assisted tape winding head (**4kW** power).
- Processes all glass to carbon reinforced fibres.
- Applications: **Energy storage tanks, cryogenic tanks, and others.**

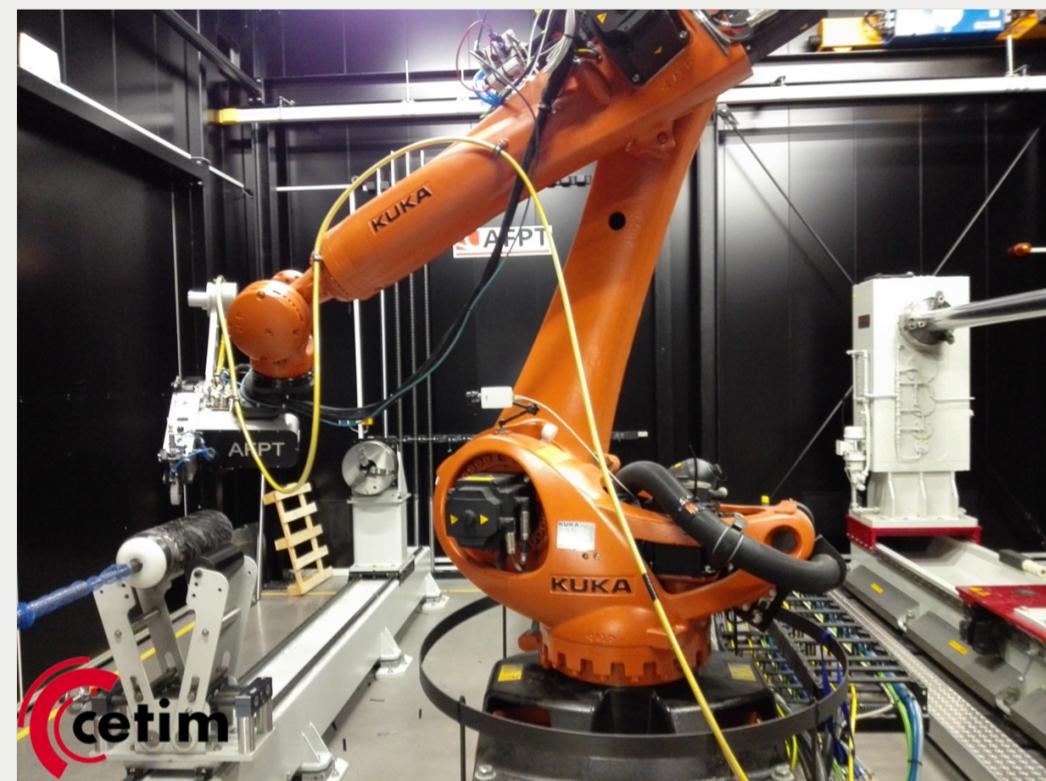


Figure: SPIDE-TP platform.

## Key Challenges

- Trajectories generated from Composicad software.
- Kinematic redundancy** of the system not fully exploited.
- Discontinuities** in the trajectory (near the domes).
- High raw material cost.

## Objective

To **increase the productivity** by optimizing the robot and positioner trajectories with improved management of kinematic redundancy.

## Practical Considerations

- Additional joint limits** due to optical fibre over-bending.
- Adjusting **TCP frame** to accommodate ideal laser incidence angle.
- Modification of shaft geometry** to avoid possible collisions.

## Further Work

- Robot programming with different motion strategies.
- Actual implementation on the SPIDE-TP platform.
- Comparison and analysis with previous methods.
- Working with more complex components & trajectories.

