

DC, AC

**Sinusoidal** 

# Steady-State Analysis

We consider circuits energized by time-varying voltage or current sources.

Textbook:

**Electric Circuits**

James W. Nilsson & Susan A. Riedel

9th Edition.

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# Outline

- **Complex Numbers Tutorial**
- **Sinusoids**
- **Phasors**
- **Techniques of Circuit Analysis**
- **Phasor Diagrams**

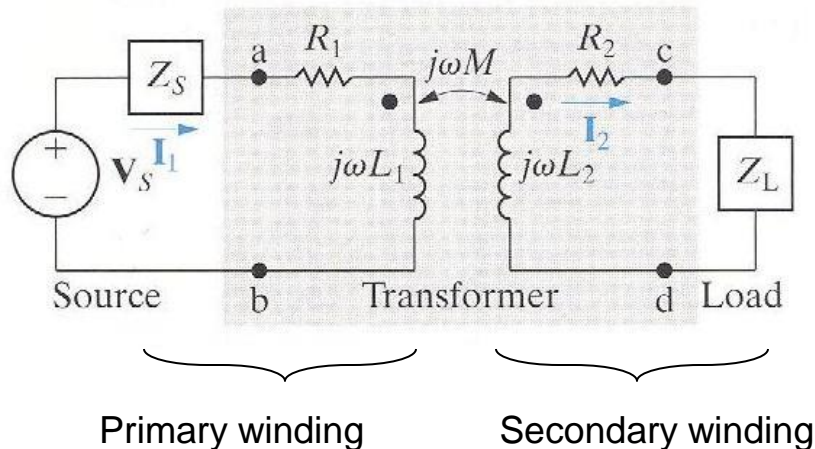
# The transformer

- A transformer is a device that is based on magnetic coupling.
- Are used in both communication and power circuits.
- In communication circuits: transformer is used to matched impedance and eliminate dc signals from portions of the systems
- In power circuits: transformer is used to establish ac voltage levels that facilitate the transmission, distribution and consumption of electrical power.

only AC

# Linear transformer

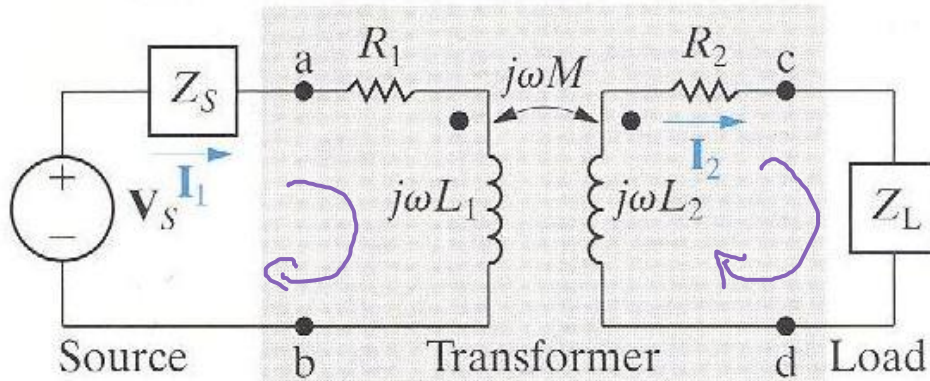
- Primarily used in communication circuits.
- Is formed when two coils are wound on a single core to ensure magnetic coupling.
- Frequency domain circuit model of a transformer



$R_1$  = the resistance of the primary winding  
 $R_2$  = the resistance of the secondary winding  
 $L_1$  = the self-inductance of the primary winding  
 $L_2$  = the self-inductance of the secondary winding  
 $M$  = the mutual inductance  
 $V_s$  = sinusoidal source  
 $Z_S$  = internal impedance of the source  
 $Z_L$  = the load  
 $I_1$  = primary current  
 $I_2$  = secondary current

$$M = k\sqrt{L_1 L_2}$$

# Transformer circuit analysis



Mesh-current equations:

$$V_s = (Z_s + R_1 + j\omega L_1)I_1 - j\omega M I_2$$

$$0 = -j\omega M I_1 + (R_2 + j\omega L_2 + Z_L)I_2$$

$Z_{11} = Z_s + R_1 + j\omega L_1$  = total self - impedance of the primary winding

