

MHD LIMIT CALCULATIONS

MHD GROUP

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1. TEMPERATURE AND DENSITY PROFILES:

$$(1) \quad n = \bar{n}(1 + \nu_n)(1 - \rho^2)^{\nu_n}$$

$$(2) \quad T = \bar{T}(1 + \nu_T)(1 - \rho^2)^{\nu_T}$$

2. MODEL FOR PLASMA SHAPE

$$(3) \quad \begin{aligned} x &= \sigma(1 - \rho^2) + c_0\rho^4 + c_1\rho \cos(\alpha) + c_2\rho^2 \cos(2\alpha) + c_3\rho^3 \cos(3\alpha) \\ y &= \kappa\rho \sin(\alpha) \end{aligned}$$

$$(4) \quad \begin{aligned} x_{\alpha\alpha} &= 0.3(1 - \delta^2) \\ c_0 &= -\frac{\delta}{2} \\ c_1 &= \frac{1}{8}[9 - 2\delta - x_{\alpha\alpha}] \\ c_2 &= \frac{\delta}{2} \\ c_3 &= \frac{1}{8}[-1 + 2\delta + x_{\alpha\alpha}] \end{aligned}$$

3. ELONGATION κ AND TRIANGULARITY δ

	ITER	ARC	Ignitor	ARIES	FIRE	Mean
Triangularity (δ)	0.33	0.45	0.4	0.5	0.5	0.42
Elongation (κ)	1.7	1.77	1.83	1.7	1.81	1.76

TABLE 1. Triangularity and elongation values for the 5 fusion machines at the 95% flux surface

Chosen parameters:

- $\kappa = 1.8$
- $\delta = 0.45$

4. TROYON β LIMIT CALCULATION

$$(5) \quad \beta = \frac{2\mu_0\bar{p}}{B_p^2 + B_0^2} \approx \frac{2\mu_0\bar{p}}{B_0^2}$$

$$(6) \quad \bar{p} = \frac{\int 2n(\mathbf{r})T(\mathbf{r})d\mathbf{r}}{V}$$

$$(7) \quad \beta_{crit} = \frac{\beta_N I_{MA}}{a B_0}$$

$$(8) \quad \frac{2\mu_0 \bar{p}}{B_0^2} \leq \frac{\beta_N I_{MA}}{a B_0}$$

For a general function $Q(\rho)$.

$$(9) \quad Q_v = 4\pi^2 a^2 \kappa c_1 \int_0^1 Q(\rho) \rho R_0 d\rho + 2\pi^2 a^3 \kappa \int_0^1 Q(\rho) \rho [2c_1(c_2 \rho^2 + 3c_0 \rho^4 - 2\rho^2 \sigma + \sigma) + 3c_2 c_3 \rho^4] d\rho$$

Evaluating the integral for pressure, we have:

$$(10) \quad \bar{p} = 2\bar{n}\bar{T} \frac{(1+\nu_n)(1+\nu_T)}{1+\nu_n+\nu_T} \left(c_1 + \frac{a}{R_0} \frac{6c_0 c_1 + 3c_2 c_3 + c_1(3+\nu_n+\nu_T)(c_2 + \sigma(\nu_n+\nu_T))}{(2+\nu_n+\nu_T)(3+\nu_n+\nu_T)} \right)$$

$$(11) \quad \bar{n}\bar{T} \leq \frac{\beta_N I_{MA} B_0}{4a\mu_0} \frac{(1+\nu_n+\nu_T)}{(1+\nu_n)(1+\nu_T)} \times \left[c_1 + \frac{a}{R_0} \frac{6c_0 c_1 + 3c_2 c_3 + c_1(3+\nu_n+\nu_T)(c_2 + \sigma(\nu_n+\nu_T))}{(2+\nu_n+\nu_T)(3+\nu_n+\nu_T)} \right]^{-1}$$

$$(12) \quad \bar{n}_{20} \bar{T}_k \leq 12.44 \frac{\beta_N I_{MA} B_0}{a} \frac{(1+\nu_n+\nu_T)}{(1+\nu_n)(1+\nu_T)} \times \left[c_1 + \frac{a}{R_0} \frac{6c_0 c_1 + 3c_2 c_3 + c_1(3+\nu_n+\nu_T)(c_2 + \sigma(\nu_n+\nu_T))}{(2+\nu_n+\nu_T)(3+\nu_n+\nu_T)} \right]^{-1}$$

5. KINK STABILITY LIMIT

Assuming as limit $q_\star \geq 2$, the kink stability limit becomes

$$(13) \quad I \leq I_{max} = \frac{\pi a^2 B_0 \kappa}{\mu_0 R_0}$$