

# Real-Time Digital Signal Processing : Lab 5 - Real-time Implementation of IIR Filters

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# 1 Objectives

- Learn to design IIR filters using Matlab
- Implement the IIR filters using the C6713 DSK system in real-time
- Measure the filter characteristics using a netowkr or spectrum analyzer

# 2 Equipment

- Spectrum Digital DSK-EVM-eZdsp onboard USB Emulator(DSK6713)
- Oscilloscope
- Software signal generator
- APX520 audio analyzer

# 3 IIR Filter

IIR filter has a difference equation shown below. Current output is a weighted sum of current and previous M inputs and of previous N outputs. This is different from FIR filters such that IIR filters can not only have zeroes anywhere (determined by coefficients b) but also poles anywhere (determined by coefficients a). As a result, IIR filters are not inherently stable with the feedback present and become unstable when any pole is outside the unit circle on z plane.

$$y(n) = \sum_{k=0}^M b(k)x(n-k) - \sum_{k=1}^N a(k)y(n-k)$$

Taking Z-transform of difference equation would produce the transfer function below. Intuitively, for a given order, IIR filter can have sharper roll off and narrower transition band compared to FIR filter by placing poles adjacent to zeroes that are closer to the unit circle at either side of the transition band. This is because poles close to the unit circle can pull gain magnitude up to infinity while zeroes close to the unit circle drag it down close to zero. If the poles and zeros are close enough, the gain is kept at approximately one before reaching passband edge frequencies, because the product of distance from those zeros is approximately equal to the product of distance from those poles, hence a sharp narrower transition band or wider pass band could be achieved. However, it is impossible for IIR filters to have a linear phase response.

$$H(z) = \frac{b_0 + b_1 z^{-1} + \dots + b_M z^{-M}}{1 + a_1 z^{-1} + a_2 z^{-2} + \dots + a_N z^{-N}}$$

# 4 Single-Pole Filter

To implement **digital IIR filter design**, it is better to first design the filter in continuous time, then convert it to discrete time. There are standard analogue filters, such as Butterworth and Elliptic filters, of which coefficients can be found through a look-up table for a given performance. Note the transfer function of a continuous-time filter is described in Laplace domain  $s$ , where multiplying  $e^{-sT_s}$  delays the signal by  $T_s$ . The equivalent in discrete time is multiplying  $z^{-1}$  in z domain, therefore we can write:

$$z = e^{sT_s} \implies s = \frac{1}{T_s} \ln(z)$$

An approximation of the series expansion of the logarithm leads to:

$$\begin{aligned}
s &= \frac{1}{T_s} \ln(z) \\
&= \frac{2}{T_s} \left[ \frac{z-1}{z+1} + \frac{1}{3} \left( \frac{z-1}{z+1} \right)^3 + \frac{1}{5} \left( \frac{z-1}{z+1} \right)^5 + \frac{1}{7} \left( \frac{z-1}{z+1} \right)^7 + \dots \right] \\
&\approx \frac{2}{T_s} \frac{z-1}{z+1}
\end{aligned}$$

The mapping between the analogue and digital frequencies by the bilinear transform is not linear. In other words, the relationship between analogue and digital frequencies should be:

$$w_a = w_d \quad \text{both in radians per second}$$

However, in the bilinear transform:

$$\begin{aligned}
jw_a &= \frac{2}{T_s} \frac{e^{jw_d T_s} - 1}{e^{jw_d T_s} + 1} \\
&= \frac{2}{T_s} \frac{e^{j \frac{w_d T_s}{2}} - e^{-j \frac{w_d T_s}{2}}}{e^{j \frac{w_d T_s}{2}} + e^{-j \frac{w_d T_s}{2}}} \\
&= j \frac{2}{T_s} \frac{(e^{j \frac{w_d T_s}{2}} - e^{-j \frac{w_d T_s}{2}})/2j}{(e^{j \frac{w_d T_s}{2}} + e^{-j \frac{w_d T_s}{2}})/2} \\
&= j \frac{2}{T_s} \frac{\sin(w_d T_s/2)}{\cos(w_d T_s/2)} \\
&= j \frac{2}{T_s} \tan(w_d T_s/2) \\
\Rightarrow w_a &= \frac{2}{T_s} \tan(w_d T_s/2)
\end{aligned}$$

The two frequencies are almost equal for small  $w_d T_s$  since  $\lim_{w_d T_s \rightarrow 0} \tan(w_d T_s/2) \approx \frac{w_d T_s}{2}$ . Therefore, the higher the sampling frequency (smaller the  $T_s$ ), the better the approximation.

#### 4.1 Coefficients Calculation

Given an analogue low-pass filter:

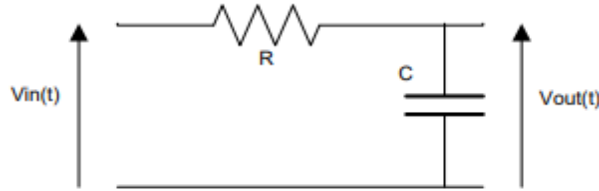


Figure 1: RC low pass filter with  $R = 1k\Omega$  and  $C = 1\mu F$

Since in this case the cut-off frequency:

$$f_c = \frac{1}{2\pi RC} = \frac{1}{2\pi 10^{-3}} \approx 159.15 Hz \ll f_s = 8kHz$$

a good approximation can be achieved by converting it to discrete time using bilinear transform:

$$\begin{aligned}
H_a(s) &= \frac{1/sC}{R + 1/sC} = \frac{1}{sRC + 1} \\
H_d(z) &= H_a(s) \Big|_{s=\frac{2}{T_s} \frac{z+1}{z-1}} \\
&= \frac{1}{RC \frac{2}{T_s+1} \frac{z+1}{z-1}} \\
&= \frac{z+1}{(1-2RCf_s) + (1+2RCf_s)z} \\
&= \frac{1+z^{-1}}{(1-2RCf_s) + (1+2RCf_s)z^{-1}}
\end{aligned}$$

$$R = 1k\Omega \quad C = 1\mu F \quad f_s = 8kHz \quad \implies H(z) = \frac{1/17+1/17z^{-1}}{1-15/17z^{-1}}$$

Coefficients  $b[0] = \frac{1}{17}$ ,  $b[1] = \frac{1}{17}$ ,  $a[0] = 1$ ,  $a[1] = \frac{-15}{17}$  are checked with Matlab and are put into text file called *single\_pole\_coef.txt* with double precision and included in the C program.

```

R = 1000; %Resistor value
C = 10^-6; %Capacitor value
fs = 8000; %Sampling frequency
H = tf([1],[R*C,1]); %Find transfer function of RC filter in s domain
Hd = c2d(H,1/fs,'tustin') %Complete Tustin transform
[b,a] = tfdata(Hd); %Find coefficients in z domain
b = cell2mat(b);
a = cell2mat(a);
%save to single_pole_coef.txt
fileID = fopen('single_pole_coef.txt','w');
formSpec1 = 'double b[]={%.16e';
fprintf(fileID,formSpec1,b(1));
formSpec2 = ', %.16e';
fprintf(fileID,formSpec2,b(2:end));
fprintf(fileID,'};\n');
formSpec3 = 'double a[]={%.16e';
fprintf(fileID,formSpec3,a(1));
fprintf(fileID,formSpec2,a(2:end));
fprintf(fileID,'};\n');
fclose(fileID);

```

Figure 2: Matlab code for bilinear transformation

## 4.2 C Implementation

The implementation of IIR filter in Direct Form I requires two delay lines and two separate adders to perform convolution sum computations. We need two arrays  $v[]$  and  $w[]$  to maintain history of input and output samples in the delay line:

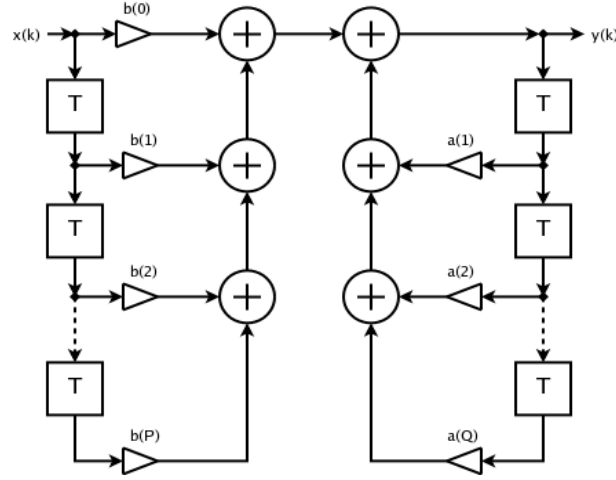


Figure 3: Direct form I

We can dynamically allocate the array sizes based on the length of numerator and denominator coefficient arrays using the function `calloc`. Hence, when filter order alters, we could always create the memory we need without manually changing array length definitions.  $v$  and  $w$  are first defined as pointers to doubles. Assume that  $a[]$  (numerator coefficients, including 1) and  $b[]$  (denominator coefficients) are of the same length.

```
//dynamically allocate array sizes to store input and output samples
order = sizeof(a)/sizeof(a[0]) - 1;
w = (double *) calloc(order+1, sizeof(double)); //dynamic memory, order+1 elements, each of size double
v = (double *) calloc(order+1, sizeof(double));
```

Figure 4: Dynamic allocation of memory

$v$  and  $w$  are now the pointers to the first element of an array of doubles and thus the array can be accessed with normal way of  $v[]$  and  $w[]$ .

The algorithm needs to complete two separate steps when a new input sample arrives: calculate output sample through convolution sum and updating values in 2 delay lines for next iteration. Note that the case of  $i=0$  is handled separately and  $v[0]$  and  $w[0]$  are not used, such that  $b[k]$  can be directly multiplied with  $v[k]$  and  $a[k]$  directly multiplied with  $w[k]$  within the *for* loop. Shifting of samples to represent delay elements are also done within the *for* loop at each iteration, hence avoiding a second *for* loop.  $v[1]$  and  $w[1]$  are updated at the end of the function.

```
void single_pole_IIR(void){
    int k;
    samp = b[0]*sampin; //calculation with b[0] done individually
                        //so within for loop can multiply v[k] with b[k]
                        //and w[k] with a[k]

    for(k = order; k>0; k--){
        samp += v[k]*b[k] - w[k]*a[k]; //perform convolution sum following
                                      //IIR difference equation
        w[k] = w[k-1]; //perform delay for input values stored in v
        v[k] = v[k-1]; //perform delay for output values stored in w
    }
    v[1] = sampin; //update first delayed element v[1], or x(n-1) for next iteration
    w[1] = samp; //update w[1], or y(n-1) for next iteration
}
```

Figure 5: Direct form I Implementation

### 4.3 Results

By driving the input with a square wave of  $140Hz$  with  $V_{pp} < 5.66V$  from the signal generator, we could find the time constant of the filter. Time constant is time taken for the system's step response to reach  $1 - 1/e \approx 63.2\%$  of its final asymptotic value say from a step increase. Frequency of  $140Hz$  is chosen so that it is greater than the cut-off frequency of the output high-pass filter( $7Hz$ ) and it is low enough for the output to reach the final value(steady state) for a single step increase.

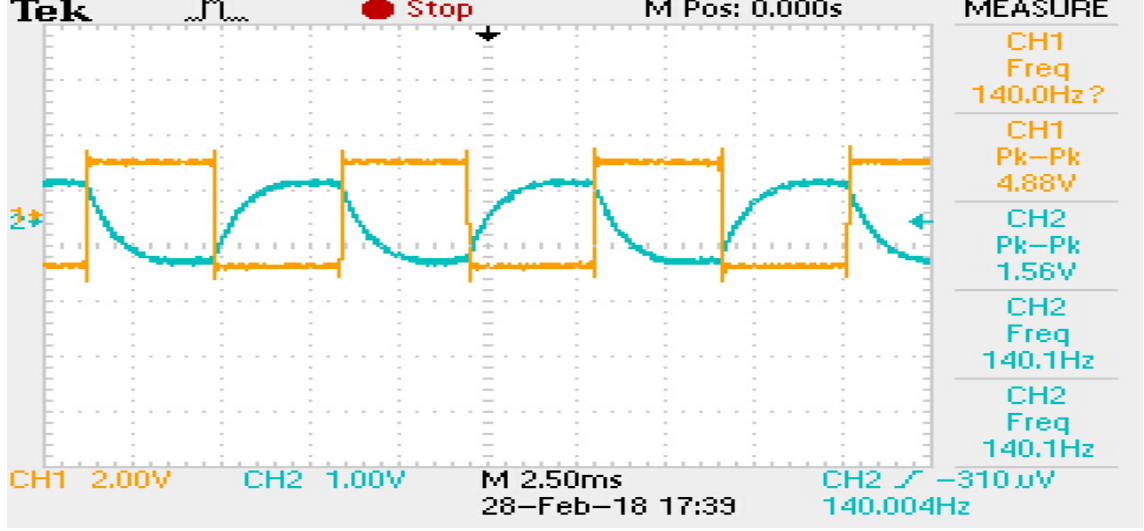


Figure 6: Square wave of  $140Hz$  is applied, output could reach steady state within half of the period

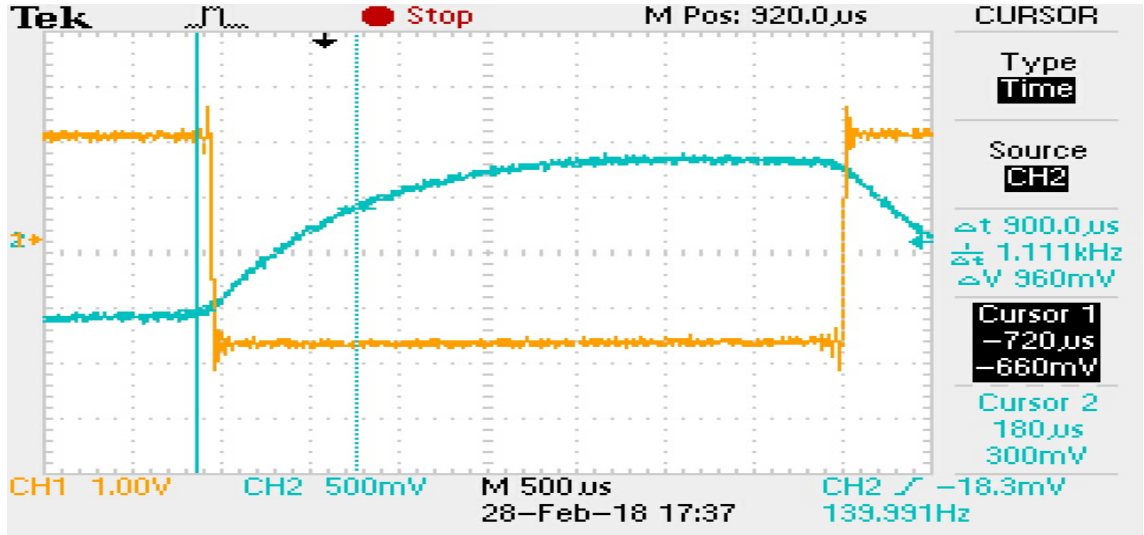


Figure 7: Step response

The time constant measured using oscilloscope is  $\tau_{square\ wave} = 900\mu s$  (measured with cursors).  $\Delta V = 1.56V$ , cursor1 should be situated at  $-660mV + \Delta V \times (1-1/e) = 325.92mV$ , and time constant can be measured. However, this time constant is not accurate since the frequency response is also affected by other filters inside the AIC23 audio chip. In addition, as shown, cursor1 cannot be placed accurately at  $325.92mV$ , hence accuracy is reduced. In the following section, the ideal discrete IIR response is found in MATLAB and time constant extracted using *damp* function.

```

R = 1000; %Resistor value
C = 10^-6; %Capacitor value
fs = 8000; %Sampling frequency
H = tf([1],[R*C,1]); %Find transfer function of RC filter
Hd = c2d(H,1/fs,'tustin') %Complete Tustin transform
[num,den] = tfdata(Hd); %Find coefficients
num = cell2mat(num)
[den] = cell2mat(den)
damp(Hd);

```

Figure 8: Matlab for Plotting Ideal Digital IIR Filter

$$\tau_{IIR,ideal} = 999\mu s$$

The frequency response of the discrete IIR filter and all-pass response are obtained with Audio Precision APX520. To obtain all-pass response, in the ISR the samples are simply read and written out directly, with no filtering applied:

```

void ISR_AIC (void)
{
    // samp = 0; //reset output
    //sampin = mono_read_16Bit();
    //single_pole_IIR();
    //bandpass_direct2_IIR();
    //bandpass_direct2_transposed_IIR();
    //samp = (short)samp; //rounding purpose
    mono_write_16Bit(mono_read_16Bit());
}

