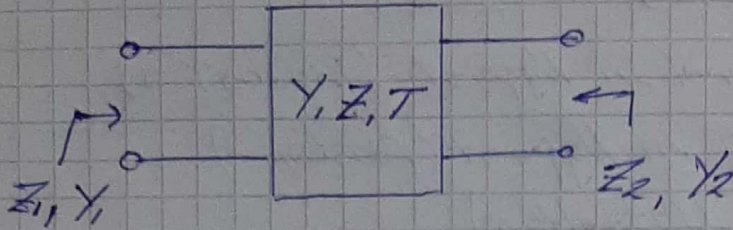


Síntesis de funciones de excitación. (Cap 4 Arauto, Cap 10 Kuo)



$F(s)$: Inmitancia = $\frac{P(s)}{Q(s)} \rightarrow$ Realizabilidad

- \rightarrow no implementable con componentes de valores reales.
- \rightarrow sistema causal y estable.

Si $F(s)$ es estable \Rightarrow Funciones Reales y positivas (FPR)

F. transformada $\rightarrow F(s) \rightarrow$ FPR? \rightarrow Z? \rightarrow Y? $\left. \vphantom{\begin{matrix} F(s) \\ FPR \end{matrix}} \right\}$ Red circuital

Condiciones necesarias y suficientes de $F(s)$ para ser FPR

- 1- $F(s)$ no tendrá polos en el semiplano derecho
- 2- $F(s)$ podría tener polos simples en el $j\omega$, con residuos ≥ 0
- 3- $\operatorname{Re} \{ F(j\omega) \} \geq 0 \quad \forall \omega$

Propiedades de las FPR

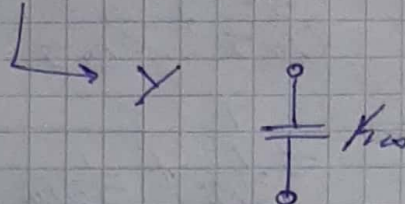
- Polos y ceros serán reales o estarán dispuestos como complejos conjugados
- $F(s) = \frac{P(s)}{Q(s)} \Rightarrow \operatorname{Gr}\{P\} - \operatorname{Gr}\{Q\} \begin{matrix} \rightarrow +1 \\ \rightarrow 0 \\ \rightarrow -1 \end{matrix}$
diferencia entre órdenes del den y num.
- Teniendo $F_1(s)$ y $F_2(s)$ FPR
 $\Rightarrow F_3 = F_1 + F_2$ es FPR
 $\Rightarrow F_3 = F_1 \parallel F_2$ es FPR
- $F(s) = \frac{P(s)}{Q(s)}$; si $P(s)$ tiene FPR pares y $Q(s)$ impares o viceversa \Rightarrow No pueden tener términos faltantes

NOTA 21:00 \rightarrow 22:00

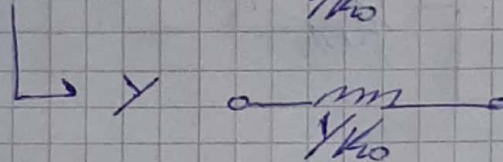
Preparato de residuos

$$F(s) = \frac{P(s)}{Q(s)} = \frac{K_0}{s} + \sum_j^N \frac{K_j}{s + \sigma_j} + \sum_i^H \frac{2K_i s}{s^2 + \omega_i^2} + K_{\infty} s$$

$$\bullet F(s) = K_{\infty} s \rightarrow Z \circ \text{---} K_{\infty} \text{---} \circ$$



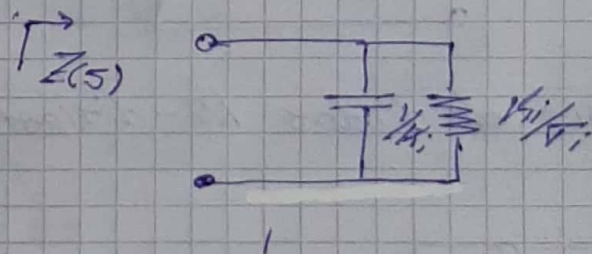
$$\bullet F(s) = \frac{K_0}{s} \rightarrow Z \circ \text{---} \frac{1}{K_0} \text{---} \circ$$