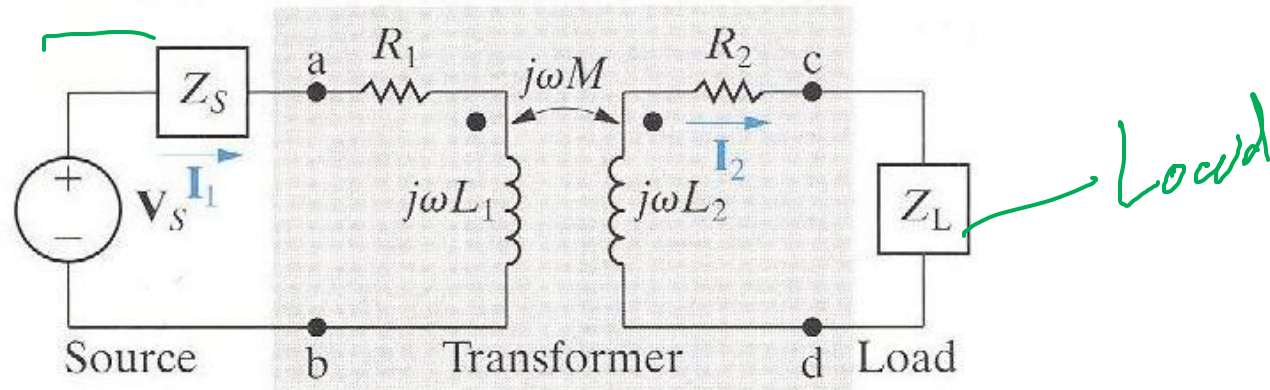
$Z_{22} = R_2 + j\omega L_2 + Z_L$  = total self - impedance of the secondary winding

Yield:

$$I_1 = \frac{Z_{22}}{Z_{11}Z_{22} + \omega^2 M^2} V_s$$

$$I_2 = \frac{j\omega M}{Z_{11}Z_{22} + \omega^2 M^2} V_s = \frac{j\omega M}{Z_{22}} I_1$$

# Transformer circuit analysis



Impedance at the terminal of the source:

$$\mathbf{Z}_{ab} = \mathbf{R}_1 + j\omega \mathbf{L}_1 + \frac{\omega^2 \mathbf{M}^2}{(\mathbf{R}_2 + j\omega \mathbf{L}_2 + \mathbf{Z}_L)}$$

$\mathbf{Z}_{ab}$  is independent of the magnetic polarity of the transformer.

$\mathbf{Z}_{ab}$  shows how the transformer affects the impedance of the load as seen from the source

## Reflected impedance

$$Z_{ab} = R_1 + j\omega L_1 + \frac{\omega^2 M^2}{\underbrace{(R_2 + j\omega L_2 + Z_L)}}_Z$$

$Z_r$  = reflected impedance

= the impedance of the secondary circuit as seen from the terminals of the primary circuit or vice versa.

### Notes:

- 1) The reflected impedance is due solely to the existence of mutual inductance
- 2) The linear transformer reflects the conjugate of the self-impedance of the secondary circuit ( $Z_{22}^*$ ) into the primary winding by a scalar multiplier

$$Z_r = \frac{\omega^2 M^2}{|Z_{22}|^2} \underbrace{[(R_2 + R_L) - j(\omega L_2 + X_L)]}_{Z_{22}^*}$$

