

Lecture #13

# Balanced Three-Phase Circuits

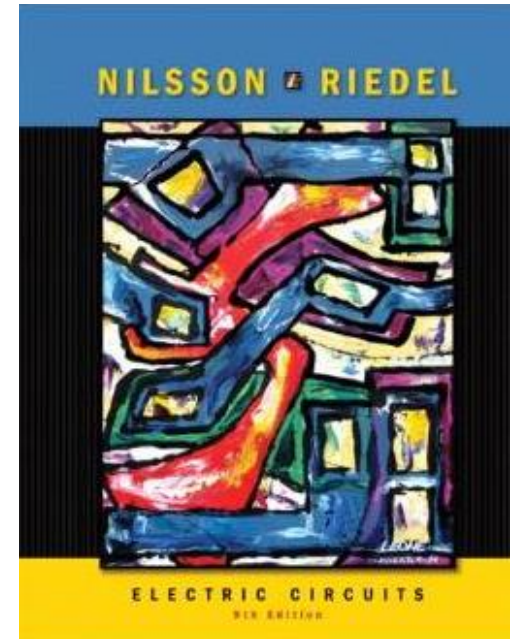
Text book: **Electric Circuits**

James W. Nilsson & Susan A. Riedel

9<sup>th</sup> Edition.

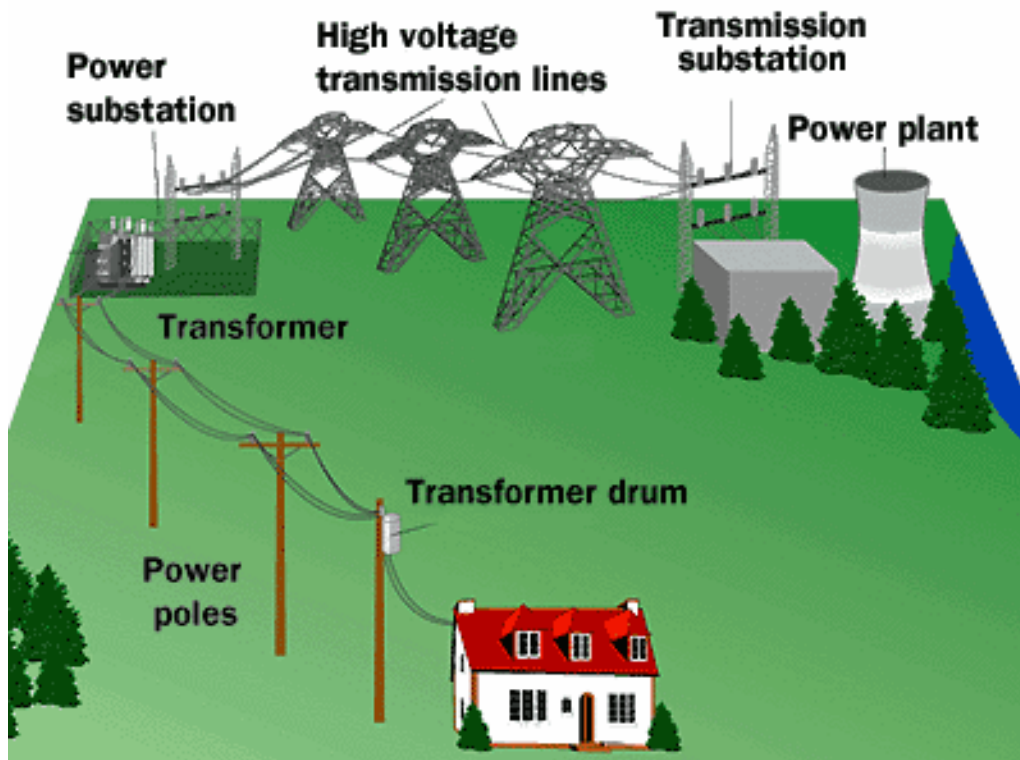
link: <http://blackboard.hcmiu.edu.vn/>

to download materials



# Overview

An electric power distribution system looks like:

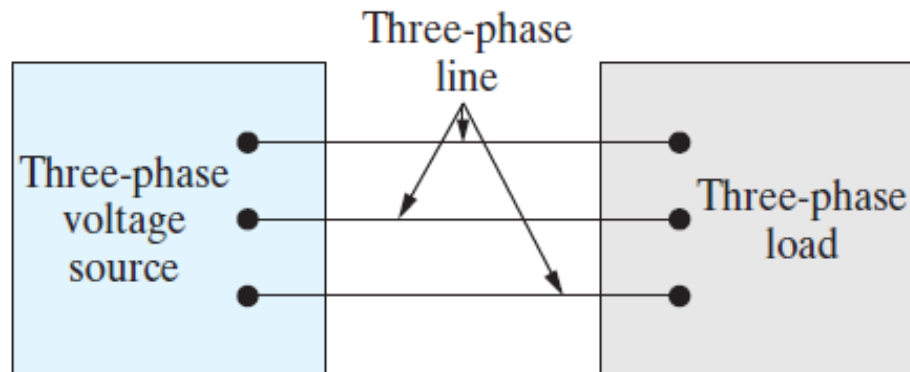


where the power transmission uses “balanced three-phase” configuration.