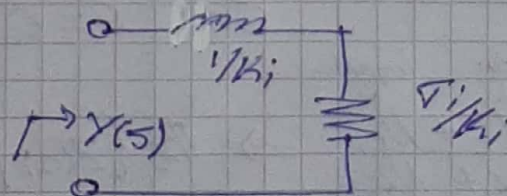
$$\bullet F(s) = \frac{K_i}{s + \sigma_i} \rightarrow Z(s) = \frac{1}{s \frac{1}{K_i} + \frac{\sigma_i}{K_i}}$$

\rightarrow suma de admitancias

Un polo sobre el eje σ da lugar a un filtro disipativo.



$$\hookrightarrow Y(s) = \frac{s}{K_i} + \frac{\sigma_i}{K_i}$$



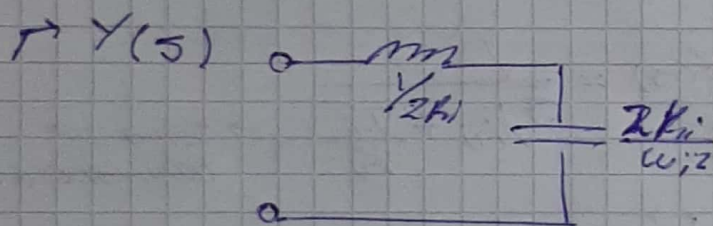
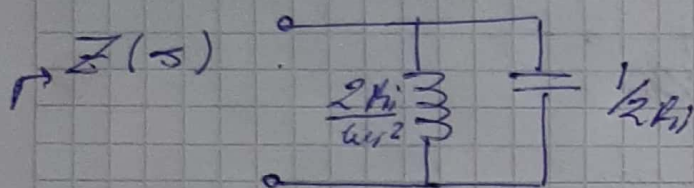
$$F(s) = \frac{2K_i s}{s^2 + \omega_i^2} \quad ; \quad F(s) = \frac{K_{i1}}{s + j\omega_i} + \frac{K_{i2}}{s - j\omega_i}$$

$$\rightarrow K_{i1} = K_{i2}^* \quad ; \quad K_{ii} \in \mathbb{R}$$

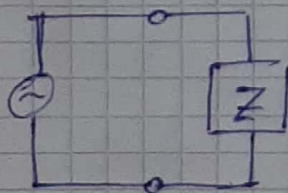
$$F(s) = \frac{K_{i1} (s - j\omega_i) + K_{i2} (s + j\omega_i)}{s^2 - j^2 \omega_i^2} = \frac{K_{i1} s - j\omega_i K_{i1} + K_{i2} s + j\omega_i K_{i2}}{s^2 + \omega_i^2}$$

$$F(s) = \frac{2K_i s}{s^2 + \omega_i^2} = \frac{1}{\frac{s^2}{2K_i s} + \frac{\omega_i^2}{2K_i s}}$$

$$F(s) = \frac{1}{s \frac{1}{2K_i} + \frac{1}{s \frac{2K_i}{\omega_i^2}}}$$



Síntesis de dipolos No-disipativos



$$\bar{P} = \frac{1}{2} \operatorname{Re} \{ Z(j\omega) \} \cdot |I(j\omega)|^2$$

$$\text{Si } \bar{P} = 0 \Rightarrow \operatorname{Re} \{ Z(j\omega) \} = 0$$

$$Z(s) = \frac{\overset{\text{por}}{H_1} + \overset{\text{impon}}{N_1}}{H_2 + N_2} \Rightarrow \operatorname{Re} \{ Z(s) \} = \operatorname{Por} \{ Z(s) \} = \frac{H_1 H_2 - N_1 N_2}{H_2^2 - N_2^2}$$

$$\text{Si } \operatorname{Re} \{ Z(s) \} = 0 \Rightarrow H_1 H_2 - N_1 N_2 = 0$$

$$\bullet \quad H_2 = N_1 = 0 \quad Z(s) = \frac{H_1}{N_2} \quad \vee \quad \bullet \quad H_1 = N_2 = 0 \quad Z(s) = \frac{N_1}{H_2}$$

NOTA

9:30 \rightarrow 10:30 \rightarrow 12:00

10:50

Si queremos que la impedancia sea no disipativa

$$\Rightarrow F(s) = \frac{\text{Par}}{\text{Impar}} \vee \frac{\text{Impar}}{\text{Par}}$$

