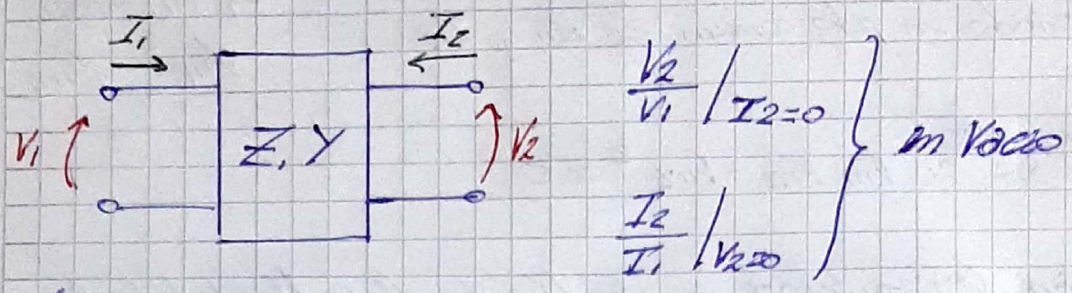


Síntesis de funciones transferencia

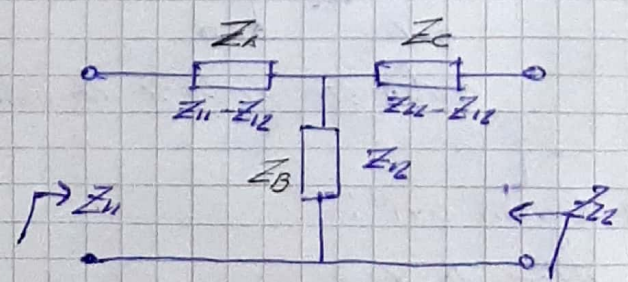


$$\begin{cases} V_1 = Z_{11} I_1 + Z_{12} I_2 \\ V_2 = Z_{21} I_1 + Z_{22} I_2 \end{cases} \Rightarrow \frac{V_2}{V_1} \Big|_{I_2=0} = \frac{Z_{21}}{Z_{11}} = -\frac{Y_{11}}{Y_{12}}$$

$$\begin{cases} I_1 = Y_{11} V_1 + Y_{12} V_2 \\ I_2 = Y_{21} V_1 + Y_{22} V_2 \end{cases} \Rightarrow \frac{I_2}{I_1} \Big|_{V_2=0} = \frac{Y_{21}}{Y_{11}} = -\frac{Z_{21}}{Z_{12}}$$

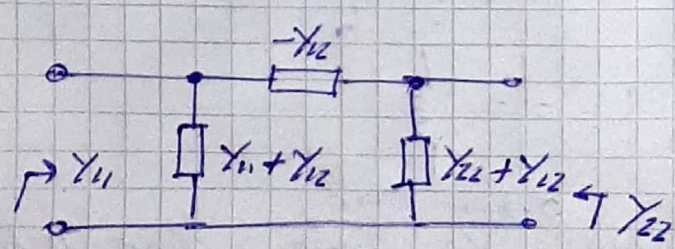
Describimos props de las T(s)

- $T(s) = \frac{P(s)}{Q(s)}$; T(s) debe ser real si s es real
 $\Rightarrow P$ y Q tendrán coeficientes reales
 $\hookrightarrow \text{Gr}\{P\} \leq \text{Gr}\{Q\}$
- Pólos en el semiplano izquierdo
- Ceros sin restricciones.
- T no necesariamente es FRAP.



$$\frac{V_2}{V_1} \Big|_{I_1=0} = \frac{Z_{12}}{Z_{11}} ; \begin{matrix} Z_{11} = Z_k + Z_c \\ Z_{12} = Z_B \end{matrix}$$

Pólos de $Z_{12} \rightarrow Z_{11}$
 " Z_{11} no necesariamente están en Z_{12}
 " Z_{22} " " " "



