

Increased Productivity of an Automated Tape Winding Process: SPIDE-TP Platform

Divya SHAH

Supervisors: B. Courtemanche; S. Caro; A. Pashkevich

Master Thesis Defense

29 August, 2017



- 1 Introduction
- 2 Automated Tape Winding Process
- 3 SPIDE-TP Platform
- 4 System & Task Modelling
- 5 Optimal Trajectory Generation
- 6 Optimal Motion Implementation
- 7 Conclusions

- 1 Introduction
- 2 Automated Tape Winding Process
- 3 SPIDE-TP Platform
- 4 System & Task Modelling
- 5 Optimal Trajectory Generation
- 6 Optimal Motion Implementation
- 7 Conclusions

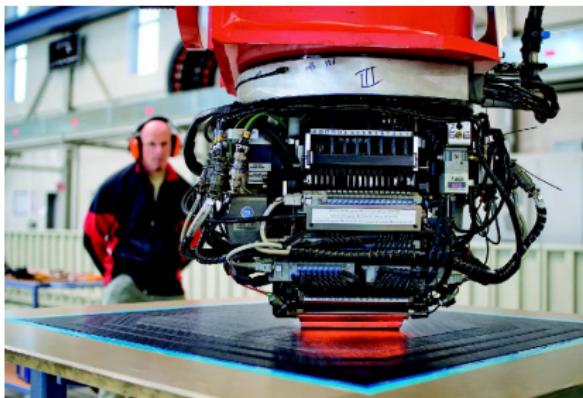
- Extensive use in recent times
- Excellent material properties

Mike Garry. *Polymer Composites vs. Steel.*

- Extensive use in recent times
- Excellent material properties
- Manufacturing of high performance structures
- Applications: Aerospace & Automotive Industries

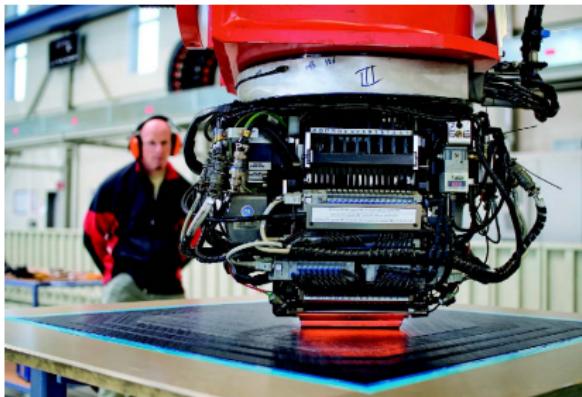


Mike Garry. Polymer Composites vs. Steel.



- **Automated Tape Laying (ATL)**
- Laying on molds
- Shape limitations

George Marsh (2011). "Automating aerospace composites production with fibre placement". In: *REINFORCED plastics*

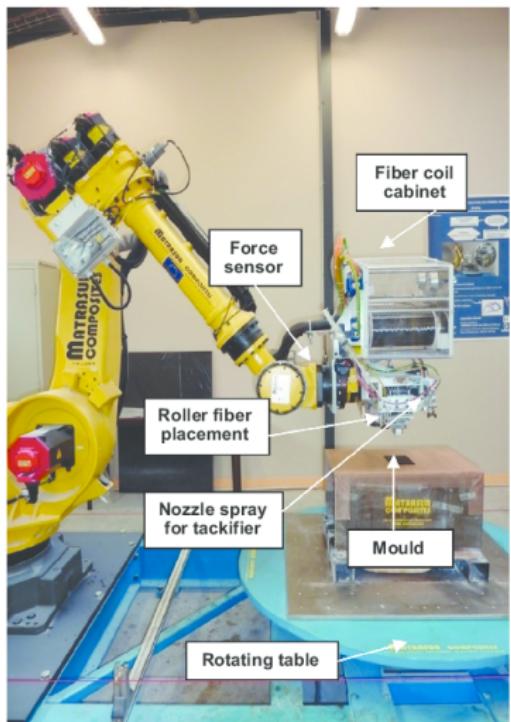
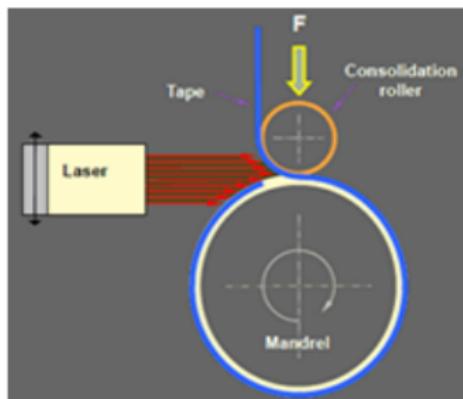


- **Automated Tape Laying (ATL)**
- Laying on molds
- Shape limitations

- **Automated Tape Winding (ATW)**
- Workpiece on rotating mandrel
- Complex geometries

George Marsh (2011). "Automating aerospace composites production with fibre placement". In: *REINFORCED plastics*

- 1 Introduction
- 2 Automated Tape Winding Process**
- 3 SPIDE-TP Platform
- 4 System & Task Modelling
- 5 Optimal Trajectory Generation
- 6 Optimal Motion Implementation
- 7 Conclusions



Mariem Belhaj et al. (2013). "Dry fiber automated placement of carbon fibrous preforms". In: *Composites Part B: Engineering*

Advantages

- Precise control of placement head
- In-situ consolidation
- Repeatability

Advantages

- Precise control of placement head
- In-situ consolidation
- Repeatability

Challenges

- Kinematic redundancy management
- Manipulator motion planning

Advantages

- Precise control of placement head
- In-situ consolidation
- Repeatability

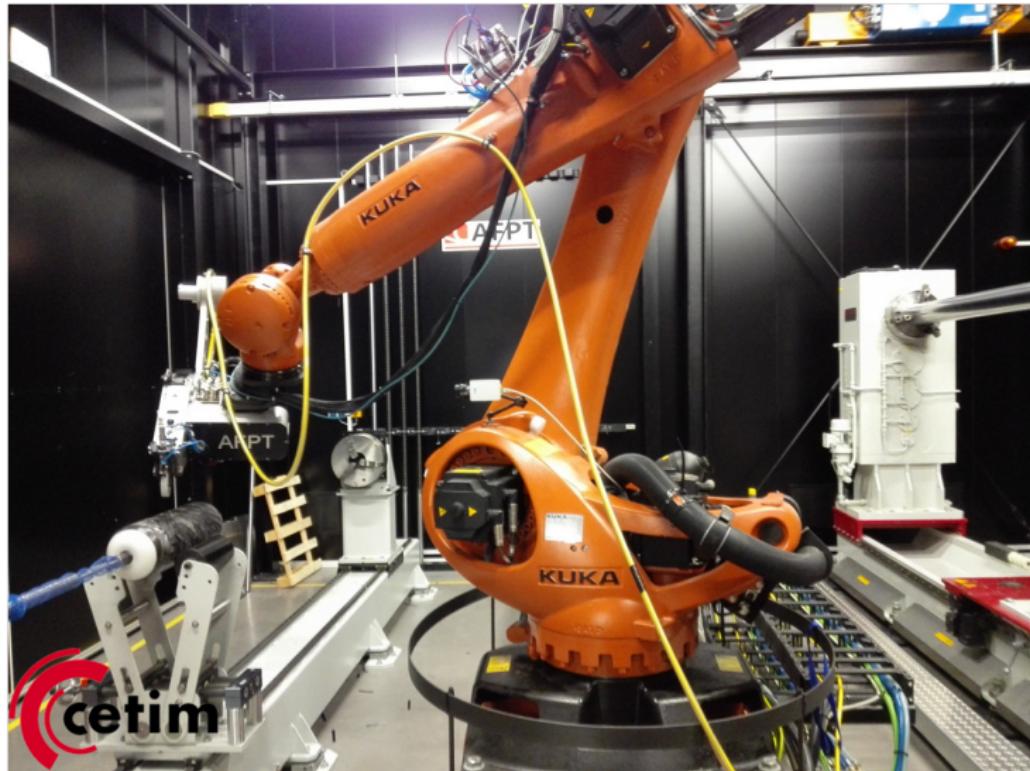
Challenges

- Kinematic redundancy management
- Manipulator motion planning

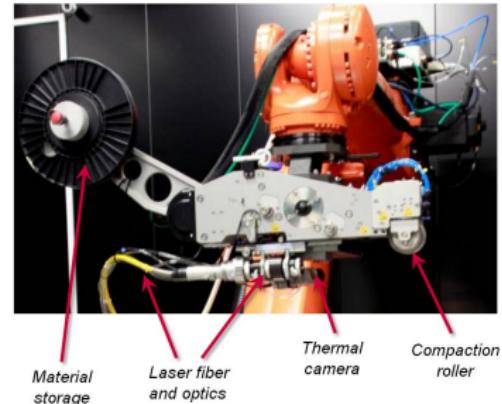
Solution

- Graph-based Discrete Optimization

- 1 Introduction
- 2 Automated Tape Winding Process
- 3 SPIDE-TP Platform**
- 4 System & Task Modelling
- 5 Optimal Trajectory Generation
- 6 Optimal Motion Implementation
- 7 Conclusions



Centre technique des industries mécaniques [CETIM].



- **Different Winding Axes**
- Large Axis: Diameter $0.25m$ to $2.50m$
- Small Axis: Diameter $25mm$ to $500mm$

- **Winding Head Assembly**
- Laser ($4kW$)
- Thermal Camera
- Compaction Roller

Centre technique des industries mécaniques [CETIM].