Singularidades serán imaginarias. (Polos y ceros)

$$F(s) = \frac{\text{Par}}{\text{Impar}} = \frac{a_4 s^4 + a_2 s^2 + a_0}{b_3 s^3 + b_1 s} = \frac{K_1 (s^2 + \omega_2^2) (s^2 + \omega_3^2)}{s (s^2 + \omega_1^2)}$$

$$F(s) = \frac{\text{Impar}}{\text{Par}} = \frac{K_1 s (s^2 + \omega_1^2)}{(s^2 + \omega_2^2)}$$

Si $\frac{\text{Par}}{\text{Impar}} \rightarrow +1 \Rightarrow F(s) = \frac{K_0}{s} + \frac{2K_1 s}{(s^2 + \omega_1^2)} + \dots + K_n s$
(polo en infinito)

$$F(j\omega) = j \left(-\frac{K_0}{\omega} + \frac{2K_1 \omega}{\omega_1^2 - \omega^2} + \dots + K_n \omega \right)$$

$$F(j\omega) = j \rightarrow \begin{cases} X(\omega) & \text{Reactancia} \\ B(\omega) & \text{Susceptancia} \end{cases}$$

$$\frac{dX(\omega)}{d\omega} = \frac{K_0}{\omega^2} + \frac{2K_1(\omega_1^2 + \omega^2)}{(\omega_1^2 - \omega^2)^2} + K_n \omega \Rightarrow \text{siempre } > 0$$

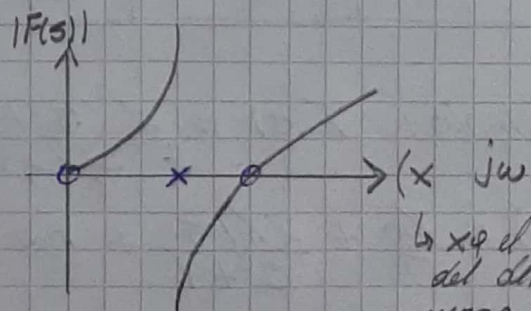
$\Rightarrow F(s)$ siempre creciente con la frecuencia.

Ejemplo

$$F(s) = s \frac{(s^2 + \omega_1^2)}{(s^2 + \omega_2^2)}$$

que $\frac{dX(\omega)}{d\omega} > 0$ impone una

alternancia de singularidades $\Rightarrow 0 \times 0 \times 0 \times$
 $\quad \quad \quad \vee$
 $\quad \quad \quad \times 0 \times 0 \times 0$



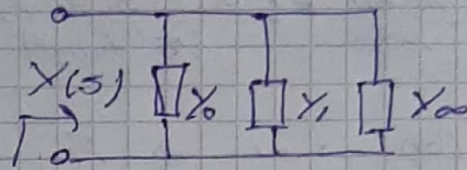
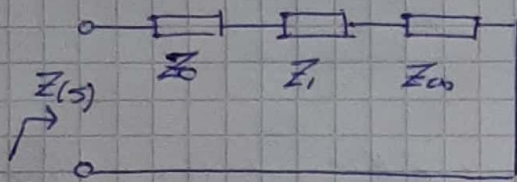
→ xq el orden del den es menor que el del num.

Teorema de Foster

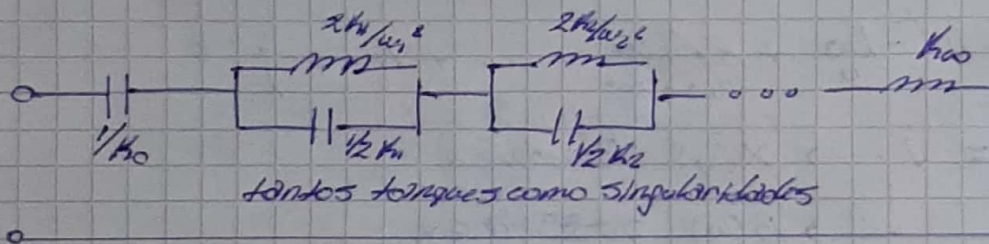
$$F(s) = \frac{P(s)}{Q(s)} = \frac{(s^2 + \omega_{n1}^2)(s^2 + \omega_{n2}^2) + \dots}{s(s^2 + \omega_1^2)(s^2 + \omega_2^2) + \dots} =$$

$$= \frac{K_0}{s} + \frac{2K_1 s}{s^2 + \omega_1^2} + \dots + \frac{K_{\infty}}{s}$$