NOTA 11:40 \Rightarrow 13:00

Condición de residuos

garantizado

$$K_{11} K_{22} - K_{12}^2 \geq 0$$

(reciprocidad)

y simetría

↪ " entre Z_{11} y Z_{12}

$$\hookrightarrow K_{11} = K_{22}$$

Residuo calculado en polo común de Z_{11} y Z_{12}

$$K_{11}^2 - K_{12}^2 \geq 0$$

cuadrupolo compacto

$$K_{11} K_{22} - K_{12}^2 = 0$$

⇒ condición de residuos en un límite de realizabilidad

Ceros de transmisión de una transferencia (red pasiva)

↪ son los mismos para todos los tipos de parámetros

$$Z_1 = Z_2 = -\frac{Y_{12}}{\Delta Y}$$

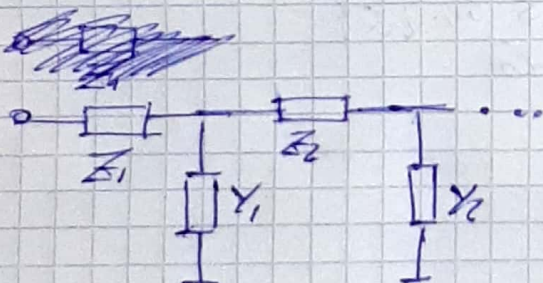
$$Y_{11} = Y_{12} = -\frac{Z_{12}}{\Delta Z}$$

ceros en el SPI

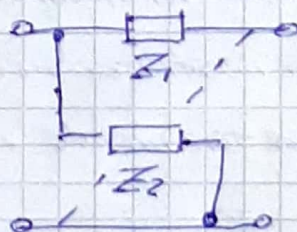
↪ Fase mínima

ceros en el BPO

↪ Fase NO mínima.



salen ser de fase mínima
(red escalera)

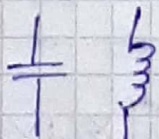
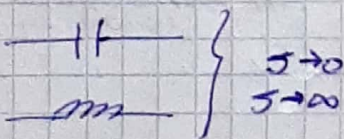


salen ser de fase no mínima.

Los ceros de transmisión se logran con:

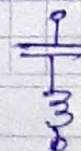
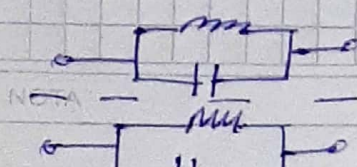
Polos de Z

Polos de Y



$s \rightarrow \infty$ $s \rightarrow 0$

Polo de impedancia o admitancia dan lugar a ceros de transmisión



polos de imp sobre el eje s

$$\frac{V_2}{V_1} \Big|_{I_2=0} = \frac{Z_{12}}{Z_{11}} = -\frac{Y_{12}}{Y_{22}}$$

$$= \frac{P}{Q} = \frac{P/D}{Q/D}$$

D es un denominador auxiliar
los ceros los impone P

Sea que Q/D coincida con Y_{22} o Z_{11}

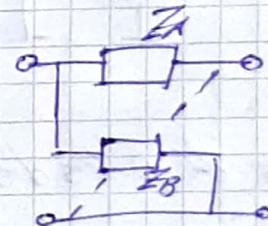
⇒ sintetizar como FE (FRP) respetando ceros de TX
de $\begin{cases} T(s) = V_2/V_1 \\ T(s) = I_2/I_1 \end{cases}$

Síntesis de transformancias descargadas

Sínt. Balanceada

• Sínt. desbalanceada

$$\begin{matrix} \nearrow \oplus \\ \searrow \ominus \end{matrix} \quad \begin{cases} Z_A = Z_{11} - Z_{12} \\ Z_B = Z_{11} + Z_{12} \end{cases}$$



$$Z_{11} = R_{12\oplus} + R_{12\ominus} \quad ; \quad Z_{12} = R_{12\oplus} - (R_{12\ominus})$$

