

# Control Systems

G V V Sharma\*

## CONTENTS

<b>1</b>	<b>Signal Flow Graph</b>	<b>1</b>
<b>2</b>	<b>Gain of Feedback Circuits</b>	<b>1</b>
2.1	Current Amplifiers . . . . .	1
<b>3</b>	<b>Bode Plot</b>	<b>4</b>
<b>4</b>	<b>Second order System</b>	<b>4</b>
<b>5</b>	<b>Routh Hurwitz Criterion</b>	<b>4</b>
<b>6</b>	<b>State-Space Model</b>	<b>4</b>
<b>7</b>	<b>Nyquist Plot</b>	<b>4</b>
<b>8</b>	<b>Compensators</b>	<b>4</b>
<b>9</b>	<b>Gain Margin</b>	<b>4</b>
<b>10</b>	<b>Phase Margin</b>	<b>4</b>
<b>11</b>	<b>Oscillator</b>	<b>4</b>
<b>12</b>	<b>Root Locus</b>	<b>4</b>
<b>13</b>	<b>Polar Plot</b>	<b>4</b>
<b>14</b>	<b>PID Controller</b>	<b>4</b>

**Abstract**—This manual is an introduction to control systems based on GATE problems. Links to sample Python codes are available in the text.

Download python codes using

```
svn co https://github.com/gadepall/school/trunk/
control/codes
```

\*The author is with the Department of Electrical Engineering, Indian Institute of Technology, Hyderabad 502285 India e-mail: gadepall@iith.ac.in. All content in this manual is released under GNU GPL. Free and open source.

## 1 SIGNAL FLOW GRAPH

## 2 GAIN OF FEEDBACK CIRCUITS

### 2.1 Current Amplifiers

2.1.1. For the feedback current amplifier shown in 2.1.1, Draw the Small-Signal Model. Neglect the Early effect in  $Q_1$  and  $Q_2$ .

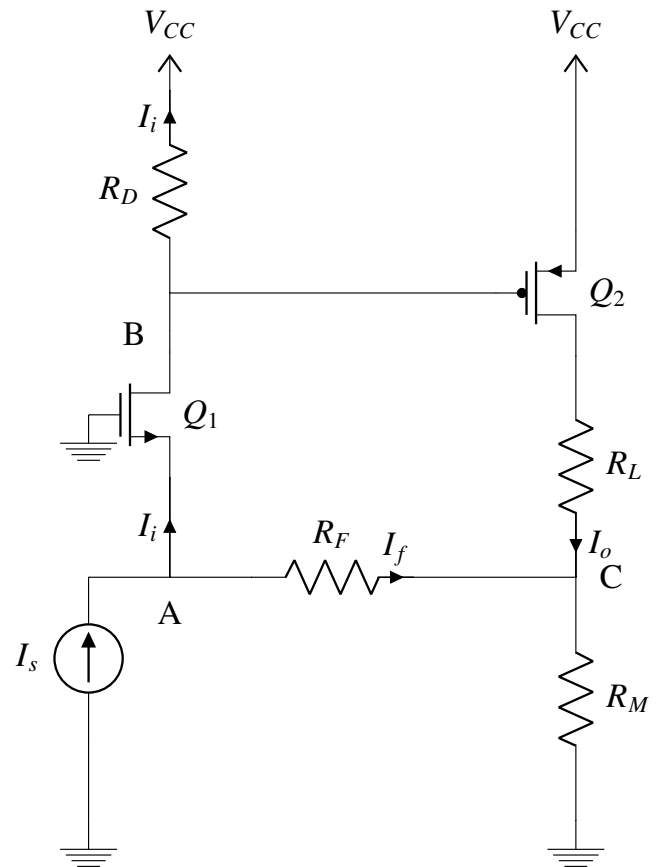


Fig. 2.1.1

**Solution:** While drawing a Small-Signal Model, we ground all constant voltage sources and open all constant current sources. All Small-Signal parameters are obtained from DC-Analysis of the circuit. Neglecting Early effect, in Small-Signal Analysis a N-MOSFET is modelled as a Current Source with value of current equal to  $g_m v_{gs}$  flowing from Drain to

Source. Whereas a P-MOSFET is modelled as a Current Source with value of current equal to  $g_m v_{sg}$  flowing from Source to Drain.