```

Figure 9: ISR to obtain all-pass response

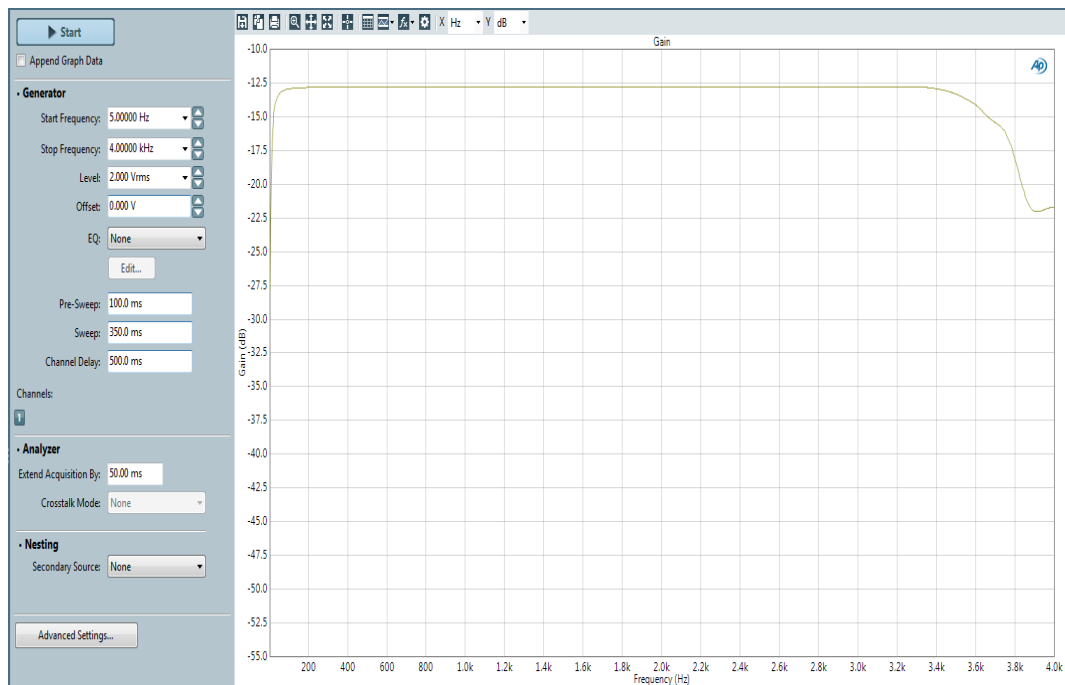


Figure 10: All Pass Magnitude Response

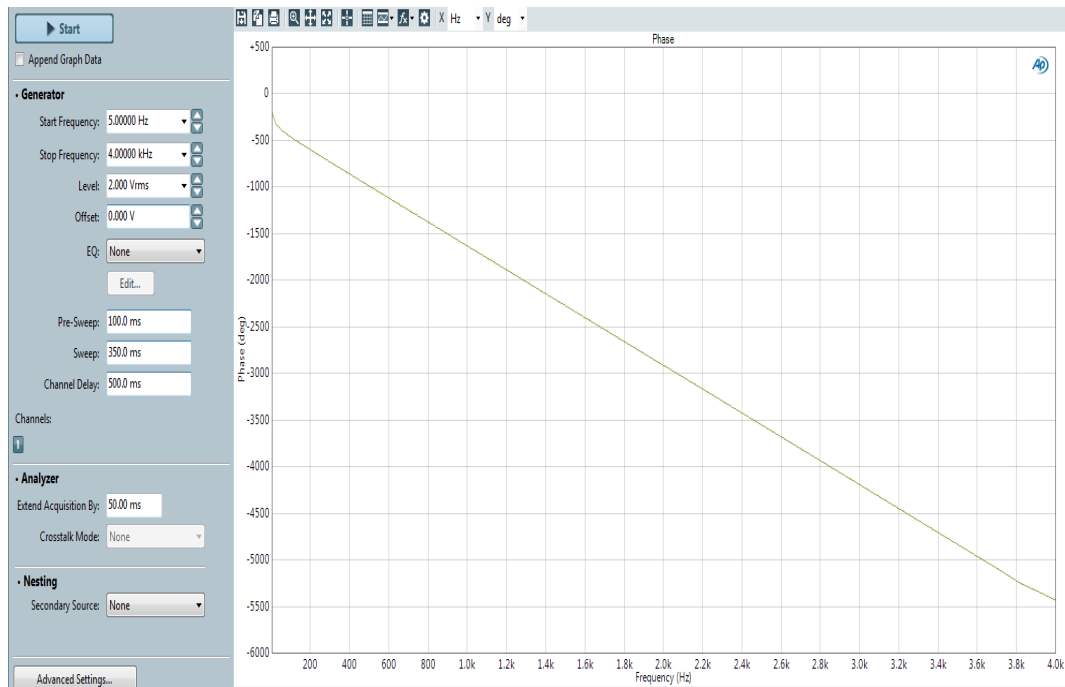


Figure 11: All Pass Phase Response

As mentioned in Lab 4, the gain of  $\frac{1}{4}$  at the input of DSK unit plus some other attenuation introduces an overall attenuation of about -12.9dB. Roll-off at roughly 4kHz can be attributed to anti-aliasing filter and reconstruction filter at the input and output of the AIC23 audio chip respectively, which have cutoff at Nyquist Frequency ( $f_N=4\text{kHz}$ ). Roll-off at small frequencies can be explained by high-pass filter with cut-off at 7Hz at output of Audio Chip. Note that final magnitude response in dBs equals sum of that of series filters.

IIR is applied and frequency response measured again using the same equipment:

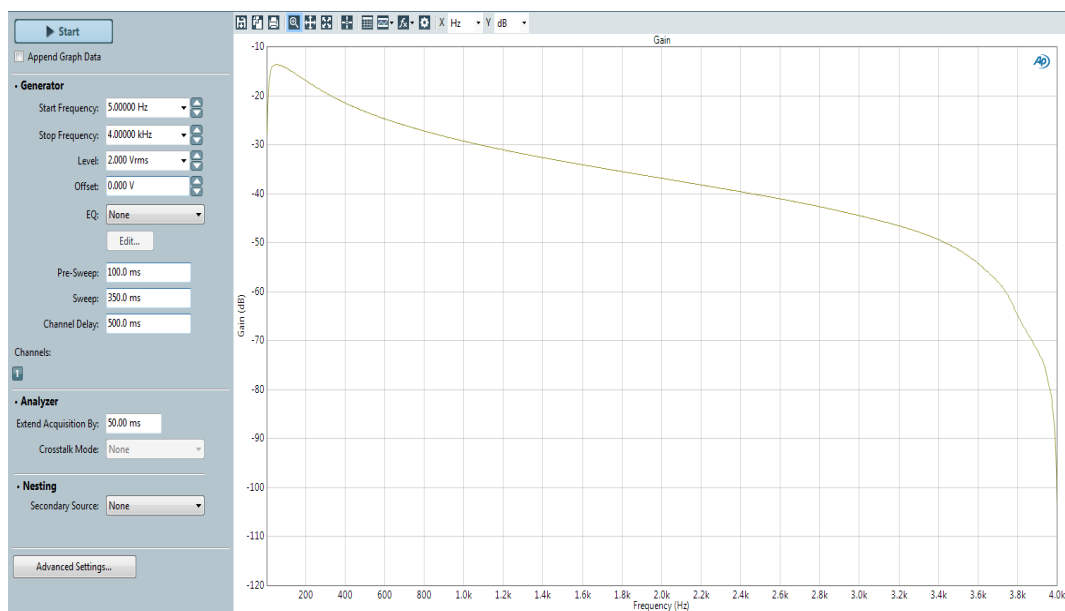


Figure 12: Measured Magnitude Response(IIR Filter Applied)



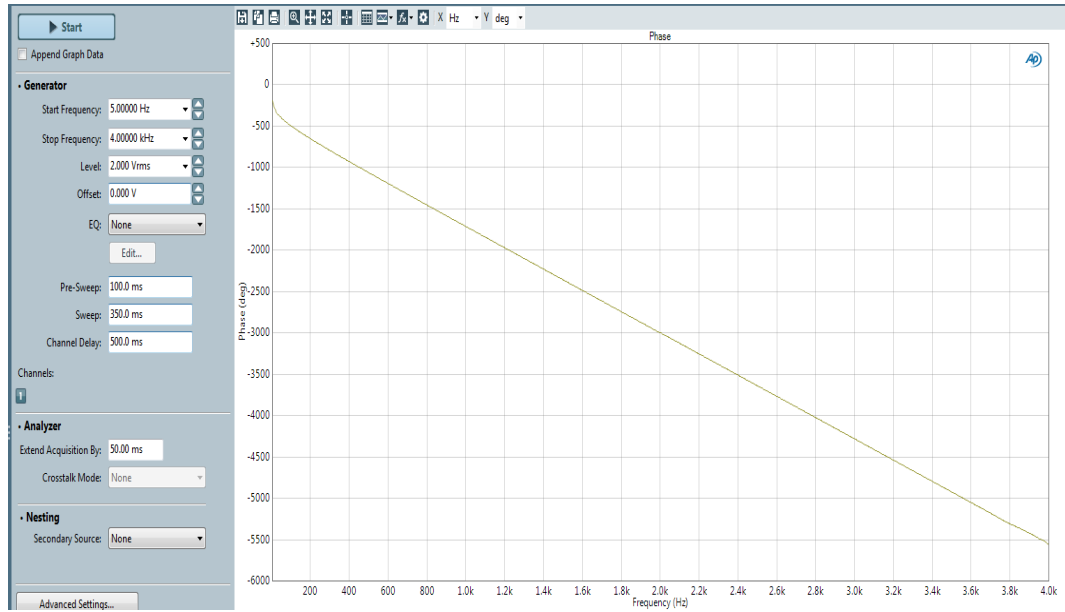


Figure 13: Measured Phase Response(IIR Filter Applied)

By exporting the graph data from APX500 to Matlab, actual discrete IIR filter frequency response is extracted by subtracting all pass response from measured IIR filter response. This is shown below. The time constant of this filter is found:

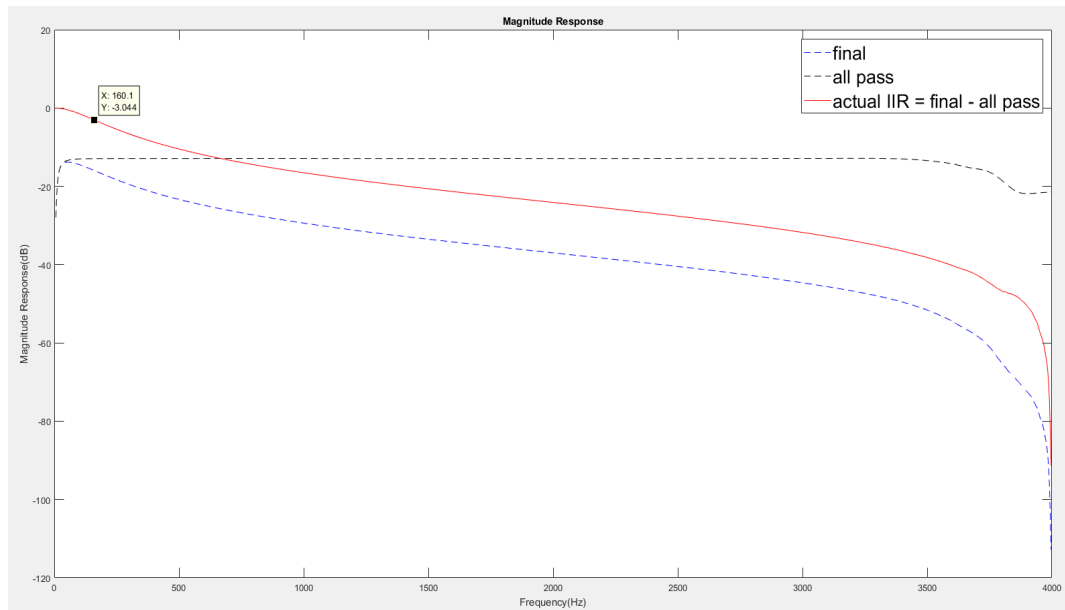


Figure 14: Final response here refers to measured response. Measured response minus all pass response to obtain actual IIR discrete filter response

The extracted actual digital IIR filter frequency response is very close to the ideal digital IIR frequency response given by the Matlab:

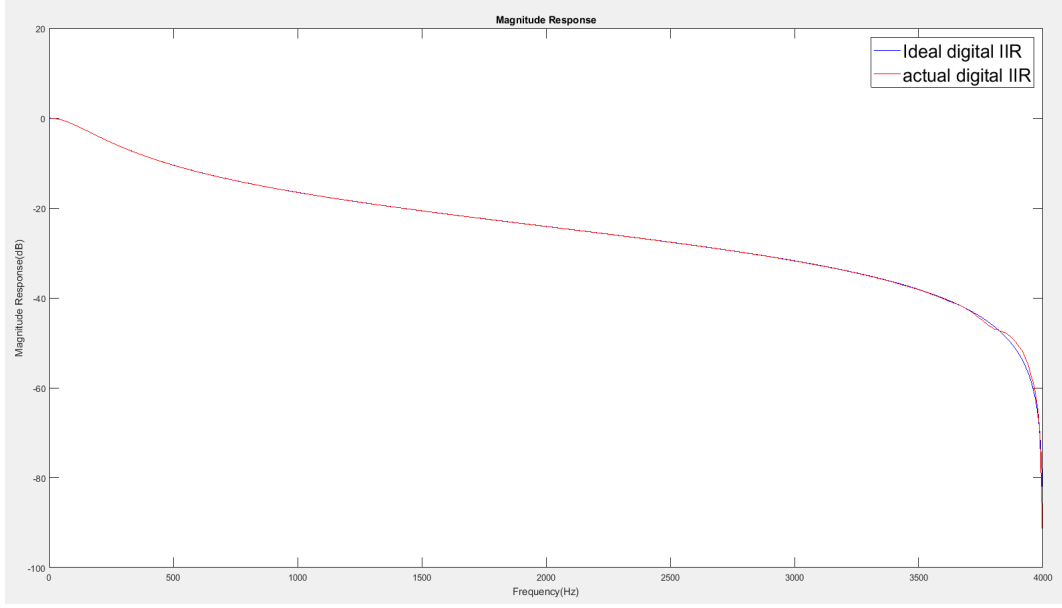


Figure 15: Final Magnitude Response

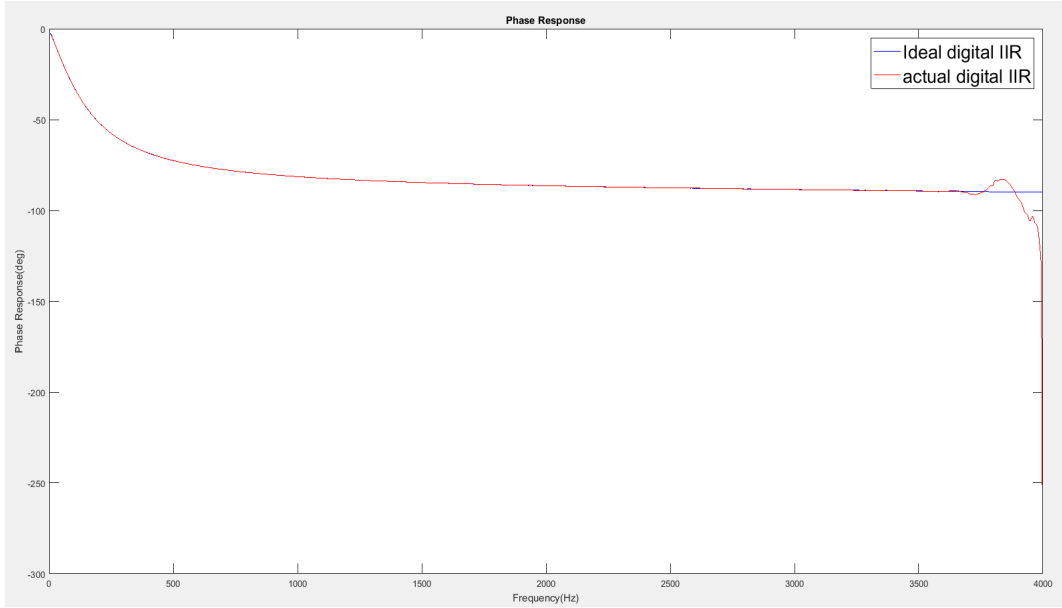


Figure 16: Final Phase Response

Both magnitude and phase response are almost identical to ideal response and only deviates when approaching to the Nyquist Frequency ( $f_N = 4kHz$ ). This might be due to non-ideal anti-aliasing filter inside AIC23 audio chip, where the frequency response above the Nyquist Frequency is non-zero, hence there is small portion of overlap in frequency domain of the reconstructed signal. This explains the deviation, which can be resulted from the magnitude and phase response of aliasing components from the image around  $f_s = 8kHz$  when measuring response using APX500.

Since time constant for a first-order time-invariant system is also equal to  $\tau = \frac{1}{2\pi f_c}$ , where  $f_c$  is the cut-off frequency, or the frequency for which the gain is 3 dB smaller than the nominal pass band value (0 dB). Use the cursor to find the 3dB drop point on the plot,  $f_c = 160.1Hz$ . The actual time constant of the IIR filter implemented on DSK is found to be  $\tau_{IIR,actual} = \frac{1}{2\pi 160.1} = 994\mu s$ . Note that for the RC circuit shown above, analogue measurements are taken:  $f_c = \frac{1}{2\pi RC} = 159.15 Hz$

and  $\tau = RC = 1\text{ ms}$ .

-	Time Constant( $\mu\text{s}$ )	Corner Frequency( $\text{Hz}$ )
Analogue IIR response	1000	159.15
Ideal Digital IIR response (from Matlab)	999	
Actual Digital IIR response (Measured - All Pass)	994	160.1
Measured Digital IIR response (from Audio Precision)	900	

As shown in table, the time constant and the corner frequency of the actual "processed" digital IIR filter are very close to that of the analogue filter, hence in this case we can say that the bilinear transformation gives a good approximation of the analogue filter frequency response. The time constant  $\tau_{\text{square wave}} = 900\mu\text{s}$  measured from oscilloscope deviates a little from that of continuous filter and actual discrete IIR filter, since attenuation within the board and influence from reconstruction/anti-aliasing filters are taken into account.

Comparing the frequency response of analogue and actual discrete IIR filters in Matlab gives us:

```
close all;
R = 1000; %Resistor value
C = 10^-6; %Capacitor value
H = tf([1],[R*C,1]); %Find transfer function of RC filter in s domain
w = f(3:1249).*2.*pi;
[mag,phase,wout] = bode(H,w); %return the value at frequencies specified by vector w(rad/s)
mag = 20.*log10(squeeze(mag(1,1,:))); %absolute value of gain(not in dBs)
phase = squeeze(phase(1,1,:)); %in degrees
```

Figure 17: Matlab code for generating analog filter response

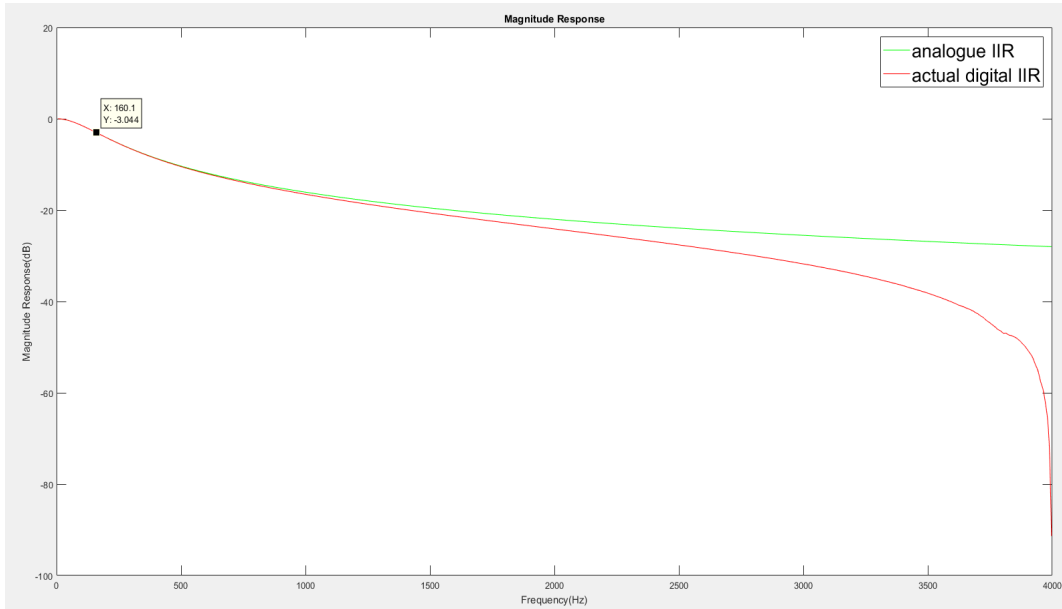


Figure 18: Comparison of Magnitude Response of Analogue and Digital IIR Filters

The gain response of actual discrete IIR filter closely follows that of the analogue IIR filter at low frequency and deviates quite significantly as approaching Nyquist frequency  $f_N$ . Intuitively, one has to recognize that Bilinear transform performs non-linear warping of frequency scales, because an approximation is used during series expansion. In this case of first order low pass filter, in the z domain, an extra zero at  $z = -1$  (corresponding to  $f_N$ ) is introduced in addition to a pole very close to cut-off frequency.