# Why three-phase?

Three-phase circuits are used for **generating, transmitting, distributing** and using large blocks of electric power.

The basic structure of a three-phase system consist of voltage sources connected to loads by means of transformers and transmission lines. To analyze such a circuit, we can reduce it to a voltage source connected to a load via a line.





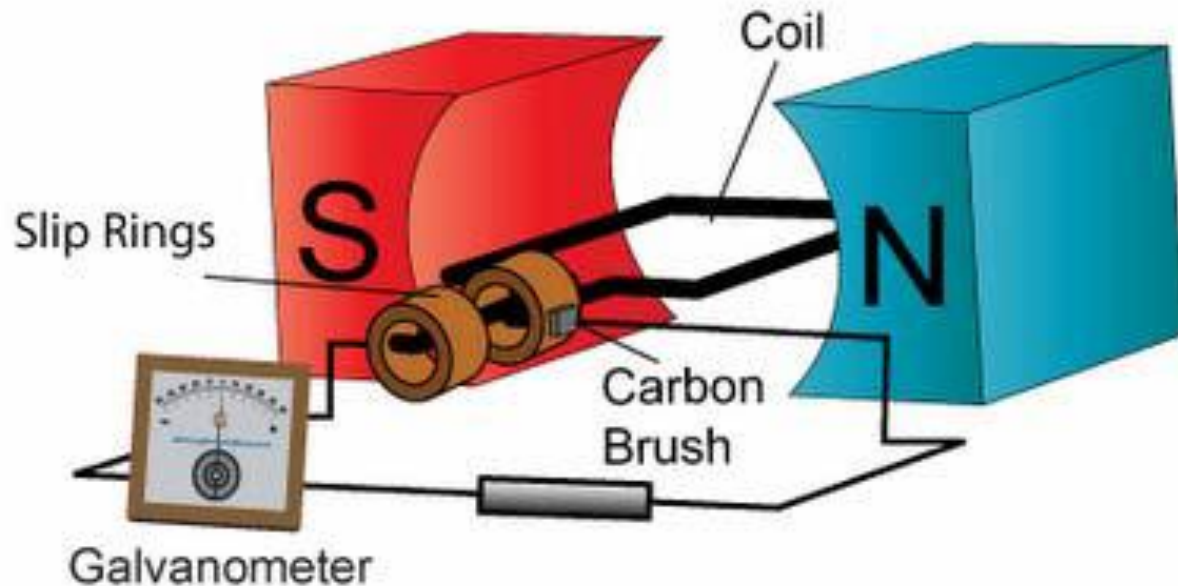
## Faraday's Law

“The **EMF induced** in a circuit is directly proportional to the time rate of change of magnetic flux through the circuit.”

The EMF can be produced by **changing B** (induced EMF) or by **changing the area**, e.g., by moving the wire (motional EMF).

# One-phase voltage sources

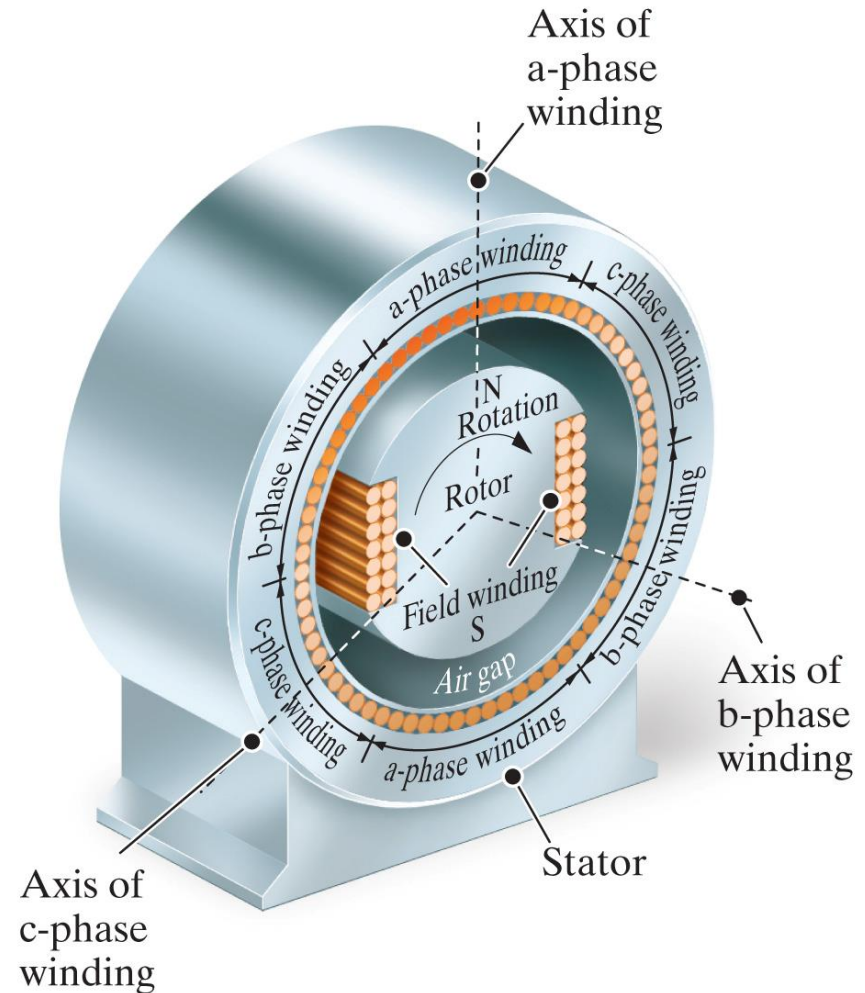
One-phase ac generator: static magnets, one rotating coil, single output voltage  $v(t) = V_m \cos \omega t$



