

# Control Systems

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**Abstract**—This manual is an introduction to control systems based on GATE problems. Links to sample Python codes are available in the text.

Download python codes using

```
svn co https://github.com/gadepall/school/trunk/
control/codes
```

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## 1 SIGNAL FLOW GRAPH

### 2 GAIN OF FEEDBACK CIRCUITS

#### 2.1 Current Amplifiers

- 2.1.1. For the feedback current amplifier shown in 2.1.1, Draw the Small-Signal Model. Neglect the Early effect in  $Q_1$  and  $Q_2$ .

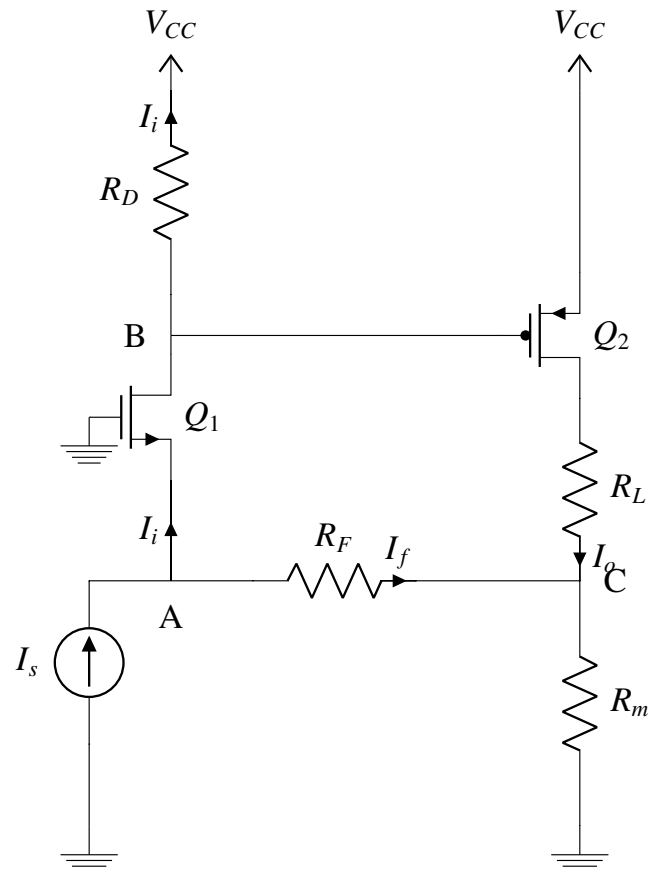


Fig. 2.1.1

**Solution:** While drawing a Small-Signal Model, we ground all constant voltage sources and open all constant current sources. All Small-Signal parameters are obtained from DC-Analysis of the circuit. Neglecting Early effect, in Small-Signal Analysis a N-MOSFET is modelled as a Current Source with value of current equal to  $g_m v_{gs}$  flowing from Drain to

Source. Whereas a P-MOSFET is modelled as a Current Source with value of current equal to  $g_m v_{sg}$  flowing from Source to Drain.

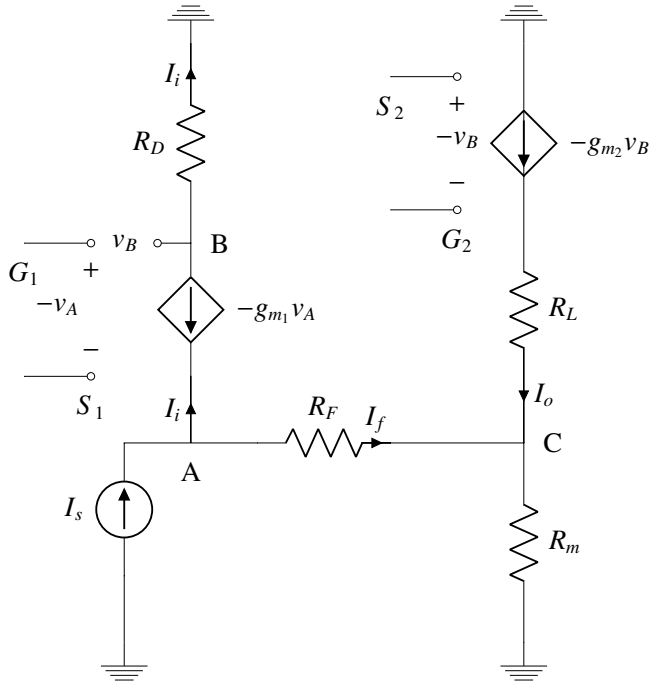


Fig. 2.1.1: Small Signal Model

2.1.2. Describe how the given circuit is a Negative Feedback Current Amplifier.

**Solution:** For the feedback to be negative,  $I_f$  must have the same polarity as  $I_s$ . To ascertain that this is the case, we assume an increase in  $I_s$  and follow the change around the loop: An increase in  $I_s$  causes  $I_i$  to increase and the drain voltage of  $Q_1$  will increase. Since this voltage is applied to the gate of the p-channel device  $Q_2$ , its increase will cause  $I_o$ , the drain current of  $Q_2$ , to decrease. Thus, the voltage across  $R_M$  will decrease, which will cause  $I_f$  to increase. This is the same polarity assumed for the initial change in  $I_s$ , verifying that the feedback is indeed negative.