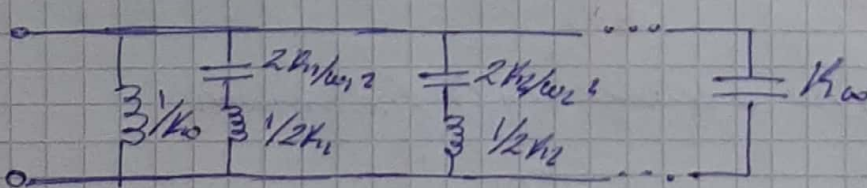
$F(s) \xrightarrow{\quad} Z(s) \rightarrow \text{serie}$
 $\xrightarrow{\quad} Y(s) \rightarrow \text{derivación}$



Foster serie

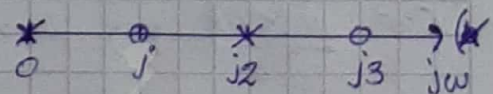


Foster paralelo



Ejemplo: $F(s) = \frac{2(s^2 + 1)(s^2 + 9)}{s(s^2 + 4)} = Z(s)$

$$Z(s) = \frac{K_0}{s} + \frac{2K_1 s}{s^2 + 4} + \frac{K_{\infty}}{s}$$

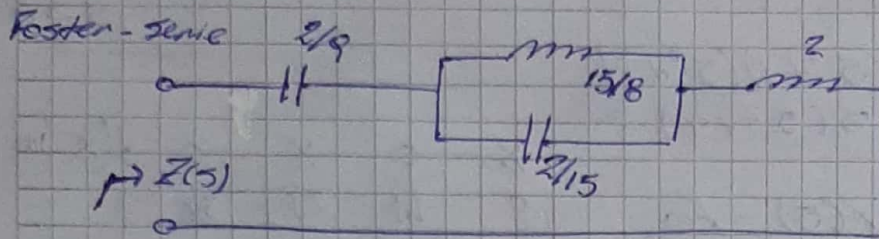


$$K_0 = \lim_{s \rightarrow 0} Z(s) = \lim_{s \rightarrow 0} \frac{2(s^2 + 1)(s^2 + 9)}{s(s^2 + 4)} = \frac{2 \cdot 1 \cdot 9}{4} = \frac{9}{2}$$

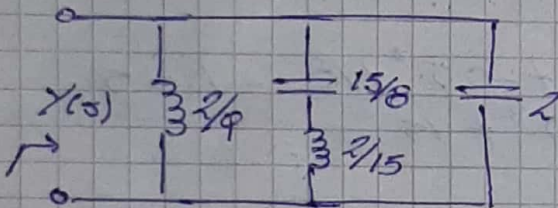
$$2K_1 = \lim_{s \rightarrow -4} \frac{s^2+9}{s} \cdot \frac{2(s^2+1)(s^2+4)}{s(s^2+4)} = \frac{2(-4+1)(-4+9)}{-4}$$

$$2K_1 = \frac{2(-3)(+5)}{-4} = \frac{30}{4} = \frac{15}{2}$$

$$K_{\infty} = \lim_{s \rightarrow \infty} \frac{Z(s)}{s} = \frac{2(s^2+1)(s^2+4)}{s^2(s^2+4)} = 2$$