## System & Task Modelling

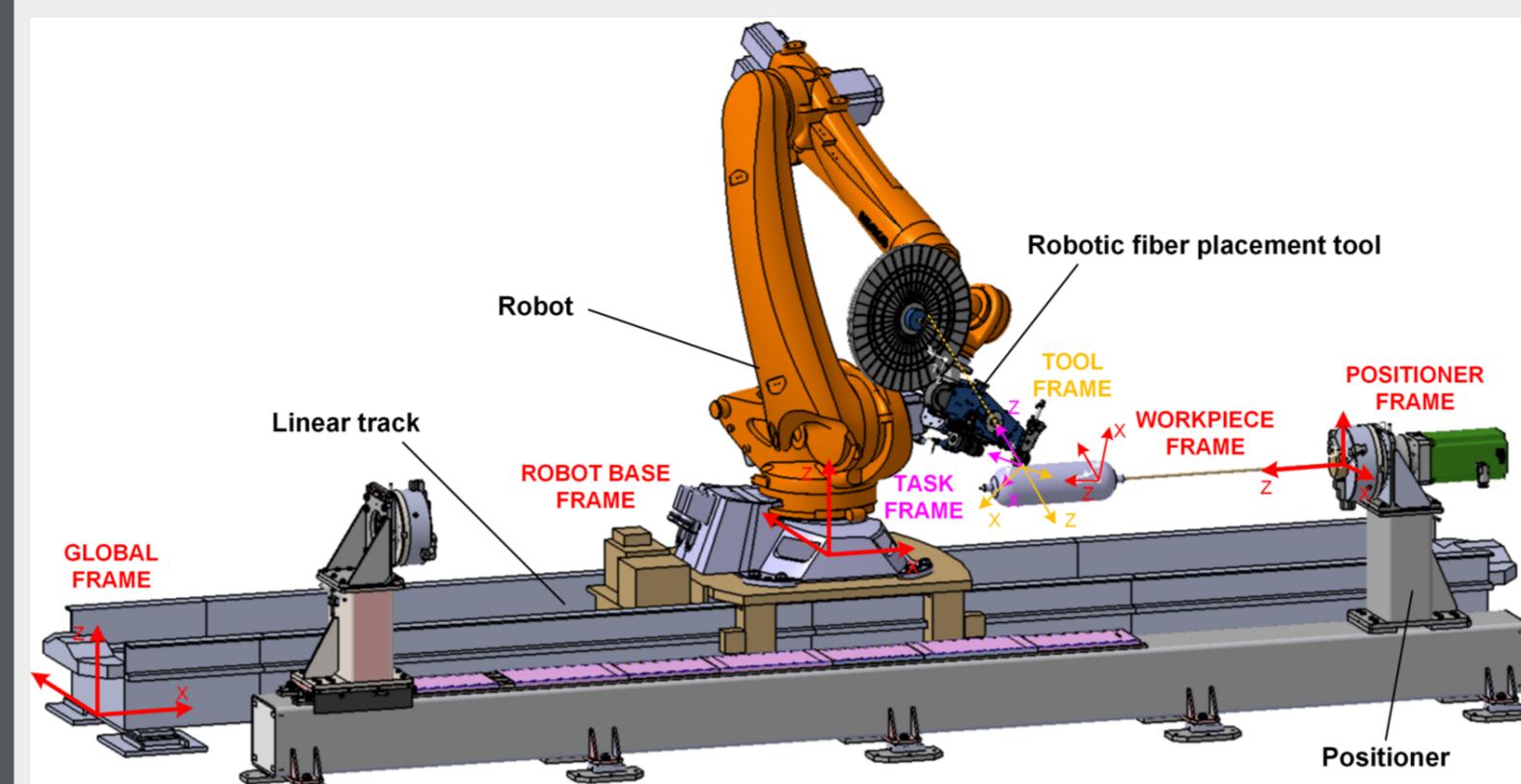


Figure: CAD model of the SPIDE-TP Platform with assigned frames.

**CAD Modelling:** 3D model of the SPIDE-TP Platform created in **CATIA V5** environment with joint-space kinematic simulation.