This is straight forward by looking at the bilinear equation,  $s = k \frac{z-1}{z+1}$ , every pole in s domain will give an extra zero at Nyquist Frequency in z domain, since in the process of rearranging we need to multiply both numerator and denominator by  $(z + 1)$ . The larger the difference between cut-off frequency to sampling frequency, the better the approximation of transform. As a result of this extra zero introduced, discrete response rolls off faster when approaching  $f_N$ .

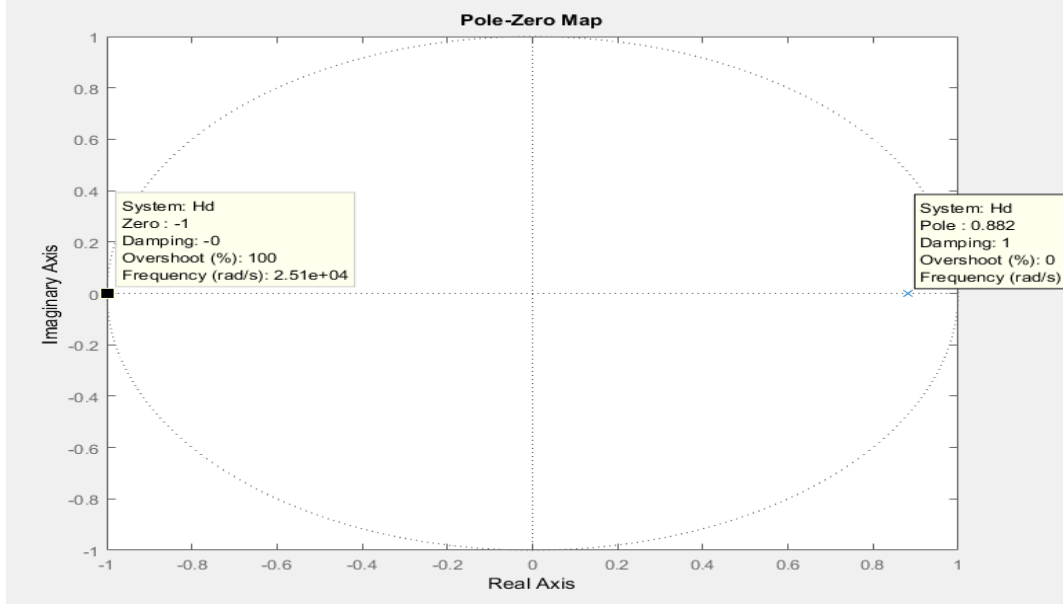


Figure 19: Pole and zero location in z-domain after applying Bilinear Transform

The non-linear mapping is apparent in  $w_a = \frac{2}{T_s} \tan(w_d T_s / 2)$  as  $w_d$  approaches  $2\pi f_N$ .  $\lim_{w_d \rightarrow 2\pi f_N} \frac{2}{T_s} \tan(w_d T_s / 2) = \infty$ . Since gain of analogue filter approaches  $-\infty$  dB as  $w_a$  approaches  $\infty$ . This hence explains the deviation.

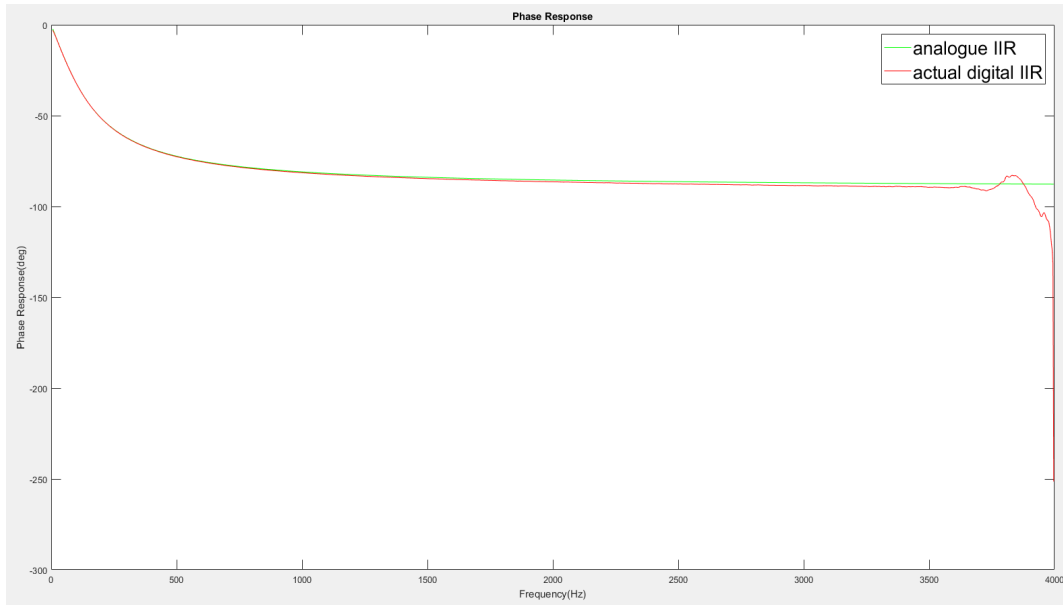


Figure 20: Comparison of Phase Response of Analogue and Digital IIR Filters

The same explanation above can be used to explain the deviation between phase response as  $f_N$  is reached.

## 5 Bandpass Filter: Direct Form II

In this exercise, we will first design a bandpass filter in Matlab to satisfy given specification, then implement it on the DSK using Direct Form II. Measure the frequency response of the digital IIR bandpass filter with APX500 and verify it with the Matlab plot. Finally, we need to find the relationship between number of instruction cycles per sample needed in C implementation and the filter order.

### 5.1 Filter Specification

Order: 4th

Passband edge frequencies =  $[270, 450] \text{ Hz}$

Peak-to-Peak Passband Ripple = 0.3dB

Stopband Attenuation: 20dB

### 5.2 Filter Design

In this case we are designing an elliptic digital bandpass filter using Matlab function *ellip*. It takes input arguments of filter order( $n$ ), peak-to-peak passband ripple( $R_n$ ), stopband attenuation( $R_s$ ) and a vector of passband edge frequencies( $w$ ), and returns the numerator and denominator coefficients of transfer function of the filter with order  $2n$ . The coefficients are then automatically saved into declarations of arrays with double precision into the file *bandpass\_coef.txt* and included in the C program.  $b$  and  $a$  contain the numerator and denominator coefficients(including 1) respectively.

```
close all;
fs = 8000;%sampling frequency
Rn = 0.3;%peak to peak pass band ripple in dB
n = 2;%bandpass filter order = 2n = 4
Rs = 20;%stopband attenuation
w = [270,450].*2./fs;%passband edge frequencies normalized to Nyquist Frequency
[b, a] = ellip (n,Rn,Rs,w , 'bandpass');%return filter coefficients
freqz(b,a,1249,fs);%plot the frequency response
%save filter coefficients into array declarations in bandpass_coef.txt
%with double precision
fileID = fopen('bandpass_coef.txt','w');
formSpec1 = 'double b[]={%.16e';
fprintf(fileID,formSpec1,b(1));
formSpec2 = ', %.16e';
fprintf(fileID,formSpec2,b(2:end));
fprintf(fileID,');\n');
formSpec3 = 'double a[]={%.16e';
fprintf(fileID,formSpec3,a(1));
fprintf(fileID,formSpec2,a(2:end));
fprintf(fileID,');\n');
fclose(fileID);
```

Figure 21: Matlab Code for Bandpass Filter Design

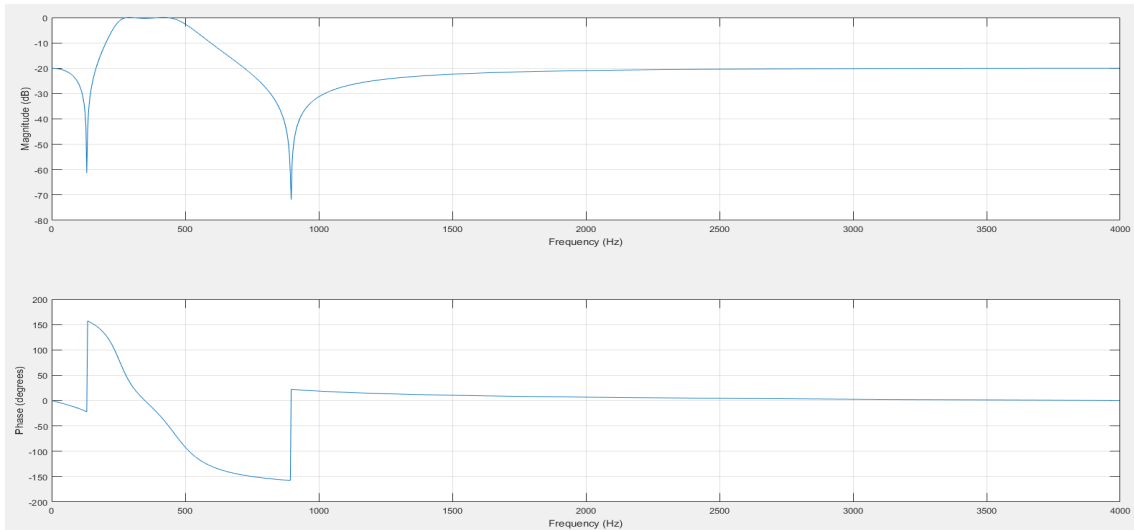


Figure 22: Matlab plot of the Frequency Response

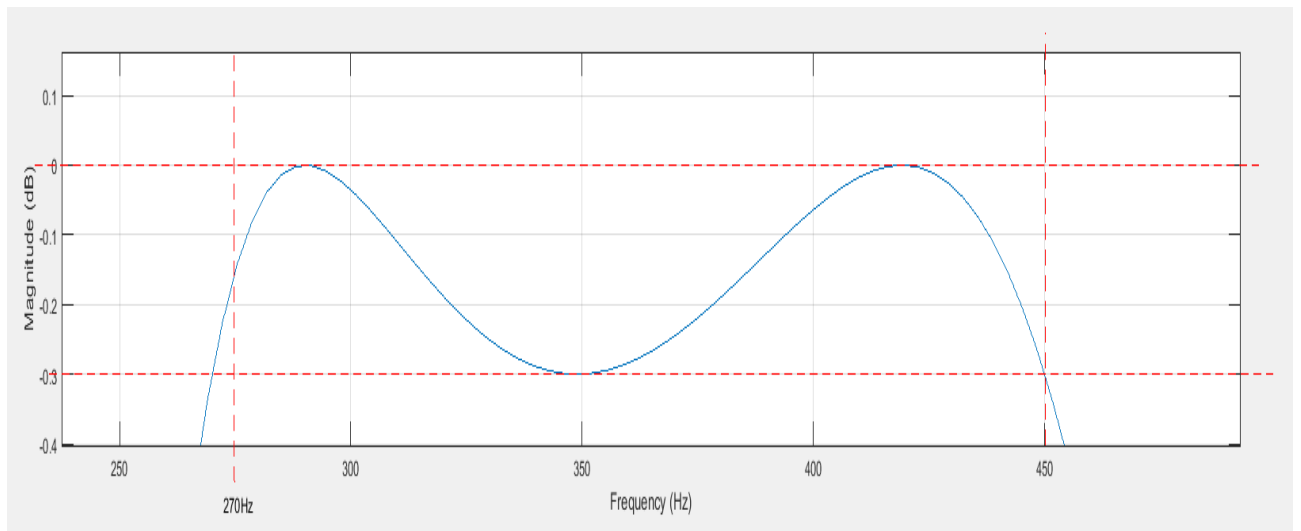


Figure 23: Passband Edge Frequencies and Passband Ripple specifications are satisfied

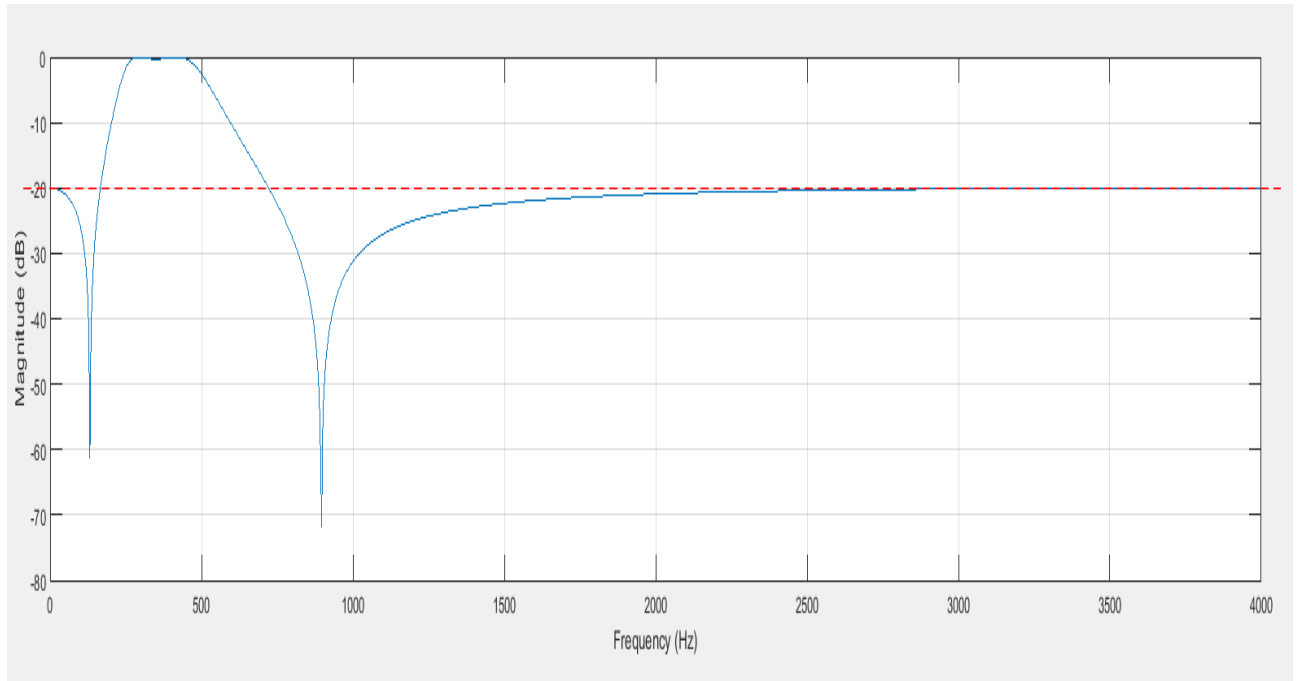


Figure 24: Stopband Attenuation specification is satisfied

An Elliptic filter has ripple in both the pass and stop bands but has the sharpest cut off of all the common filter types. In  $s$  domain, similar to Chebyshev filters, an elliptical filter has poles placed on an ellipse, but in addition it also has zeros placed on the imaginary axis adjacent to poles, which contributes a faster roll-off than Chebyshev filters. Nonetheless, introducing zeros add ripple in the stopband and placing poles on an ellipse close to the axis introduces passband ripple. Since the imaginary axis in  $s$  plane corresponds to the unit circle in  $z$  plane, as we can see from the pole-zero map below, there are four poles in ellipse shape close to unit circle and four zeros on the unit circle outside the pass band pulling the gain to zero.

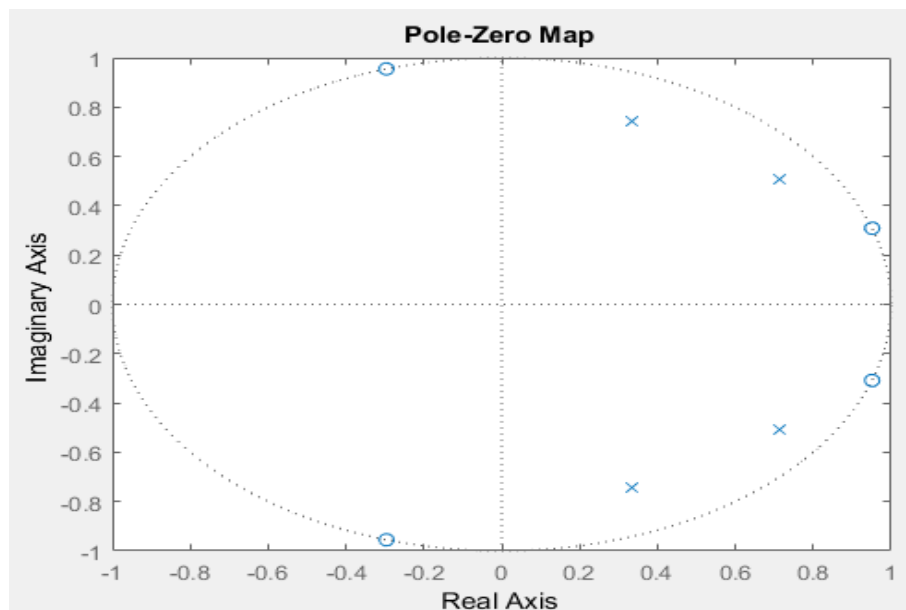


Figure 25: Pole-Zero Pole of the Digital Elliptic Filter

### 5.3 C Implementation

Now we would implement this filter in the Direct Form II. This form is obtained by swapping around the order of the two parts of IIR transfer function (the polynomial in numerator and denominator) and combining the delay line. In terms of implementation, compared to Direct form I, delay units are reduced by half and we only need one array in our C implementation to store delay line values, which is more efficient.