([www.ac-motors.us](http://www.ac-motors.us))

# Three-phase voltage sources

Three static coils, rotating magnets, three output voltages  $v_a(t)$ ,  $v_b(t)$ ,  $v_c(t)$ .



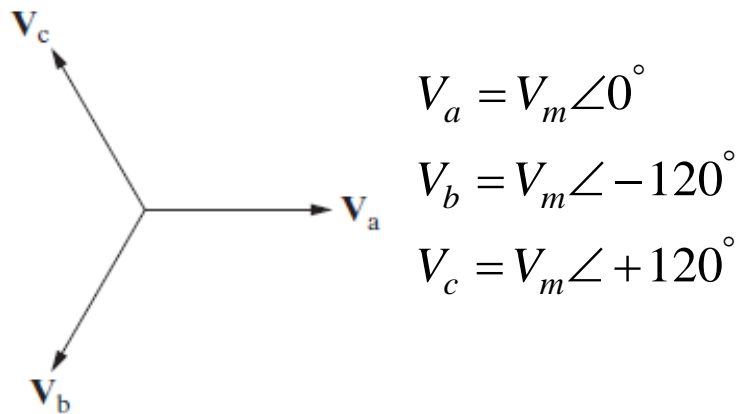
# Balanced Three-phase Voltages

Three sinusoidal voltages of the same amplitude, frequency, but differing by  $120^\circ$  phase difference with one another.

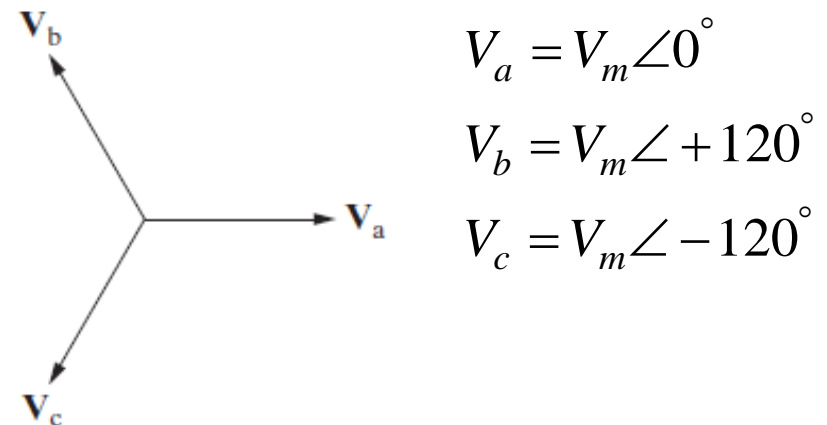
There are two possible sequences:

1. abc (positive) sequence:  $v_b(t)$  lags  $v_a(t)$  by  $120^\circ$ .
2. acb (negative) sequence:  $v_b(t)$  leads  $v_a(t)$  by  $120^\circ$ .