### Kinematic Modelling:

Robot Model:

$$rob(\vec{q}_r) = {}^{RB} T_1(q_1). {}^1 T_2(q_2). {}^2 T_3(q_3). {}^3 T_4(q_4). {}^4 T_5(q_5). {}^5 T_{RF}(q_6) \quad (1)$$

Positioner Model:

$$pos(q_p) = Rot_z(q_p) \quad (2)$$

Task Model:

$${}^w T_{TL_i} = \begin{bmatrix} \vec{n}_i & \vec{s}_i & \vec{a}_i & \vec{p}_i \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} R(\varphi_i) & \vec{p}_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad |i = 1, 2, \dots, n \quad (3)$$

Closed loop kinematic chain:

$${}^0 T_{RB}.rob(\vec{q}_r).{}^{RF} T_{Tool}.{}^{Tool} T_{TL_i} = {}^0 T_{PB}.pos(q_p).{}^{PF} T_W.{}^W T_{TL_i} \quad (4)$$

## Optimal Trajectory Generation

Positioner coordinate discretization:

$$q_p^k = q_p^{\min} + \Delta q_p \cdot k; \quad k = 0, 1, \dots, (q_p^{\max} - q_p^{\min}) / \Delta q_p \quad (5)$$

Computing solutions for each candidate:

$$q_r^k(t_i) = g_r^{-1}(g_p(q_p^k(t_i)), \mu); \quad k = 0, \dots, m; \quad i = 1, \dots, n \quad (6)$$

Location cell representing different joint configurations:

$$L_c^{(k,i)} = (q_r^{(k)}(t_i), q_p^{(k)}(t_i)) \quad (7)$$

Inter-nodal distance corresponds to the travelling time:

$$dist(L_c^{(k,i)}, L_c^{(k+1,i+1)}) = \max_{j=0,\dots,6} \left( \frac{|q_{j,i}^{(k)} - q_{j,i+1}^{(k+1)}|}{\dot{q}_j^{\max}} \right) \quad (8)$$

