

2061 Chapter 7

2062 Planning Future Work for the Model

2063 This model may run and produce interesting results, but there is always more to be
2064 done. This chapter explores three potential fusion reactors that could help guide real
2065 world designs. These are: a stellarator (Ladon), a steady-state/pulsed composite hybrid
2066 (Janus), and a tokamak capable of reaching H, L, and I modes (Daedalus). The
2067 chapter then concludes by describing several possible model improvements, includ-
2068 ing: adding radiation sources, using pedestal profiles, and improving flux balance.

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2073 ~~(Janus), and a tokamak capable of reaching H, L, and I modes (Daedalus).~~

2074 7.1 Incorporating Stellarator Technology – Ladon

2075 A stellarator is, at a basic level, a tokamak helically twisted along the length of its
2076 major circle. For a long time they were dismissed because of their poor transport
2077 properties.~~the difficulty involved in building spiraled magnets.~~ Recent technological
2078 improvements, though, have eased this situation – as seen with the Wendelstein 7-

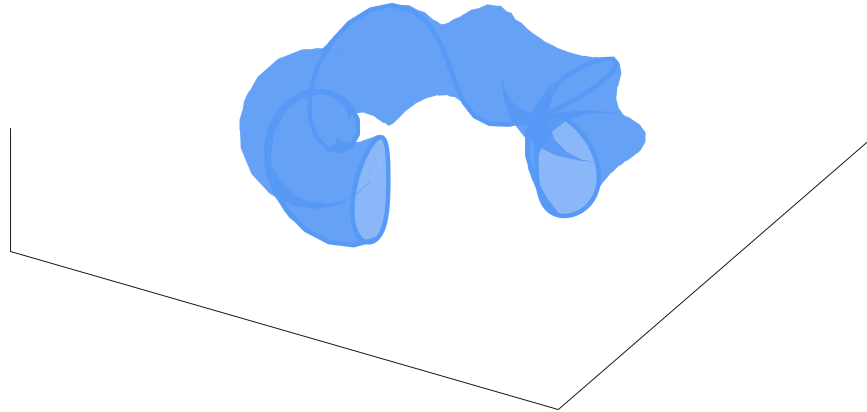
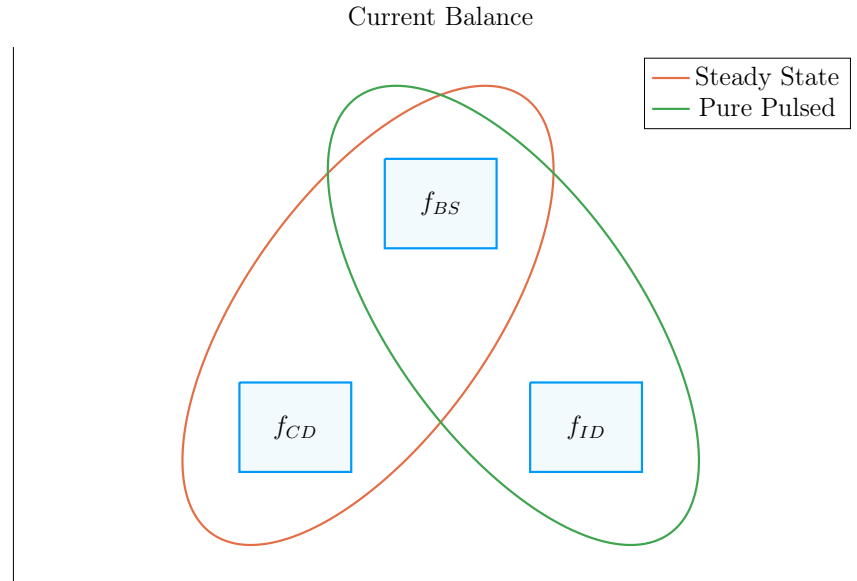


Figure 7-1: Cut-Away of Stellarator Reactor

2079 X device in Germany. The problem now is engrained in the ~~underdeveloped~~~~missing~~
 2080 scaling laws stemming from a lack of machines and, more fundamentally, data points.

2081 To model Ladon, this paper's proposed stellarator, one would need to replace at
 2082 least: the Greenwald density limit and the confinement time scaling law. In place of
 2083 the Greenwald density will likely be some other density or current limit, possibly the
 2084 Bremsstrahlung density limit.³² This may require the density to be carried throughout
 2085 analysis – thus appearing explicitly in one column of Table 5.1.

2086 ~~Optimistically, expanding this model would just involve developing a new confinement~~
 2087 ~~time scaling law and replacing the Greenwald density limit. The reason the Greenwald~~
 2088 ~~density limit is no longer important is because stability is much easier to maintain in~~
 2089 ~~a stellarator. Most likely, the density limit will now be governed by Bremsstrahlung~~
 2090 ~~radiation. If this were the case, each equation would need to be redivided using it.~~
 2091 ~~Ladon would be the reactor built using this enhancement.~~



In a tokamak, there needs to be a certain amount of current – and that current has to come from somewhere. All good reactors have an adequate bootstrap current. What provides the remaining current is what distinguishes steady state from pulsed operation.

2092 7.2 Making a CompositeHybrid Reactor – Janus

2093 The next interesting reactor would be a ~~composite~~hybrid tokamak incorporating
 2094 pulsed and steady-state operation: Janus. Fundamentally, this would involve cur-
 2095 rent coming from both LHCD (steady-state), as well as inductive (pulsed) sources.
 2096 This was actually used in Demo Pulsed, but the current drive was not handled self-
 2097 consistently. Coupling these two current sources could reduce reliance on bootstrap
 2098 current and lead to much more compact machines.

