

Finite element models for the study of hydrogen embrittlement of steel structures

Daniella LOPES PINTO ^{1,2*}

`daniella.lopes_pinto@minesparis.psl.eu`

Academic advisor: Jacques BESSON ¹

Industrial advisors: Nikolay OSIPOV ²

¹ Centre des Matériaux, Mines Paris

² Transvalor S.A.

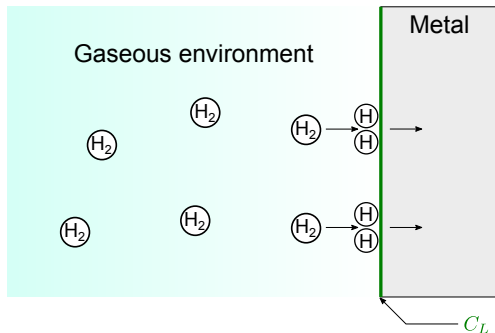
Thesis defense

March 7th 2025

Hydrogen inside metals

Finite element formulation

- **Sieverts' law:** The solubility of a diatomic gas in a metal is proportional to the square root of the gas pressure



$$C_L = \gamma \sqrt{P}$$

Hydrogen solubility (H at./ Iron at.) $\leftarrow C_L$

γ Thermally activated term

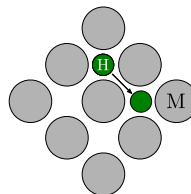
P H_2 pressure (MPa)

- ▶ Model from Sofronis and McMeeking (1989) and corrected by Krom *et al.* (1999)

- ▶ **Hydrogen concentration:** $C = C_L + C_T$

- ▶ Lattice concentration: $C_L = \beta N_L \theta_L$

- ▶ Trapped concentration: $C_T = N_T(\kappa) \theta_T$



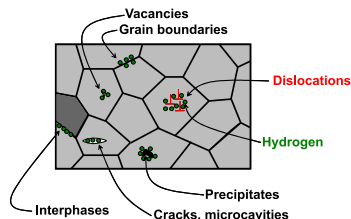
- ▶ **Hydrogen flux:**

$$J = -D_L \nabla C_L + \frac{D_L C_L V_H}{RT} \nabla P$$

- ▶ **Oriani's equilibrium:**

$$\frac{1 - \theta_L}{\theta_L} \frac{\theta_T}{1 - \theta_T} = K$$

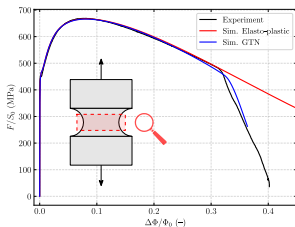
(Coupling terms)



- ▶ The **ductile behavior** of the metal is described by the **GTN model** (Tvergaard *et al.* 1984):

$$\frac{\sigma_{eq}^2}{\sigma_F^2} + 2q_1 f_* \cosh\left(\frac{q_2}{2} \frac{\sigma_{ii}}{\sigma_F}\right) - 1 - q_1^2 f_*^2 = 0$$

$$\dot{f} = \dot{f}_{nucleation} + \dot{f}_{growth}$$



Impurities or second phase particles



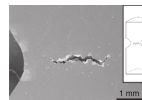
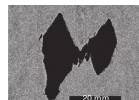
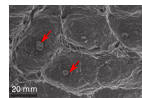
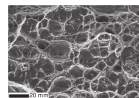
Void nucleation



Void growth



Void coalescence and fracture



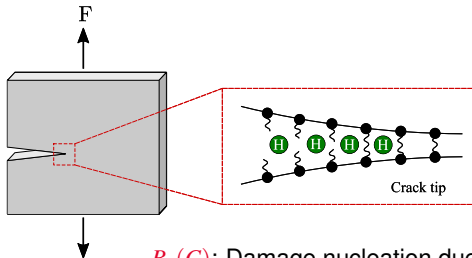
- **Void growth:** Unchanged due to mass conservation

$$\dot{f}_g = (1 - f_g)\text{trace}(\dot{\epsilon}_p)$$

- **Void nucleation:** Proposed dependance on hydrogen concentration

$$\dot{f}_n = A_n(\kappa)\dot{\kappa} + B_n(C)\dot{\kappa}$$

(Coupling terms)



Hydrogen weakens
the cohesive bonds
between atoms

$B_n(C)$: Damage nucleation due to hydrogen
HEDE (Hydrogen Enhanced Decohesion)

Hydrogen inside metals

Finite element formulation

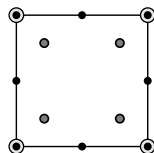
- ▶ Fully implicit finite strain framework
- ▶ Based on a mixed formulation: \underline{u}, P, θ (Zhang *et al.* 2017) and C_L
- ▶ Quadratic elements with reduced integration
- ▶ **Aim:** better pressure fields by avoiding volumetric locking



Advantage

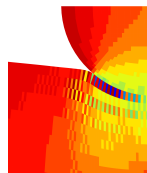
∇P can be directly computed from nodal values

$$J = -D_L \nabla C_L + \frac{D_L C_L V_H}{RT} \nabla P$$



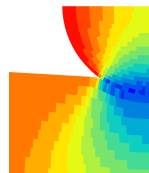
- \underline{u}
- p, θ, C_L
- Integration point

DOF: \underline{u}, C_L



-7500 σ_{ii} 1400

DOF: $\underline{u}, p, \theta, C_L$



-4200 σ_{ii} 1400

- ▶ The use of quadratic element lead to high simulation times
- ▶ B -bar formulation:

Thank you for your attention

Daniella LOPES PINTO

`daniella.lobes_pinto@minesparis.psl.eu`