## 1. Task Graph Generation

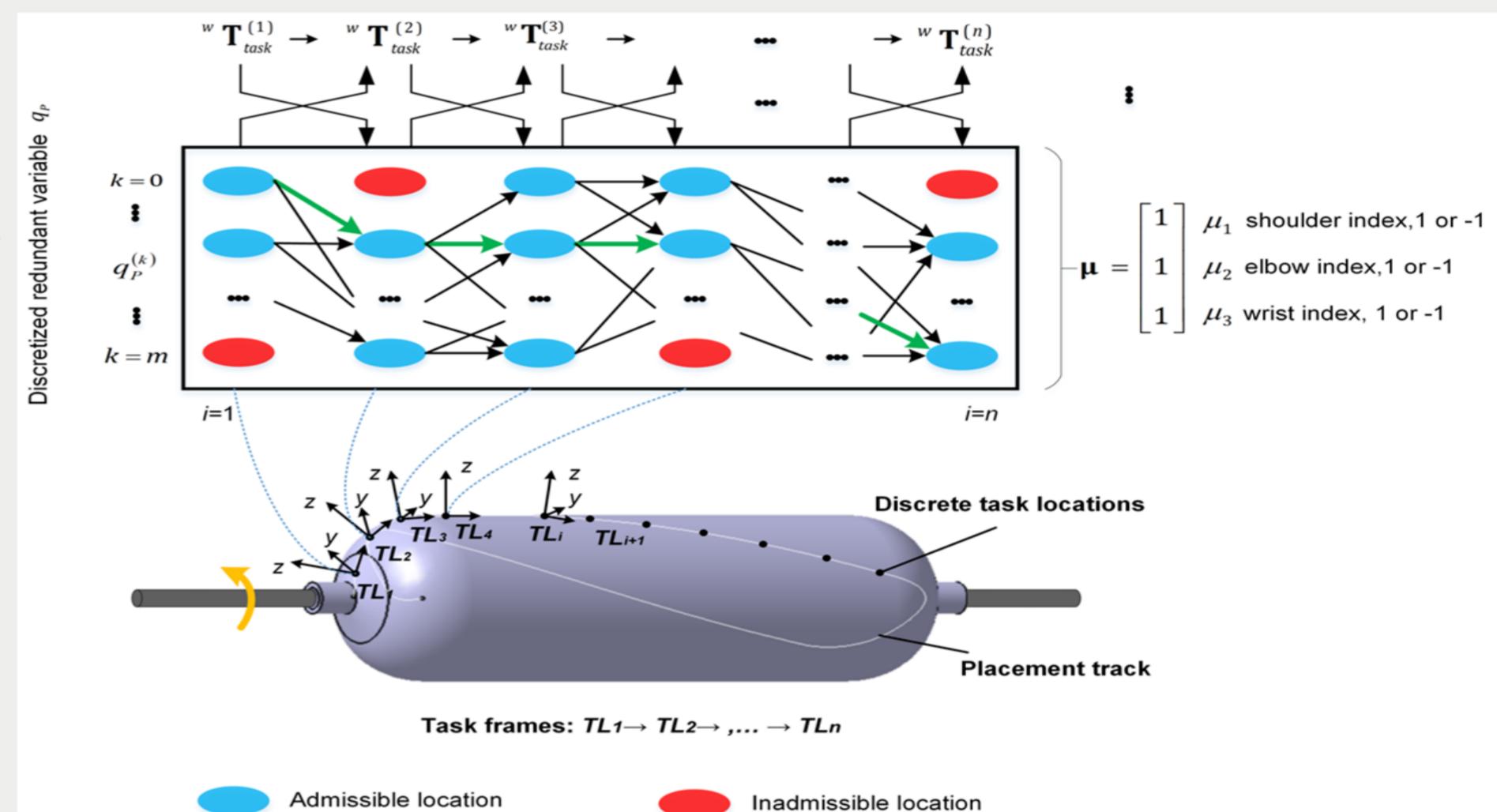


Figure: Graph based representation of discrete search space.

## 2. Collision Detection

Running the task graph on the CAD model. Checks for defined interferences between workcell components, highlights the detected collisions and returns inadmissible locations.

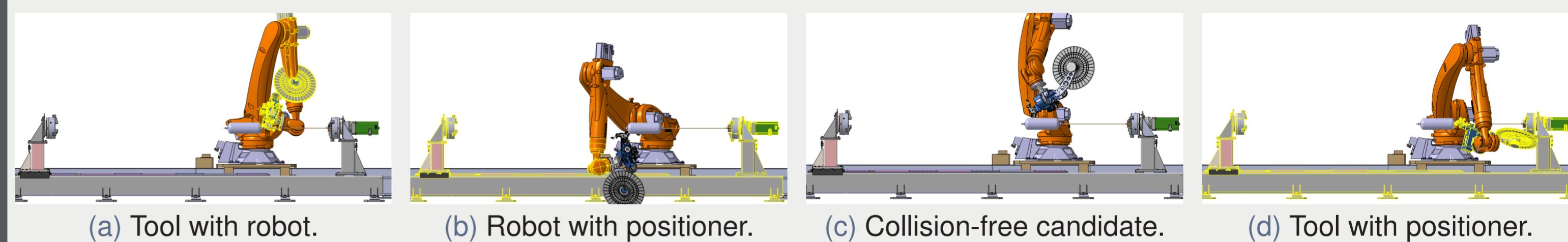


Figure: Examples of collisions detected in the CAD model.

## 3. Optimal Path Planning

Path planning using the Dynamic Programming principle:

$$d_{k,i+1} = \min_{k'} \{ d_{k',i} + dist(L_c^{(k,i+1)}, L_c^{(k',i)}) \} \quad (10)$$

Objective function: total travelling time to be minimized

$$T = \min_{q_r(t), q_p(t)} ; \quad T = \sum_{j=1}^{n-1} dist(L_c^{(k,j)}, L_c^{(k+1,j+1)}) \quad (9)$$

## Simulation Results & Analysis

- Determining optimal robot base location on linear axis.

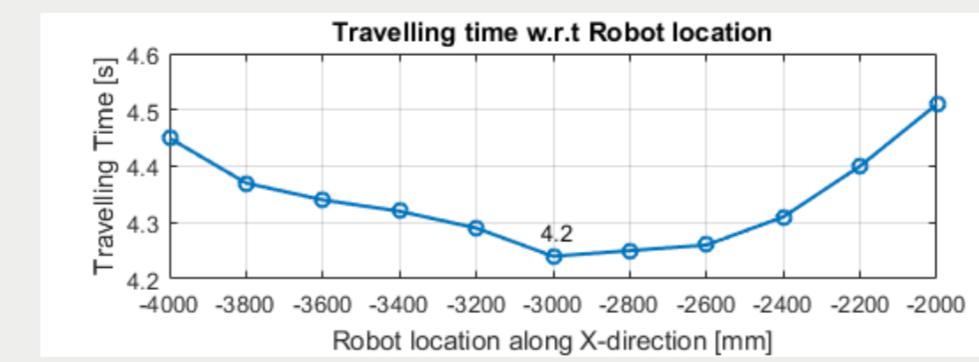


Figure: Optimal robot base location.

