

08 — Hazen-Williams & Equivalent Pipe

Water Resources, CIVL318

Last revision on October 2, 2018

We begin this module by looking at a variety of pipes that are common in installed systems or are increasingly common in new systems.

Cast Iron Pipe

Cast iron pipe showing bell end. It is coated with yellow plastic to minimize corrosion.



Cast Iron Pipe

Cast iron pipe used under 16th Avenue, Bowness. Note the connection guides for correct overlap at joints.



PVC Plastic Pipe Connector

The rubber O-ring visible inside the bell is used to seal pipe connections



PVC Plastic Pipe Connector

This "Blue Brute" pipe has a maximum operating pressure of 150 psi or 1000 kPa

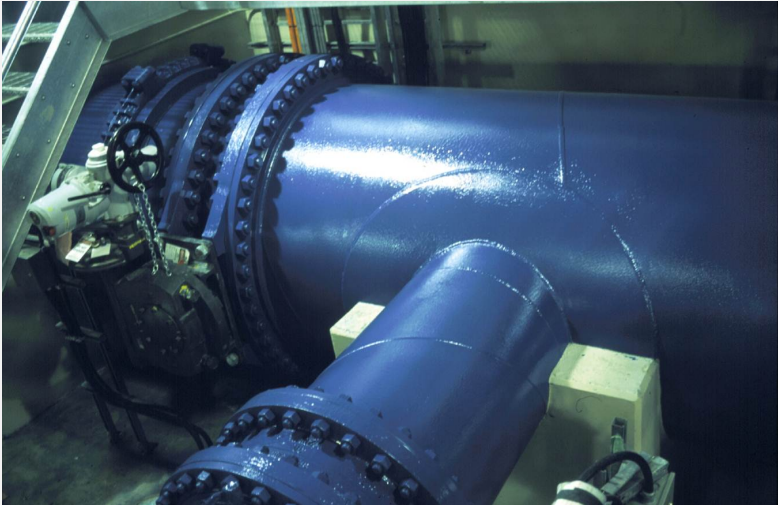


Asbestos Cement Pipe and Connector

Not used in new installations



Inside a water distribution plant



Welded Steel Pipe

Welded steel header in a filter backwash system — Bearspaw Water Treatment Plant



Welded steel pipe fittings and connections



South Feeder from Bearspaw Plant



Banff Middle Springs Plant; three pumps are to satisfy fire flow requirements



Fittings - Benchlands, Canmore



New Hyprescon installation, 14th St SW.



River crossing, 14th St SW



Hyprescon steel pipe with cement lining and mortar coating



Mortar coating



Cement lining



Custom welded section



Custom welded section in place



Butterfly valve in Hyprescon pipe



Butterfly valve in Hyprescon pipe



Concrete inspection chamber for valve maintenance



Glenmore Water Treatment Plant



We have used Darcy's equation to analyze the flow of liquids in pipes, where the volume flow rate has been provided.

It is more complicated to apply Darcy's equation to calculate flow, requiring an iterative process to find the friction factor and associated headloss.

We will now continue our analysis using the Hazen-Williams equation to solve for head loss, pipe diameter or flow in water systems.

Hazen-Williams Equation

Darcy's equation, $h_L = f \cdot \frac{L}{D} \cdot \frac{v^2}{2g}$, works for all liquids and for laminar and turbulent flow conditions.

Darcy's equation is not directly suited to calculations to determine flow rates or diameters. (We have been provided with both for all the questions we have done using Darcy's equation.)

The Hazen-Williams equation is widely used for calculations relating to the flow of water.

It is also more practical for the analysis of flow through parallel pipe systems.

Hazen-Williams Equation

$$Q = 0.849ACR^{0.63}s^{0.54}$$

where:

Q is the volume flow rate in m^3/s

A is the pipe area in m^2

C is a dimensionless roughness coefficient

R is the hydraulic radius of the pipe ($R = D/4$ for circular pipes)

s is the hydraulic slope, the energy loss per length of pipe, h_L/L

We shall use the formula in a slightly different form...