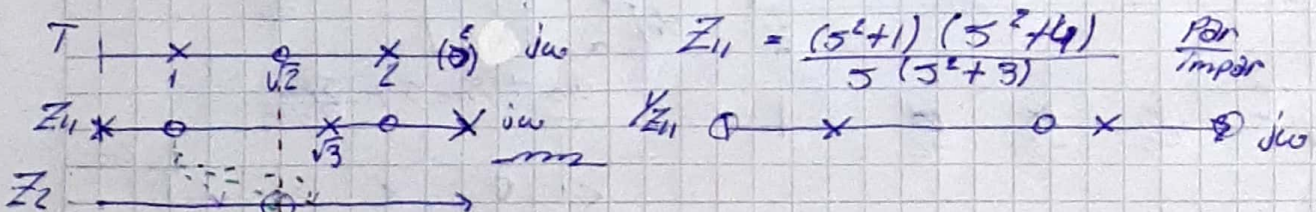
$$\Rightarrow \begin{cases} Z_A = +2 R_{12\ominus} \\ Z_B = 2 R_{12\oplus} \end{cases}$$

$$T(s) = \frac{V_2}{V_1} \Big|_{I_2=0} = \frac{Z_{12}}{Z_{11}} = -\frac{Y_{12}}{Y_{22}} \quad \begin{cases} V_1 = I_1 Z_{11} + I_2 Z_{12} \\ V_2 = I_1 Z_{12} + I_2 Z_{22} \end{cases}$$

EJ:

$$\frac{V_2}{V_1} = \frac{(s^2+2)}{(s^2+1)(s^2+4)} = \frac{P}{Q} = \frac{P/D}{Q/D}$$

→ Z_{11} y Y_{22}



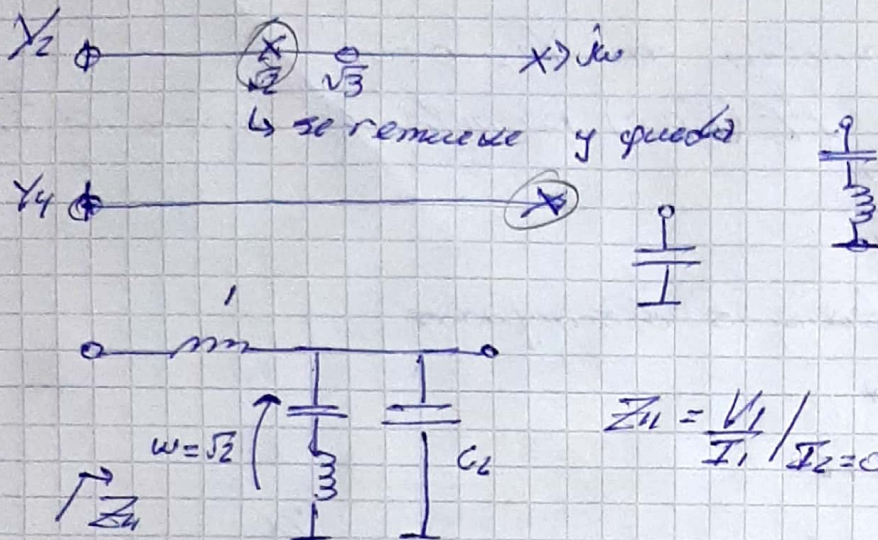
NOTA 14:12 17:13

$$Z_2 = Z_{11} - 5 R_{100}$$

$$R_{100} = \lim_{s \rightarrow \infty} \frac{Z_{11}}{s} = \lim_{s \rightarrow \infty} \frac{(s^2+1)(s^2+4)}{s^2(s^2+3)} = 1$$

$$Z_2 = Z_{11} - 5 R_{100} \Rightarrow Z_2 = \frac{s^4 + s^2 5 + 4 - s^4 - 3s^2}{s^3 + 3s} = \frac{2s^2 + 4}{s^3 + 3s}$$

$$Z_2 = \frac{2(s^2+2)}{s^3+3s} \rightarrow \text{en este caso la cancelación completa justo llevó el cero a 2}$$



$$Z_{11} = \frac{V_1}{I_1} \bigg|_{I_2=0}$$

Síntesis de redes disipativas y descargados.