Current Methodology

- Composicad software: Workpiece modelling & Track generation
- Post-processor: Robot program

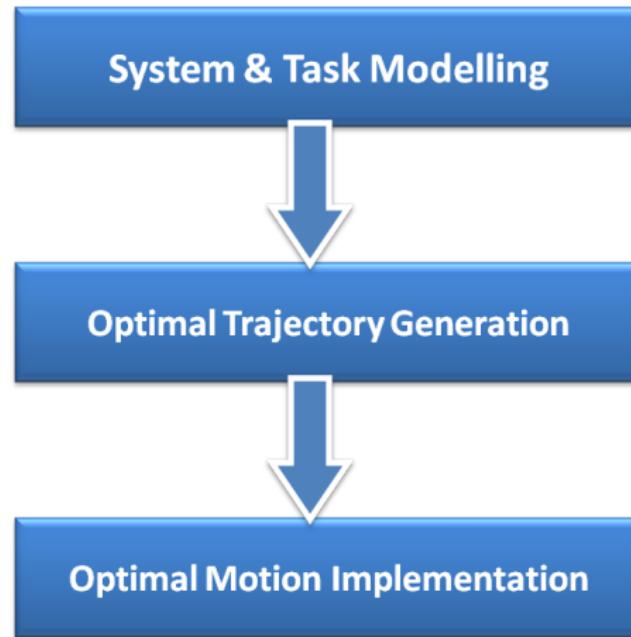
Current Methodology

- Composicad software: Workpiece modelling & Track generation
- Post-processor: Robot program

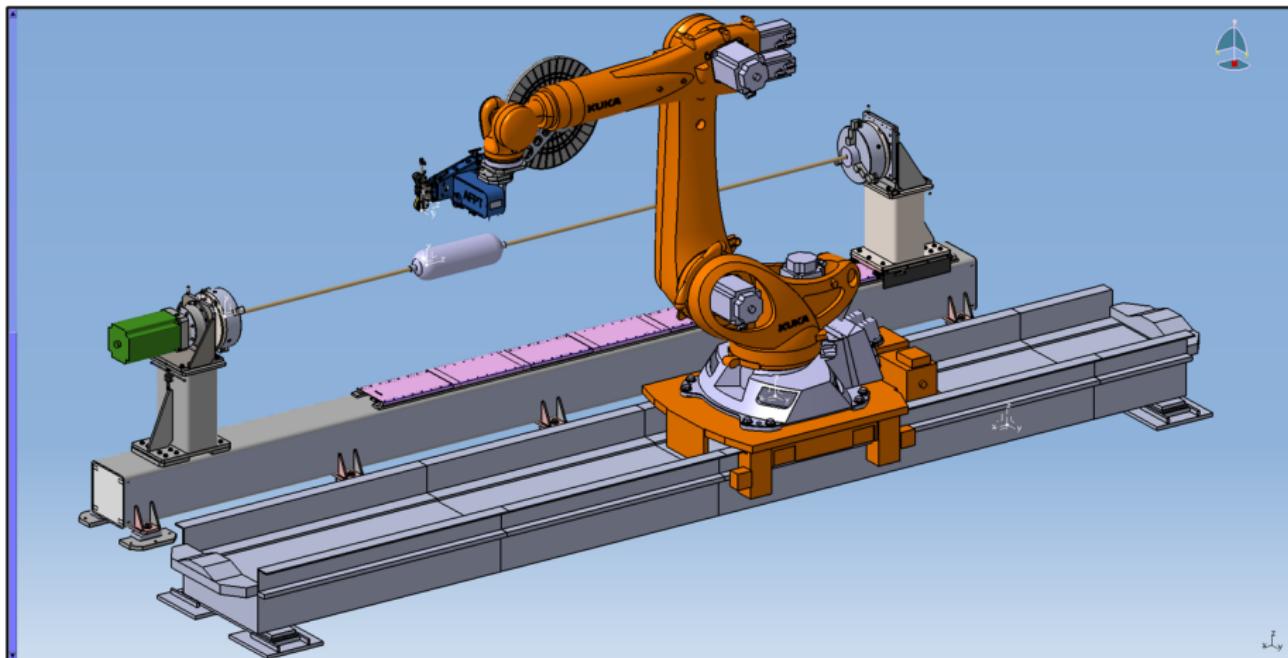
Key Challenges

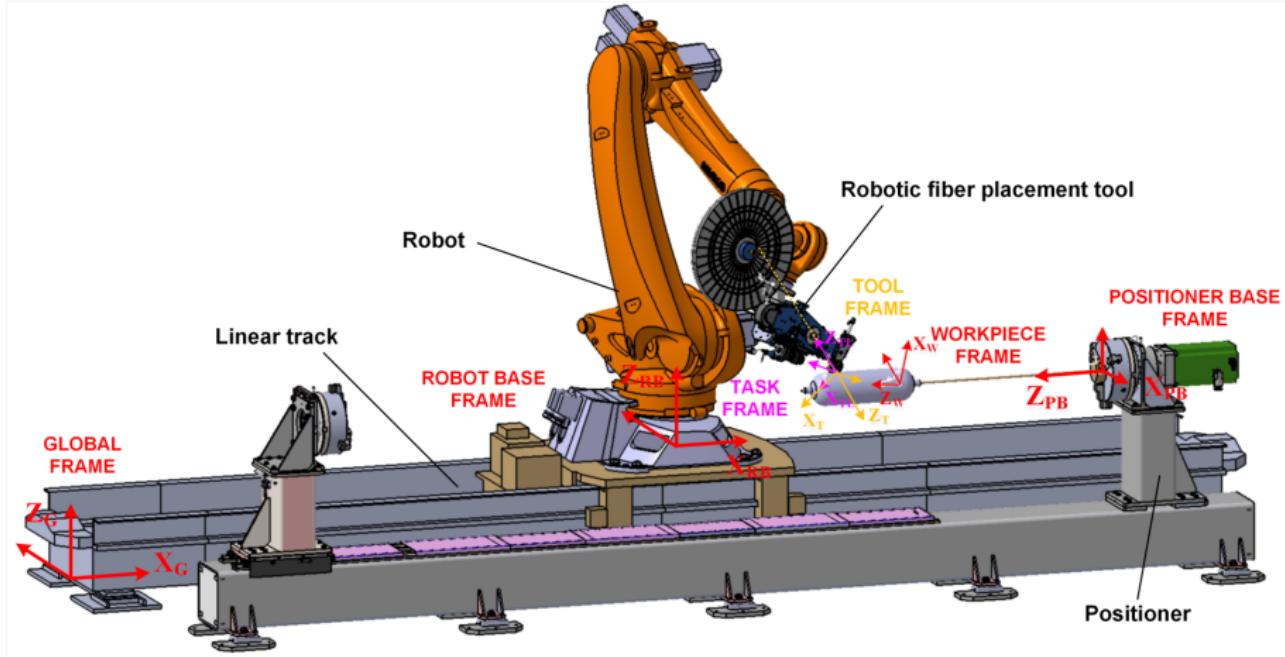
- Kinematic redundancy not fully exploited
- Discontinuities in the trajectory
- High Raw material cost

- Estimate maximum production time of a given track
- Identify the limiting axis
- Select the tools to manage kinematic redundancy
- Estimate the gain of productivity expected
- Implement proposed methods



- 1 Introduction
- 2 Automated Tape Winding Process
- 3 SPIDE-TP Platform
- 4 System & Task Modelling**
- 5 Optimal Trajectory Generation
- 6 Optimal Motion Implementation
- 7 Conclusions





Robot Model

$$\text{rob}(\vec{q}_r) = {}^{\text{RB}}\mathbf{T}_1(q_1) \cdot {}^1\mathbf{T}_2(q_2) \cdot {}^2\mathbf{T}_3(q_3) \cdot {}^3\mathbf{T}_4(q_4) \cdot {}^4\mathbf{T}_5(q_5) \cdot {}^5\mathbf{T}_{RF}(q_6) \quad (1)$$

Winding Axis Model

$$\text{pos}(q_p) = \text{Rot}_Z(q_p) \quad (2)$$

Linear Axis Model

$$\text{lin}(q_l) = \text{Trans}_X(q_l) \quad (3)$$

Robot Model

$$\textit{rob}(\vec{q}_r) = {}^{\textit{RB}} \mathbf{T}_1(q_1) \cdot {}^1 \mathbf{T}_2(q_2) \cdot {}^2 \mathbf{T}_3(q_3) \cdot {}^3 \mathbf{T}_4(q_4) \cdot {}^4 \mathbf{T}_5(q_5) \cdot {}^5 \mathbf{T}_{\textit{RF}}(q_6) \quad (1)$$

Winding Axis Model

$$\textit{pos}(q_p) = \textit{Rot}_Z(q_p) \quad (2)$$

Linear Axis Model

$$\textit{lin}(q_l) = \textit{Trans}_X(q_l) \quad (3)$$

Robot Model

$$\textit{rob}(\vec{q}_r) = {}^{\textit{RB}}\textbf{T}_1(q_1) \cdot {}^1\textbf{T}_2(q_2) \cdot {}^2\textbf{T}_3(q_3) \cdot {}^3\textbf{T}_4(q_4) \cdot {}^4\textbf{T}_5(q_5) \cdot {}^5\textbf{T}_{RF}(q_6) \quad (1)$$