Hazen-Williams Equation

Since we are only concerned with circular pipes, we shall use D , the diameter of the pipe, instead of A and R :

$$\begin{aligned} Q &= 0.849 A C R^{0.63} s^{0.54} \\ &= 0.849 \left(\frac{\pi D^2}{4} \right) C \left(\frac{D}{4} \right)^{0.63} s^{0.54} \\ &= 0.27842 C D^{2.63} s^{0.54} \end{aligned}$$

Hazen-Williams Equation

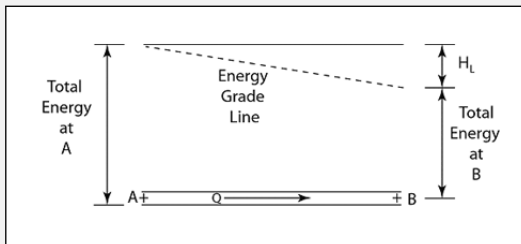
Since we are only concerned with circular pipes, we shall use D , the diameter of the pipe, instead of A and R :

$$\begin{aligned} Q &= 0.849 A C R^{0.63} s^{0.54} \\ &= 0.849 \left(\frac{\pi D^2}{4} \right) C \left(\frac{D}{4} \right)^{0.63} s^{0.54} \\ &= 0.27842 C D^{2.63} s^{0.54} \end{aligned}$$

It is more useful to have Q in L/s and D in mm:

$$\begin{aligned} Q &= 1000 \times 0.278 C \left(\frac{D}{1000} \right)^{2.63} s^{0.54} \\ &= 0.0000035867 C D^{2.63} s^{0.54} \\ &= \frac{C D^{2.63} s^{0.54}}{279000} \end{aligned}$$

Energy Grade Line



Consider a horizontal pipe from A to B; energy is lost due to friction as water flows along the pipe such that the total energy at any point is shown by the dotted line – the energy grade line.

Total energy loss between A and B is h_L , in length L of pipe, so the slope of the energy grade line is h_L/L

We will replace the s term in the Hazen-Williams with h_L/L :

$$Q = \frac{C D^{2.63} \left(\frac{h_L}{L} \right)^{0.54}}{279000}$$

Hazen-Williams Equation

The Hazen-Williams is an empirical formula, derived from experimental results. The exponents 2.63 and 0.54 are to make observed results fit the formula more consistently.

Units are not consistent on sides of the equation.

$$Q = \frac{C D^{2.63} \left(\frac{h_L}{L} \right)^{0.54}}{279000}$$

C is a unitless coefficient so units are L/s on the left and $\text{mm}^{2.63}$ on the right.

Approximate Roughness Coefficients, C

Pipe Material	New Pipe	Design C
PVC	150	150
Polyethylene	140	140
Welded Steel	140	100
Cement-lined steel (Hyprescon)	150	140
Cast Iron	130	100
Cast Iron - 10 years old		110
Cast Iron - 20 years old		95
Cast Iron - 30 years old		85
Cast Iron - 40 years old		75

<http://media.toro.com/Documents/Agriculture/HazenWilliamsEquation.pdf>

The Hazen-Williams equation works under the following conditions:

- ▶ Water flowing at approximately 10°C - 15°C in fully pressurised pipe
- ▶ Flow velocity not in excess of 3.0 m/s
- ▶ Flow is in pipe with a diameter larger than 50 mm and smaller than 2.0 m

Use of the Hazen-Williams under other conditions from those specified above will result in some error.

(In practice, there is always error. C is an estimated value; pipe does not stay new for long!)

$$Q = \frac{C D^{2.63} \left(\frac{h_L}{L} \right)^{0.54}}{279000}$$

$$\Rightarrow \left(\frac{h_L}{L} \right)^{0.54} = \frac{279000 Q}{C D^{2.63}}$$

$$\Rightarrow \frac{h_L}{L} = \left(\frac{279000 Q}{C D^{2.63}} \right)^{\frac{1}{0.54}}$$

$$\Rightarrow h_L = L \left(\frac{279000 Q}{C D^{2.63}} \right)^{1.852}$$

Alternative Form - Solving for Diameter

$$Q = \frac{C D^{2.63} \left(\frac{h_L}{L} \right)^{0.54}}{279000}$$

$$\Rightarrow D^{2.63} = \frac{279000 Q}{C \left(\frac{h_L}{L} \right)^{0.54}}$$

$$\Rightarrow D = \left(\frac{279000 Q}{C \left(\frac{h_L}{L} \right)^{0.54}} \right)^{\frac{1}{2.63}}$$

$$\Rightarrow D = \left(\frac{279000 Q}{C \left(\frac{h_L}{L} \right)^{0.54}} \right)^{0.3802}$$