$$Z_r = \left[ \frac{\omega M}{|Z_{22}|} \right]^2 Z_{22}^*$$

## Example

$$M = K \sqrt{L_1 L_2}$$

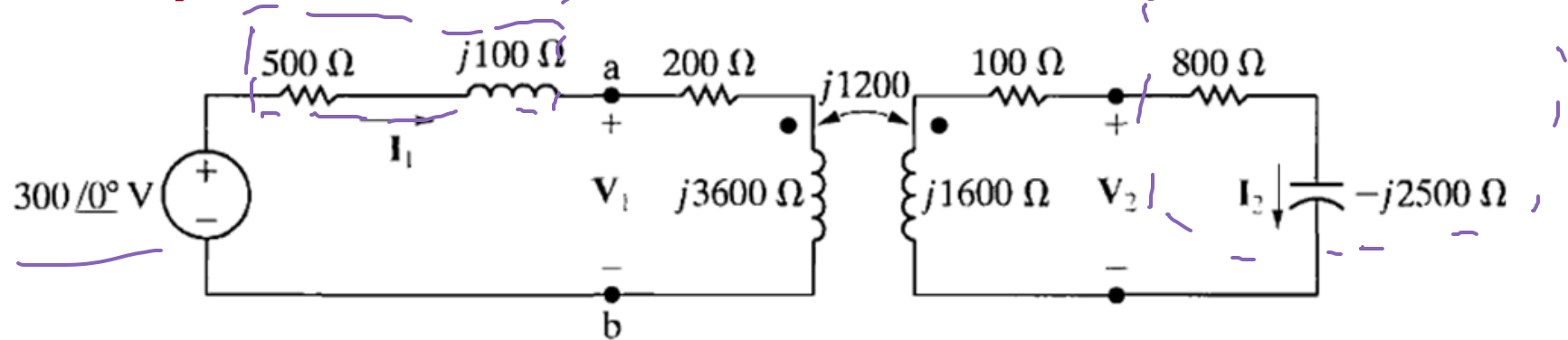
The parameters of a certain linear transformer are  $R_1 = 200 \, \Omega$ ,  $R_2 = 100 \, \Omega$ ,  $L_1 = 9H$ ,  $L_2 = 4H$ , and  $k = 0.5$ . The transformer couples an impedance consisting of an  $800 \, \Omega$  resistor in series with a  $1 \, \mu F$  capacitor to a sinusoidal voltage source. The  $300 \, V$  (rms) source has an internal impedance of  $500 + j100 \, \Omega$  and a frequency of  $400 \, \text{rad/s}$ .

- Construct a frequency-domain equivalent circuit of the system.
- Calculate the self-impedance of the primary circuit.  $\rightarrow Z_{11}$
- Calculate the self-impedance of the secondary circuit.  $\rightarrow Z_{22}$
- Calculate the impedance reflected into the primary winding.
- Calculate the scaling factor for the reflected impedance.
- Calculate the impedance seen looking into the primary terminals of the transformer.
- Calculate the Thevenin equivalent with respect to the terminals c, d.

$$\omega = 400 \, \text{rad/s}$$



## Example – Sol.



The figure shows the frequency-domain equivalent circuit. Note that the internal voltage of the source serves as the reference phasor, and that  $V_1$  and  $V_2$  represent the terminal voltages of the transformer. In the circuit of the figure, we made the following calculations:

$$j\omega L_1 = j(400)(9) = j3600 \Omega, \quad L_1$$

$$j\omega L_2 = j(400)(4) = j1600 \Omega, \quad L_2$$

$$k\sqrt{L_1 L_2} = M = 0.5\sqrt{(9)(4)} = 3 \text{ H},$$

$$j\omega M = j(400)(3) = j1200 \Omega,$$

$$\frac{1}{j\omega C} = \frac{10^6}{j400} = -j2500 \Omega. \quad C$$

## Example – Sol.

b) The self-impedance of the primary circuit is

$$Z_{11} = 500 + j100 + 200 + j3600 = 700 + j3700 \Omega.$$

$Z_{11}$  ①

c) The self-impedance of the secondary circuit is

$$Z_{22} = 100 + j1600 + 800 - j2500 = 900 - j900 \Omega.$$

$Z_{22}$  ②

d) The impedance reflected  
into the primary winding is

$$Z_r = \left( \frac{1200}{|900 - j900|} \right)^2 (900 + j900)$$

$$Z_r = \left( \frac{\omega M}{|Z_{22}|} \right)^2 Z_{22}^*$$

$$= \frac{8}{9} (900 + j900) = 800 + j800 \Omega.$$

e) The scaling factor by which  $Z_{22}^*$  is reflected is 8/9.