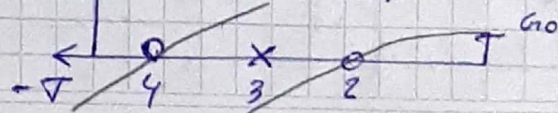
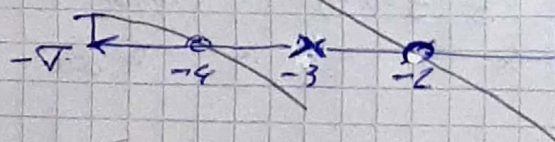
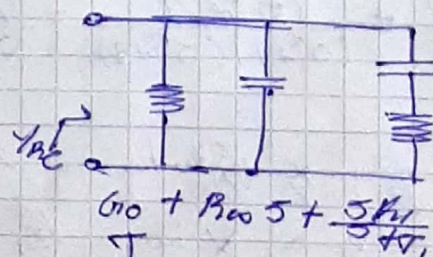
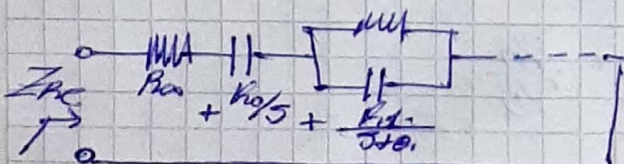
$$T = \frac{V_2}{V_1} = \frac{K_1 (s+1)}{(s+2)(s+4)} = \frac{P/D}{Q/D}$$

$$Q/D = Z_{11} \vee Y_{22} \begin{matrix} \rightarrow Z_{AC} \\ \rightarrow Y_{AC} \end{matrix}$$