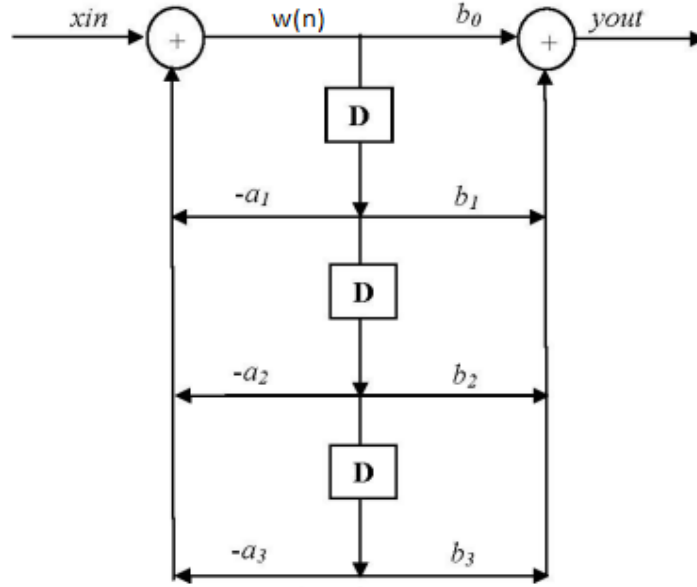


Figure 26: Direct Form II

Define an intermediate state  $w$ , we can say that:

$$w(n) = x(n) - a_1w(n-1) - a_2w(n-2) - \dots - a_Nw(n-N)$$

$$y(n) = b_0w(n) + b_1w(n-1) + b_2w(n-2) + \dots + b_Mw(n-M)$$

In this case  $N = M = 4$  since the filter order is 4. Length of coefficient arrays equals to order + 1. We use *calloc* function again to dynamically allocate the array size as shown in section 4. The algorithm calculates  $w(n)$  and  $y(n)$  step by step inside the *for* loop.  $i$  iterates from *order* to 1 since the current value of  $y$  and  $w$  depend on previous values of  $w$ . At each iteration  $w[i]$  data is shifted to next higher index to represent delay elements. After the *for* loop is finished, the correct value of  $w(n)$  is computed and its product with  $b[0]$  is added to the current output. Note that  $w[0]$  of code below refers to  $w(n)$  of diagram above.

```
void bandpass_direct2_IIR(void){
    int i;
    w[0] = sampin; //write input sample to w[0] (w(n))
    for(i=order; i>0; i--){ //for loop to carry out convolution sum
        //we are not using w[0] yet, so can multiply w[i] with a[i]
        //and b[i]
        w[0] -= a[i]*w[i]; // w[0] (w(n)) =x(n)-a[order]*w[order]-a[order-1]*w[order-1]...
        samp += b[i]*w[i]; //yout = b[order]*w[order]+b[order-1]*w[order-1]...
        w[i] = w[i-1]; //perform delay after the value is used in the calculation
    }
    samp += b[0]*w[0]; //finish output computation since the correct w[0] (w(n)) is ready
}
```

Figure 27: Direct Form II



## 5.4 Results

Measure the frequency response using APX500 audio analyzer. Note that the audio preci

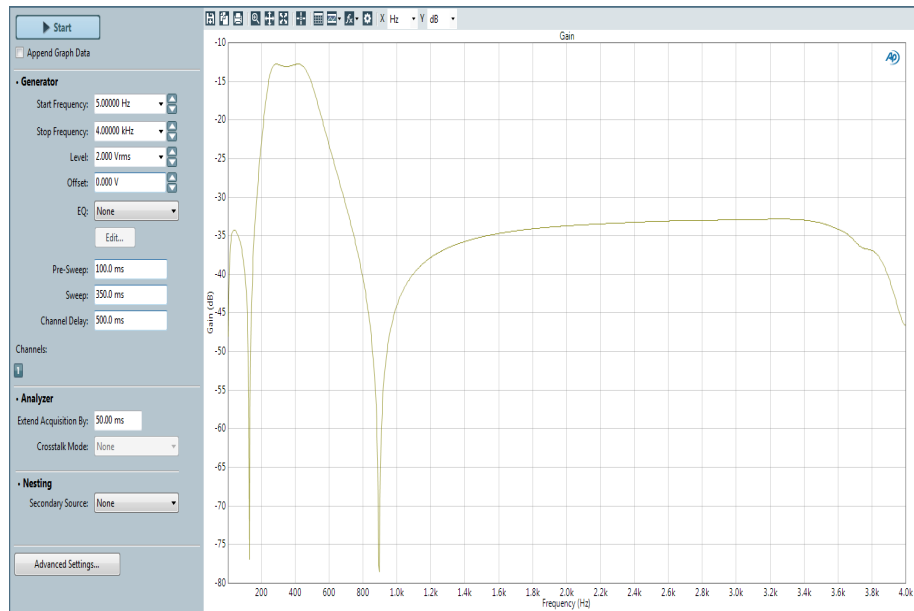


Figure 28: Measured Magnitude Response

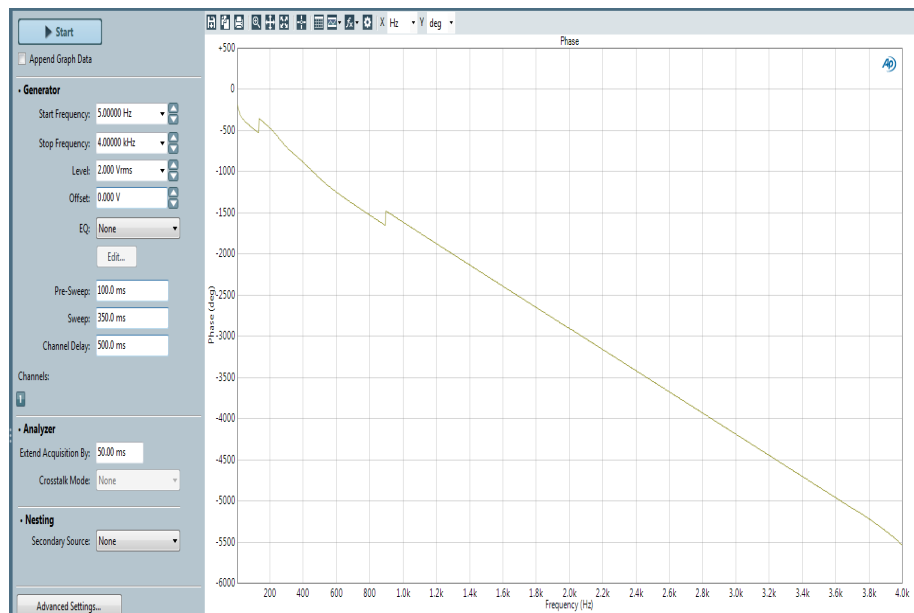


Figure 29: Measured Phase Response

Now we will repeat the steps similar to section 4.3, that is exporting the graph data of the measured response and subtract it by the all pass response for both magnitude and phase to extract the actual frequency response of the elliptic filter alone.

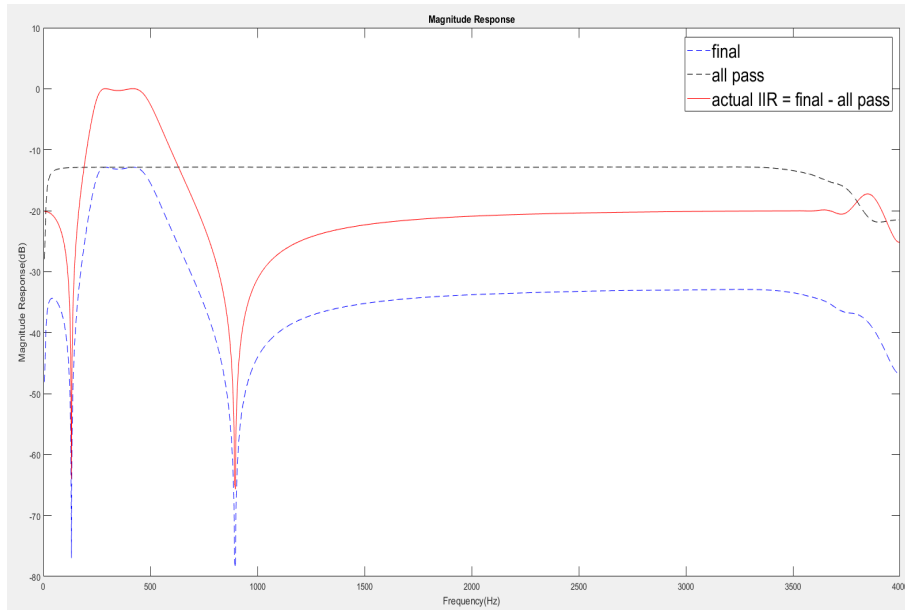


Figure 30: Actual Digital Bandpass Filter Magnitude Response. This is calculated with measured gain response minus all pass response.

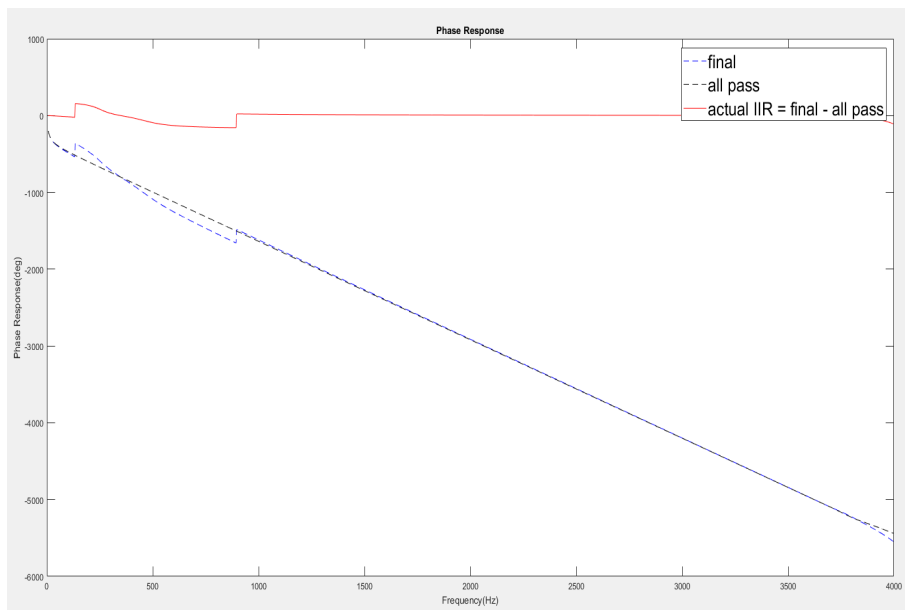


Figure 31: Actual Digital Bandpass Phase Response. This is calculated with measured phase response minus all pass response.

Compare the actual digital bandpass filter with the plot in Matlab:

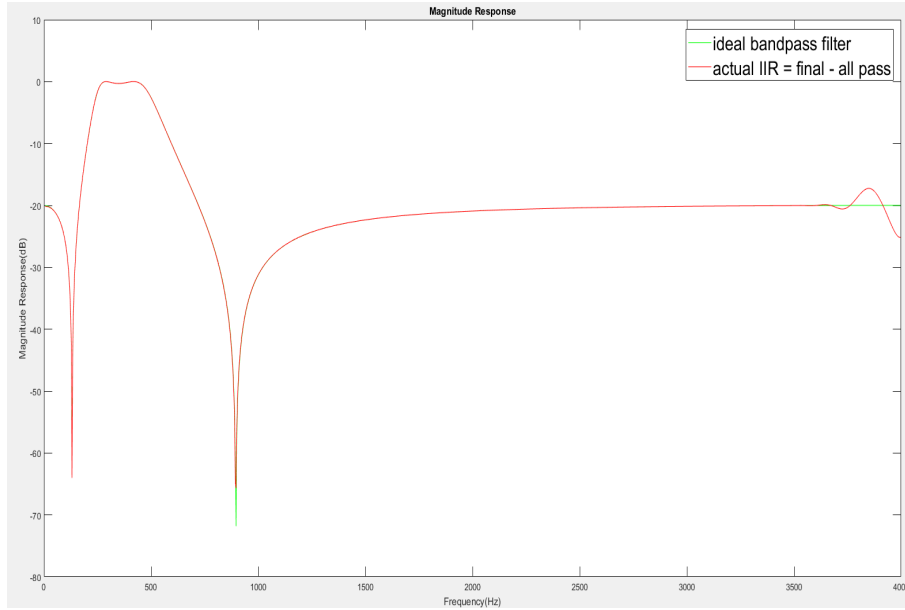


Figure 32: Comparison of Ideal bandpass filter and actual implemented filter

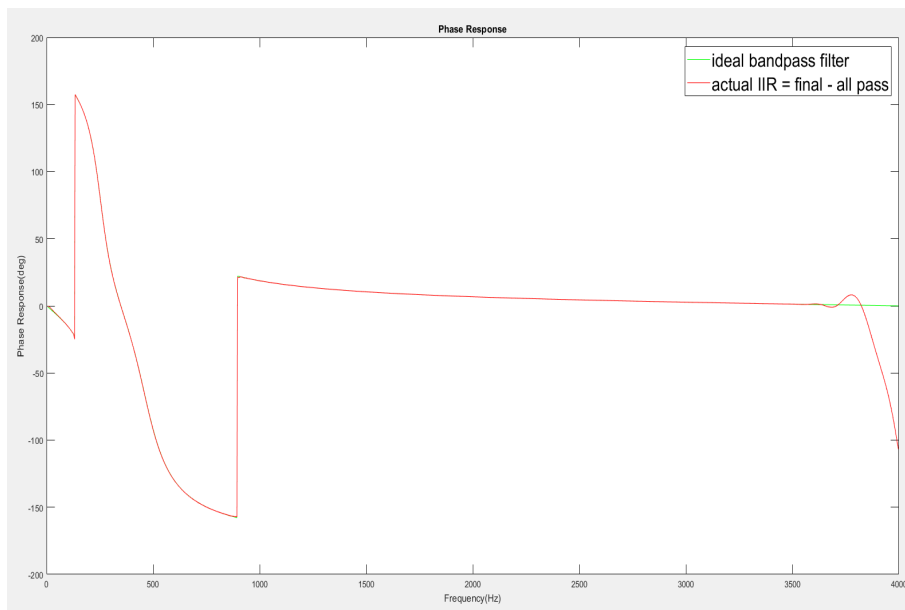


Figure 33: Actual Digital Bandpass Phase Response

The actual bandpass elliptical filter response of order 4 closely tracks the ideal response given by Matlab for except the little peak occurring at high frequencies. This deviation is due to filtering operations, which is explained above.

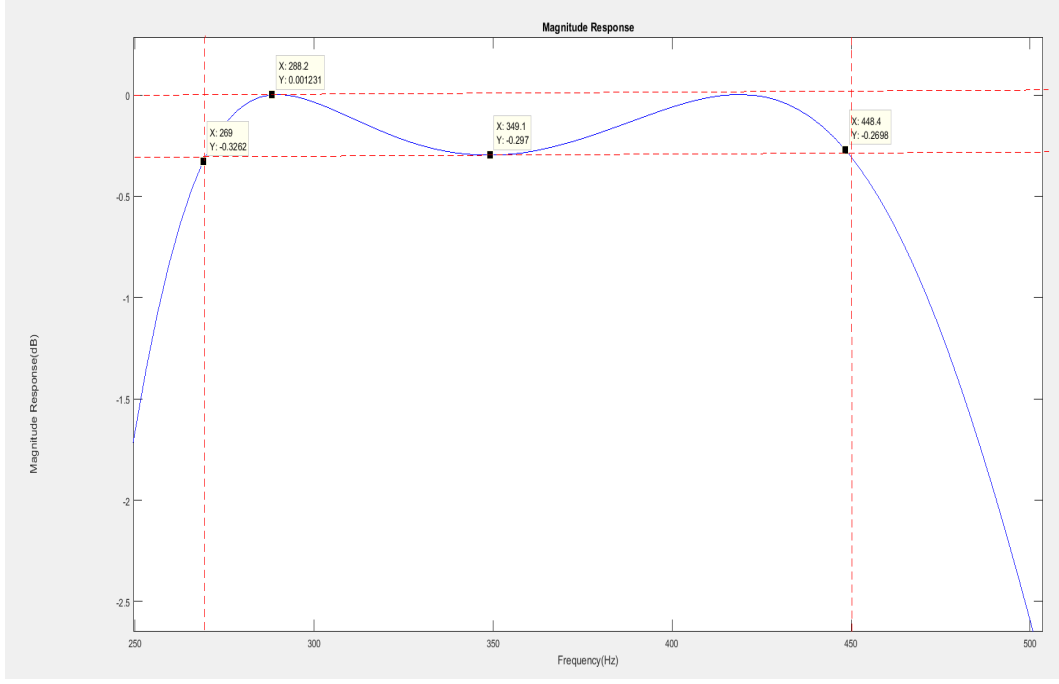


Figure 34: Graph of Actual Bandpass Response

As shown, all specifications as mentioned in the **Filter Specification** are satisfied.

## 5.5 C Implementation for Direct Form II Transposed Form

The Direct II Transposed form is unchanged in behavior comparing to the traditional Direct II form. The direction for each branch is reversed, branch divisions and branch summations are interchanged and input is swapped for output. This form avoids specific shifting of samples, because shifting is inherent in the calculations of output. This would become more obvious in the following example. In the following diagram,  $x[n]$  represents operation of delay elements.

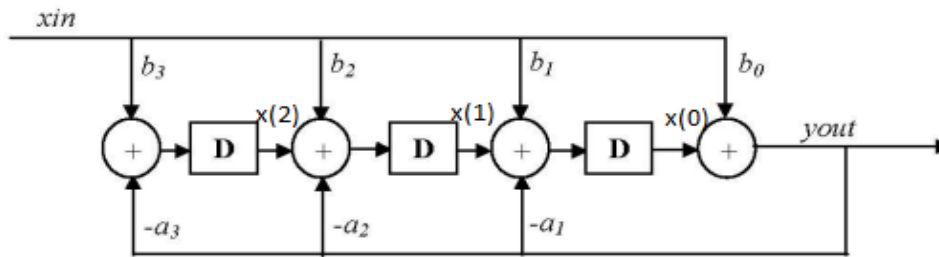


Figure 6 Direct form II transposed structure

Figure 35: Direct II transposed form

It can be deduced that:

$$\begin{aligned}
 y_{out} &= b_0 X_{in} + x_0 \\
 x_0 &= b_1 X_{in} - a_1 y_{out} + x_1 \\
 x_1 &= b_2 X_{in} - a_2 y_{out} + x_2 \\
 x_2 &= b_3 X_{in} - a_3 y_{out}
 \end{aligned}$$

Hence in C implementation, at each iteration of *for* loop a sample within buffer  $x[m-1]$  is updated with previous buffer value  $x[m]$  and coefficients  $b[m]$ ,  $a[m]$  following formula:

$$x[m-1] = X_{in} * b[m] - y_{out} * a[m] + x[m]$$

Outside the loop, the  $x[\text{order}-1]$  would be calculated individually, because it is the first value in the buffer that is not weighted by previous buffer values.

```
void bandpass_direct2_transposed_IIR(void){
    int m;
    samp = b[0]*sampin + x[0]; //calculate current sample output
    for(m=1; m < order; m++){ //no circular buffer or shifting needed
        x[m-1] = sampin*b[m] - samp*a[m] + x[m]; //Update each buffer value, except x[order-1]
                                                //with previous buffer values and coefficients
                                                //a and b
    }
    x[order-1] = sampin*b[order] - samp*a[order]; //x[order-1] is not influenced by other values in x
                                                //hence computed individually
}
```

Figure 36: Direct II transposed form Implementation

## 5.6 Results for Direct Form II Transposed Form

Measure the frequency response using APX500 audio analyzer:

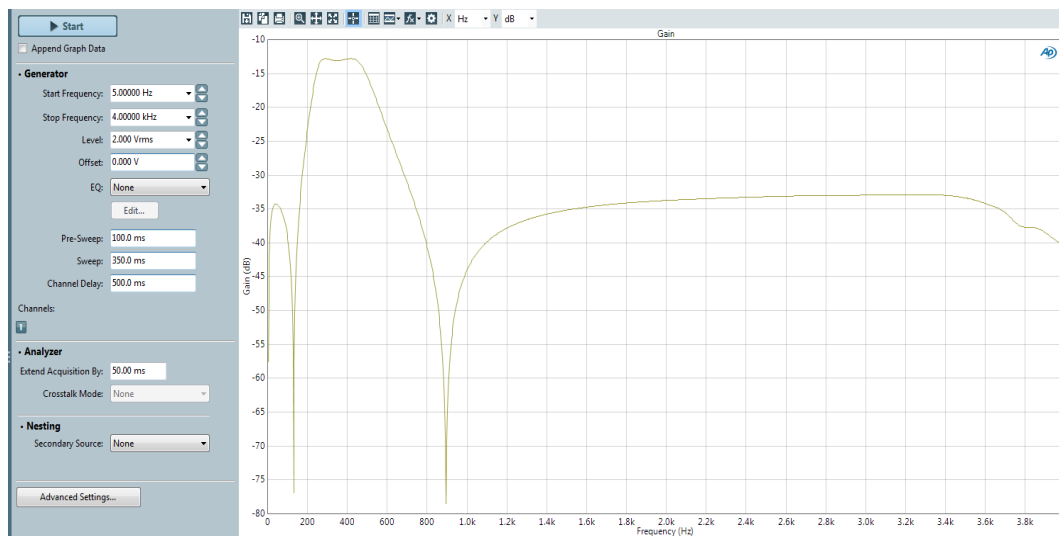


Figure 37: Direct II transposed Magnitude response

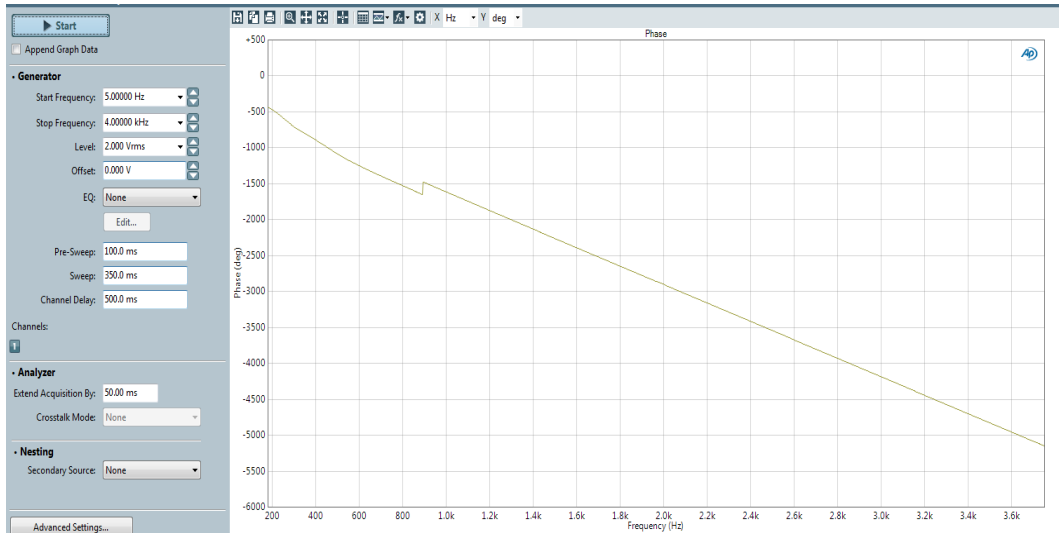


Figure 38: Direct II transposed Phase response

Same as before, measured data from Audio Precision are extracted and subtract all pass response to obtain actual discrete IIR filter response. The actual response is then compared with ideal response from Matlab.