Winding Axis Model

$$\textit{pos}(q_p) = \textit{Rot}_Z(q_p) \quad (2)$$

Linear Axis Model

$$\textit{lin}(q_l) = \textit{Trans}_X(q_l) \quad (3)$$

Robot Model

$$\textit{rob}(\vec{q}_r) = {}^{\textit{RB}} \mathbf{T}_1(q_1) \cdot {}^1 \mathbf{T}_2(q_2) \cdot {}^2 \mathbf{T}_3(q_3) \cdot {}^3 \mathbf{T}_4(q_4) \cdot {}^4 \mathbf{T}_5(q_5) \cdot {}^5 \mathbf{T}_{\textit{RF}}(q_6) \quad (1)$$

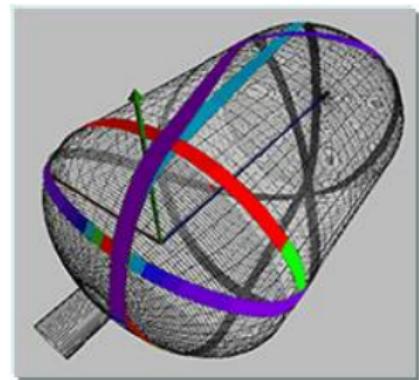
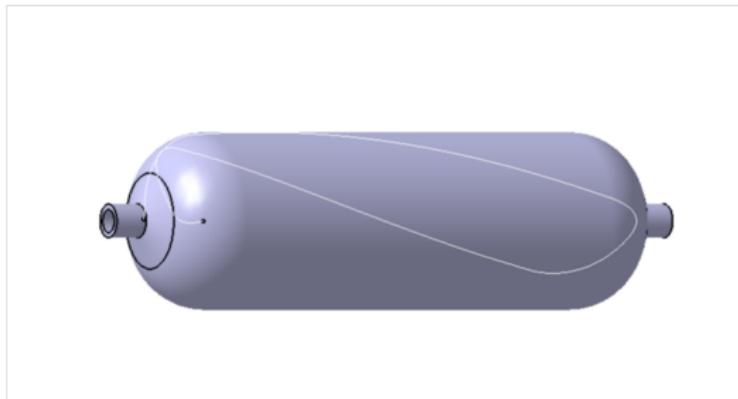
Winding Axis Model

$$\textit{pos}(q_p) = \textit{Rot}_Z(q_p) \quad (2)$$

Linear Axis Model

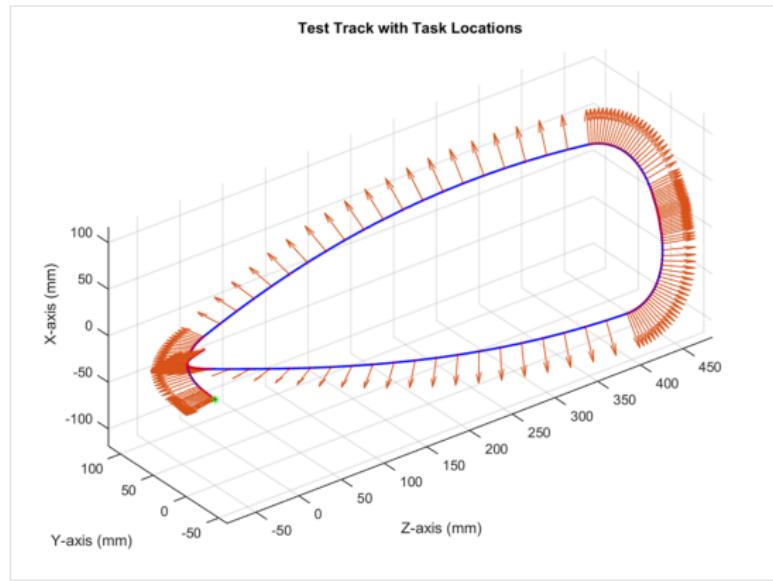
$$\textit{lin}(q_l) = \textit{Trans}_X(q_l) \quad (3)$$

- Cylindrical workpiece with hemi-spherical domes on the ends.
- Winding path generated from the Composicad software.
- Current Travelling time: 14sec.



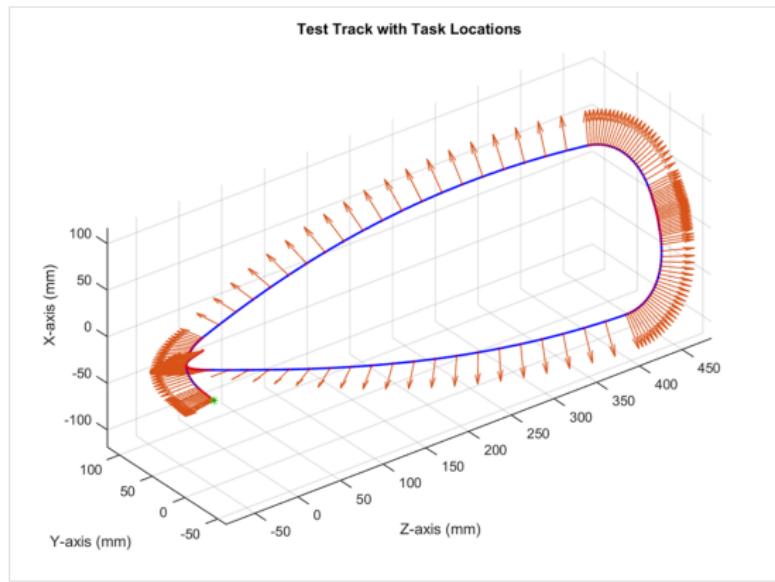
Centre technique des industries mécaniques [CETIM].

Video for the test track.



Task Model

$${}^w T_{TL_i} = \begin{bmatrix} \vec{n}_i & \vec{s}_i & \vec{a}_i & \vec{p}_i \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \text{Rot}(\vec{\varphi}_i) & \vec{p}_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad |i = 1, 2, \dots, n \quad (4)$$



Task Model

$${}^w T_{TL_i} = \begin{bmatrix} \vec{n}_i & \vec{s}_i & \vec{a}_i & \vec{p}_i \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \textbf{Rot}(\vec{\varphi}_i) & \vec{p}_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad |i = 1, 2, \dots, n \quad (4)$$

- 1 Introduction
- 2 Automated Tape Winding Process
- 3 SPIDE-TP Platform
- 4 System & Task Modelling
- 5 Optimal Trajectory Generation**
- 6 Optimal Motion Implementation
- 7 Conclusions

Task Representation

$${}^0T_{TL_i}(\vec{q}_r) = {}^0T_{RB} \cdot rob(\vec{q}_r) \cdot {}^{RF}T_T \cdot {}^T T_{TL_i} \quad (5)$$

$${}^0T_{TL_i}(q_p) = {}^0T_{PB} \cdot pos(q_p) \cdot {}^{PF}T_W \cdot {}^W T_{TL_i} \quad (6)$$

Task Constraint

$${}^0T_{RB} \cdot rob(\vec{q}_r) \cdot {}^{RF}T_T \cdot {}^T T_{TL_i} = {}^0T_{PB} \cdot pos(q_p) \cdot {}^{PF}T_W \cdot {}^W T_{TL_i} \quad (7)$$

Task Representation

$${}^0 T_{TL_i}(\vec{q}_r) = {}^0 T_{RB} \cdot rob(\vec{q}_r) \cdot {}^{RF} T_T \cdot {}^T T_{TL_i} \quad (5)$$

$${}^0 T_{TL_i}(q_p) = {}^0 T_{PB} \cdot pos(q_p) \cdot {}^{PF} T_W \cdot {}^W T_{TL_i} \quad (6)$$

Task Constraint

$${}^0 T_{RB} \cdot rob(\vec{q}_r) \cdot {}^{RF} T_T \cdot {}^T T_{TL_i} = {}^0 T_{PB} \cdot pos(q_p) \cdot {}^{PF} T_W \cdot {}^W T_{TL_i} \quad (7)$$

Task Representation

$${}^0 T_{TL_i}(\vec{q}_r) = {}^0 T_{RB} \cdot rob(\vec{q}_r) \cdot {}^{RF} T_T \cdot {}^T T_{TL_i} \quad (5)$$

$${}^0 T_{TL_i}(q_p) = {}^0 T_{PB} \cdot pos(q_p) \cdot {}^{PF} T_W \cdot {}^W T_{TL_i} \quad (6)$$

Task Constraint

$${}^0 T_{RB} \cdot rob(\vec{q}_r) \cdot {}^{RF} T_T \cdot {}^T T_{TL_i} = {}^0 T_{PB} \cdot pos(q_p) \cdot {}^{PF} T_W \cdot {}^W T_{TL_i} \quad (7)$$

Discretization

$$q_p^{(k)} \in [q_p^{\min}, q_p^{\max}]; \text{with step } \Delta q_p \quad (8)$$

Kinematic Equation

$$\mathbf{q}_r^k(t_i) = \mathbf{rob}^{-1}(\mathbf{pos}(q_p^{(k)}(t_i)), \mu); \ k = 0, 1 \dots m; \ i = 1, 2 \dots, n \quad (9)$$

Location Cell

$$L_c^{(k,i)} = (\mathbf{q}_r^{(k)}(t_i), q_p^{(k)}(t_i)) \quad (10)$$

Discretization

$$q_p^{(k)} \in [q_p^{\min}, q_p^{\max}]; \text{with step } \Delta q_p \quad (8)$$

Kinematic Equation

$$\mathbf{q}_r^k(t_i) = \mathbf{rob}^{-1}(\mathbf{pos}(q_p^{(k)}(t_i)), \mu); \ k = 0, 1 \dots m; \ i = 1, 2 \dots, n \quad (9)$$