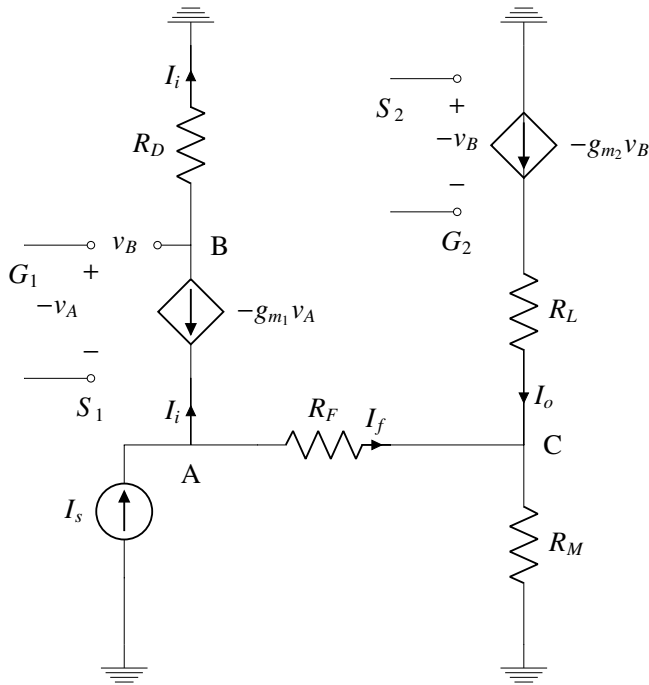


Fig. 2.1.1: Small Signal Model

2.1.2. Describe how the given circuit is a Negative Feedback Current Amplifier.

**Solution:** For the feedback to be negative,  $I_f$  must have the same polarity as  $I_s$ . To ascertain that this is the case, we assume an increase in  $I_s$  and follow the change around the loop: An increase in  $I_s$  causes  $I_i$  to increase and the drain voltage of  $Q_1$  will increase. Since this voltage is applied to the gate of the p-channel device  $Q_2$ , its increase will cause  $I_o$ , the drain current of  $Q_2$ , to decrease. Thus, the voltage across  $R_M$  will decrease, which will cause  $I_f$  to increase. This is the same polarity assumed for the initial change in  $I_s$ , verifying that the feedback is indeed negative.

2.1.3. Write all KVL and KCL Equations

**Solution:**

$$I_i = g_{m1} v_A \quad (2.1.3.1)$$

$$v_B = I_i R_D \quad (2.1.3.2)$$

$$I_o = -g_{m2} v_B \quad (2.1.3.3)$$

$$v_A = I_F R_F - (I_F + I_o) R_M \quad (2.1.3.4)$$

2.1.4. Find the Expression for the Open-Loop Gain

$G = \frac{I_o}{I_i}$ , from the Small-Signal Model. For simplicity, neglect the Early effect in  $Q_1$  and  $Q_2$ .

**Solution:** In Small-Signal Model,

$$v_B = I_i R_D \quad (2.1.4.1)$$

$$v_{gs2} = v_B = I_i R_D \quad (2.1.4.2)$$

In Small-Signal Analysis, P-MOSFET is modelled as a current source where current flows from Source to Drain. So, the value of current flowing from Source to Drain in P-MOSFET is,

$$I_o = -g_{m2} v_{gs2} = -g_{m2} I_i R_D \quad (2.1.4.3)$$

So, the Open-Circuit Gain is

$$G = \frac{I_o}{I_i} = -g_{m2} R_D \quad (2.1.4.4)$$

2.1.5. Find the Expression of the Feedback Factor  $H = \frac{I_f}{I_o}$ , from Small-Signal Model. For simplicity, neglect the Early effect in  $Q_1$  and  $Q_2$ .

**Solution:**

$I_o$  is fed to a current divider formed by  $R_M$  and  $R_F$ . Assuming system has Good Gain, Most part of  $I_s$  flows as  $I_F$  leaving behind small  $I_i$ . As  $I_i$  is small, the voltage at point 'A' is very small and is considered,  $v_A \approx 0$ . So  $R_F$  and  $R_M$  are parallel and Voltage Drop across them is same.