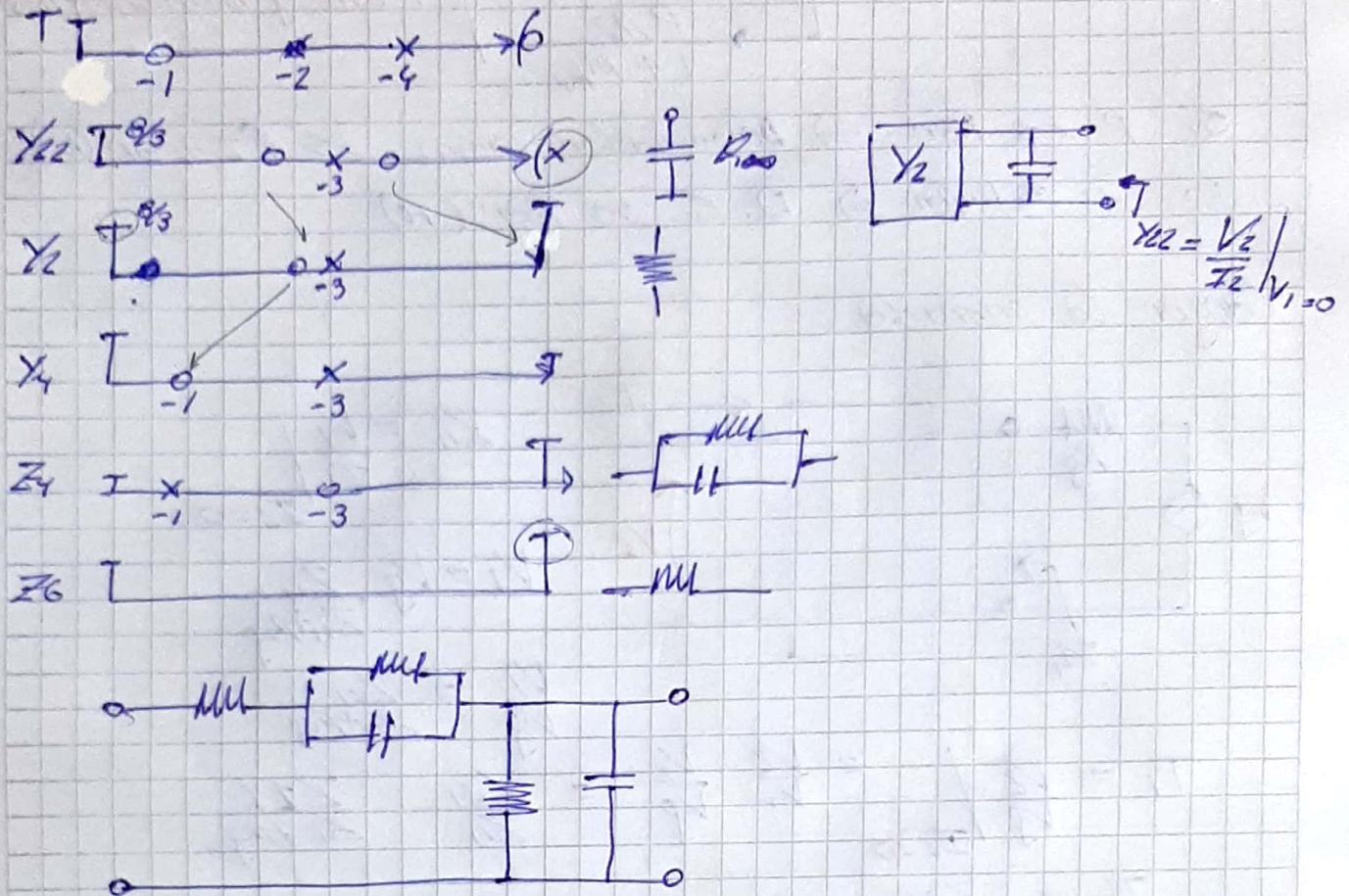
$$Z_{11} = \frac{(s+2)(s+4)}{s(s+3)}$$

\hookrightarrow x alternancia

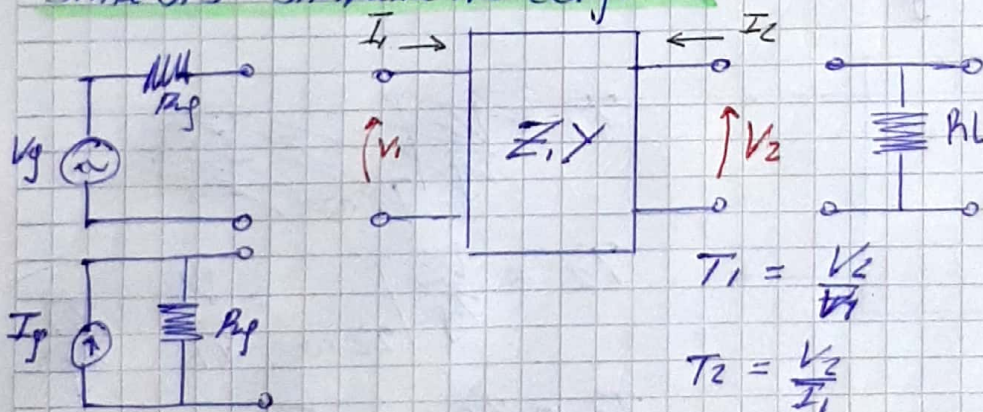
$$Y_{22} = \frac{(s+2)(s+4)}{(s+3)}$$



NOTA



Síntesis simplemente cargadas.