X Not Important.

f) The impedance seen looking into the primary terminals of the transformer is the impedance of the primary winding plus the reflected impedance; thus

$$Z_{ab} = 200 + j3600 + 800 + j800 = 1000 + j4400 \Omega.$$

$Z_R$

## Example – Sol.

g) The Thevenin voltage will equal the open circuit value of  $V_{cd}$ . The open circuit value of  $V_{cd}$  will equal  $j1200$  times the open circuit value of  $I_1$ . The open circuit value of  $I_1$  is

$$I_1 = \frac{300 \angle 0^\circ}{700 + j3700} = 79.67 \angle -79.29^\circ \text{ mA.}$$

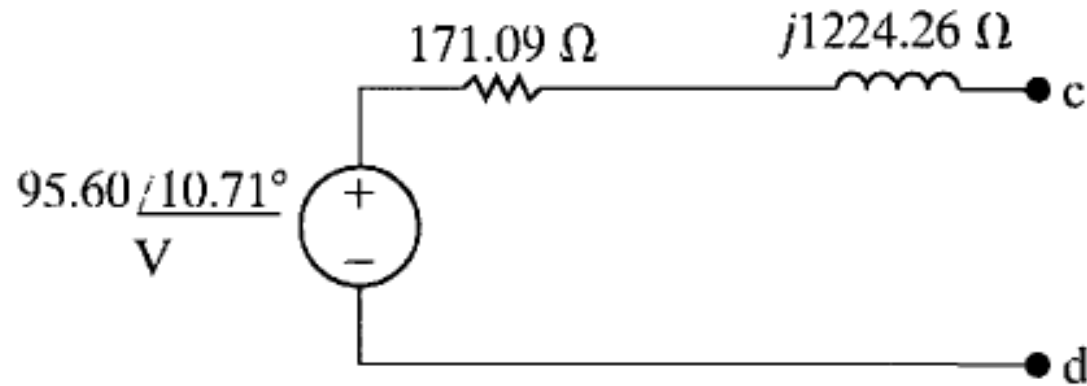
Therefore 
$$V_{Th} = j1200(79.67 \angle -79.29^\circ) \times 10^{-3}$$
$$= 95.60 \angle 10.71^\circ \text{ V.}$$

The Thevenin impedance will be equal to the impedance of the secondary winding plus the impedance reflected from the primary when the voltage source is replaced by a short-circuit. Thus

$$Z_{Th} = 100 + j1600 + \left( \frac{1200}{|700 + j3700|} \right)^2 (700 - j3700)$$
$$= 171.09 + j1224.26 \Omega.$$

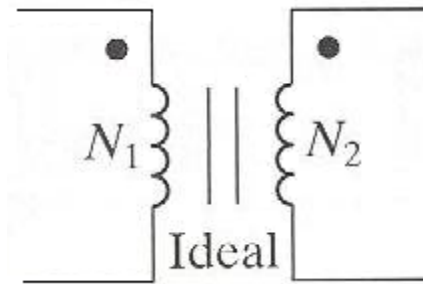
## Example – Sol.