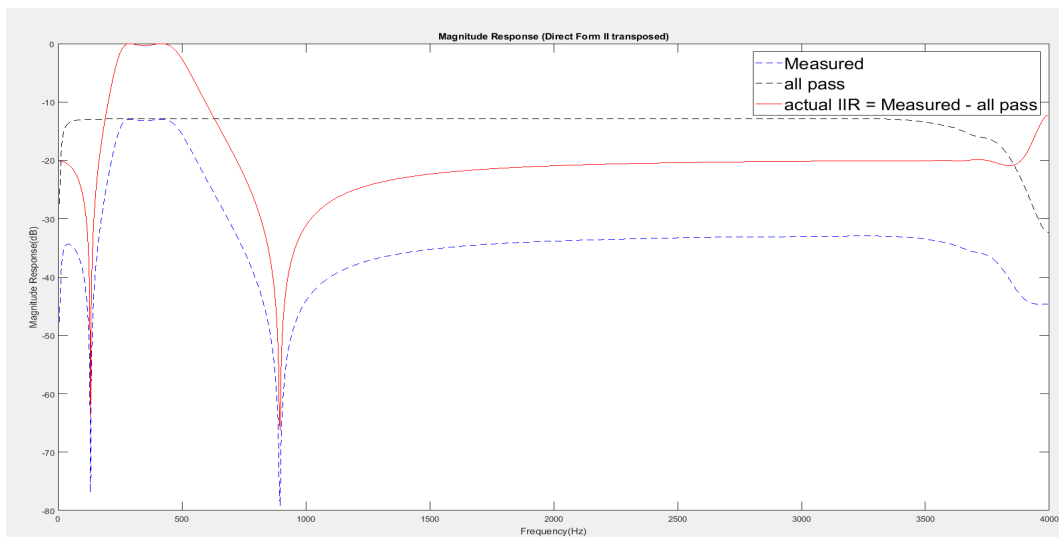


Figure 39: Actual discrete IIR Bandpass filter Magnitude response. Direct form II Transposed Implementation

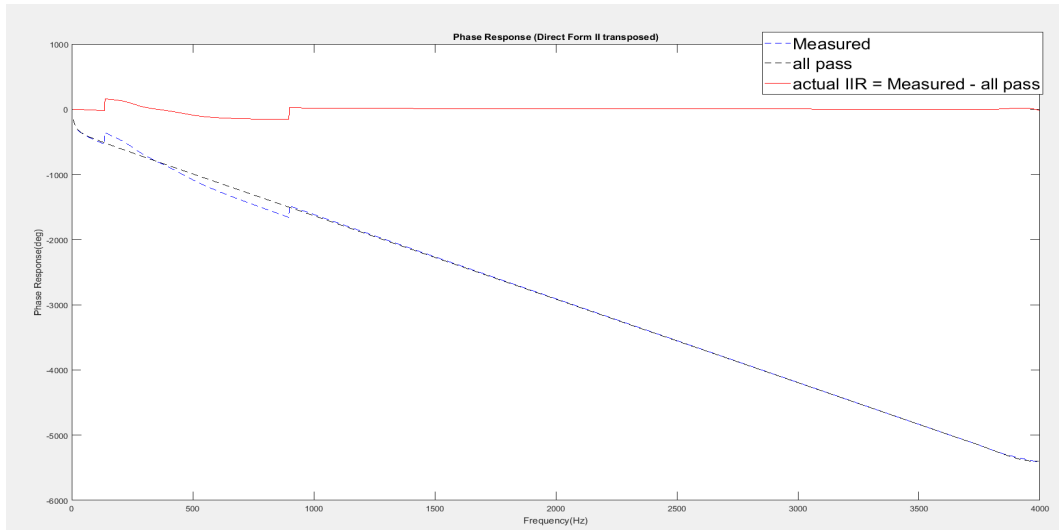


Figure 40: Actual discrete IIR Bandpass filter Phase response. Direct form II Transposed Implementation

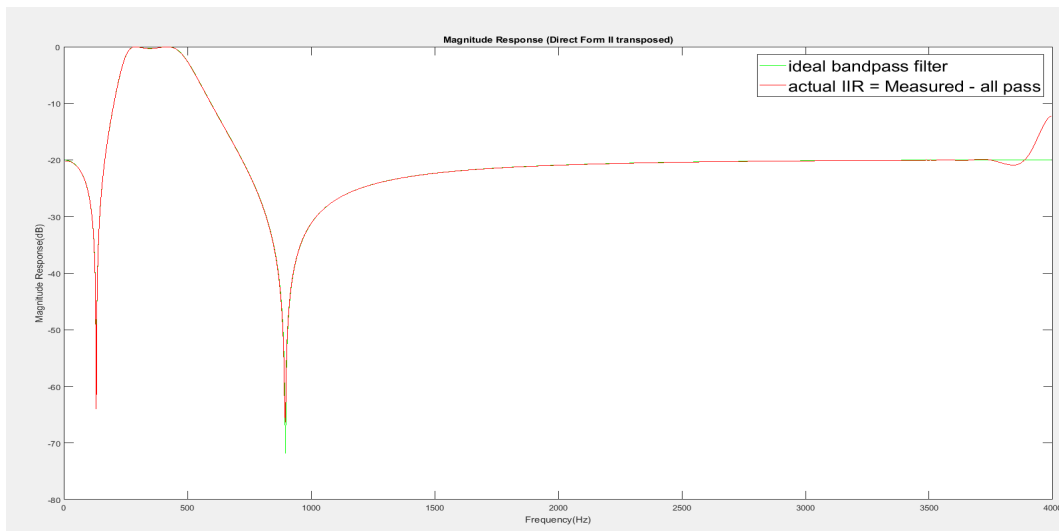


Figure 41: Comparison of Ideal bandpass filter and actual implemented filter

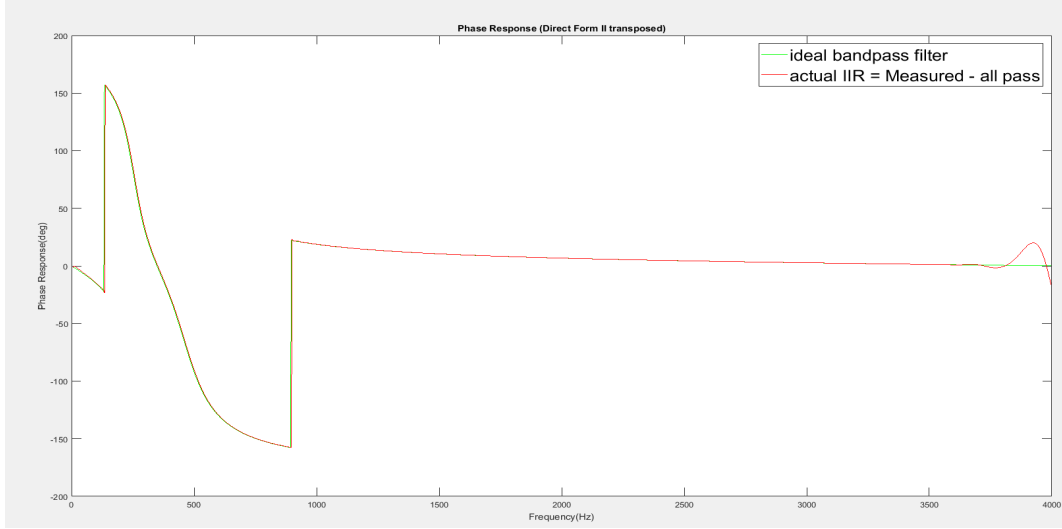


Figure 42: Comparison of Ideal bandpass filter and actual implemented filter

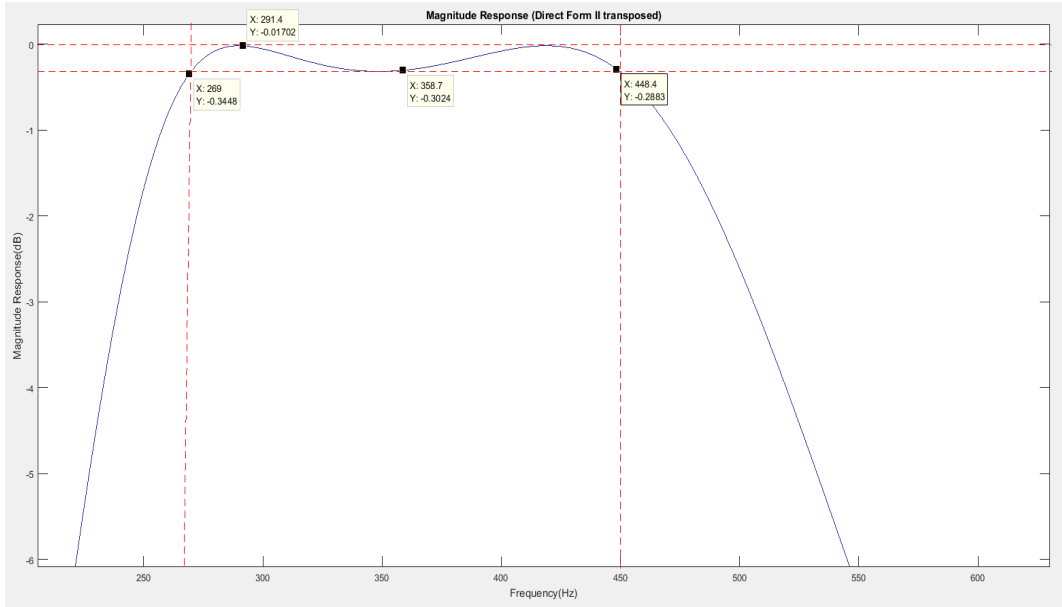


Figure 43: All specifications are satisfied

As shown, the gain and phase response for Direct Form II Transposed Form are almost identical to the results for traditional Direct II form, hence proving the unchanged behavior. The next section would explore the algorithm performance and efficiency difference of different implementations.

## 6 Performance Comparison of 2 Direct Form Filters

In this section we use the profiling clock method to measure the relationship between instruction cycles and the filter order. Two breakpoints are set at calls to *mono\_read\_16Bit()* and *mono\_write\_16Bit()* respectively so that the count only includes the filtering operations. Measurements are done for both non-transposed and transposed Direct Form II filters and for both no optimization and -o2 optimization level. Measurements are taken several times to find the average cycles needed for a given order filter under certain optimization level.



-	No optimization		-o2 optimization	
Order	Direct form 2	Direct form 2 Transposed	Direct form 2	Direct form 2 Transposed
2	321.5	229.5	286.25	240.5
4	491.75	349.25	357.25	252.25
6	661.5	469.5	433.75	262.5
8	831.25	589.5	509.5	272.25
10	1001.75	709.75	585.75	282.5
12	1171.5	829.25	661.75	293
14	1341.25	949.5	737.5	302.25
16	1511.5	1069.5	813	312.5
18	1681.75	1189.5	889.5	322.25
20	1851.5	1309.75	965	332.75
40	3551.5	2509.75	1725.75	432.25
50	4401.5	3109.5	2125.5	482.75
60	5259.5	3709.25	2529.5	3348.42
64	5627.25	3949	2677.25	1116.75
70	6150	4309.25	2883	582.75
80	7000.5	4909.5	3254.5	632.75

The results are then plotted in Matlab as shown below:

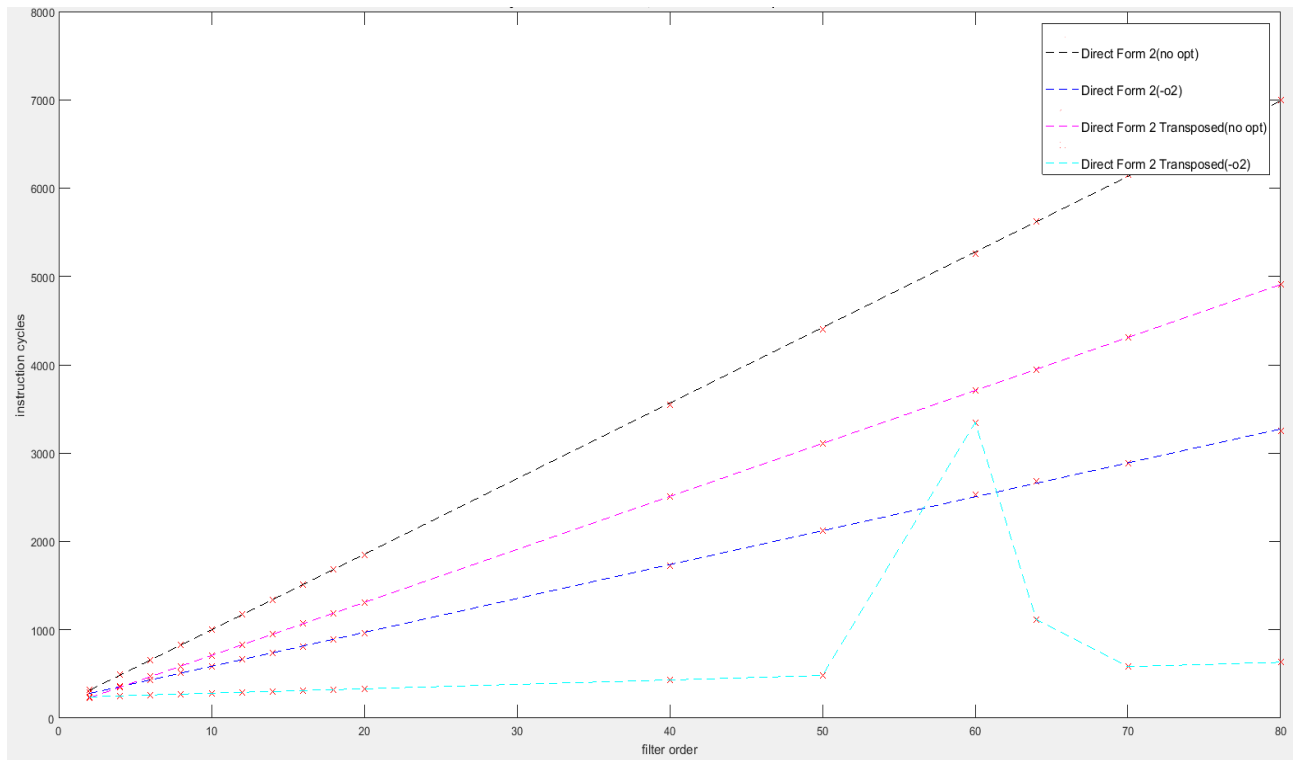


Figure 44: Plot of Instruction Cycles against Filter Order

As we can see above, all the curves have linear trend except for direct form 2 transposed filter under the -o2 optimization. The cycles needed for the transposed form under -o2 of order 60 and 64 jump out the linear trend of the other data points. This might be due to the way the compiler optimizes the code. Let's ignore the exception points on the 4th curve for the moment and only look at overall performance. At lower orders there are only small differences between 4 curves, cycles needed are almost the same for filter with order 2. Differences between performances increase as order increases. Overall, direct form 2 transposed is faster than the non-transposed form for both optimisations since in transposed form the shifting of the samples is inherent in the calculations for the output. It is also straight forward from

the prospective of the C implementation, where the non-transposed code contains a for loop with three instructions whereas the transposed contains only one. However, the transposed form implementation takes greater advantage of the optimization since difference between *noopt* and *-o2* lines are greater than of the non-transposed form given the same order.

The expressions of 4 best-fit straight lines are given below:

-	Expressions
Direct form 2(no opt)	$85.5563n + 143.8626$
Direct form 2(-o2)	$38.3912n + 202.3319$
Direct form 2 Transposed(no opt)	$59.9973n + 109.5336$
Direct form 2 Transposed(-o2)	$5.0097n + 232.1316$

Where the intercepts represent code overhead and the gradients represent the number of extra cycles raised by an extra coefficient from an increase in the filter order. Optimized codes have lower gradients and higher overheads in each form, while transposed form codes have lower gradients under each optimization level. The decrease in gradients from no optimization to -o2 optimization is about 55% for non-transposed form while it is 91% for transposed form.

The difference in the degree of improvement due to optimization between two implementations draws our attention to how the code is optimised under o2 optimization. o2 optimization takes great advantage of software pipelining and parallel instructions as it performs loop optimizations and loop unrolling. Parallel instructions that have no data or control dependencies with each other, which can be executed at the same time by utilizing all processing units. The implementation of direct form II transposed contains more parallel instruction. This is because for each stage of  $x$  (the value after each delay element), the operations with coefficients and current input/output can be calculated first. For example,  $a_i x_{in}$  and  $b_i y_{out}$  can be calculated first for  $x_{i-1}$  (the value after i-th delay element) before the correct value of  $x_i$  is available.