Location Cell

$$L_c^{(k,i)} = (\mathbf{q}_r^{(k)}(t_i), q_p^{(k)}(t_i)) \quad (10)$$

Discretization

$$q_p^{(k)} \in [q_p^{\min}, q_p^{\max}]; \text{with step } \Delta q_p \quad (8)$$

Kinematic Equation

$$\mathbf{q}_r^k(t_i) = \mathbf{rob}^{-1}(\mathbf{pos}(q_p^{(k)}(t_i)), \mu); \ k = 0, 1 \dots m; \ i = 1, 2 \dots, n \quad (9)$$

Location Cell

$$L_c^{(k,i)} = (\mathbf{q}_r^{(k)}(t_i), q_p^{(k)}(t_i)) \quad (10)$$

Discretization

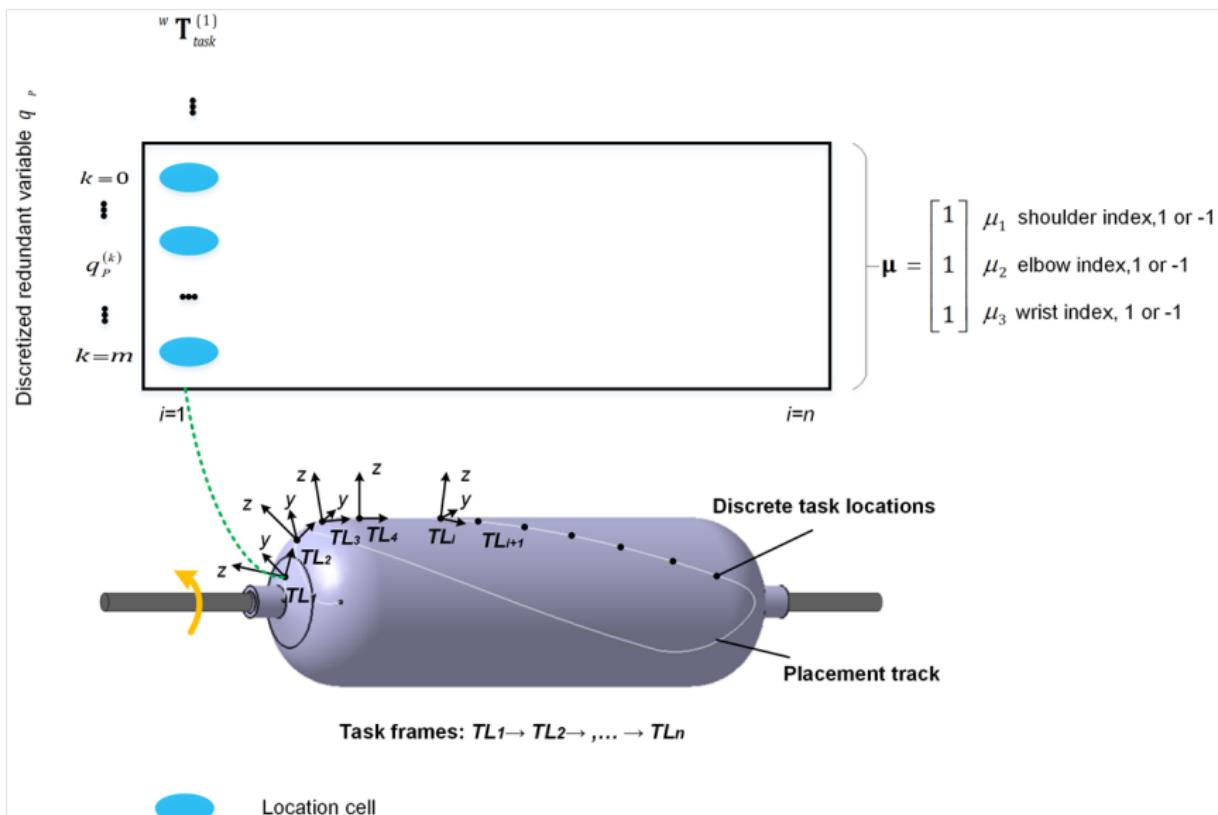
$$q_p^{(k)} \in [q_p^{\min}, q_p^{\max}]; \text{with step } \Delta q_p \quad (8)$$

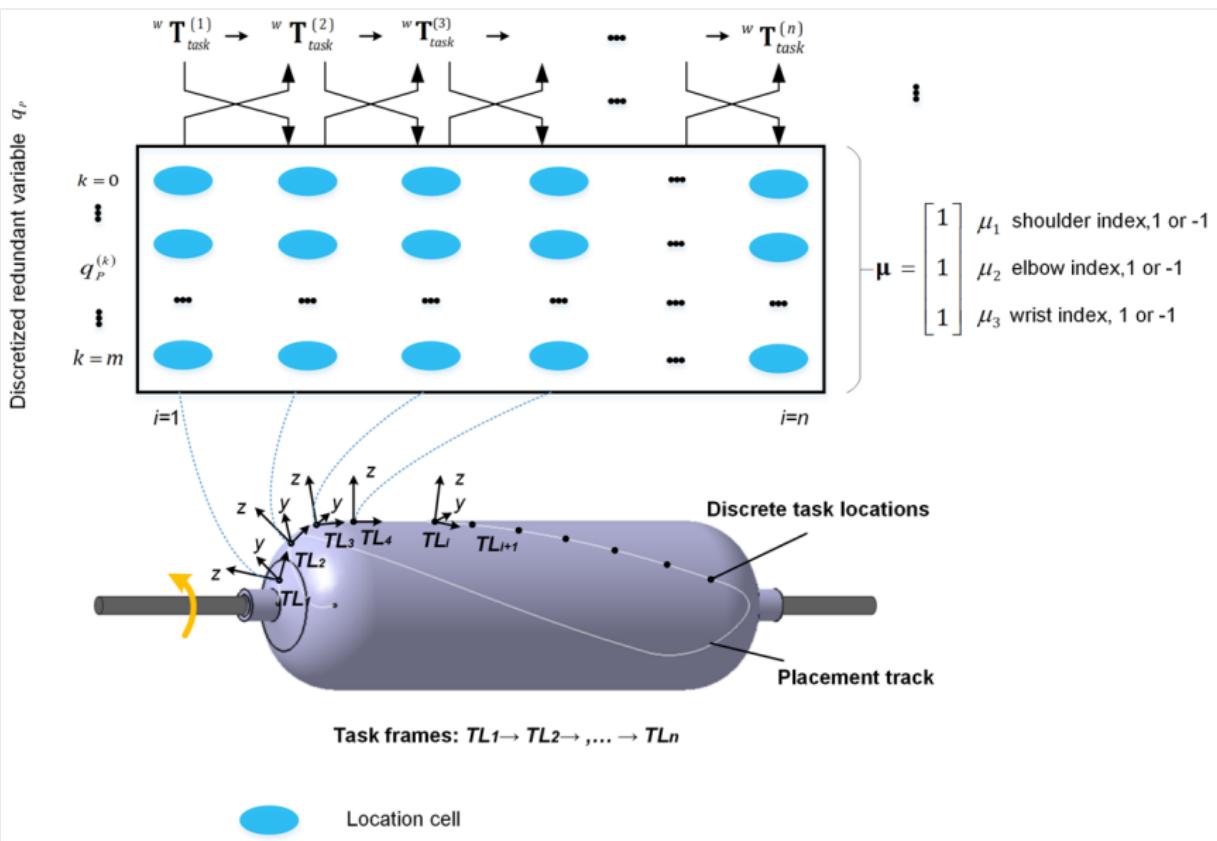
Kinematic Equation

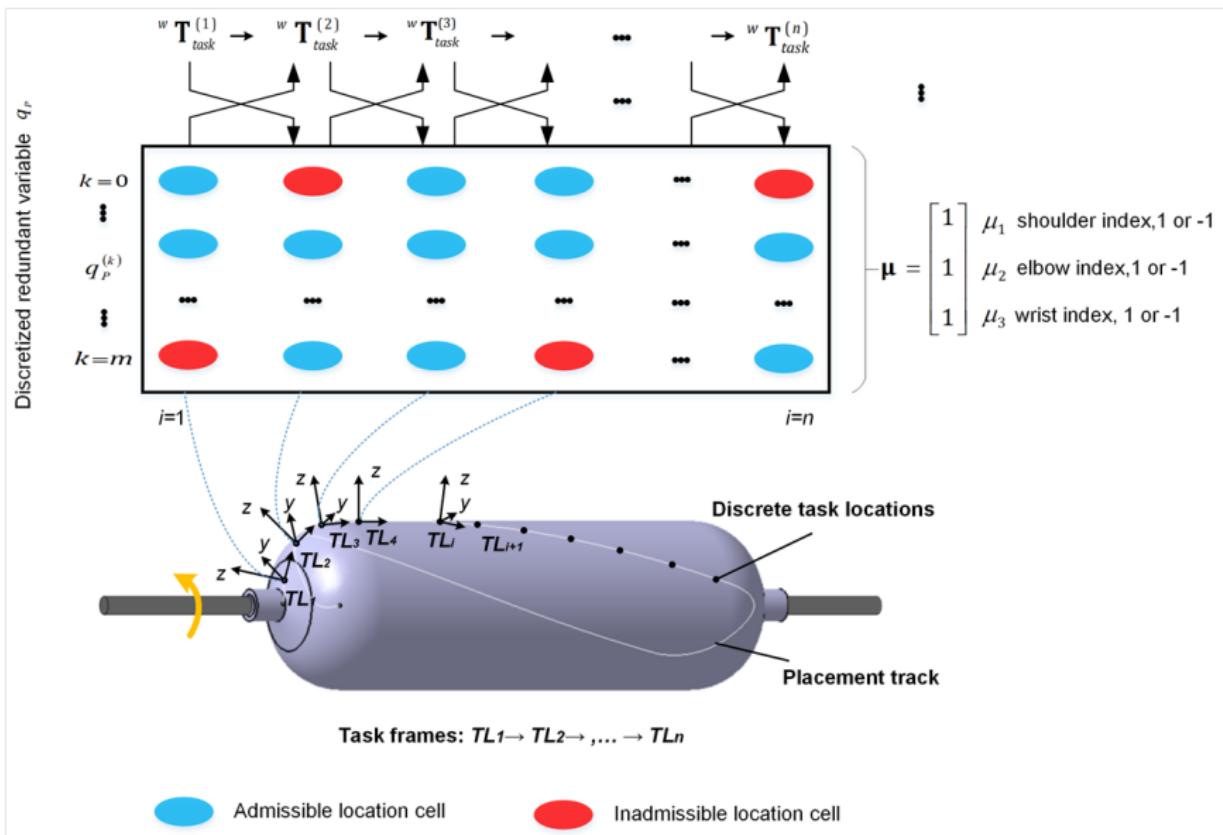
$$\mathbf{q}_r^k(t_i) = \mathbf{rob}^{-1}(\mathbf{pos}(q_p^{(k)}(t_i)), \mu); \ k = 0, 1 \dots m; \ i = 1, 2 \dots, n \quad (9)$$

