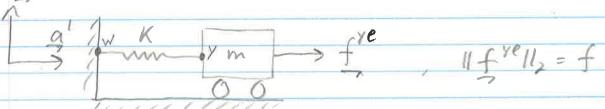
## Vibrations

Let's return to a simple particle dynamics problem:



Find The equation of motion

i) Frames and DCMs: N/A
ii) Angular Velocity: N/A
iii) Position

$$f^{ys} = f^{*} \begin{bmatrix} -kq \\ 0 \\ 0 \end{bmatrix}, \quad f^{ye} = f^{*} \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

## 3) N22

$$\frac{J}{J} = \begin{bmatrix} -kq & f \\ 0 & + 0 \\ 0 & 0 \end{bmatrix} = \frac{J}{J} = \begin{bmatrix} m\ddot{q} \\ 0 \\ 0 \end{bmatrix}$$

$$-Kg+f=mg$$

This is a second order linear ordinary differential equation that we can solve analytically. First, we will assume f=0, giving  $m\ddot{q} + Kq = 0 \qquad (*)$ A general solution to a linear ODE is q(+) = ac At q(+) = lae 1+, q(+)= lae 1+ Sub into (x)

m (1 ae 1+) + K(ae 1+) = 0  $(m\lambda^2 + K)ae^{At} = 0$ det = 0 give towal solution, so we consider 12m + K = 0  $\lambda^2 = -\frac{K}{\kappa_0}$ 1 = + Ki, where is imaginary Therefore the solution to the ODE is 9(+) = a, e i Tym + + a, e i Tym + We can rewrite this using the trip identity

 $e^{\pm i\omega t} = \cos(\omega t) \pm i\sin(\omega t)$ 

This gives

$$q(t) = A \cos(K + t) + B \sin(K + t)$$
where  $A = a_1 + a_2$ 

$$B = (a_1 - a_2)i$$
The response of  $q(t)$  will look like
$$q(t) = A \cos(k + t) + B \sin(k + t)$$
The frequency of oscillation is  $a = K + t$ 
The magnitude and phase of oscillation is detormined by  $A = A \cos(k + t)$ 

$$A = A \cos(k + t)$$

$$A =$$

What if the force acting on the mass is non-zero? Let's consider f(t) = for cos(wpt) The EoMis now mg + Kg = fp cos (wpt) (\*\*) Remember from your differential equations course g(t) = 9h(t) + 9p(t), where 9h(t) is the homogeneous solution where the right hand side of the ODE is zero. We already solved for this and found 9h (+) = A cos ( JK + ) + B sin ( Jm + ) 9p(+) is the particular solution that has the form 9p(t) = C cos (wpt) . Same form as qp(t) =- wp C sin(wpt), qp(t) = - wp C cos(wpt) (-mwp2 + K) C cos(wpt) = fp cos(wpt)

1. .

Rearranging gives
$$\begin{bmatrix}
(-m \omega p^2 + K)C - fp \end{bmatrix} \cos(\omega p t) = 0$$

$$\cos(\omega p t) \neq 0, \quad so$$

$$(-m \omega p^2 + K)C - fp = 0$$

$$C(-m \omega p^2 + K) = fp$$

$$C = fp \quad \frac{1}{m}$$

$$\frac{fp}{m} - \frac{fp}{m} = \frac{fp}{m}$$

$$\frac{fp}{m} - \frac{fp}{m} = \frac{fp}{m}$$

And The total solution is

$$q(t) = q_h(t) + q_p(t) = A\cos\left(\sqrt{\frac{K}{m}}t\right) + B\sin\left(\sqrt{\frac{K}{m}}t\right)$$

$$+ \frac{fp/m}{\omega^2 - \omega_p^2}\cos\left(\omega_p t\right)$$

Based on the salution for ap(+), what happens; f wp & w (i.e., the forcing frequency approaches the natural frequency)? lin qp(t) = lin fp/m cos(wpt) -> 00 wp > w wr-wp This is known as resonance, and is why the natural frequency of the system is some times referred to as the resonant frequency.  $|q_p(t)| = |\frac{tp/m}{\omega^2 - \omega_p^2}|$ 9p(+)/

Dynamics of a System of Particles
(4.3 Forbes)

Newton's 3rd Law (N3L)

Consider two particles y and x, connected by a massless link, a spring, or a damper. Then,

$$f^{yx} = -f^{xy}$$

That is the force acting on y due to x is equal and opposite to the force acting on x due to y.