The Thevenin equivalent is shown in the figure bellow



# Ideal transformer

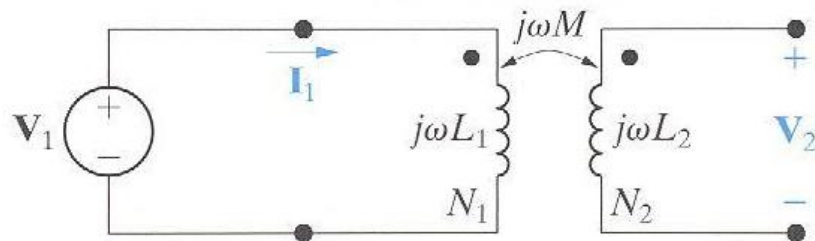
- Usually used to model the ferromagnetic transformer in power systems.
- An ideal transformer consists of two magnetically coupled coils having  $N_1$  and  $N_2$  turns, respectively, and exhibiting these three properties:
  - 1) The coefficient of coupling is unity ( $k = 1$ )
  - 2) The self-inductance of each coil is infinite ( $L_1 = L_2 = \infty$ )
  - 3) The coil losses, due to parasitic resistance, are negligible ( $R_1 = R_2 = 0$ )



# Ideal transformer

The circuit behavior is governed by the turns ratio  $a = N_2/N_1$

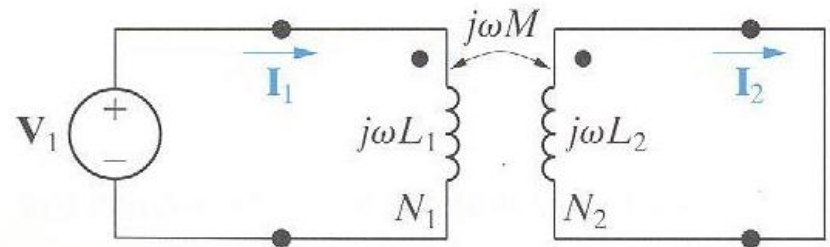
Volts per turns is the same for each winding



$$\left| \frac{V_1}{N_1} \right| = \left| \frac{V_2}{N_2} \right|$$

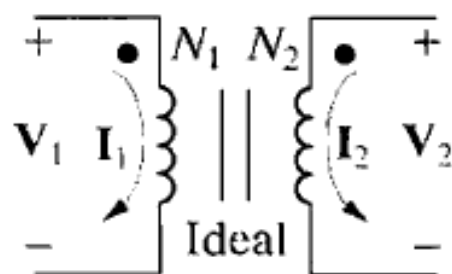
If the coil voltages  $V_1$  and  $V_2$  are both positive or negative at the dot-marked terminal, use a plus (+) sign. Otherwise, use a negative (-) sign.

Ampere turns are the same for each winding



$$|I_1 N_1| = |I_2 N_2|$$

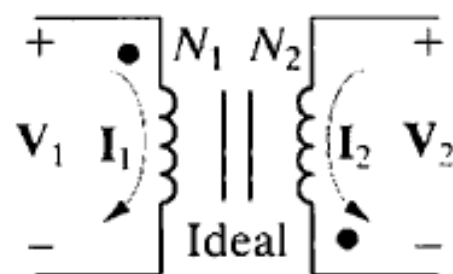
If the coil current  $I_1$  and  $I_2$  are both directed into or out of the dot-marked terminal, use a minus (-) sign. Otherwise, use a plus (+) sign.



$$\frac{V_1}{N_1} = \frac{V_2}{N_2},$$

$$N_1 I_1 = -N_2 I_2$$

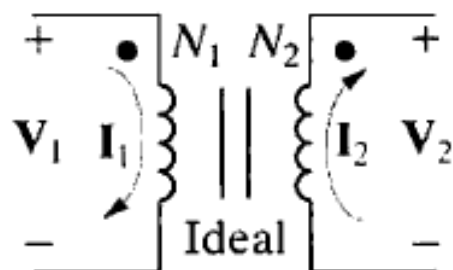
(a)



$$\frac{V_1}{N_1} = -\frac{V_2}{N_2},$$

$$N_1 I_1 = N_2 I_2$$

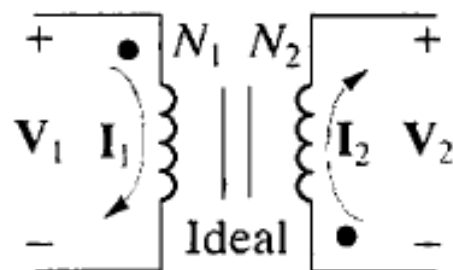
(b)