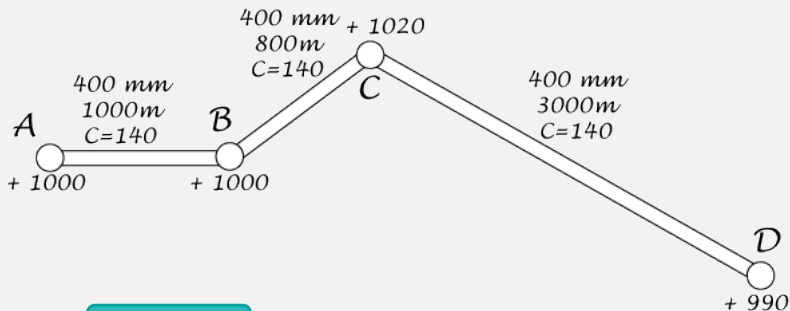
Hazen-Williams Formulae

$$Q = \frac{C D^{2.63} \left(\frac{h_L}{L} \right)^{0.54}}{279000}$$

$$h_L = L \left(\frac{279000 Q}{C D^{2.63}} \right)^{1.852}$$

$$D = \left(\frac{279000 Q}{C \left(\frac{h_L}{L} \right)^{0.54}} \right)^{0.3802}$$

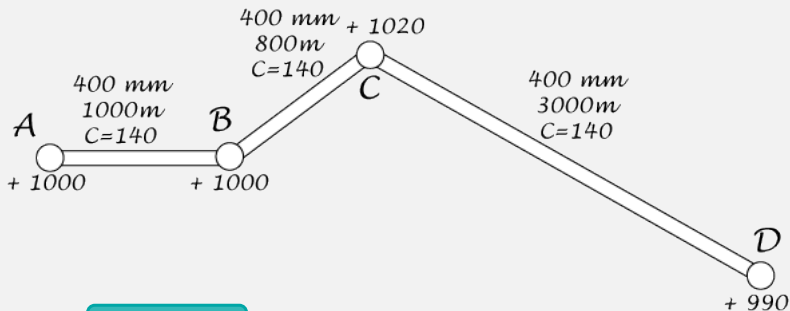
where Q is in L/s, D is in mm, h_L and L are in m.



Example 1

The pipes are cement-lined Hyprescon with a diameter of 400 mm and a roughness coefficient of $C = 140$ and flow is 200 L/s. Elevations are as indicated.

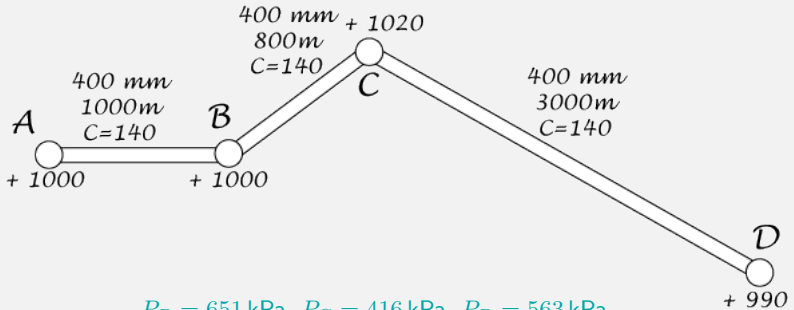
Calculate the pressure at B given that the pressure at A is 700 kPa.



Exercise 1

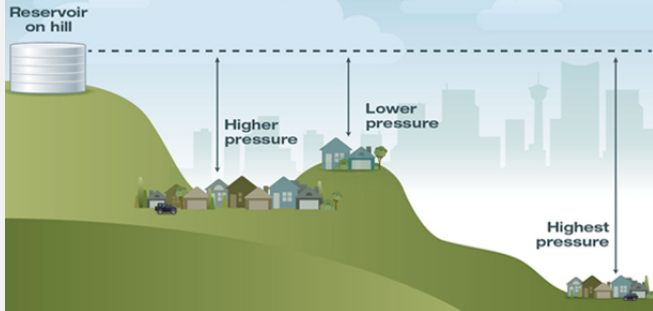
The pipes are cement-lined Hyprescon with a diameter of 400 mm and a roughness coefficient of $C = 140$ and flow is 200 L/s . Elevations are as indicated.

Calculate the pressures at C and D , given that the pressure at A is 700 kPa .