Also, the overhead of optimised code is larger than the original code for each implementation. The reason might be that the optimizer is creating a more efficient set-up in order to reduce the number of loop iterations. We could see the optimisation result by comparing the assembly code for the loop section in the Appendix.

## 7 Appendix

### • C Implementation

```
/******  
DEPARTMENT OF ELECTRICAL AND ELECTRONIC ENGINEERING  
IMPERIAL COLLEGE LONDON  
  
EE 3.19: Real Time Digital Signal Processing  
Dr Paul Mitcheson and Daniel Harvey  
  
LAB 5: Real-Time Implementation of IIR Filters  
  
***** I N T I D . C *****  
  
Demonstrates inputing and outputing data from the DSK's audio port using interrupts.  
  
*****  
Updated for use on 6713 DSK by Danny Harvey: May-Aug 2006  
Updated for CCS V4 Sept 10  
*****  
/*  
* You should modify the code so that interrupts are used to service the  
* audio port.  
*/  
/****** Pre-processor statements *****  
  
#include <stdlib.h>  
// Included so program can make use of DSP/BIOS configuration tool.  
#include "dsp_bios_cfg.h"  
  
/* The file dsk6713.h must be included in every program that uses the BSL. This  
example also includes dsk6713_aic23.h because it uses the  
AIC23 codec module (audio interface). */  
#include "dsk6713.h"  
#include "dsk6713_aic23.h"  
  
// math library (trig functions)  
#include <math.h>  
  
// Some functions to help with writing/reading the audio ports when using interrupts.  
#include <helper_functions_ISR.h>  
  
//FIR filter coefficients  
#include "single_pole_coef.txt"  
//#include "bandpass_coef.txt"  
/****** Global declarations *****  
  
/* Audio port configuration settings: these values set registers in the AIC23 audio  
interface to configure it. See TI doc SLWS106D 3-3 to 3-10 for more info. */  
DSK6713_AIC23_Config Config = { \n  
    /* *****  
    /* REGISTER FUNCTION SETTINGS */  
    /* *****  
    0x0017, /* 0 LEFTINVOL Left line input channel volume 0dB */\n    0x0017, /* 1 RIGHTINVOL Right line input channel volume 0dB */\n    0x01f9, /* 2 LEFTHPVOL Left channel headphone volume 0dB */\n    0x01f9, /* 3 RIGHTHPVOL Right channel headphone volume 0dB */\n    0x0011, /* 4 ANAPATH Analog audio path control DAC on, Mic boost 20dB*/\n    0x0000, /* 5 DIGPATH Digital audio path control All Filters off */\n    0x0000, /* 6 DPOWERDOWN Power down control All Hardware on */\n    0x0043, /* 7 DIGIF Digital audio interface format 16 bit */\n    0x008d, /* 8 SAMPLERATE Sample rate control 8 KHZ */\n    0x0001 /* 9 DIGACT Digital interface activation On */\n    /* *****  
};  
  
// Codec handle:- a variable used to identify audio interface  
DSK6713_AIC23_CodecHandle H_Codec;  
  
/****** Global Variables *****  
  
short sampin;  
double samp;  
double *w,*v,*x;//declare pointers of type double  
int order;//filter order  
/* Audio channel gain values, calculated to be less than maximum acceptable value. */  
  
/****** Function prototypes *****  
void init_hardware(void);  
void init_HWI(void);
```

```

void ISR_AIC (void);
void single_pole_IIR(void);
void bandpass_direct2_IIR(void);
void bandpass_direct2_transposed_IIR(void);
/***** Main routine *****/
void main(){

    // initialize board and the audio port
    init_hardware();
    // initialize the look-up table

    /* initialize hardware interrupts */
    init_HWI();

    //dynamically allocat array sizes to store input and output samples
    order = sizeof(a)/sizeof(a[0]) -1;
    w = (double *) calloc(order+1, sizeof(double)); //dynamic memory, order+1 elements, each of size double
    v = (double *) calloc(order+1, sizeof(double));
    x = (double *) calloc(order, sizeof(double));

    /* loop indefinitely, waiting for interrupts */
    while(1)
    {};

}

/***** init_hardware() *****/
void init_hardware()
{
    // Initialize the board support library, must be called first
    DSK6713_init();

    // Start the AIC23 codec using the settings defined above in config
    H_Codec = DSK6713_AIC23_openCodec(0, &Config);

    /* Function below sets the number of bits in word used by MSBSP (serial port) for
    receives from AIC23 (audio port). We are using a 32 bit packet containing two
    16 bit numbers hence 32BIT is set for receive */
    MCBSP_FSETS(RCR1, RWDLEN1, 32BIT);

    /* Configures interrupt to activate on each consecutive available 32 bits
    from Audio port hence an interrupt is generated for each L & R sample pair */
    MCBSP_FSETS(SPCR1, RINTM, FRM);

    /* These commands do the same thing as above but applied to data transfers to
    the audio port */
    MCBSP_FSETS(XCR1, XWDLEN1, 32BIT);
    MCBSP_FSETS(SPCR1, XINTM, FRM);

}

/***** init_HWI() *****/
void init_HWI(void)
{
    IRQ_globalDisable();           // Globally disables interrupts
    IRQ_nmiEnable();               // Enables the NMI interrupt (used by the debugger)
    IRQ_map(IRQ_EVT_RINT1,4);      // Maps an event to a physical interrupt
    IRQ_enable(IRQ_EVT_RINT1);     // Enables the event
    IRQ_globalEnable();            // Globally enables interrupts
}

/***** WRITE YOUR INTERRUPT SERVICE ROUTINE HERE*****/

void ISR_AIC (void)
{
    samp = 0; //reset output
    sampin = mono_read_16Bit();
    single_pole_IIR();
    //bandpass_direct2_IIR();
    //bandpass_direct2_transposed_IIR();
    //mono_write_16Bit(mono_read_16Bit());
    mono_write_16Bit(samp);
}

void single_pole_IIR(void){
    int k;
    samp = b[0]*sampin; //calculation with b[0] done individually
                        //so within for loop can multiply v[k] with b[k]
                        //and w[k] with a[k]

    for(k = order; k>0; k--){
        samp += v[k]*b[k] - w[k]*a[k]; //perform convolution sum following
                                      //IIR difference equation
    }
}

```

```

        w[k] = w[k-1]; //perform delay for input values stored in v
        v[k] = v[k-1]; //perform delay for output values stored in w
    }
    v[1] = sampin; //update first delayed element v[1], or x(n-1) for next iteration
    w[1] = samp; //update w[1], or y(n-1) for next iteration
}

void bandpass_direct2_IIR(void){
    int i;
    w[0] = sampin; //write input sample to w[0](w(n))
    for(i=order; i>0; i--){ //for loop to carry out convolution sum
        //we are not using w[0] yet, so can multiply w[i] with a[i]
        //and b[i]
        w[0] -= a[i]*w[i]; // w[0](w(n)) =x(n)-a[order]*w[order]-a[order-1]*w[order-1]...
        samp += b[i]*w[i]; //yout = b[order]*w[order]+b[order-1]*w[order-1]...
        w[i] = w[i-1]; //perform delay after the value is used in the calculation
    }
    samp += b[0]*w[0]; //finish output computation since the correct w[0](w(n)) is ready
}

void bandpass_direct2_transposed_IIR(void){
    int m;
    samp = b[0]*sampin + x[0]; //calculate current sample output
    for(m =1; m < order; m++){ //no circular buffer or shifting needed
        x[m-1] = sampin*b[m] - samp*a[m] + x[m]; //Update each buffer value, except x[order-1]
        //with previous buffer values and coefficients
        //a and b
    }
    x[order-1] = sampin*b[order] - samp*a[order]; //x[order-1] is not influenced by other values in x
    //hence computed individually
}

```

- Single-pole Filter Design and Graph Plotting

```

close all;
R = 1000; %Resistor value
C = 10^-6; %Capacitor value
fs = 8000; %Sampling frequency
H = tf([1],[R*C,1]); %Find transfer function of RC filter
Hd = c2d(H,1/fs,'tustin') %Complete Tustin transform

[num,den] = tfdata(Hd); %Find coefficients
num = cell2mat(num)
[den] = cell2mat(den)
%{
damp(Hd);
%save iir_coef.txt num den -ascii -double -tabs
figure;
step(H, '-', Hd, '--');
damp(Hd);
%}
figure;
pzmap(Hd)

[h,f] = freqz(num,den,1249,fs);
%freqz(num,den,1249,fs)

gaindirect = cell2mat(directgain(4,2));
phasedirect = cell2mat(directphase(4,2));
gainy = cell2mat(Gain(4,2));
phasey = cell2mat(Phase(4,2));

figure;
plot(f(3:1249),gainy,'--b');
hold on;
plot(f(3:1249),gaindirect,'--k');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
%hold on;
%plot(f(3:1250),gainy,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;
figure;
plot(f(3:1249),phasey,'--b');
hold on;
plot(f(3:1249),phasedirect,'--k');
hold on;
plot(f(3:1249),phasey-phasedirect,'-r');
%hold on;
%plot(f(3:1250),phasey,'-r');
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;
Hd
%{
%save fir_coef.txt b -ascii -double -tabs; %save to fir_coef.txt
fileID = fopen('fir_coef.txt','w');

```

```

formSpec1 = 'double b[]={%.16e';
fprintf(fileID,formSpec1,b(1));
formSpec2 = ', %.16e';
fprintf(fileID,formSpec2,b(2:end));
fprintf(fileID,'};\n');
fclose(fileID);
%}

w = f(3:1249).*2.*pi;
[mag,phase,wout] = bode(H,w);
mag = squeeze(mag(1,1,:));
phase = squeeze(phase(1,1,:));
figure;
plot(f(3:1249),20.*log10(mag),'-g');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'analogue IIR','actual digital IIR'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;
figure;
plot(f(3:1249),phase,'-g');
hold on;
plot(f(3:1249),phasey-phasedirect,'-r');
legend({'analogue IIR','actual digital IIR'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;
figure;
bode(H);

figure;
plot(f(3:1249),20.*log10(mag),'-g');
hold on;
plot(f(3:1249),20.*log10(abs(h(3:1249)))),'-r');
legend({'analogue IIR','ideal digital IIR'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),phase,'-g');
hold on;
plot(f(3:1249),unwrap(angle(h(3:1249))).*180./pi,'-r');
legend({'analogue filter','ideal digital IIR'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

```

- Bandpass Filter Design and Graph Plotting

```

close all;
fs = 8000;
Rn = 0.3;
n = 10;
Rs = 20;
w = [270,450].*2./fs;
[b, a] = ellip(n,Rn,Rs,w, 'bandpass');

%{
C = reshape([b,a],length(b),2) '
%dlmwrite('coef.txt',C, ',')
figure;
freqz(b,a,1029,fs);
figure;
H = tf(b,a,1/fs);
damp(H)

pzmap(H);
figure;
bode (H);
%}
[h,f]=freqz(b,a,1249,fs);
freqz(b,a,1249,fs);
fileID = fopen('bandpass_coef.txt','w');
formSpec1 = 'double b[]={%.16e';
fprintf(fileID,formSpec1,b(1));
formSpec2 = ', %.16e';
fprintf(fileID,formSpec2,b(2:end));
fprintf(fileID,'};\n');
formSpec3 = 'double a[]={%.16e';
fprintf(fileID,formSpec3,a(1));
fprintf(fileID,formSpec2,a(2:end));
fprintf(fileID,'};\n');
fclose(fileID);

gaindirect = cell2mat(directgain(4,2));
phasedirect = cell2mat(directphase(4,2));
gainy = cell2mat(Gain(4,2));
phasey = cell2mat(Phase(4,2));

figure;
plot(f(3:1249),gainy,'--b');
hold on;
plot(f(3:1249),gaindirect,'--k');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),phasey,'--b');
hold on;
plot(f(3:1249),phasedirect,'--k');
hold on;

```



```

plot(f(3:1249),phasey-phasedirect,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

figure;
plot(f(3:1249),20.*log10(abs(h(3:1249))),'-g');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'ideal bandpass filter','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),unwrap(angle(h(3:1249))).*180./pi,'-g');
hold on;
plot(f(3:1249),phasey-phasedirect,'-r');
legend({'ideal bandpass filter','actual IIR = final - all pass'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

```

- Find the Expressions of Cycles vs Filter Order and Plot out the Trends

```

close all;
n = [1:10].*2;
cycles = [321.5,491.75,661.5,831.25,1001.75,1171.5,1341.25,1511.5,1681.75,1851.5];

p = polyfit(n,cycles,1)
f = polyval(p,n);
a = p(1)
b = p(2)
figure;
plot(n,cycles, 'xr');
hold on;
plot(n,f,'--b')
title(horzcat('y = ',num2str(a),'n + ',num2str(b),' ', Direct Form II'));
xlabel('filter order');
ylabel('instruction cycles');
hold off;

cycles1 = [286.25,357.25,433.75,509.5,585.75,661.75,737.5,813,889.5,965];
p = polyfit(n,cycles1,1)
f = polyval(p,n);
a = p(1)
b = p(2)
figure;
plot(n,cycles1, 'xr');
hold on;
plot(n,f,'--b')
title(horzcat('y = ',num2str(a),'n + ',num2str(b),' ', Direct Form II -o2'));
xlabel('filter order');
ylabel('instruction cycles');
hold off;

cycles = [229.5,349.25,469.5,589.5,709.75,829.25,949.5,1069.5,1189.5,1309.75];
p = polyfit(n,cycles,1)
f = polyval(p,n);
a = p(1)
b = p(2)
figure;
plot(n,cycles, 'xr');
hold on;
plot(n,f,'--b')
title(horzcat('y = ',num2str(a),'n + ',num2str(b),' ', Direct Form II Transposed'));
xlabel('filter order');
ylabel('instruction cycles');
hold off;

cycles1 = [240.5,252.25,262.5,272.25,282.5,293,302.25,312.5,322.25,332.75];
p = polyfit(n,cycles1,1)
f = polyval(p,n);
a = p(1)
b = p(2)
figure;
plot(n,cycles1, 'xr');
hold on;

```

```
plot(n,f,'--b')
title(horzcat('y = ',num2str(a),'n + ',num2str(b),' , Direct Form II Transposed -o2'));
xlabel('filter order');
ylabel('instruction cycles');
hold off;
```

- Bandpass Filter Design and Graph Plotting

```

close all;
fs = 8000;
Rn = 0.3;
n = 10;
Rs = 20;
w = [270,450].*2./fs;
[b, a] = ellip(n,Rn,Rs,w, 'bandpass');

%{
C = reshape([b,a],length(b),2) '
%dlmwrite('coef.txt',C, ',')
figure;
freqz(b,a,1029,fs);
figure;
H = tf(b,a,1/fs);
damp(H)

pzmap(H);
figure;
bode (H);
%}
[h,f]=freqz(b,a,1249,fs);
freqz(b,a,1249,fs);
fileID = fopen('bandpass_coef.txt','w');
formSpec1 = 'double b[]={%.16e';
fprintf(fileID,formSpec1,b(1));
formSpec2 = ', %.16e';
fprintf(fileID,formSpec2,b(2:end));
fprintf(fileID,'};\n');
formSpec3 = 'double a[]={%.16e';
fprintf(fileID,formSpec3,a(1));
fprintf(fileID,formSpec2,a(2:end));
fprintf(fileID,'};\n');
fclose(fileID);

gaindirect = cell2mat(directgain(4,2));
phasedirect = cell2mat(directphase(4,2));
gainy = cell2mat(Gain(4,2));
phasey = cell2mat(Phase(4,2));

figure;
plot(f(3:1249),gainy,'--b');
hold on;
plot(f(3:1249),gaindirect,'--k');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),phasey,'--b');
hold on;
plot(f(3:1249),phasedirect,'--k');
hold on;

```

```

plot(f(3:1249),phasey-phasedirect,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

figure;
plot(f(3:1249),20.*log10(abs(h(3:1249))),'-g');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'ideal bandpass filter','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),unwrap(angle(h(3:1249))).*180./pi,'-g');
hold on;
plot(f(3:1249),phasey-phasedirect,'-r');
legend({'ideal bandpass filter','actual IIR = final - all pass'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

```

- Bandpass Filter Design and Graph Plotting

```

close all;
fs = 8000;
Rn = 0.3;
n = 10;
Rs = 20;
w = [270,450].*2./fs;
[b, a] = ellip(n,Rn,Rs,w, 'bandpass');

%{
C = reshape([b,a],length(b),2) '
%dlmwrite('coef.txt',C, ' ','')
figure;
freqz(b,a,1029,fs);
figure;
H = tf(b,a,1/fs);
damp(H)

pzmap(H);
figure;
bode (H);
%}
[h,f]=freqz(b,a,1249,fs);
freqz(b,a,1249,fs);
fileID = fopen('bandpass_coef.txt','w');
formSpec1 = 'double b[]={%.16e';
fprintf(fileID,formSpec1,b(1));
formSpec2 = ', %.16e';
fprintf(fileID,formSpec2,b(2:end));
fprintf(fileID,'};\n');
formSpec3 = 'double a[]={%.16e';
fprintf(fileID,formSpec3,a(1));
fprintf(fileID,formSpec2,a(2:end));
fprintf(fileID,'};\n');
fclose(fileID);

gaindirect = cell2mat(directgain(4,2));
phasedirect = cell2mat(directphase(4,2));
gainy = cell2mat(Gain(4,2));
phasey = cell2mat(Phase(4,2));

figure;
plot(f(3:1249),gainy,'--b');
hold on;
plot(f(3:1249),gaindirect,'--k');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),phasey,'--b');
hold on;
plot(f(3:1249),phasedirect,'--k');
hold on;

```

```

plot(f(3:1249),phasey-phasedirect,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

figure;
plot(f(3:1249),20.*log10(abs(h(3:1249))),'-g');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'ideal bandpass filter','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),unwrap(angle(h(3:1249))).*180./pi,'-g');
hold on;
plot(f(3:1249),phasey-phasedirect,'-r');
legend({'ideal bandpass filter','actual IIR = final - all pass'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

```

- Bandpass Filter Design and Graph Plotting

```

close all;
fs = 8000;
Rn = 0.3;
n = 10;
Rs = 20;
w = [270,450].*2./fs;
[b, a] = ellip(n,Rn,Rs,w, 'bandpass');

%{
C = reshape([b,a],length(b),2) '
%dlmwrite('coef.txt',C, ',')
figure;
freqz(b,a,1029,fs);
figure;
H = tf(b,a,1/fs);
damp(H)

pzmap(H);
figure;
bode (H);
%}
[h,f]=freqz(b,a,1249,fs);
freqz(b,a,1249,fs);
fileID = fopen('bandpass_coef.txt','w');
formSpec1 = 'double b[]={%.16e';
fprintf(fileID,formSpec1,b(1));
formSpec2 = ', %.16e';
fprintf(fileID,formSpec2,b(2:end));
fprintf(fileID,'};\n');
formSpec3 = 'double a[]={%.16e';
fprintf(fileID,formSpec3,a(1));
fprintf(fileID,formSpec2,a(2:end));
fprintf(fileID,'};\n');
fclose(fileID);

gaindirect = cell2mat(directgain(4,2));
phasedirect = cell2mat(directphase(4,2));
gainy = cell2mat(Gain(4,2));
phasey = cell2mat(Phase(4,2));

figure;
plot(f(3:1249),gainy,'--b');
hold on;
plot(f(3:1249),gaindirect,'--k');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),phasey,'--b');
hold on;
plot(f(3:1249),phasedirect,'--k');
hold on;