N3L is useful when working with a system of particles.

# Multi Degree of Freedom Vibrations The concepts we discussed for single degree of freedom vibrations apply to multi degree of freedom Let's consider two masses connected by a spring: $\int_{0}^{y_{1}w} = \int_{0}^{z_{1}} \frac{q_{1}}{0} \int_{0}^{y_{2}w} = \int_{0}^{z_{1}} \frac{1}{0} \frac{q_{2}}{0} \int_{0}^{z_{1}} \frac{1}{0} \frac{1}{0} \int_{0}^{z_{1}} \frac{1}{0} \int_{0$ For simplicity we assume unstretched length of spring is zero. Derive EoMs using 3 steps to success 1) Knewatres i) Frames and DCMs: N/A (i) Auguler Velocity N/A iv) Velocities

#### 2) FBDs

$$f_{ie} \rightarrow f_{is} - f_{is}$$

$$f^{V_1e} = f^{T} f$$

$$f^{V_1s} = f^{T} - Kq_1 + Kq_2 = f^{T} - Klq_1 - q_2$$

$$0$$

$$0$$

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### 3) NaL

$$\frac{\mathcal{F}}{\mathcal{F}} \left[ f - K(q_1 - q_2) \right] = \frac{\mathcal{F}}{\mathcal{F}} \left[ m_1 \ddot{q}_1 \right]$$

Particle 
$$y_2$$

$$-f(x) = m_2 q_2 w/n/q$$

$$f(q_2 - q_1) = f(m_2 q_2)$$

$$0$$

$$m_2 q_2 + K(q_2 - q_1) = 0$$

Writing the EoMs to gether gives 
$$m_1 \ddot{q}_1 + K(q_1 - q_2) = f \quad (*)$$

$$m_2 \ddot{q}_2 + K(q_2 - q_1) = 0 \quad (**)$$

Or in matrix form as

$$M\ddot{q} + Kq = 6f$$

This is a second order matrix ordinary differential equation that is equivalent to (x) and (xx).

Notice that M=MT and K=KT,

M must also be positive definite (all eigenvalues stricty
positive)

zero or positive). Let's solve this ODE first with f=0 M 9 + K 9 = 0 General Solution of the form q(t) = 9 eint q(t) = iwaeiwt, q(t) = -waeiwt Sub into Earl to give M(-wageint) +K(aeint) = 0 (-w2M + K) a e int = 0 eint +0, so (-w2M+K) a =0 M is invertible, so me can rewrite as alvays  $(-\omega^{2}1 + M^{-1}K)a = 0$ true because Mis positive or M-1Ka=w2a definite Is this equation familiar? (Av= xv) w2 is an eigenvalue of M-1K! In our case, M- K = 1/m, 0 K -K - K/m, -K/m, -K/m, -K/m, -K/m, -K/m,

K must be positive somi definite (all eigenralies

Solve for eigenvalues of 
$$M^{-1}K$$

$$det(\omega^{2}1 - M^{-1}K) = 0$$

$$det(\omega^{2}1 - M^{-1}K) = 0$$

$$(\omega^{2} - K/m_{1}, K/m_{2}, W^{2} - K/m_{2}) = 0$$

$$(\omega^{2} - K/m_{1})(\omega^{2} - K/m_{2}) - (K/m_{1})(W/m_{2}) = 0$$

$$(\omega^{4} - (\frac{1}{m_{1}} + \frac{1}{m_{2}})K\omega^{2} + \frac{K^{2}}{m_{1}m_{2}} - \frac{K^{2}}{m_{1}m_{2}} = 0$$

$$(\omega^{2} - K(m_{1} + m_{2}))\omega^{2} = 0$$

$$(\omega^{2} - K/m_{1})\omega^{2} = 0$$

$$(\omega^{2}$$

$$\begin{array}{c|cccc}
K & K & \begin{bmatrix} a_{11} \\ m_1 \end{bmatrix} & \begin{bmatrix} 0 \\ a_{12} \end{bmatrix} & \begin{bmatrix} 0 \\ 0 \end{bmatrix} \\
K & K \\
\hline{m_2} & m_1
\end{array}$$