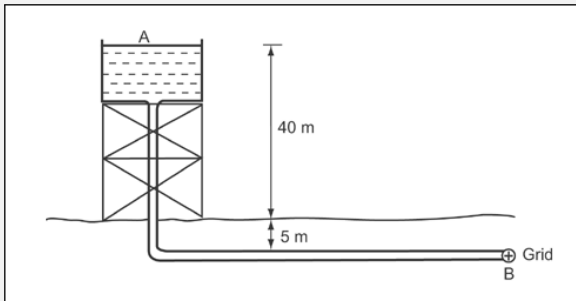


Pressures are lower at points farther away from the point of delivery (A is the point of delivery in this case) but the main pressure determinant is elevation, with higher elevations in a distribution system having lower pressures.

Water Pressure Management Diagram



<http://www.calgary.ca/UEP/Water/Pages/Drinking-water/Water-quality/Water-Pressure.aspx>

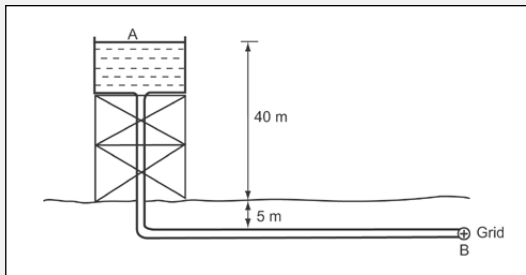


Example 2

Water flows from a storage tank through a welded steel pipe that is 1200 m long and 350 mm in diameter, entering a distribution grid at point B . Assume $C = 100$.

Determine:

- 1 The pressure at B when the flow is 150 L/s
- 2 The maximum flow rate into the grid when the minimum allowable pressure at B is 400 kPa.

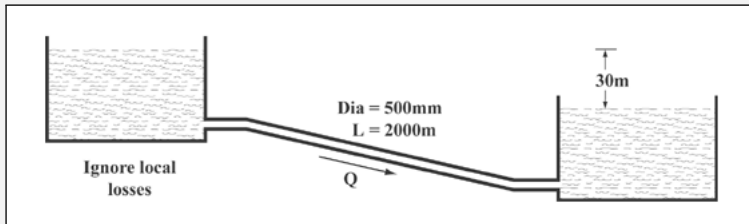


Velocity $v_B = 1.5591 \text{ m/s}$ in part (1) and velocity head was small (0.12389 m).

Omitting the velocity head term altogether would have changed P_B by about 0.3% of the calculated 317 kPa value. This is well within the error to be expected in estimation of the C -value.

In water distribution systems, velocities are normally designed to be less than 2 m/s since faster flow causes excessive head loss and may cause noise and vibration.

It is generally acceptable to ignore velocity head in cases where diameter or flow are unknown; this greatly simplifies some calculations.



Exercise 2

Water flows from one reservoir down to another, through a 500 mm diameter pipe that is 2000 m in length. The difference in elevation between the surfaces of the two reservoirs is 30 m.

Determine:

- 1 The flow with high density polyethylene pipe (HDPE) with $C = 140$
- 2 The flow with welded steel with $C = 100$
- 3 The diameter of HDPE pipe required for a flow of 1200 L/s

Neglect minor losses.

In our earlier study of minor losses, we calculated minor head losses through valves using

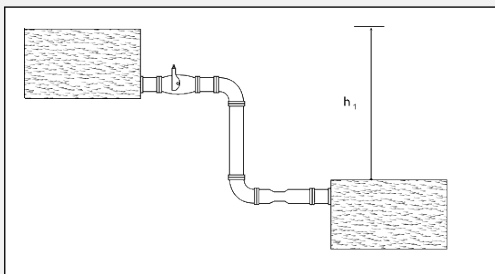
$$h_L = k \cdot \frac{v^2}{2g}$$

which required knowledge of both Q and D to calculate v .

We defined the 'equivalent length ratio,' L_e/D , of a valve or fitting where the equivalent length, L_e , is defined as the length of pipe that would produce the same (frictional) loss as the valve or fitting (minor) losses.

Thus, to determine the losses due to a fully open globe valve (with $L_e/D = 340$), we can instead calculate the frictional losses due to length L_e of pipe.

(Note that we will still need the diameter D of the pipe)



Example 3

In a water treatment plant, water flows from a filter down to a clear well through the pipe system shown. The pipe is welded steel with a diameter of 300 mm and roughness coefficient $C = 130$. The total length of pipe is 50 m. Elevation difference h_1 between the tanks is 5.0 m.