- For linear axis coordinate value of **-3000mm** and with a **1deg** discretization step for the positioner coordinate, the results obtained are as follows:

No. of Task Locations	Travelling Time
127	3.0sec
200	3.2sec

- Significant reduction in travelling time, compared to initial **14sec**.
- Smooth trajectories.
- Higher quality and increased productivity.

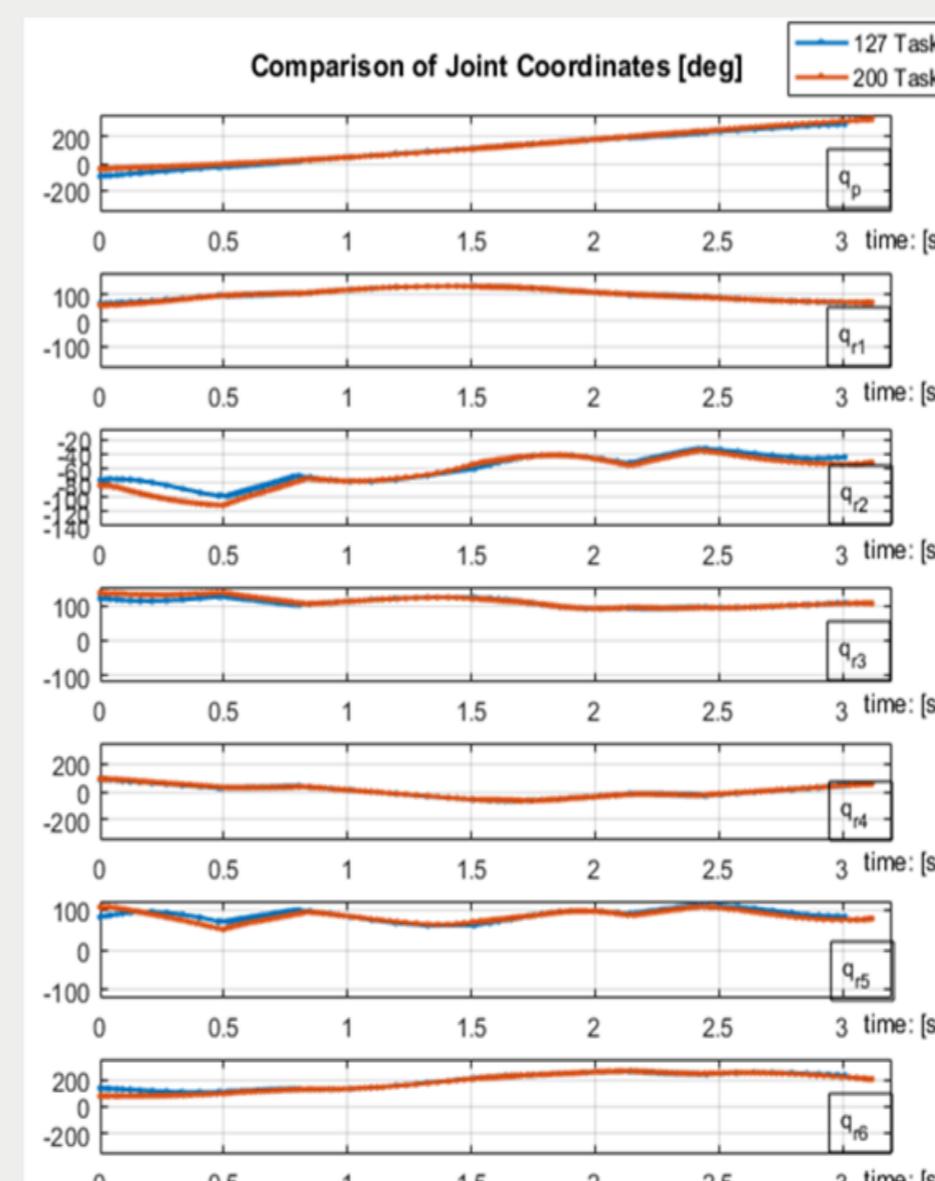


Figure: Comparison of Joint coordinates.