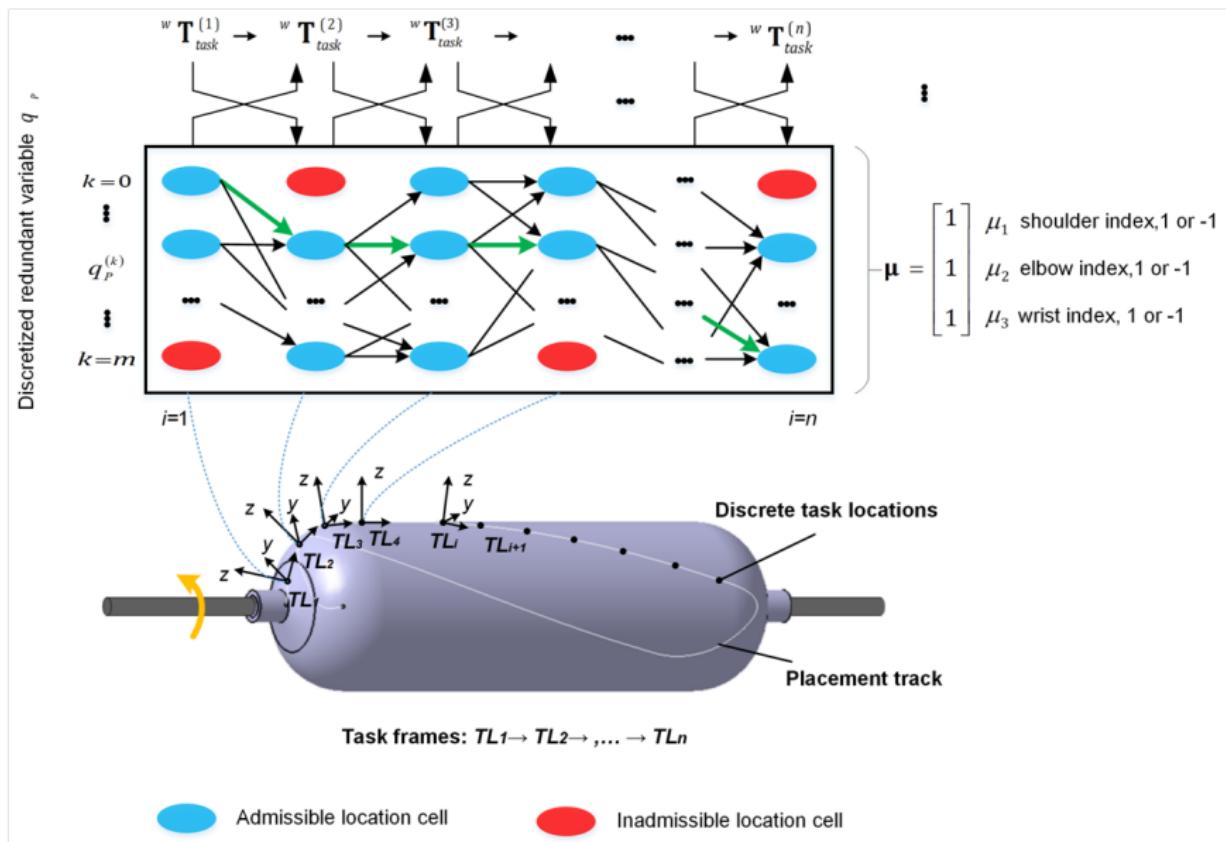
Location Cell

$$\mathcal{L}_c^{(k,i)} = (\mathbf{q}_r^{(k)}(t_i), q_p^{(k)}(t_i)) \quad (10)$$









Kinematic Constraints

$$\begin{aligned} q_j^{\min} &\leq q_j(t_i) \leq q_j^{\max} \\ \dot{q}_j^{\min} &\leq \dot{q}_j(t_i) \leq \dot{q}_j^{\max} \\ \ddot{q}_j^{\min} &\leq \ddot{q}_j(t_i) \leq \ddot{q}_j^{\max} \end{aligned} \quad (11)$$

where $j = 0, 1, \dots, 6$ is the common index for joint variables with $j = 0$ being q_p .

Collision Constraint

$$\text{cols}(q_p(t), \mathbf{q}_r(t)) = 0; \forall t \in [0, T] \quad (12)$$

Kinematic Constraints

$$\begin{aligned} q_j^{\min} &\leq q_j(t_i) \leq q_j^{\max} \\ \dot{q}_j^{\min} &\leq \dot{q}_j(t_i) \leq \dot{q}_j^{\max} \\ \ddot{q}_j^{\min} &\leq \ddot{q}_j(t_i) \leq \ddot{q}_j^{\max} \end{aligned} \quad (11)$$

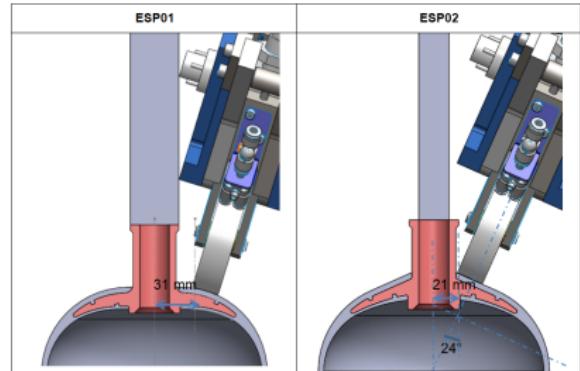
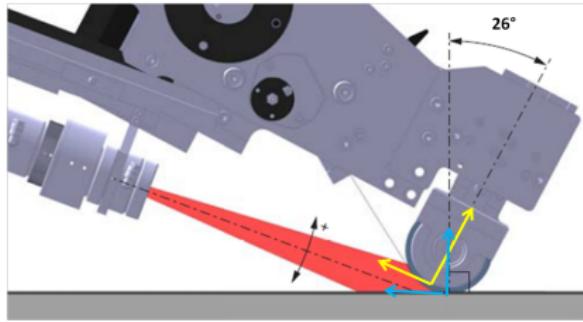
where $j = 0, 1, \dots, 6$ is the common index for joint variables with $j = 0$ being q_p .

Collision Constraint

$$\mathbf{cols}(q_p(t), \mathbf{q}_r(t)) = 0; \forall t \in [0, T] \quad (12)$$

Video for collision detection.

Video for testing the tool trajectory.



- Tool orientation correction.
- Modification of shaft geometry.

Centre technique des industries mécaniques [CETIM].

Internodal Distance

$$dist(\mathcal{L}_c^{(k_i, i)}, \mathcal{L}_c^{(k_{i+1}, i+1)}) = \max_{j=0, \dots, 6} \left(\frac{|q_{j,i}^{(k_i)} - q_{j,i+1}^{(k_{i+1})}|}{\dot{q}_j^{\max}} \right) \quad (13)$$

Objective function

$$T = \sum_{j=1}^{n-1} dist(\mathcal{L}_c^{(k_i, i)}, \mathcal{L}_c^{(k_{i+1}, i+1)}) \quad (14)$$

Dynamic Programming Principle

$$d_{k,i+1} = \min_{k'} \{ d_{k',i} + dist(\mathcal{L}_c^{(k,i+1)}, \mathcal{L}_c^{(k',i)}) \} \quad (15)$$

Jiuchun Gao, Anatol Pashkevich, and Stéphane Caro (2017). "Optimization of the robot and positioner motion in a redundant fiber placement workcell". In: *Mechanism and Machine Theory*

Internodal Distance

$$dist(\mathcal{L}_c^{(k_i, i)}, \mathcal{L}_c^{(k_{i+1}, i+1)}) = \max_{j=0, \dots, 6} \left(\frac{|q_{j,i}^{(k_i)} - q_{j,i+1}^{(k_{i+1})}|}{\dot{q}_j^{\max}} \right) \quad (13)$$