```



```

plot(f(3:1249),phasey-phasedirect,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

figure;
plot(f(3:1249),20.*log10(abs(h(3:1249))),'-g');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'ideal bandpass filter','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),unwrap(angle(h(3:1249))).*180./pi,'-g');
hold on;
plot(f(3:1249),phasey-phasedirect,'-r');
legend({'ideal bandpass filter','actual IIR = final - all pass'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

```

- Bandpass Filter Design and Graph Plotting

```

close all;
fs = 8000;
Rn = 0.3;
n = 10;
Rs = 20;
w = [270,450].*2./fs;
[b, a] = ellip(n,Rn,Rs,w, 'bandpass');

%{
C = reshape([b,a],length(b),2) '
%dlmwrite('coef.txt',C, ',')
figure;
freqz(b,a,1029,fs);
figure;
H = tf(b,a,1/fs);
damp(H)

pzmap(H);
figure;
bode (H);
%}
[h,f]=freqz(b,a,1249,fs);
freqz(b,a,1249,fs);
fileID = fopen('bandpass_coef.txt','w');
formSpec1 = 'double b[]={%.16e';
fprintf(fileID,formSpec1,b(1));
formSpec2 = ', %.16e';
fprintf(fileID,formSpec2,b(2:end));
fprintf(fileID,'};\n');
formSpec3 = 'double a[]={%.16e';
fprintf(fileID,formSpec3,a(1));
fprintf(fileID,formSpec2,a(2:end));
fprintf(fileID,'};\n');
fclose(fileID);

gaindirect = cell2mat(directgain(4,2));
phasedirect = cell2mat(directphase(4,2));
gainy = cell2mat(Gain(4,2));
phasey = cell2mat(Phase(4,2));

figure;
plot(f(3:1249),gainy,'--b');
hold on;
plot(f(3:1249),gaindirect,'--k');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),phasey,'--b');
hold on;
plot(f(3:1249),phasedirect,'--k');
hold on;

```

```

plot(f(3:1249),phasey-phasedirect,'-r');
legend({'final','all pass','actual IIR = final - all pass'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

figure;
plot(f(3:1249),20.*log10(abs(h(3:1249))),'-g');
hold on;
plot(f(3:1249),gainy-gaindirect,'-r');
legend({'ideal bandpass filter','actual IIR = final - all pass'},'FontSize',20);
title('Magnitude Response');
xlabel('Frequency(Hz)');
ylabel('Magnitude Response(dB)');
hold off;

figure;
plot(f(3:1249),unwrap(angle(h(3:1249))).*180./pi,'-g');
hold on;
plot(f(3:1249),phasey-phasedirect,'-r');
legend({'ideal bandpass filter','actual IIR = final - all pass'},'FontSize',20);
title('Phase Response');
xlabel('Frequency(Hz)');
ylabel('Phase Response(deg)');
hold off;

```

- Assembly for Direct Form II Implementation with no Optimisation

```

bandpass_direct2_IIR:
0x0000D070: 07BF005A      SUB.L2      SP,8,SP
0x0000D074: 02016E4E      LDH.D2T2   *+B14[366],B4
0x0000D078: 00006001      NOP        4
0x0000D07C: 00000000 ||      NOP
0x0000D080: 0310073B      INTDP.L2   B4,B7:B6
0x0000D084: 0200BA6E ||      LDW.D2T2   *+B14[186],B4
0x0000D088: 00006000      NOP        4
0x0000D08C: 031002F6      STW.D2T2   B6,*+B4[0]
0x0000D090: 039022F6      STW.D2T2   B7,*+B4[1]
0x0000D094: 0200BD6E      LDW.D2T2   *+B14[189],B4
0x0000D098: 00006000      NOP        4
0x0000D09C: 023C22F6      STW.D2T2   B4,*+SP[1]
0x0000D0A0: 00100ADA      CMPLT.L2   0,B4,B0
0x0000D0A4: 30001A90      B.S1       C$DW$L$bandpass_direct2_IIR$2$E (PC+212 = 0x0000d174)
0x0000D0A8: 00008000      NOP        5
C$DW$L$bandpass_direct2_IIR$2$B, C$L4:
0x0000D0AC: 0300BA6C      LDW.D2T1   *+B14[186],A6
0x0000D0B0: 02881428      MVK.S1     0x1028,A5
0x0000D0B4: 028000E8      MVKH.S1    0x10000,A5
0x0000D0B8: 02101059      MV.L1X     B4,A4
0x0000D0BC: 00000000 ||      NOP
0x0000D0C0: 01901059      MV.L1X     B4,A3
0x0000D0C4: 02148B64 ||      LDDW.D1T1  *+A5[A4],A5:A4
0x0000D0C8: 03186B64      LDDW.D1T1  *+A6[A3],A7:A6
0x0000D0CC: 0480BA6C      LDW.D2T1   *+B14[186],A9
0x0000D0D0: 00004000      NOP        3
0x0000D0D4: 0310C700      MPYDP.M1   A7:A6,A5:A4,A7:A6
0x0000D0D8: 02240364      LDDW.D1T1  *+A9[0],A5:A4
0x0000D0DC: 0000E000      NOP        8
0x0000D0E0: 02188338      SUBDP.L1   A5:A4,A7:A6,A5:A4
0x0000D0E4: 0000A000      NOP        6
0x0000D0E8: 02A42274      STW.D1T1   A5,*+A9[1]
0x0000D0EC: 02240274      STW.D1T1   A4,*+A9[0]
0x0000D0F0: 023C22E6      LDW.D2T2   *+SP[1],B4
0x0000D0F4: 0200BA6C      LDW.D2T1   *+B14[186],A4
0x0000D0F8: 02880C2A      MVK.S2     0x1018,B5
0x0000D0FC: 028000EA      MVKH.S2    0x10000,B5
0x0000D100: 00000000      NOP
0x0000D104: 01901058      MV.L1X     B4,A3
0x0000D108: 02106B65      LDDW.D1T1  *+A4[A3],A5:A4
0x0000D10C: 02148BE6 ||      LDDW.D2T2  *+B5[B4],B5:B4
0x0000D110: 00006000      NOP        4
0x0000D114: 02109700      MPYDP.M1X  A5:A4,B5:B4,A5:A4
0x0000D118: 0280B96E      LDW.D2T2   *+B14[185],B5
0x0000D11C: 0200B86E      LDW.D2T2   *+B14[184],B4
0x0000D120: 0000C000      NOP        7
0x0000D124: 0210931A      ADDDP.L2X  B5:B4,A5:A4,B5:B4
0x0000D128: 0000A000      NOP        6
0x0000D12C: 0280B97E      STW.D2T2   B5,*+B14[185]
0x0000D130: 0200B87E      STW.D2T2   B4,*+B14[184]
0x0000D134: 0300BA6C      LDW.D2T1   *+B14[186],A6
0x0000D138: 028FE058      SUB.L1     A3,1,A5
0x0000D13C: 00004000      NOP        3
0x0000D140: 0218AB66      LDDW.D1T2  *+A6[A5],B5:B4
0x0000D144: 02180058      MV.L1      A6,A4
0x0000D148: 01907E40      ADDAD.D1   A4,A3,A3
0x0000D14C: 00002000      NOP        2
0x0000D150: 028C2276      STW.D1T2   B5,*+A3[1]

```

0x0000D154:	020C0276	STW.D1T2	B4,*+A3[0]
0x0000D158:	023C22E6	LDW.D2T2	*+SP[1],B4
0x0000D15C:	00006000	NOP	4
0x0000D160:	0213E05A	SUB.L2	B4,1,B4
0x0000D164:	023C22F6	STW.D2T2	B4,*+SP[1]
0x0000D168:	00100ADA	CMPLT.L2	0,B4,B0
0x0000D16C:	2FFFE990	[ B0] B.S1	C\$L4 (PC-180 = 0x0000d0ac)
0x0000D170:	00008000	NOP	5
C\$L5, C\$DW\$L\$_bandpass_direct2_IIR\$2\$E:			
0x0000D174:	0200BA6E	LDW.D2T2	*+B14[186],B4
0x0000D178:	01880C28	MVK.S1	0x1018,A3
0x0000D17C:	018000E8	MVKH.S1	0x10000,A3
0x0000D180:	020C0364	LDDW.D1T1	*+A3[0],A5:A4
0x0000D184:	0380B96E	LDW.D2T2	*+B14[185],B7
0x0000D188:	021003E6	LDDW.D2T2	*+B4[0],B5:B4
0x0000D18C:	0300B86E	LDW.D2T2	*+B14[184],B6
0x0000D190:	00004000	NOP	3
0x0000D194:	02109702	MPYDP.M2X	B5:B4,A5:A4,B5:B4
0x0000D198:	00010000	NOP	9
0x0000D19C:	0218831A	ADDDP.L2	B5:B4,B7:B6,B5:B4
0x0000D1A0:	0000A000	NOP	6
0x0000D1A4:	0200B87E	STW.D2T2	B4,*+B14[184]
0x0000D1A8:	0280B97E	STW.D2T2	B5,*+B14[185]
0x0000D1AC:	07BD005A	ADD.L2	8,SP,SP
0x0000D1B0:	000C0362	B.S2	B3
0x0000D1B4:	00008000	NOP	5

- Assembly for Direct Form II Implementation with o2 Optimisation

```

bandpass_direct2_IIR:
0x0000D2BC: 02016E4E      LDH.D2T2      *+B14[366],B4
0x0000D2C0: 0480BA6C      LDW.D2T1      *+B14[186],A9
0x0000D2C4: 00004000      NOP           3
0x0000D2C8: 0210073A      INTDP.L2      B4,B5:B4
0x0000D2CC: 00006000      NOP           4
0x0000D2D0: 02240276      STW.D1T2      B4,*+A9[0]
0x0000D2D4: 02A42276      STW.D1T2      B5,*+A9[1]
0x0000D2D8: 00088C29      MVK.S1        0x1118,A0
0x0000D2DC: 0200BD6E ||    LDW.D2T2      *+B14[189],B4
0x0000D2E0: 0288942A      MVK.S2        0x1128,B5
0x0000D2E4: 0380B96C      LDW.D2T1      *+B14[185],A7
0x0000D2E8: 028000EA      MVKH.S2       0x10000,B5
0x0000D2EC: 000000E8      MVKH.S1       0x10000,A0
0x0000D2F0: 00100ADA      CMPLT.L2      0,B4,B0
0x0000D2F4: 30002610      [|B0] B.S1     C&L18 (PC+304 = 0x0000d410)
0x0000D2F8: 0300B86C      LDW.D2T1      *+B14[184],A6
0x0000D2FC: 02949E42      ADDAD.D2      B5,B4,B5
0x0000D300: 01901058      MV.L1X        B4,A3
0x0000D304: 02007E40      ADDAD.D1      A0,A3,A4
0x0000D308: 01A47E40      ADDAD.D1      A9,A3,A3
0x0000D30C: 008403E3      MVC.S2        CSR,B1
0x0000D310: 00901059 ||    MV.L1X        B4,A1
0x0000D314: 010000A9 ||    MVK.S1        0x0001,A2
0x0000D318: 0010105B ||    MV.L2X        A4,B0
0x0000D31C: 00000000 ||    NOP
0x0000D320: 0207CF5B      AND.L2        -2,B1,B4
0x0000D324: 04141059 ||    MV.L1X        B5,A8
0x0000D328: 028C11A2 ||    MV.S2X        A3,B5
0x0000D32C: 009003A2      MVC.S2        B4,CSR
C$DW$L$ bandpass_direct2_IIR$4$B, C$L16, C$L15:
0x0000D330: 03240364      LDDW.D1T1     *+A9[0],A7:A6
0x0000D334: 00006000      NOP           4
0x0000D338: 0210C338      SUBDP.L1      A7:A6,A5:A4,A5:A4
0x0000D33C: 0000A000      NOP           6
0x0000D340: B2240274      [|A2] STW.D1T1 A4,*+A9[0]
0x0000D344: B2A42274      [|A2] STW.D1T1 A5,*+A9[1]
0x0000D348: B40035E7      [|A2] LDDW.D2T2 *B0--[1],B9:B8
0x0000D34C: B30C2364 || [|A2] LDDW.D1T1 *+A3[1],A7:A6
0x0000D350: 0380B96F      LDW.D2T2      *+B14[185],B7
0x0000D354: B20C0364 || [|A2] LDDW.D1T1 *+A3[0],A5:A4
0x0000D358: 0300B86E      LDW.D2T2      *+B14[184],B6
0x0000D35C: 00002000      NOP           2
0x0000D360: 04191702      MPYDP.M2X     B9:B8,A7:A6,B9:B8
0x0000D364: 00004000      NOP           3
0x0000D368: 0410105A      MV.L2X        A4,B8
0x0000D36C: 0214105A      MV.L2X        A5,B4
0x0000D370: B41454F6      [|A2] STW.D2T2 B8,*B5--[2]
0x0000D374: B21462F6      [|A2] STW.D2T2 B4,*+B5[3]
0x0000D378: 02203564      LDDW.D1T1     *A8--[1],A5:A4
0x0000D37C: 030C3564      LDDW.D1T1     *A3--[1],A7:A6
0x0000D380: 0319031A      ADDDP.L2      B9:B8,B7:B6,B7:B6
0x0000D384: 00000000      NOP
0x0000D388: 8087E058      [ A1] SUB.L1   A1,1,A1
0x0000D38C: 8FFFF610      [ A1] B.S1     C&L15 (PC-80 = 0x0000d330)
0x0000D390: 0210C700      MPYDP.M1      A7:A6,A5:A4,A5:A4
0x0000D394: 00002000      NOP           2

```

0x0000D398:	B300B87F	[!A2]	STW.D2T2	B6,*+B14[184]
0x0000D39C:	00000000		NOP	
0x0000D3A0:	A10BE059	[ A2]	SUB.L1	A2,1,A2
0x0000D3A4:	B380B97E	[!A2]	STW.D2T2	B7,*+B14[185]
C\$L17, C\$DW\$L\$_bandpass_direct2_IIR\$4\$E:				
0x0000D3A8:	03240364		LDDW.D1T1	*+A9[0],A7:A6
0x0000D3AC:	00006000		NOP	4
0x0000D3B0:	0210C338		SUBDP.L1	A7:A6,A5:A4,A5:A4
0x0000D3B4:	0000A000		NOP	6
0x0000D3B8:	02240274		STW.D1T1	A4,*+A9[0]
0x0000D3BC:	02A42274		STW.D1T1	A5,*+A9[1]
0x0000D3C0:	040035E7		LDDW.D2T2	*B0--[1],B9:B8
0x0000D3C4:	030C2364		LDDW.D1T1	*+A3[1],A7:A6
0x0000D3C8:	0380B96F		LDW.D2T2	*+B14[185],B7
0x0000D3CC:	020C0364		LDDW.D1T1	*+A3[0],A5:A4
0x0000D3D0:	0300B86E		LDW.D2T2	*+B14[184],B6
0x0000D3D4:	00002000		NOP	2
0x0000D3D8:	04191702		MPYDP.M2X	B9:B8,A7:A6,B9:B8
0x0000D3DC:	00004000		NOP	3
0x0000D3E0:	0410105A		MV.L2X	A4,B8
0x0000D3E4:	0214105A		MV.L2X	A5,B4
0x0000D3E8:	041454F6		STW.D2T2	B8,*B5--[2]
0x0000D3EC:	021462F6		STW.D2T2	B4,*+B5[3]
0x0000D3F0:	00002000		NOP	2
0x0000D3F4:	0319031A		ADDDP.L2	B9:B8,B7:B6,B7:B6
0x0000D3F8:	008403A2		MVC.S2	B1,CSR
0x0000D3FC:	00008000		NOP	5
0x0000D400:	0380B97F		STW.D2T2	B7,*+B14[185]
0x0000D404:	039C1058		MV.L1X	B7,A7
0x0000D408:	03181059		MV.L1X	B6,A6
0x0000D40C:	0300B87E		STW.D2T2	B6,*+B14[184]
C\$L18:				
0x0000D410:	02000364		LDDW.D1T1	*+A0[0],A5:A4
0x0000D414:	04240364		LDDW.D1T1	*+A9[0],A9:A8
0x0000D418:	00006000		NOP	4
0x0000D41C:	02110700		MPYDP.M1	A9:A8,A5:A4,A5:A4
0x0000D420:	00010000		NOP	9
0x0000D424:	02188318		ADDDP.L1	A5:A4,A7:A6,A5:A4
0x0000D428:	0000A000		NOP	6
0x0000D42C:	0200B87C		STW.D2T1	A4,*+B14[184]
0x0000D430:	0280B97C		STW.D2T1	A5,*+B14[185]
0x0000D434:	000C0362		B.S2	B3
0x0000D438:	00008000		NOP	5