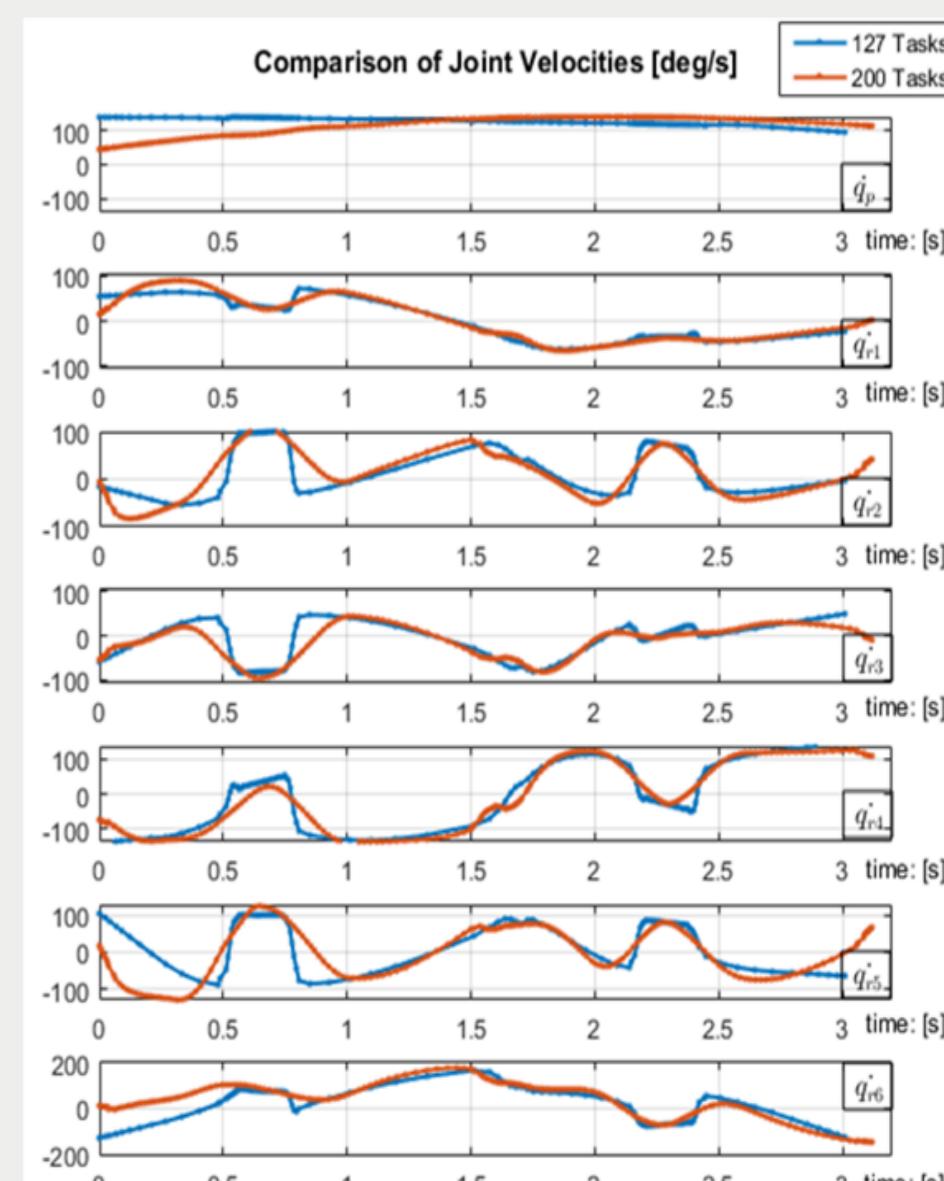


Figure: Comparison of Joint Velocities.