$$\frac{V_1}{N_1} = \frac{V_2}{N_2},$$

$$N_1 I_1 = N_2 I_2$$

(c)



$$\frac{V_1}{N_1} = -\frac{V_2}{N_2},$$

$$N_1 I_1 = -N_2 I_2$$

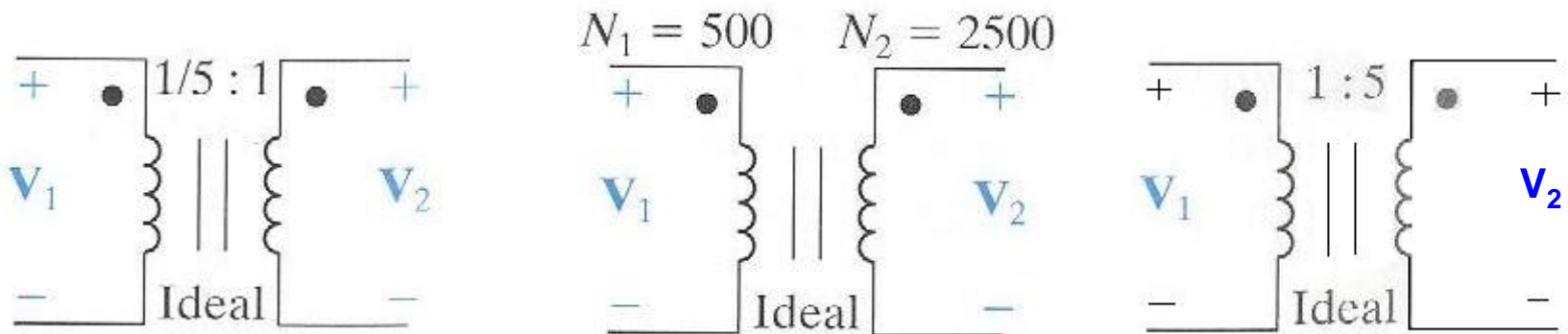
(d)

# Ideal transformer

Turns ratio:

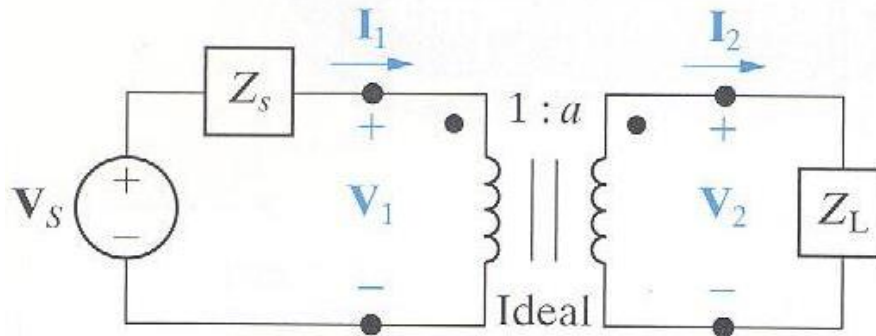
$$a = \frac{N_2}{N_1}$$

Three ways to show the turns ratio of an ideal transformer





# Impedance matching by using ideal transformer



Relation of  $V_1$  and  $I_1$  by the transformer turns ratio:

$$V_1 = \frac{V_2}{a} \quad \text{and} \quad I_1 = aI_2$$

Impedance seen by the source and load respectively:

$$Z_{IN} = \frac{V_1}{I_1} \quad \text{and} \quad Z_L = \frac{V_2}{I_2}$$

Yield:

$$Z_{IN} = \frac{1}{a^2} Z_L$$

→ *The ideal transformer's secondary coil reflects the load impedance back to the primary coil with the scaling factor  $1/a^2$ .*