Equivalent length ratios, L_e/D , are:

Entrance and exit losses:	50	Butterfly valve:	35
Large radius elbows:	25	Venturi meter:	100

Determine the flow through the system.

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Equivalent length ratios, L_e/D , are:

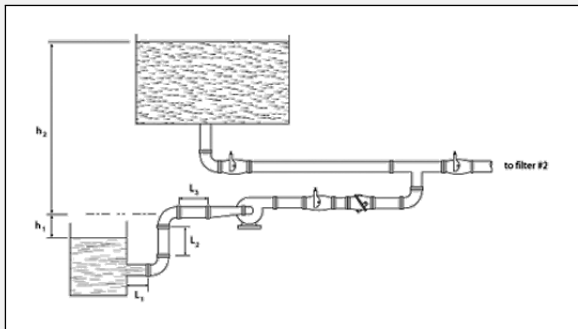
Entrance:	10	Elbow (inlet):	25
Eccentric Reducer:	2	Butterfly Valve:	40
Check Valve:	120	Elbow (outlet):	35
Tee Connection (through):	60		

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Determine:

- 1 The head losses on the inlet side (clear well to pump)
- 2 The head losses on the outlet side (pump to filter)

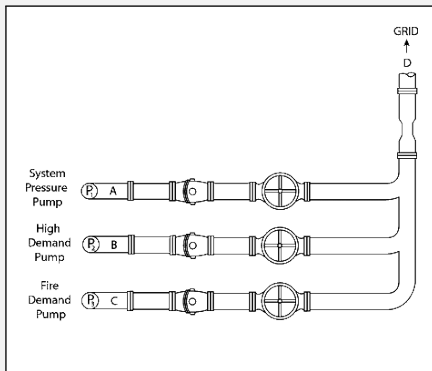
Neglect exit losses into the filter.



Exercise 3

This exercise is a continuation of the previous example. Determine:

- 3 The head added by the pump
- 4 The pressure at the pump outlet



Example 5

The pumps and piping system are used to supply a municipal grid. Pump P_1 (P_2 and P_3 are not running at this time) runs continuously and maintains the basic pressure in the distribution grid beyond point D . The elevations are the same at the pump and the discharge point D .

The outlet pipe, from the pump to point D , is welded steel ($C = 130$) with a diameter of 200 mm and a total length between fittings of 10 m.

The minimum pressure required at D is 500 kPa for a design flow of 150 L/s.

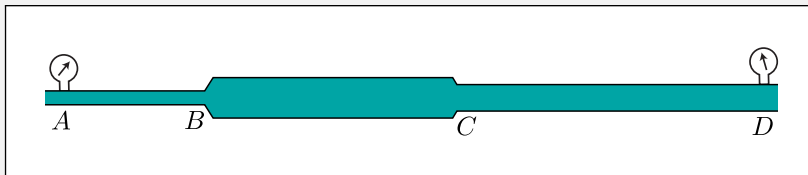
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Check Valve:	120	Gate Valve:	15
Tee Connection (through):	60	Venturi Meter:	100

There is no flow from pumps P_2 and P_3 . Determine:

- 1 the head losses between A and D
- 2 the pressure at A required for the required pressure and flow at D

Determining Flow Through Pipes in Series



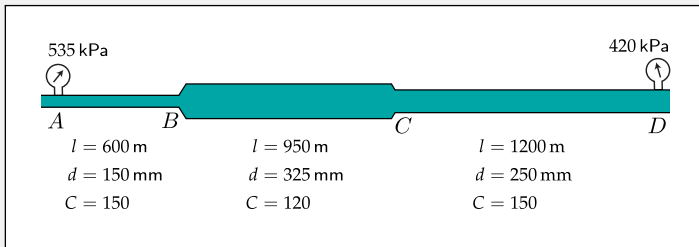
We have used the Hazen-Williams Equation to find flow through a single pipe but how can we find the flow through a system of pipes in series (such as pipes *AB*, *BC* and *CD* shown above)?

Note that, **for pipes in series**, the volume flow rate is constant through each pipe and that the head loss is cumulative.

Pipes in Series

$$Q_{AB} = Q_{BC} = Q_{CD}$$
$$h_{AD} = h_{AB} + h_{BC} + h_{CD}$$

These are **important** properties of pipes in series!



Example 6

Determine Q , the volume flow rate, through the system shown.