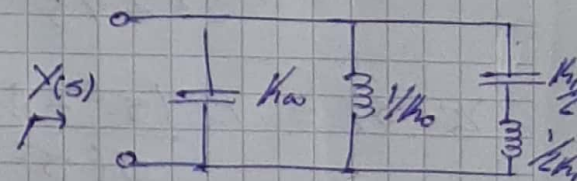
Foster - paralelo



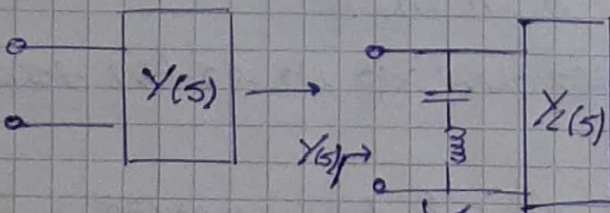
Método de Coover

• Concepto de remoción

$$F(s) = \frac{2(s^2+9)(s^2+1)}{(s^2+4)s}$$



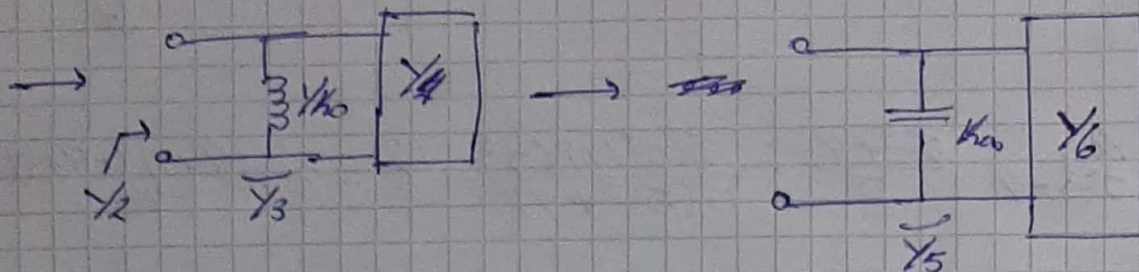
$$Y(s) = \frac{K_0}{s} + K_{\infty} s + \frac{2K_1 s}{s^2+4}$$



$$Y_2 = Y(s) - Y_1(s)$$

$$Y_1(s) = \frac{2K_1 s}{s^2+4}$$

NOTA

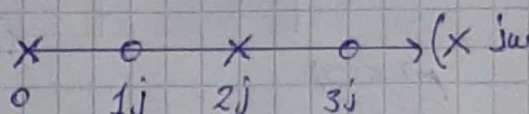


$$\Rightarrow Y(s) = Y_1 + Y_3 + Y_5$$

El orden de remoción es arbitrario.

¿Qué tal si siempre removemos singularidades en $s \rightarrow \infty$?

$$F(s) = Y(s) = \frac{2(s^2 + 1)(s^2 + 4)}{s(s^2 + 4)}$$



Caso I $Y_2(s) = Y(s) - \frac{K_{\infty}}{s}$

Caso II $Y_2(s) = Y(s) - K_{\infty} s$

$$\hookrightarrow Y(s) - K_{\infty} s = \frac{2s^4 + 20s^2 + 18}{s^3 + 4s} - K_{\infty} s$$

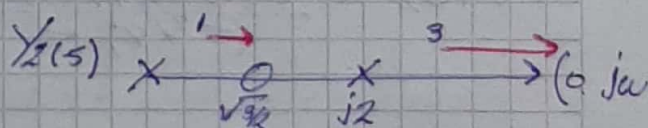
$$K_{\infty} = \lim_{s \rightarrow \infty} \frac{Y(s)}{s} = 2$$

$$\Rightarrow Y(s) - K_{\infty} s = \frac{2s^4 + 20s^2 + 18 - 2s(s^3 + 4s)}{s^3 + 4s}$$

$$Y_2(s) = \frac{12s^2 + 18}{s^3 + 4s}$$

Se cancela el orden mayor y queda en orden 2

$$Y_2(s) = \frac{12(s^2 + 3/2)}{s(s^2 + 4)}$$



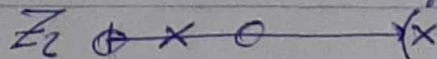
Los polos se mantienen en su lugar cuando se hace una remoción

Los ceros se movieron (solo se mueven si no están en cero o en inf)

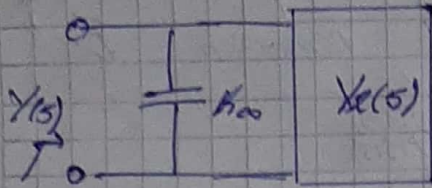
Los ceros no se pueden remover xq no están asociados a los residuos.