Objective function

$$T = \sum_{j=1}^{n-1} dist(\mathcal{L}_c^{(k_i, i)}, \mathcal{L}_c^{(k_{i+1}, i+1)}) \quad (14)$$

Dynamic Programming Principle

$$d_{k,i+1} = \min_{k'} \{ d_{k',i} + dist(\mathcal{L}_c^{(k,i+1)}, \mathcal{L}_c^{(k',i)}) \} \quad (15)$$

Jiuchun Gao, Anatol Pashkevich, and Stéphane Caro (2017). "Optimization of the robot and positioner motion in a redundant fiber placement workcell". In: *Mechanism and Machine Theory*

Internodal Distance

$$dist(\mathcal{L}_c^{(k_i, i)}, \mathcal{L}_c^{(k_{i+1}, i+1)}) = \max_{j=0, \dots, 6} \left(\frac{|q_{j,i}^{(k_i)} - q_{j,i+1}^{(k_{i+1})}|}{\dot{q}_j^{\max}} \right) \quad (13)$$

Objective function

$$T = \sum_{j=1}^{n-1} dist(\mathcal{L}_c^{(k_i, i)}, \mathcal{L}_c^{(k_{i+1}, i+1)}) \quad (14)$$

Dynamic Programming Principle

$$d_{k,i+1} = \min_{k'} \{ d_{k',i} + dist(\mathcal{L}_c^{(k,i+1)}, \mathcal{L}_c^{(k',i)}) \} \quad (15)$$

Jiuchun Gao, Anatol Pashkevich, and Stéphane Caro (2017). "Optimization of the robot and positioner motion in a redundant fiber placement workcell". In: *Mechanism and Machine Theory*

Internodal Distance

$$dist(\mathcal{L}_c^{(k_i, i)}, \mathcal{L}_c^{(k_{i+1}, i+1)}) = \max_{j=0, \dots, 6} \left(\frac{|q_{j,i}^{(k_i)} - q_{j,i+1}^{(k_{i+1})}|}{\dot{q}_j^{\max}} \right) \quad (13)$$

Objective function

$$T = \sum_{j=1}^{n-1} dist(\mathcal{L}_c^{(k_i, i)}, \mathcal{L}_c^{(k_{i+1}, i+1)}) \quad (14)$$

Dynamic Programming Principle

$$d_{k,i+1} = \min_{k'} \{ d_{k',i} + dist(\mathcal{L}_c^{(k,i+1)}, \mathcal{L}_c^{(k',i)}) \} \quad (15)$$

Jiuchun Gao, Anatol Pashkevich, and Stéphane Caro (2017). "Optimization of the robot and positioner motion in a redundant fiber placement workcell". In: *Mechanism and Machine Theory*

Algorithm 1: Path Planning (Dynamic Programming)

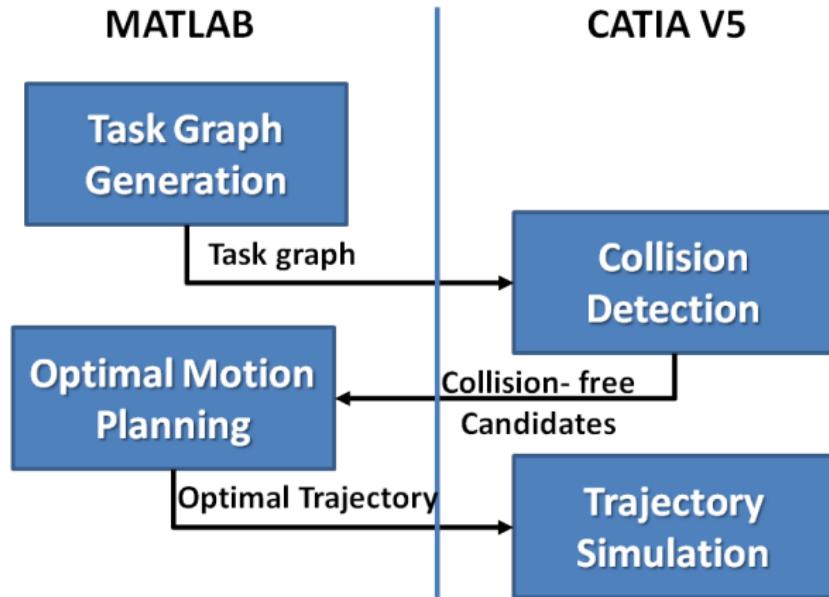
Data: Matrix of locations $L(k, i)$ of size $m \times n$
Result: Minimum path length D_{min} & Optimal path indices $k^0(i)$, $i = 1, 2, \dots, n$

```

 $D(k, 1) = 0 ;$ 
 $P(k, 1) = \text{null}, \forall k = 1, 2, \dots, m ;$ 
for  $i = 2$  to  $n$  do
    for  $k = 1$  to  $m$  do
        for  $j = 1$  to  $m$  do
            if  $\text{cols}(L(j, i - 1)) = 0 \ \& \ \text{cols}(L(k, i)) = 0 \ \& \ (\text{accl}(L(j, i - 1), L(k, i)) = 0)$ 
            then
                 $| \quad r(j) = D(j, i - 1) + \text{dist}(L(k, i), L(j, i - 1)) ;$ 
            else
                 $| \quad r(j) = \text{inf} ;$ 
            end
            end
             $D(j, i) = \min(r) ;$ 
             $P(j, i) = \arg \min(r) ;$ 
        end
         $D_{min} = \min(D(k, n)) ;$ 
         $k^0(n) = \arg \min(r) ;$ 
    end
    for  $i = n$  to  $2$  do
         $| \quad k^0(i - 1) = P(k^0(i), i) ;$ 
    end

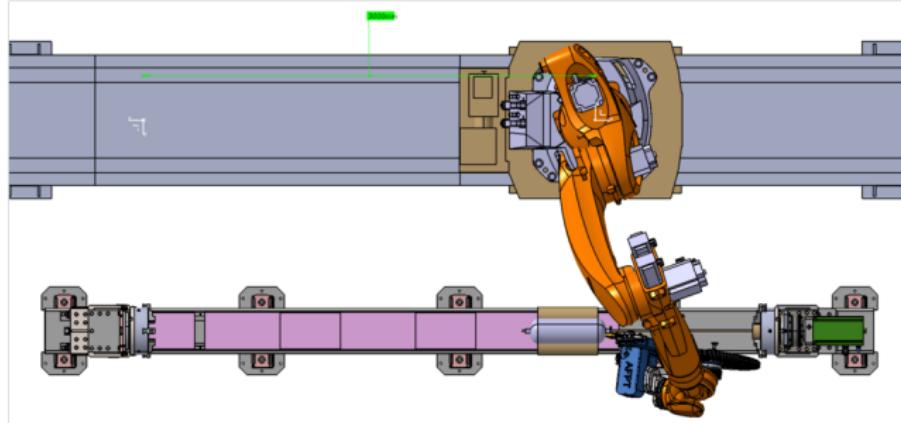
```

Jiuchun Gao, Anatol Pashkevich, and Stéphane Caro (2017). "Optimization of the robot and positioner motion in a redundant fiber placement workcell". In: *Mechanism and Machine Theory*

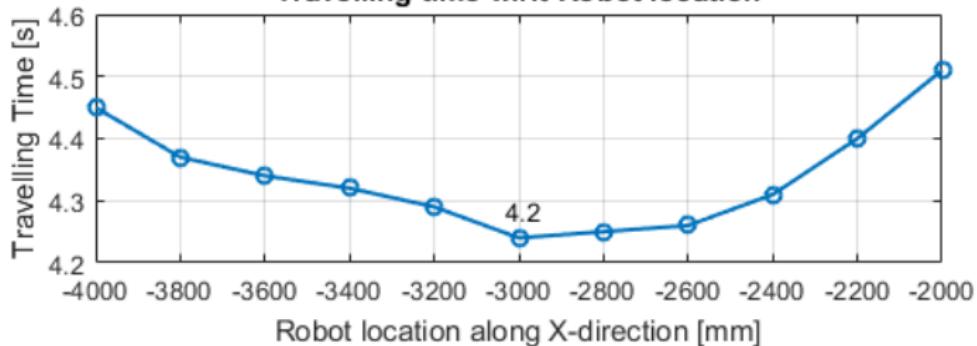


- 1 Introduction
- 2 Automated Tape Winding Process
- 3 SPIDE-TP Platform
- 4 System & Task Modelling
- 5 Optimal Trajectory Generation
- 6 Optimal Motion Implementation
- 7 Conclusions

Selection of the robot base location on the linear axis.