- Assembly for Direct Form II Transposed Implementation with no Optimisation

```

bandpass_direct2_transposed_IIR:
0x0000D1B8: 07BF005A      SUB.L2      SP,8,SP
0x0000D1BC: 02016E4E      LDH.D2T2   *+B14[366],B4
0x0000D1C0: 01880C28      MVK.S1     0x1018,A3
0x0000D1C4: 018000E8      MVKH.S1    0x10000,A3
0x0000D1C8: 020C0364      LDDW.D1T1  **A3[0],A5:A4
0x0000D1CC: 0300BC6E      LDW.D2T2   *+B14[188],B6
0x0000D1D0: 0210073A      INTDP.L2   B4,B5:B4
0x0000D1D4: 00006000      NOP        4
0x0000D1D8: 02109702      MPYDP.M2X  B5:B4,A5:A4,B5:B4
0x0000D1DC: 031803E6      LDDW.D2T2  **B6[0],B7:B6
0x0000D1E0: 0000E000      NOP        8
0x0000D1E4: 0210C31A      ADDDP.L2   B7:B6,B5:B4,B5:B4
0x0000D1E8: 0000A000      NOP        6
0x0000D1EC: 0200B87E      STW.D2T2   B4,*+B14[184]
0x0000D1F0: 0280B97E      STW.D2T2   B5,*+B14[185]
0x0000D1F4: 020000AA      MVK.S2     0x0001,B4
0x0000D1F8: 023C22F6      STW.D2T2   B4,*+SP[1]
0x0000D1FC: 0200BD6E      LDW.D2T2   *+B14[189],B4
0x0000D200: 02BC22E6      LDW.D2T2   **SP[1],B5
0x0000D204: 00006000      NOP        4
0x0000D208: 0010AAFA      CMPLT.L2   B5,B4,B0
0x0000D20C: 30001410      [!B0] B.S1  C$DW$L$_bandpass_direct2_transposed_IIR$2$E (PC+160 = 0x0000d2a0)
0x0000D210: 00008000      NOP        5
C$DW$L$_bandpass_direct2_transposed_IIR$2$B, C$L6:
0x0000D214: 02016E4E      LDH.D2T2   *+B14[366],B4
0x0000D218: 0408142B      MVK.S2     0x1028,B8
0x0000D21C: 0380B96E      LDW.D2T2   *+B14[185],B7
0x0000D220: 0300B86E      LDW.D2T2   *+B14[184],B6
0x0000D224: 040000EA      MVKH.S2    0x10000,B8
0x0000D228: 0420ABE6      LDDW.D2T2  **B8[B5],B9:B8
0x0000D22C: 02080C28      MVK.S1     0x1018,A4
0x0000D230: 01941058      MV.L1X     B5,A3
0x0000D234: 020000E8      MVKH.S1    0x10000,A4
0x0000D238: 02106B64      LDDW.D1T1  **A4[A3],A5:A4
0x0000D23C: 0210073A      INTDP.L2   B4,B5:B4
0x0000D240: 03190702      MPYDP.M2   B9:B8,B7:B6,B7:B6
0x0000D244: 0480BC6C      LDW.D2T1   *+B14[188],A9
0x0000D248: 0300BC6C      LDW.D2T1   *+B14[188],A6
0x0000D24C: 040FE058      SUB.L1     A3,1,A8
0x0000D250: 02109702      MPYDP.M2X  B5:B4,A5:A4,B5:B4
0x0000D254: 00010000      NOP        9
0x0000D258: 0218833A      SUBDP.L2   B5:B4,B7:B6,B5:B4
0x0000D25C: 02246B64      LDDW.D1T1  **A9[A3],A5:A4
0x0000D260: 01991E40      ADDAD.D1   A6,A8,A3
0x0000D264: 00006000      NOP        4
0x0000D268: 02109318      ADDDP.L1X  A5:A4,B5:B4,A5:A4
0x0000D26C: 0000A000      NOP        6
0x0000D270: 028C2274      STW.D1T1   A5,*+A3[1]
0x0000D274: 020C0274      STW.D1T1   A4,*+A3[0]
0x0000D278: 023C22E6      LDW.D2T2   **SP[1],B4
0x0000D27C: 00006000      NOP        4
0x0000D280: 0210205A      ADD.L2     1,B4,B4
0x0000D284: 023C22F6      STW.D2T2   B4,*+SP[1]
0x0000D288: 0200BD6E      LDW.D2T2   *+B14[189],B4
0x0000D28C: 02BC22E6      LDW.D2T2   **SP[1],B5
0x0000D290: 00006000      NOP        4
0x0000D294: 0010AAFA      CMPLT.L2   B5,B4,B0

```



```

0x0000D298: 2FFFF290 [ B0] B.S1 C$L6 (PC-108 = 0x0000d214)
0x0000D29C: 00008000 NOP 5
C$L7, C$DW$L$_bandpass_direct2_transposed_IIR$2$E:
0x0000D2A0: 02816E4E LDH.D2T2 *+B14[366],B5
0x0000D2A4: 0308142B MVK.S2 0x1028,B6
0x0000D2A8: 0480B96E || LDW.D2T2 *+B14[185],B9
0x0000D2AC: 0400B86E LDW.D2T2 *+B14[184],B8
0x0000D2B0: 030000EA MVKH.S2 0x10000,B6
0x0000D2B4: 03188BE6 LDDW.D2T2 *+B6[B4],B7:B6
0x0000D2B8: 02080C28 MVK.S1 0x1018,A4
0x0000D2BC: 01901058 MV.L1X B4,A3
0x0000D2C0: 020000E8 MVKH.S1 0x10000,A4
0x0000D2C4: 02106B64 LDDW.D1T1 *+A4[A3],A5:A4
0x0000D2C8: 0214073A INTDP.L2 B5,B5:B4
0x0000D2CC: 0320C702 MPYDP.M2 B7:B6,B9:B8,B7:B6
0x0000D2D0: 00004000 NOP 3
0x0000D2D4: 02109702 MPYDP.M2X B5:B4,A5:A4,B5:B4
0x0000D2D8: 00010000 NOP 9
0x0000D2DC: 0218833A SUBDP.L2 B5:B4,B7:B6,B5:B4
0x0000D2E0: 0380BC6E LDW.D2T2 *+B14[188],B7
0x0000D2E4: 030FF05A SUB.L2X A3,1,B6
0x0000D2E8: 00004000 NOP 3
0x0000D2EC: 031CDE42 ADDAD.D2 B7,B6,B6
0x0000D2F0: 021802F6 STW.D2T2 B4,*+B6[0]
0x0000D2F4: 029822F6 STW.D2T2 B5,*+B6[1]
0x0000D2F8: 07BD005A ADD.L2 8,SP,SP
0x0000D2FC: 000C0362 B.S2 B3
0x0000D300: 00008000 NOP 5
0x0000D304: 00000000 NOP
0x0000D308: 00000000 NOP
0x0000D30C: 00000000 NOP
0x0000D310: 00000000 NOP
0x0000D314: 00000000 NOP
0x0000D318: 00000000 NOP
0x0000D31C: 00000000 NOP

```

- Assembly for Direct Form II Transposed Implementation with o2 Optimisation

```

C$DW$LS_main$3$E, bandpass_direct2_transposed_IIR:
0x0000D018: 04BC1059      MV.L1X      SP,A9
0x0000D01C: 07BD54F4 ||    STW.D2T1    FP,*SP--[10]
0x0000D020: 05BD22F6      STW.D2T2    B11,*+SP[9]
0x0000D024: 053D02F6      STW.D2T2    B10,*+SP[8]
0x0000D028: 01BCE2F6      STW.D2T2    B3,*+SP[7]
0x0000D02C: 07248074      STW.D1T1    A14,*-A9[4]
0x0000D030: 06A4A074      STW.D1T1    A13,*-A9[5]
0x0000D034: 0624C074      STW.D1T1    A12,*-A9[6]
0x0000D038: 05A4E074      STW.D1T1    A11,*-A9[7]
0x0000D03C: 05250074      STW.D1T1    A10,*-A9[8]
0x0000D040: 05016E4E      LDH.D2T2    *+B14[366],B10
0x0000D044: 07888C28      MVK.S1      0x1118,FP
0x0000D048: 078000E8      MVKH.S1     0x10000,FP
0x0000D04C: 023C0364      LDDW.D1T1    *+FP[0],A5:A4
0x0000D050: 0680BC6C      LDW.D2T1    *+B14[188],A13
0x0000D054: 0328073A      INTDP.L2     B10,B7:B6
0x0000D058: 00006000      NOP          4
0x0000D05C: 03189700      MPYDP.M1X    A5:A4,B7:B6,A7:A6
0x0000D060: 02340364      LDDW.D1T1    *+A13[0],A5:A4
0x0000D064: 0000E000      NOP          8
0x0000D068: 03188318      ADDDP.L1     A5:A4,A7:A6,A7:A6
0x0000D06C: 0000A000      NOP          6
0x0000D070: 0300B87C      STW.D2T1    A6,*+B14[184]
0x0000D074: 0380B97C      STW.D2T1    A7,*+B14[185]
0x0000D078: 0700BD6C      LDW.D2T1    *+B14[189],A14
0x0000D07C: 00006000      NOP          4
0x0000D080: 00B848D8      CMPGT.L1     2,A14,A1
0x0000D084: 80003C10      [ A1] B.S1    C&L14 (PC+480 = 0x0000d260)
0x0000D088: 00008000      NOP          5
0x0000D08C: 04889429      MVK.S1      0x1128,A9
0x0000D090: 0235E0F9 ||    SUB.L1      FP,A13,A4
0x0000D094: 02803C2B ||    MVK.S2     0x0078,B5
0x0000D098: 01B5E8C1 ||    SUB.D1     A13,FP,A3
0x0000D09C: 003BF05A ||    SUB.L2X    A14,1,B0
0x0000D0A0: 048000E9      MVKH.S1     0x10000,A9
0x0000D0A4: 0200442B ||    MVK.S2     0x0088,B4
0x0000D0A8: 01BD105B ||    ADD.L2X    8,FP,B3
0x0000D0AC: 06340059 ||    MV.L1      A13,A12
0x0000D0B0: 00340940 ||    MV.D1      A13,A0
0x0000D0B4: 02803C29      MVK.S1      0x0078,A5
0x0000D0B8: 0480442B ||    MVK.S2     0x0088,B9
0x0000D0BC: 00000000      NOP
0x0000D0C0: 04148AF9      CMPLT.L1     A4,A5,A8
0x0000D0C4: 0225A5E1 ||    SUB.S1     A13,A9,A4
0x0000D0C8: 02A5A8C0 ||    SUB.D1     A9,A13,A5
0x0000D0CC: 02109AF9      CMPLT.L1X    A4,B4,A4
0x0000D0D0: 0214B8FA ||    CMPGT.L2X  B5,A5,B4
0x0000D0D4: 02109F7B      AND.L2X     B4,A4,B4
0x0000D0D8: 02247AF9 ||    CMPLT.L1X  A3,B9,A4
0x0000D0DC: 00000000 ||    NOP
0x0000D0E0: 02208F79      AND.L1      A4,A8,A4
0x0000D0E4: 02102DDA ||    XOR.L2     1,B4,B4
0x0000D0E8: 02102DD9      XOR.L1      1,A4,A4
0x0000D0EC: 0428073A ||    INTDP.L2   B10,B9:B8
0x0000D0F0: 00909F7A      AND.L2X     B4,A4,B1
0x0000D0F4: 40001290      [ B1] B.S1    C&L8 (PC+148 = 0x0000d174)
0x0000D0F8: 02BBE058      SUB.L1      A14,1,A5
0x0000D0FC: 01A50058      ADD.L1      8,A9,A3
0x0000D100: 023D0058      ADD.L1      8,FP,A4

```

```

0x0000D104: 0225105A      ADD.L2X      8,A9,B4
0x0000D108: 40802ADA      [ B1] CMPLT.L2 1,B0,B1
0x0000D10C: 048403E3      MVC.S2      CSR,B9
0x0000D110: 01901059 ||    MV.L1X      B4,A3
0x0000D114: 0014105A ||    MV.L2X      A5,B0
0x0000D118: 0227CF5B      AND.L2      -2,B9,B4
0x0000D11C: 041011A2 ||    MV.S2X      A4,B8
0x0000D120: 009003A2      MVC.S2      B4,CSR
C$DW$L$_bandpass_direct2_transposed_IIR$5$B, C$L6, C$L5:
0x0000D124: 020C3765      LDDW.D1T1   *A3++[1],A5:A4
0x0000D128: 022037E6 ||    LDDW.D2T2   *B8++[1],B5:B4
0x0000D12C: 00006000      NOP         4
0x0000D130: 0210C701      MPYDP.M1    A7:A6,A5:A4,A5:A4
0x0000D134: 0210C702 ||    MPYDP.M2    B7:B6,B5:B4,B5:B4
0x0000D138: 00010000      NOP         9
0x0000D13C: 021093B8      SUBDP.L1X   B5:B4,A5:A4,A5:A4
0x0000D140: 00000000      NOP
0x0000D144: 04003364      LDDW.D1T1   *++A0[1],A9:A8
0x0000D148: 00006000      NOP         4
0x0000D14C: 02110318      ADDDP.L1    A9:A8,A5:A4,A5:A4
0x0000D150: 00000000      NOP
0x0000D154: 2003E05A      [ B0] SUB.L2  B0,1,B0
0x0000D158: 2FFFFC92      [ B0] B.S2     C$L5 (PC-28 = 0x0000d124)
0x0000D15C: 00004000      NOP         3
0x0000D160: 02004074      STW.D1T1    A4,*-A0[2]
0x0000D164: 02802074      STW.D1T1    A5,*-A0[1]
C$L7, C$DW$L$_bandpass_direct2_transposed_IIR$5$E:
0x0000D168: 00002010      B.S1        C$L14 (PC+256 = 0x0000d260)
0x0000D16C: 00A403A2      MVC.S2      B9,CSR
0x0000D170: 00006000      NOP         4
C$L8:
0x0000D174: 40000D10      [ B1] B.S1        C$L10 (PC+104 = 0x0000d1c8)
0x0000D178: 00008001      NOP         5
0x0000D17C: 00000000 ||    NOP
C$DW$L$_bandpass_direct2_transposed_IIR$9$B, C$L9:
0x0000D180: 020C3765      LDDW.D1T1   *A3++[1],A5:A4
0x0000D184: 020C37E6 ||    LDDW.D2T2   *B3++[1],B5:B4
0x0000D188: 00006000      NOP         4
C$DW$L$_bandpass_direct2_transposed_IIR$10$B, C$DW$L$_bandpass_direct2_transposed_IIR$9$E:
0x0000D18C: 0210C701      MPYDP.M1    A7:A6,A5:A4,A5:A4
0x0000D190: 02110702 ||    MPYDP.M2    B9:B8,B5:B4,B5:B4
0x0000D194: 04302364      LDDW.D1T1   *+A12[1],A9:A8
0x0000D198: 0003E05A      SUB.L2      B0,1,B0
0x0000D19C: 0000C000      NOP         7
0x0000D1A0: 021093B8      SUBDP.L1X   B5:B4,A5:A4,A5:A4
0x0000D1A4: 0000A000      NOP         6
0x0000D1A8: 02110318      ADDDP.L1    A9:A8,A5:A4,A5:A4
0x0000D1AC: 00002000      NOP         2
0x0000D1B0: 2FFFFC10      [ B0] B.S1        C$L9 (PC-32 = 0x0000d180)
0x0000D1B4: 30001810      [!B0] B.S1       C$L14 (PC+192 = 0x0000d260)
0x0000D1B8: 00002000      NOP         2
0x0000D1BC: 02303674      STW.D1T1    A4,*A12++[1]
0x0000D1C0: 02B03674      STW.D1T1    A5,*A12++[1]
C$DW$L$_bandpass_direct2_transposed_IIR$10$E:
0x0000D1C4: 00000000      NOP
C$L10:
0x0000D1C8: 058403E3      MVC.S2      CSR,B11
0x0000D1CC: 0000405B ||    ADD.L2      2,B0,B0
0x0000D1D0: 030C37E7 ||    LDDW.D2T2   *B3++[1],B7:B6
0x0000D1D4: 040C3764 ||    LDDW.D1T1   *A3++[1],A9:A8

```

```

0x0000D1D8: 022FCF5B      AND.L2      -2,B11,B4
0x0000D1DC: 008001AA ||    MVK.S2      0x0003,B1
0x0000D1E0: 009003A2      MVC.S2      B4,CSR
0x0000D1E4: 010002AA      MVK.S2      0x0005,B2
C$L11:
0x0000D1E8: 051801A1      MV.S1       A6,A10
0x0000D1EC: 059C0941 ||    MV.D1       A7,A11
0x0000D1F0: 0103B059 ||    SUB.L1X     B0,3,A2
0x0000D1F4: 00000312 ||    B.S2        C$L12 (PC+24 = 0x0000d1f8)
C$DW$L$_bandpass_direct2_transposed_IIR$14$B, C$L12:
0x0000D1F8: 0010C319      ADDDP.L1     A7:A6,A5:A4,A1:A0
0x0000D1FC: 53303364 || [!B1] LDDW.D1T1    *++A12[1],A7:A6
0x0000D200: 00000000      NOP
0x0000D204: A40C3764 [A2] LDDW.D1T1    *A3++[1],A9:A8
0x0000D208: 7030C075 [!B2] STW.D1T1    A0,*-A12[6]
0x0000D20C: 2003E05B || [B0] SUB.L2      B0,1,B0
0x0000D210: 021893B9 ||    SUBDP.L1X   B5:B4,A7:A6,A5:A4
0x0000D214: 03214701 ||    MPYDP.M1     A11:A10,A9:A8,A7:A6
0x0000D218: 02190703 ||    MPYDP.M2     B9:B8,B7:B6,B5:B4
0x0000D21C: A30C37E6 || [A2] LDDW.D2T2    *B3++[1],B7:B6
0x0000D220: 4087E05B [B1] SUB.L2      B1,1,B1
0x0000D224: 610829C3 || [B2] SUB.D2      B2,0x1,B2
0x0000D228: A10BE1A1 || [A2] SUB.S1      A2,1,A2
0x0000D22C: 70B0A075 || [!B2] STW.D1T1    A1,*-A12[5]
0x0000D230: 2FFFFB12 || [B0] B.S2        C$L12 (PC-40 = 0x0000d1f8)
C$L13, C$DW$L$_bandpass_direct2_transposed_IIR$14$E:
0x0000D234: 0010C318      ADDDP.L1     A7:A6,A5:A4,A1:A0
0x0000D238: 00002000      NOP          2
0x0000D23C: 00308074      STW.D1T1     A0,*-A12[4]
0x0000D240: 00B06074      STW.D1T1     A1,*-A12[3]
0x0000D244: 00AC03A2      MVC.S2       B11,CSR
0x0000D248: 00000000      NOP
0x0000D24C: 00B02074      STW.D1T1     A1,*-A12[1]
0x0000D250: 03AC0059      MV.L1        A11,A7
0x0000D254: 032801A1 ||    MV.S1       A10,A6
0x0000D258: 00304075 ||    STW.D1T1    A0,*-A12[2]
0x0000D25C: 00000000 ||    NOP
C$L14:
0x0000D260: 01889429      MVK.S1       0x1128,A3
0x0000D264: 0228073B ||    INTDP.L2     B10,B5:B4
0x0000D268: 043DCB64 ||    LDDW.D1T1     *+FP[A14],A9:A8
0x0000D26C: 018000E8      MVKH.S1      0x10000,A3
0x0000D270: 020DCB64      LDDW.D1T1     *+A3[A14],A5:A4
0x0000D274: 01B5DE40      ADDAD.D1     A13,A14,A3
0x0000D278: 00002000      NOP          2
0x0000D27C: 02209702      MPYDP.M2X    B5:B4,A9:A8,B5:B4
0x0000D280: 0210C700      MPYDP.M1     A7:A6,A5:A4,A5:A4
0x0000D284: 00010000      NOP          9
0x0000D288: 0210933A      SUBDP.L2X    B5:B4,A5:A4,B5:B4
0x0000D28C: 0000A000      NOP          6
0x0000D290: 020C4076      STW.D1T2     B4,*-A3[2]
0x0000D294: 028C2076      STW.D1T2     B5,*-A3[1]
0x0000D298: 053C83E7      LDDW.D2T2     *+SP[4],B11:B10
0x0000D29C: 04BC1058 ||    MV.L1X       SP,A9
0x0000D2A0: 01BCE2E6      LDW.D2T2     *+SP[7],B3
0x0000D2A4: 0724C264      LDW.D1T1     *+A9[6],A14
0x0000D2A8: 06244364      LDDW.D1T1     *+A9[2],A13:A12
0x0000D2AC: 05242364      LDDW.D1T1     *+A9[1],A11:A10
0x0000D2B0: 07BD52E4      LDW.D2T1     *++SP[10],FP
0x0000D2B4: 000C0362      B.S2         B3

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