$$T_1 = \frac{V_2}{V_1}$$

$$T_3 = \frac{I_2}{V_1}$$

$$T_2 = \frac{V_2}{I_1}$$

$$T_4 = \frac{I_2}{I_1}$$

$$T_1 = \frac{V_2}{V_1} \Rightarrow V_2 = -I_2 R$$

$$I_2 = -\frac{V_2}{R} = K_1 Y_{21} + V_2 Y_{22} \Rightarrow \frac{V_2}{V_1} = \frac{-Y_{21}}{\frac{1}{R} + Y_{22}} \quad T_1$$

$$T_2 = \frac{V_2}{I_1} ; V_2 = I_1 Z_{21} - \frac{V_1}{R} Z_{22}$$

$$T_2 = \frac{V_2}{I_1} = \frac{Z_{21}}{1 + Z_{22}/R}$$

$$T_3 = \frac{Y_{21}}{1 + Y_{22}/\frac{1}{R}}$$

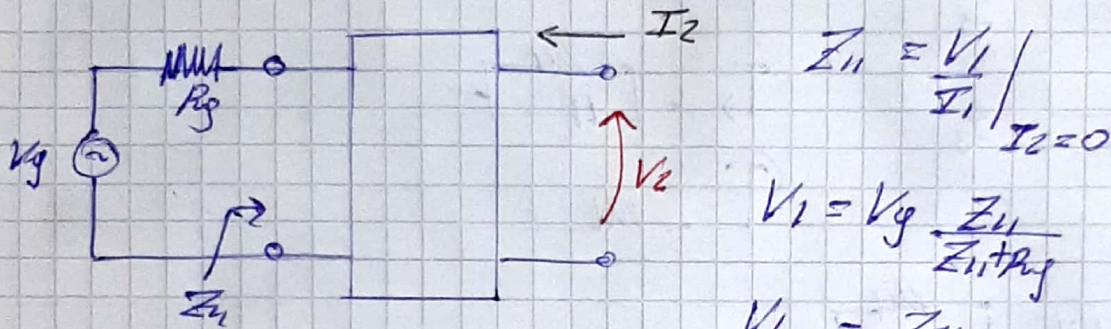
$$T_4 = \frac{-Z_{21}}{R_L + Z_{21}}$$

$$T_x = \frac{P}{Q} = \frac{P}{H+N} = \rightarrow \frac{\frac{P/H}{1+H/N}}{\frac{P/N}{1+H/N}} \quad \left. \vphantom{\frac{P}{H+N}} \right\} \text{FBP y no disipativos}$$

5) P es Par \Rightarrow Denominador comun es P Impar (N)

1) " es Impar \Rightarrow D.C es Par (H)

Cargar la entrada



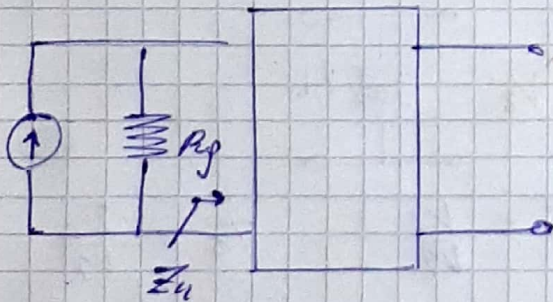
$$Z_{ii} = \frac{V_1}{I_1} \Big|_{I_2=0}$$

$$V_1 = V_g \frac{Z_{ii}}{Z_{ii} + P_g}$$

$$\frac{V_1}{V_g} = \frac{Z_{ii}}{Z_{ii} + P_g}$$

$$T_1 = \frac{V_2}{V_g} \Big|_{I_2=0} = \frac{V_2}{V_1} \cdot \frac{V_1}{V_g} = \frac{Z_{21}}{Z_{ii}} \cdot \frac{Z_{ii}}{Z_{ii} + P_g}$$

$$T_1 = \frac{Z_{21}}{Z_{ii} + P_g}$$



$$T_1 = \frac{V_2}{V_g} \Big|_{I_2=0} = \frac{Z_{21}}{Z_{ii}}$$

$$T_2 = \frac{V_2}{I_g} \Big|_{I_2=0} = \frac{V_2}{I_1} \cdot \frac{I_1}{I_g}$$

$$I_g \cdot \frac{P_g}{P_g + Z_{ii}} = I_1$$

$$\Rightarrow T_2 = Z_{21} \frac{P_g}{P_g + Z_{ii}} = \frac{Z_{21}}{1 + Z_{ii}/P_g}$$