2099 The arguments against this are mainly technical: why build two difficult auxiliary
 2100 systems when one is needed – especially when they probably work against each other.
 2101 Although rational, it may turn out that the larger current achievable with two sources
 2102 leads to a smaller, more economic machine.~~the argument implicitly assumes a current~~
 2103 ~~is achievable through only one source (i.e. either through LHCD or from a central~~
 2104 ~~solenoid). Using two may allow for stronger plasma currents.~~

2105 7.3 Bridging Confinement Scalings – Daedalus

2106 The final potential reactor – Daedalus – is designed ~~so that it can beto collect as~~
 2107 ~~many scaling laws as possible. As a baseline, it should be able to~~ run in H-Mode,
 2108 L-Mode, and I-Mode. Because L-Mode is available on any machine, the first step is
 2109 ~~actually~~ building under H-Mode. The goal then is to find reactors that can also reach
 2110 I-Mode – ~~simultaneouslythus~~ improving the scaling law’s fit and ~~possibly~~ making the
 2111 actual reactor more ~~economiceost effective~~.

2112 Presented below are the three confinement scaling laws, as well as the generalized
 2113 formula. As should be noted, the I-Mode scaling currently lacks a true radial de-
 2114 pendence – as it has only been found on two machines. This is one reason Daedalus
 2115 would be so valuable.

$$\tau_E^G = K_\tau H \frac{I_P^{\alpha_I} R_0^{\alpha_R} a^{\alpha_a} \kappa^{\alpha_\kappa} \bar{n}^{\alpha_n} B_0^{\alpha_B} A^{\alpha_A}}{P_{src}^{\alpha_P}} \quad (3.26)$$

$$\tau_E^H = 0.145 H \frac{I_P^{0.93} R_0^{1.39} a^{0.58} \kappa^{0.78} \bar{n}^{0.41} B_0^{0.15} A^{0.19}}{P_{src}^{0.69}} \quad (3.28)$$

2116

$$\tau_E^L = 0.048 H \frac{I_P^{0.85} R_0^{1.2} a^{0.3} \kappa^{0.5} \bar{n}^{0.1} B_0^{0.2} A^{0.5}}{P_{src}^{0.5}} \quad (7.1)$$

2117

$$\tau_E^I = \frac{0.014 H}{0.68^{\lambda_R} \cdot 0.22^{\lambda_a}} \cdot \frac{I_P^{0.69} R_0^{\lambda_R} a^{\lambda_a} \kappa^{0.0} \bar{n}^{0.17} B_0^{0.77} A^{0.0}}{P_{src}^{0.29}} \quad (7.2)$$

2118

$$\lambda_R + \lambda_a = 2.2 \quad (7.3)$$

2119 A final point to make is reemphasizing that the I-Mode scaling law is ~~significantly~~
 2120 ~~underdevelopednot battle-tested~~. It is the target of ongoing research at the MIT
 2121 PSFC.

2122 7.4 Addressing Model Shortcomings

2123 Before moving on to the final conclusions, we will give a quick recap of several of the
2124 more overly simplified phenomena in the more audacious simplifications used within
2125 this fusion systems framework. These include: approximating temperature profiles as
2126 simple parabolas, neglecting all radiation except Bremsstrahlung, and handling flux
2127 sources at too basic a level. This list is non-comprehensive, as more sophisticated
2128 analysis would also help: the divertor heat load, the neutron wall loading, etc.

2129 7.4.1 Integrating Pedestal Temperature Profiles

2130 One of the biggest shortcomings of this model is not handling plasma profiles self-
2131 consistently – instead replacing them with simple parabolas. The most dubious simplification
2132 in the code at this point is modeling temperature profiles as parabolas. Although these
2133 parabolas work for densities and L-Mode plasma temperatures, the same cannot be
2134 said about H-Mode temperatures. This is because they have a distinct pedestal region
2135 on the outer edge of the plasma.

2136 The usage of pedestal temperatures – discussed in the appendix – improves two as-
2137 pects of the model: the fusion power and the bootstrap current. These were shown in
2138 the results to be over-calculated and underestimated, respectively. Pedestals, having
2139 a lower core temperature, would decrease the total fusion power. As well, they would
2140 boost bootstrap current due to the quick drop near the plasma’s edge (i.e. they have
2141 a large derivative there).

2142 These improvements could easily be added to the code, because temperature was
2143 addressed as a difficult parameter to handle from the beginning.

2144 7.4.2 Expanding the Radiation Loss Term

2145 The next area that would be improved by more sophisticated theory would be the
2146 radiation loss term. From before, it was pointed out that the Bremsstrahlung ra-

2147 diation was the dominant term within the plasma core and, therefore, provided a
2148 first-order approximation. Drawing the radiation losses closer to real world values
2149 would involve adding line radiation and synchrotron radiation. The former of which
2150 would be needed as high-Z impurities become more important.

2151 7.4.3 Taking Flux Sources Seriously

2152 The final oversimplification in the model deals with the flux sources involved in a
2153 pulsed reactor – existing at almost every level. First, the derivation of flux balance
2154 started with a simple transformer between a solenoid primary and a plasma secondary.

2155 ~~Even this initial step is probably too simple.~~

2156 After we developed an equation for flux balance, we compared it to ones in the
2157 literature (i.e. PROCESS) to build confidence in the model. To draw this equation
2158 closer to theirs, we then added a PF coil contribution a posteriori. This implicitly
2159 ignored coupling between most of the components. Thus leading to another source
2160 of error for the model. Moreover, this formula for PF coil contribution was much
2161 simpler than ones found in other fusion systems codes.

2162 Even though this model may be extremely simple, it does remarkably well at matching
2163 more sophisticated codes – and does so at a much faster pace. These suggestions were
2164 ~~all just ways to account for more realistic physics. draw results closer to real world~~
2165 ~~values.~~

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