From (2.1.3.4),

$$(I_o + I_f) R_M \approx -I_f R_F \quad (2.1.5.1)$$

$$\frac{I_f}{I_o} \approx -\frac{R_M}{R_F + R_M} \quad (2.1.5.2)$$

So, the Feedback Factor,

$$H \equiv \frac{I_f}{I_o} \approx -\frac{R_M}{R_F + R_M} \quad (2.1.5.3)$$

2.1.6. Find the Expression for the Closed-Loop Gain  $T = \frac{I_o}{I_s}$ . For simplicity, neglect the Early effect in  $Q_1$  and  $Q_2$ .

**Solution:**

From Open-Loop Gain and Feedback Factor,

$$I_s = I_i + I_f \quad (2.1.6.1)$$

$$I_s = \frac{I_o}{G} + HI_o \quad (2.1.6.2)$$

$$GI_s = I_o(1 + GH) \quad (2.1.6.3)$$

$$\frac{I_o}{I_s} = \frac{G}{1 + GH} \quad (2.1.6.4)$$

$$\frac{I_o}{I_s} = -\frac{g_{m2}R_D}{1 + g_{m2}R_D / \left(1 + \frac{R_F}{R_M}\right)} \quad (2.1.6.5)$$

So the Block Diagram of Feedback Current Amplifier is

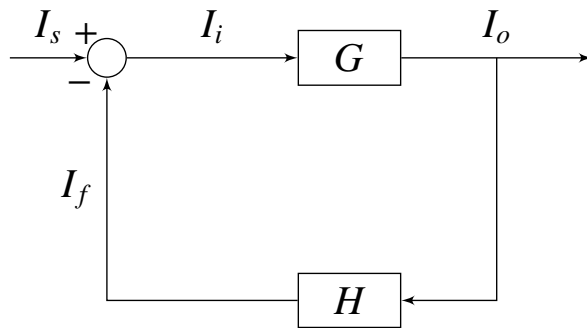


Fig. 2.1.6

where  $G = -g_{m2}R_D$  and  $H = -\frac{R_M}{R_F + R_M}$

So, the value of Closed-Loop Gain is

$$T = \frac{I_o}{I_s} = -\frac{g_{m2}R_D}{1 + g_{m2}R_D / \left(1 + \frac{R_F}{R_M}\right)} \quad (2.1.6.6)$$

2.1.7. Draw the Circuit Diagram of Feedback Network.

**Solution:** The Circuit Diagram of Feedback Network is 2.1.7

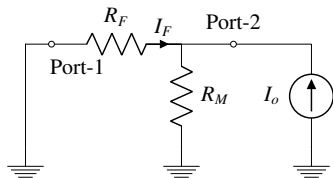


Fig. 2.1.7: Feedback Network

By KVL and KCL,

$$(I_o + I_f)R_M = -I_f R_F \quad (2.1.7.1)$$

$$\frac{I_f}{I_o} = -\frac{R_M}{R_F + R_M} \quad (2.1.7.2)$$

So, Gain of Feedback Network is

$$H = -\frac{R_M}{R_F + R_M} \quad (2.1.7.3)$$

The Block Diagram of Feedback Network is

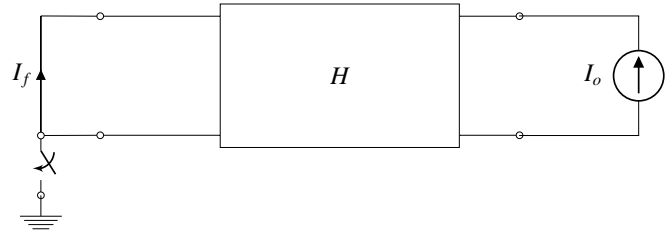


Fig. 2.1.7: Feedback Block Diagram

2.1.8. Find  $R_{11}$  and  $R_{22}$  of Feedback Network where  $R_{11}$  is input resistance through Port-1 and  $R_{22}$  is Input Resistance through Port-2.