2.1.3. Write all KVL and KCL Equations

**Solution:**

$$I_i = g_{m1} v_A \quad (2.1.3.1)$$

$$v_B = I_i R_D \quad (2.1.3.2)$$

$$I_o = -g_{m2} v_B \quad (2.1.3.3)$$

$$v_A = I_F R_F - (I_F + I_o) R_M \quad (2.1.3.4)$$

2.1.4. Find the Expression for the Open-Loop Gain

$G = \frac{I_o}{I_i}$ , from the Small-Signal Model. For simplicity, neglect the Early effect in  $Q_1$  and  $Q_2$ .

**Solution:** In Small-Signal Model,

$$v_B = I_i R_D \quad (2.1.4.1)$$

$$v_{gs2} = v_B = I_i R_D \quad (2.1.4.2)$$

In Small-Signal Analysis, P-MOSFET is modelled as a current source where current flows from Source to Drain. So, the value of current flowing from Source to Drain in P-MOSFET is,

$$I_o = -g_{m2} v_{gs2} = -g_{m2} I_i R_D \quad (2.1.4.3)$$

So, the Open-Circuit Gain is

$$G = \frac{I_o}{I_i} = -g_{m2} R_D \quad (2.1.4.4)$$

2.1.5. Find the Expression of the Feedback Factor  $H = \frac{I_f}{I_o}$ , from Small-Signal Model. For simplicity, neglect the Early effect in  $Q_1$  and  $Q_2$ .

**Solution:**

$I_o$  is fed to a current divider formed by  $R_M$  and  $R_F$ . Assuming system has Good Gain, Most part of  $I_s$  flows as  $I_F$  leaving behind small  $I_i$ . As  $I_i$  is small, the voltage at point 'A' is very small and is considered,  $v_A \approx 0$ . So  $R_F$  and  $R_M$  are parallel and Voltage Drop across them is same.

From (2.1.3.4),

$$(I_o + I_f) R_M \approx -I_f R_F \quad (2.1.5.1)$$

$$\frac{I_f}{I_o} \approx -\frac{R_M}{R_F + R_M} \quad (2.1.5.2)$$

So, the Feedback Factor,

$$H \equiv \frac{I_f}{I_o} \approx -\frac{R_M}{R_F + R_M} \quad (2.1.5.3)$$

2.1.6. Find the Expression for the Closed-Loop Gain  $T = \frac{I_o}{I_s}$ . For simplicity, neglect the Early effect in  $Q_1$  and  $Q_2$ .

**Solution:**

From Open-Loop Gain and Feedback Factor,

$$I_s = I_i + I_f \quad (2.1.6.1)$$

$$I_s = \frac{I_o}{G} + HI_o \quad (2.1.6.2)$$

$$GI_s = I_o(1 + GH) \quad (2.1.6.3)$$

$$\frac{I_o}{I_s} = \frac{G}{1 + GH} \quad (2.1.6.4)$$

$$\frac{I_o}{I_s} = -\frac{g_{m2}R_D}{1 + g_{m2}R_D / \left(1 + \frac{R_F}{R_M}\right)} \quad (2.1.6.5)$$

So the Block Diagram of Feedback Current Amplifier is

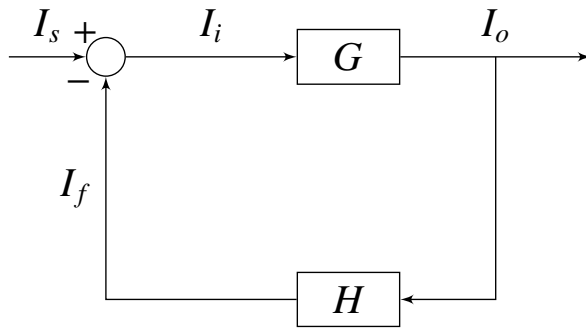


Fig. 2.1.6

where  $G = -g_{m2}R_D$  and  $H = -\frac{R_M}{R_F + R_M}$

So, the value of Closed-Loop Gain is

$$T = \frac{I_o}{I_s} = -\frac{g_{m2}R_D}{1 + g_{m2}R_D / \left(1 + \frac{R_F}{R_M}\right)} \quad (2.1.6.6)$$

### 3 BODE PLOT

#### 4 SECOND ORDER SYSTEM

#### 5 ROUTH HURWITZ CRITERION

#### 6 STATE-SPACE MODEL

#### 7 NYQUIST PLOT

#### 8 COMPENSATORS

#### 9 GAIN MARGIN

#### 10 PHASE MARGIN

#### 11 OSCILLATOR

#### 12 ROOT LOCUS

#### 13 POLAR PLOT

#### 14 PID CONTROLLER