Travelling time w.r.t Robot location

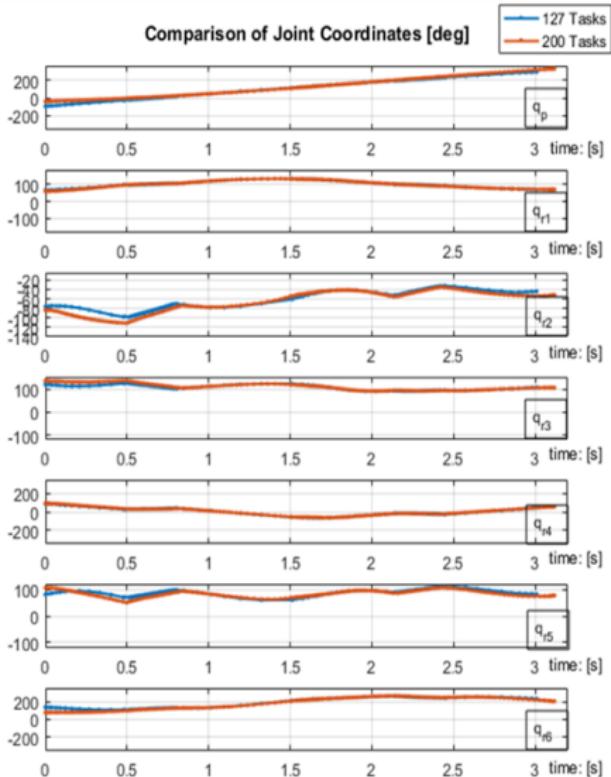


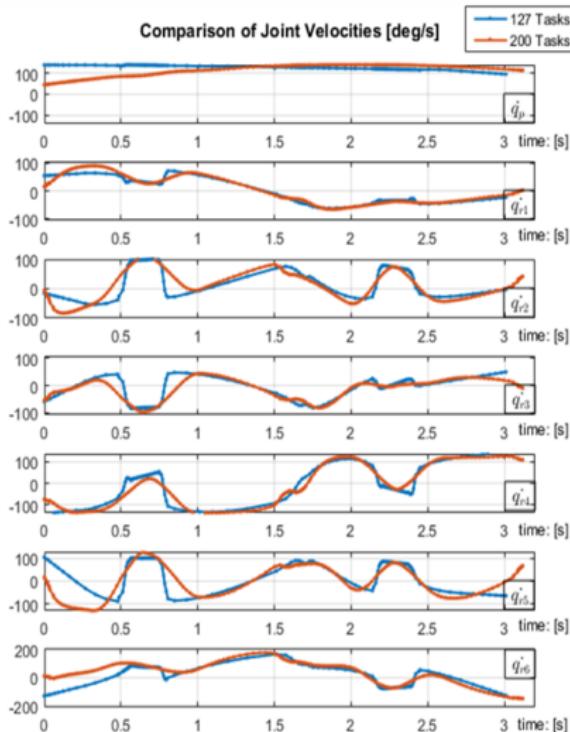
For linear axis coordinate value of $-3000mm$ and with a $1\ deg$ discretization step for the positioner coordinate, the results obtained are as follows:

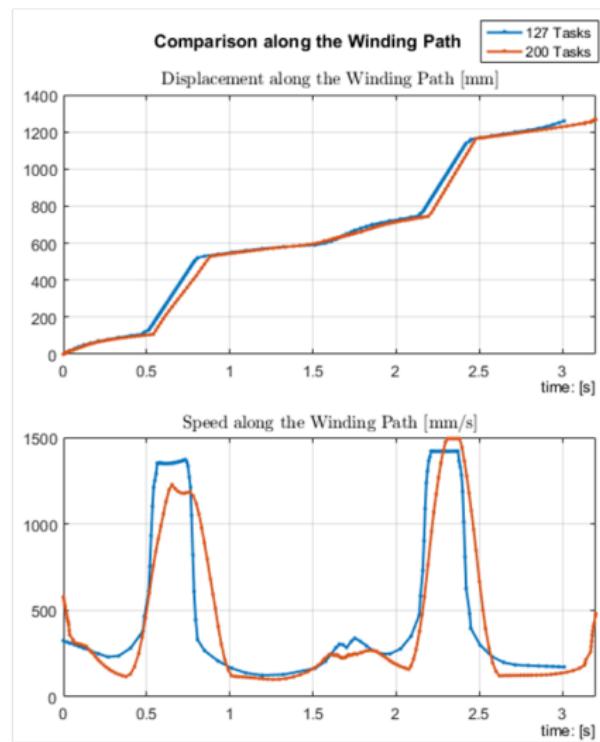
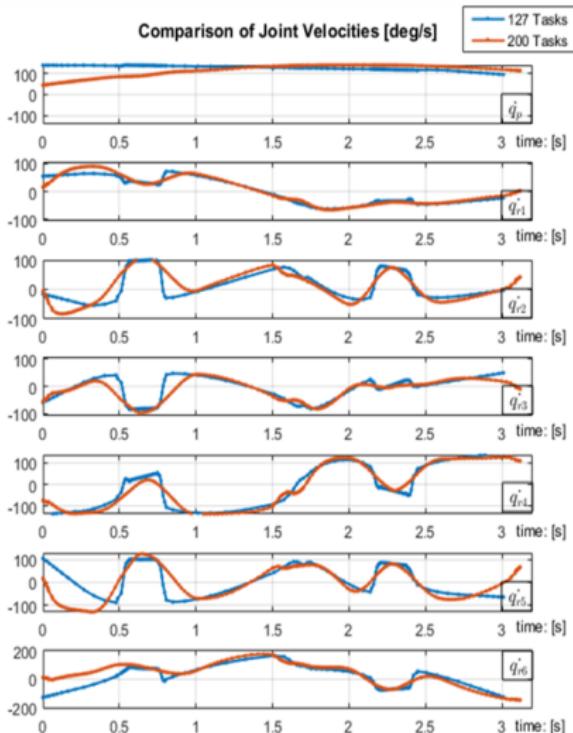
No. of Task Locations	Travelling Time
127	3.0sec
200	3.2sec

For linear axis coordinate value of -3000mm and with a 1deg discretization step for the positioner coordinate, the results obtained are as follows:

No. of Task Locations	Travelling Time
127	3.0sec
200	3.2sec





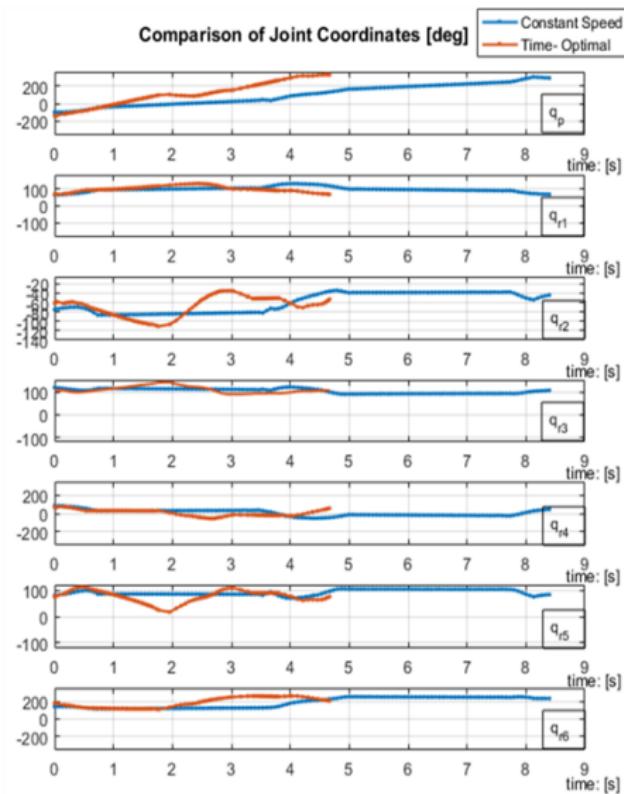


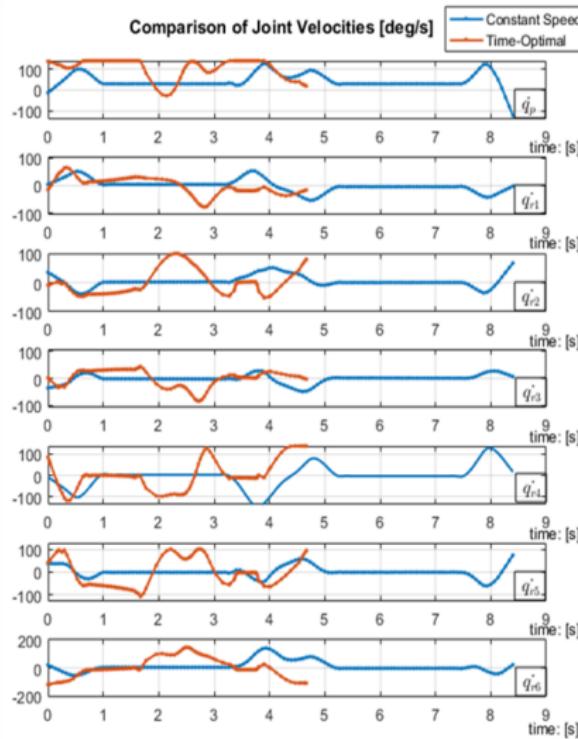
Trajectory with 127 task locations:

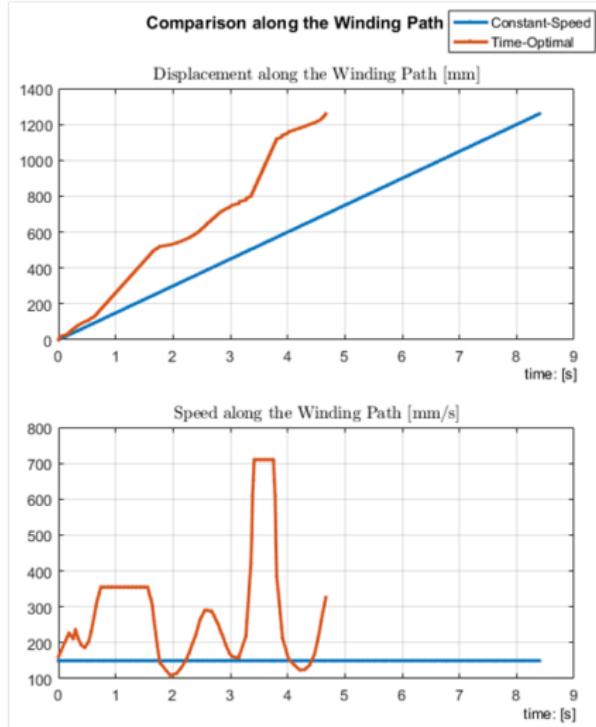
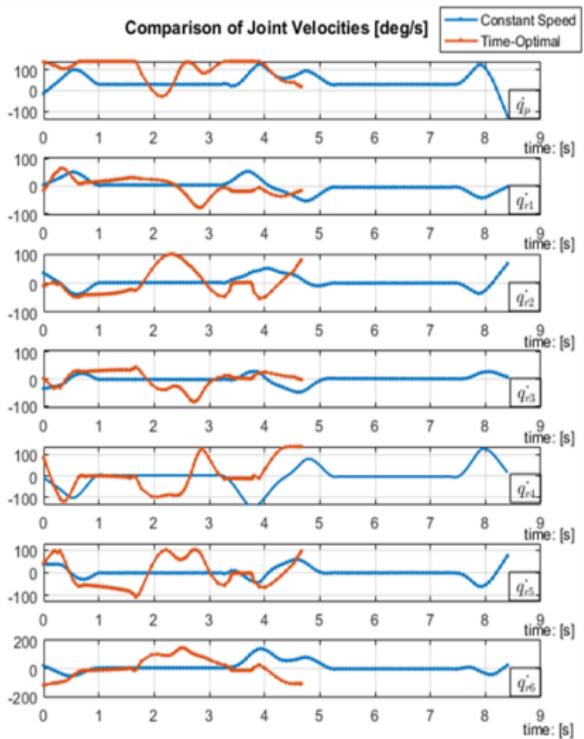
Trajectory with 200 task locations:

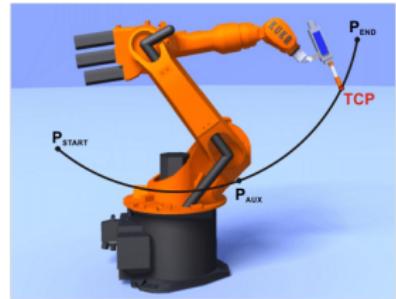
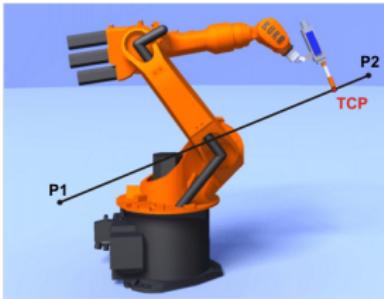
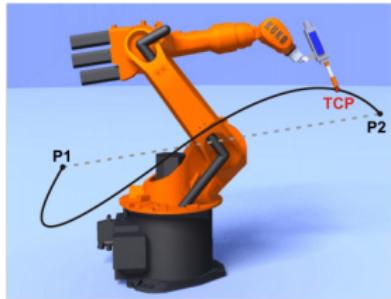
For 127 task locations, linear axis coordinate value of -3000mm and with a 2deg discretization step for the positioner coordinate, the results obtained are as follows:

Objective Function	Travelling Time
Constant Speed	8.4sec
Time-Optimal	4.7sec







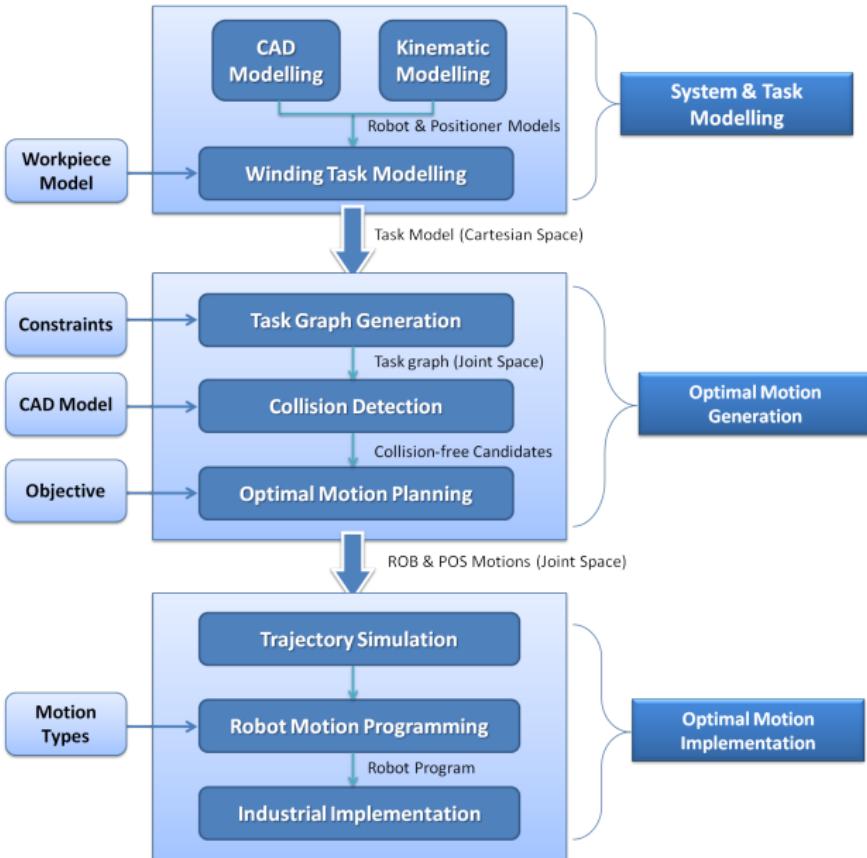


KUKA System Software 8.2, Operating and Programming Instructions for System Integrators (2011).

PTP	LIN/CIRC	SPLINE
Discrete start-stop movement	Continuous movement	Continuous movement
Joint space interpolation	Cartesian space interpolation	Both
Exact positioning	Approximate positioning	Exact positioning
Does not allow time adjustment	Does not allow time adjustment	Allows time adjustment

- 1 Introduction
- 2 Automated Tape Winding Process
- 3 SPIDE-TP Platform
- 4 System & Task Modelling
- 5 Optimal Trajectory Generation
- 6 Optimal Motion Implementation
- 7 Conclusions

Overall Schematic



- Development of CAD model to complement the computational algorithm.
- Intensive and robust collision detection.
- Time-optimal trajectories for the system.
- Simulation results show reduction of processing time by **75%**.
- The methodology will be presented and published at *The 3rd International Conference on Mechanical Engineering (ICOME), 2017*, to be held in Surabaya, Indonesia; on October 5th-6th, 2017.

- Development of CAD model to complement the computational algorithm.
- Intensive and robust collision detection.
- Time-optimal trajectories for the system.
- Simulation results show reduction of processing time by 75%.
- The methodology will be presented and published at *The 3rd International Conference on Mechanical Engineering (ICOME), 2017*, to be held in Surabaya, Indonesia; on October 5th-6th, 2017.

- Development of CAD model to complement the computational algorithm.
- Intensive and robust collision detection.
- Time-optimal trajectories for the system.
- Simulation results show reduction of processing time by 75%.
- The methodology will be presented and published at *The 3rd International Conference on Mechanical Engineering (ICOME), 2017*, to be held in Surabaya, Indonesia; on October 5th-6th, 2017.

- Development of CAD model to complement the computational algorithm.
- Intensive and robust collision detection.
- Time-optimal trajectories for the system.
- Simulation results show reduction of processing time by **75%**.
- The methodology will be presented and published at *The 3rd International Conference on Mechanical Engineering (ICOME), 2017*, to be held in Surabaya, Indonesia; on October 5th-6th, 2017.

- Development of CAD model to complement the computational algorithm.
- Intensive and robust collision detection.
- Time-optimal trajectories for the system.
- Simulation results show reduction of processing time by **75%**.
- The methodology will be presented and published at *The 3rd International Conference on Mechanical Engineering (ICOME), 2017*, to be held in Surabaya, Indonesia; on October 5th-6th, 2017.

- Testing for trajectories with different geometries and complexities.
- For workpiece liners with large lengths, use of linear axis on-line (8 DOF).
- Appropriate calibration methods to eliminate dimensional inaccuracy.
- Ways to reduce computing time, especially in collision detection.
- Optimizing the workpiece placement or the cell layout.

- Testing for trajectories with different geometries and complexities.
- For workpiece liners with large lengths, use of linear axis on-line (8 DOF).
- Appropriate calibration methods to eliminate dimensional inaccuracy.
- Ways to reduce computing time, especially in collision detection.
- Optimizing the workpiece placement or the cell layout.

- Testing for trajectories with different geometries and complexities.
- For workpiece liners with large lengths, use of linear axis on-line (8 DOF).
- Appropriate calibration methods to eliminate dimensional inaccuracy.
- Ways to reduce computing time, especially in collision detection.
- Optimizing the workpiece placement or the cell layout.

- Testing for trajectories with different geometries and complexities.
- For workpiece liners with large lengths, use of linear axis on-line (8 DOF).
- Appropriate calibration methods to eliminate dimensional inaccuracy.
- Ways to reduce computing time, especially in collision detection.
- Optimizing the workpiece placement or the cell layout.

- Testing for trajectories with different geometries and complexities.
- For workpiece liners with large lengths, use of linear axis on-line (8 DOF).
- Appropriate calibration methods to eliminate dimensional inaccuracy.
- Ways to reduce computing time, especially in collision detection.
- Optimizing the workpiece placement or the cell layout.



Advanced Robotics



Thank You!!!

divya-haresh.shah@eleves.ec-nantes.fr