**Solution:**

While calculating  $R_{11}$ , Port-2 should be Opened. So, Net-Resistance seen through Port-1 is

$$R_{11} = R_F + R_M \quad (2.1.8.1)$$

While calculating  $R_{22}$ , Port-1 should be Shorted. So, Net-Resistance seen through Port-2 is

$$R_{22} = R_F || R_M \quad (2.1.8.2)$$

$$R_{22} = \frac{R_F R_M}{R_F + R_M} \quad (2.1.8.3)$$

So,

$$R_{11} = R_F + R_M \quad (2.1.8.4)$$

$$R_{22} = \frac{R_F R_M}{R_F + R_M} \quad (2.1.8.5)$$

$R_{11}$	$R_{22}$
$R_F + R_F$	$\frac{R_F R_M}{R_F + R_M}$

TABLE 2.1.8

2.1.9. Draw the Circuit Diagram of Open-Loop Network.

**Solution:**

As the circuit is Shunt-Series Topology,  $R_{11}$  is shunted across the Input Terminal and  $R_{22}$  is added in series to Output Terminal.

Current Flowing through  $R_D$  is approximately same as  $I_i$ , as  $R_F$  is a Large Resistance.

The Circuit Diagram of Open-Loop Network is 2.1.9

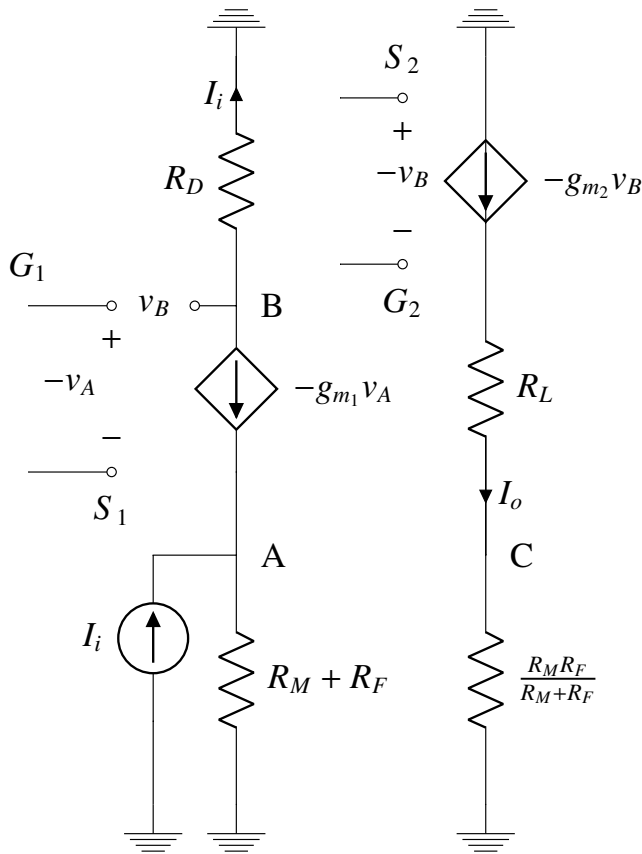


Fig. 2.1.9: Open-Loop Network

By KVL and KCL,

$$v_B = I_i R_D \quad (2.1.9.1)$$

$$v_{gs2} = v_B = I_i R_D \quad (2.1.9.2)$$

$$I_o = -g_{m2} v_{gs2} = -g_{m2} I_i R_D \quad (2.1.9.3)$$

$$\frac{I_o}{I_i} = -g_{m2} R_D \quad (2.1.9.4)$$

So, Open-Loop Gain is

$$G = \frac{I_o}{I_i} = -g_{m2} R_D \quad (2.1.9.5)$$

The Block Diagram of Open-Loop Network is

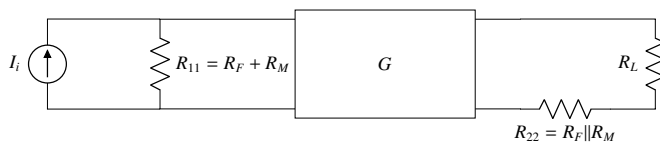


Fig. 2.1.9: Open-Loop Block Diagram

### 3 BODE PLOT

#### 4 SECOND ORDER SYSTEM

#### 5 ROUTH HURWITZ CRITERION

#### 6 STATE-SPACE MODEL

#### 7 NYQUIST PLOT

#### 8 COMPENSATORS

#### 9 GAIN MARGIN

#### 10 PHASE MARGIN

#### 11 OSCILLATOR

#### 12 ROOT LOCUS

#### 13 POLAR PLOT

#### 14 PID CONTROLLER