Si quiero sacar el cero de inf tengo que pasar a una conf. de impedancia

$$\frac{1}{Y_2} = Z_2 = \frac{s^3 + 4s}{12s^2 + 18}$$

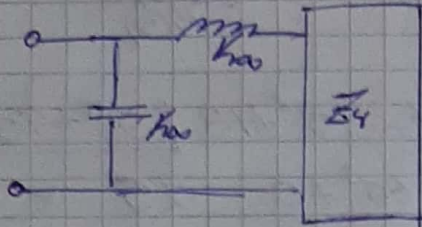


NOTA



$$Y_2 = \frac{125^2 + 18}{5^3 + 45}$$

$$\Rightarrow \frac{1}{Y_2} = Z_2 = \frac{5^3 + 45}{125^2 + 18}$$



$$\rightarrow Z_4 = Z_2 - K_{12, \infty} 5$$

$$K_{12, \infty} = \lim_{5 \rightarrow \infty} \frac{Z_2}{5} = \frac{1}{12}$$

$$\Rightarrow Z_4 = \frac{5/12 \cdot 5}{125^2 + 18}$$

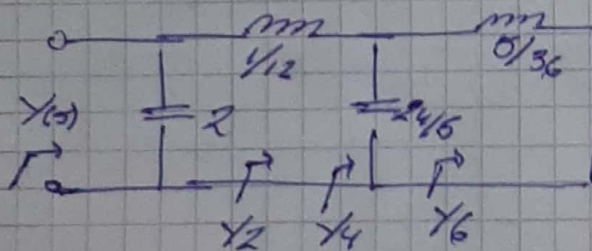
$$\oplus \quad \times \quad \rightarrow (0 \text{ jw})$$

$$Y_4 = \frac{125^2 + 18}{5/12 \cdot 5}$$

$$\rightarrow Y_6 = Y_4 - K_{4, \infty} 5$$

$$K_{4, \infty} = \lim_{5 \rightarrow \infty} \frac{Y_4}{5} = \frac{24}{5}$$

$$Y_6 = \frac{125^2 + 18}{5/12 \cdot 5} - \frac{24}{5} \cdot 5 \Rightarrow Y_6 = \frac{36}{5} \cdot \frac{1}{5}$$



Se sintetiza
removiendo polos

\rightarrow cant. de singularidades críticas (son todas las singularidades menos las que están en \oplus y en ∞)

$$C_c = C_f + 1$$

\rightarrow cant. de componentes

$$\frac{P(s)}{Q(s)} = \frac{C(s)}{Q(s)} + \frac{B(s)}{Q(s)} \Rightarrow F(s) = \frac{C(s)}{Q(s)} + \frac{B(s)}{Q(s)}$$

$$\frac{1}{s^2} \rightarrow \frac{1}{s^2} = \frac{1}{s^2} \Rightarrow F(s) = \frac{C(s)}{Q(s)} + \frac{1}{\frac{Q(s)}{B(s)}} = \frac{C(s)}{Q(s)} + \frac{1}{\frac{C(s) + B(s)}{B(s)}}$$

$$F(s) = \frac{25^4 + 205^2 + 18}{s^3 + 45}$$

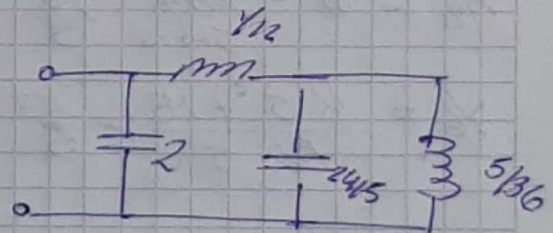
$$\begin{array}{r} 25^4 + 205^2 + 18 \mid s^3 + 45 \\ - 25^4 + 85^3 + 0 \\ \hline 0 + 125^2 + 18 \end{array} \quad \begin{array}{l} \rightarrow \text{nuevo dividendo} \\ 25 \rightarrow \frac{1}{1} \end{array}$$

Ahora

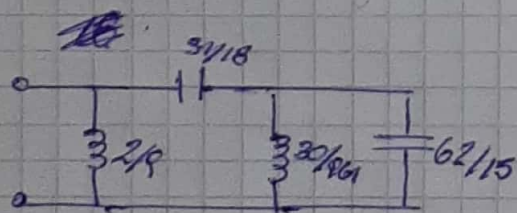
$$\begin{array}{r} s^3 + 45 \mid 125^2 + 18 \\ - s^3 + 3/2 s \\ \hline 5/2 s \end{array} \quad \begin{array}{l} \rightarrow \text{nuevo cociente} \\ 1/2 s \rightarrow \frac{mm}{1/2} \end{array}$$

$$\begin{array}{r} 125^2 + 18 \mid 5/2 s \\ - 125^2 \\ \hline 18 \end{array} \quad \begin{array}{l} 24/5 s \rightarrow \frac{24/5}{6} \end{array}$$

$$\begin{array}{r} 5/2 s \mid 18 \\ - 5/2 s \\ \hline 0 \end{array} \quad \begin{array}{l} 5/36 s \rightarrow \frac{mm}{5/36} \end{array}$$