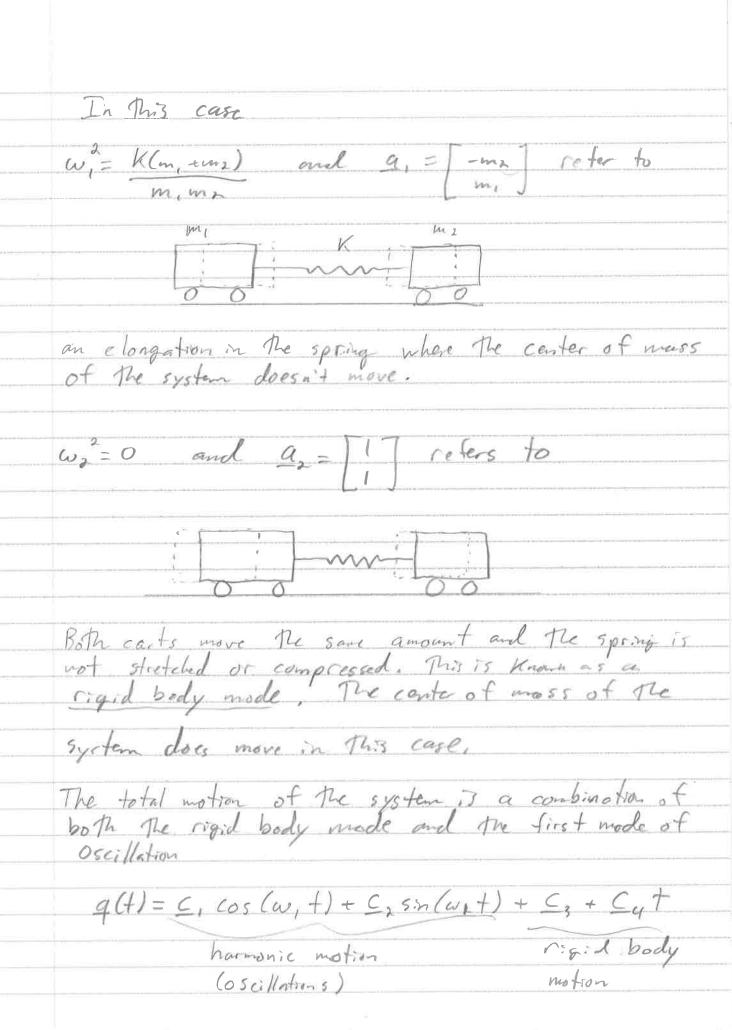
$$a_{11} = -\frac{m_2}{m_1}$$
  $a_{12} = -\frac{m_2}{m_1}$ 

$$\omega_{2} = 0$$
 $(\omega_{2}^{2} - M^{-1} K) \alpha_{2} = 0$ 

$$\begin{bmatrix} -K & K & a_{21} \\ m_1 & m_1 \\ k & -K \\ m_2 & m_3 \end{bmatrix} = \begin{bmatrix} 0 \\ a_{21} \\ a_{22} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$-a_{21} + a_{22} = 0 = 7 \quad \alpha_{2} = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

a, and a are the mode shapes associated with w, and wa that describe the motion coused by vibrating at Those frequencies.



ě.	The same procedure applies to multi-degree of freedom vibrations. Consider n carts
	m, maken mn
	The EoMs will have the form
	$M \dot{q} + K q = \dot{b} f$ where $M, K \in \mathbb{R}^{n \times n}$ and $q \in \mathbb{R}^{n \times 1}$ .
	The natural frequencies of vibration are the eigenvalues
	M-1 K
	Notes
	- Natural frequencies are system properties and do not depend on external forces.
	- External forces are set to zero when solving for natural frequencies. This becomes an eigenvalue problem.