Si en vez de remover singularidades en ∞ las removemos en cero ordeno el polinomio de menor a mayor



$$\begin{array}{r} 18 + 205^2 + 25^4 \mid 45 + s^3 \\ - 18 \\ \hline 9/25^2 + 0 \end{array} \quad \begin{array}{l} 8/2 \frac{1}{5} \rightarrow \frac{mm}{2/5} \end{array}$$

$$\begin{array}{r} 45 + s^3 \mid 3/2 s^2 + 25^4 \\ - 45 + 143/5 s \\ \hline 15/31 s^3 \end{array} \quad \begin{array}{l} 8/31 \frac{1}{5} \rightarrow \frac{mm}{8/31} \end{array}$$

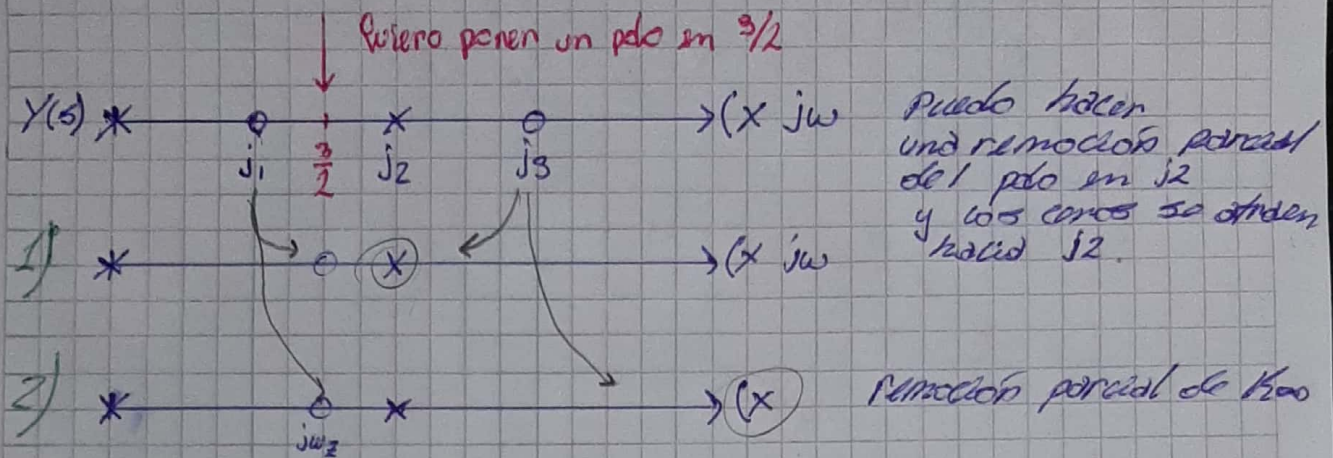
$$\begin{array}{r} 3/2 s^2 + 25^4 \mid 15/31 s^3 \\ - 3/2 s^2 + 0 \\ \hline 90/30 \frac{1}{5} \end{array} \quad \begin{array}{l} 90/30 \frac{1}{5} \rightarrow \frac{mm}{90/30} \end{array}$$

$$\begin{array}{r} 15/31 s^3 \mid 25^4 \\ - 15/31 s^3 \\ \hline 0 \end{array} \quad \begin{array}{l} 13/62 \frac{1}{5} \rightarrow \frac{mm}{13/62} \end{array}$$

NOTA

Remociones parciales

↳ Fijar un cero en una determinada frecuencia.



caso 2) $Y(s) - K'_{\infty} s = Y_2$ siendo $K'_{\infty} < K_{\infty}$

$$Y(s) - K'_{\infty} s \Big|_{s=jw_2} = Y_2(s) = 0$$

$$K'_{\infty} = \frac{Y(s)}{s} \Big|_{s=jw_2}$$

$$\Rightarrow Y_2 \Big|_{s=jw_2} = Y(s) - \frac{2K_1' s}{s^2 + \omega_1^2} \quad K_1' < K_1$$

$$2K_1' = Y(s) \cdot \frac{(s^2 + \omega_1^2)}{s} \Big|_{s=jw_2}$$