abc (positive) phase sequence



acb (negative) phase sequence



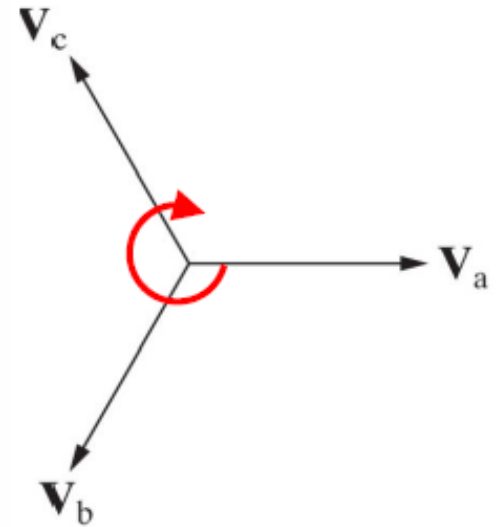
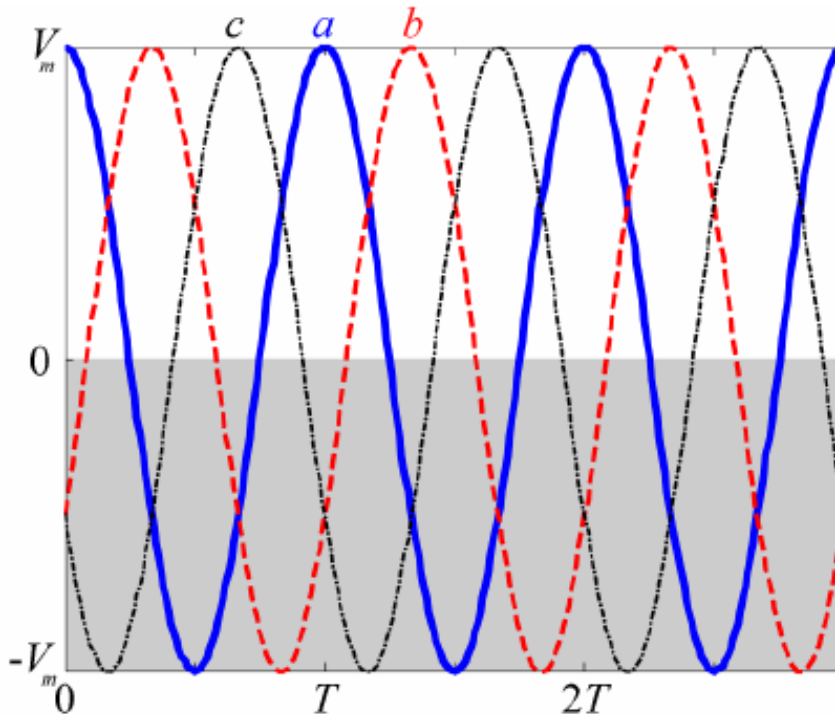
An important characteristic of a set of balanced three-phase voltages is that the sum of the voltages is zero

$$V_a + V_b + V_c = 0$$

# Balanced Three-phase Voltages

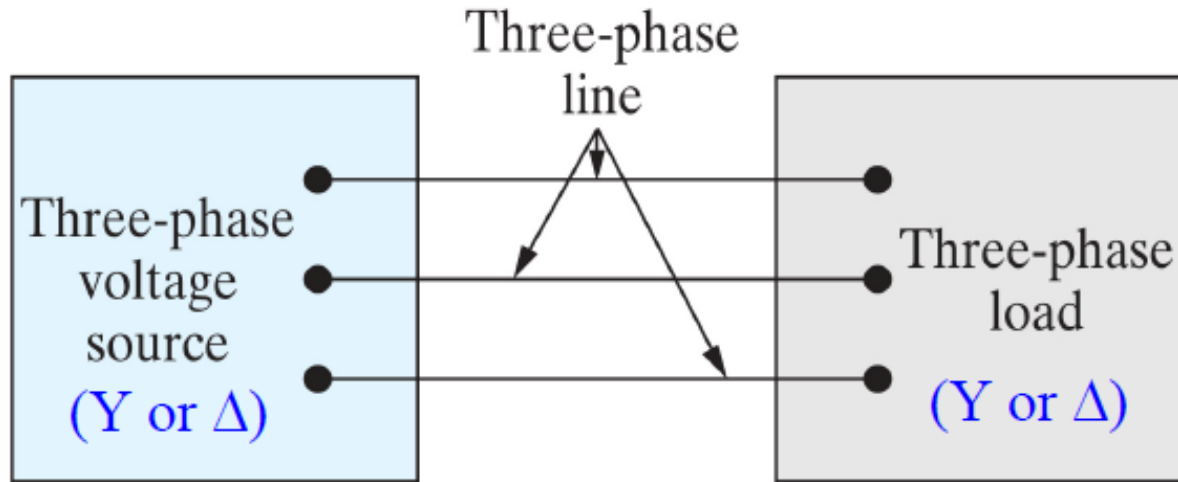
abc sequence

- $v_b(t)$  lags  $v_a(t)$  by  $120^\circ$  or  $T/3$ .
- $\mathbf{V}_a = V_m \angle 0^\circ$ ,  $\mathbf{V}_b = V_m \angle -120^\circ$ ,  $\mathbf{V}_c = V_m \angle +120^\circ$ .



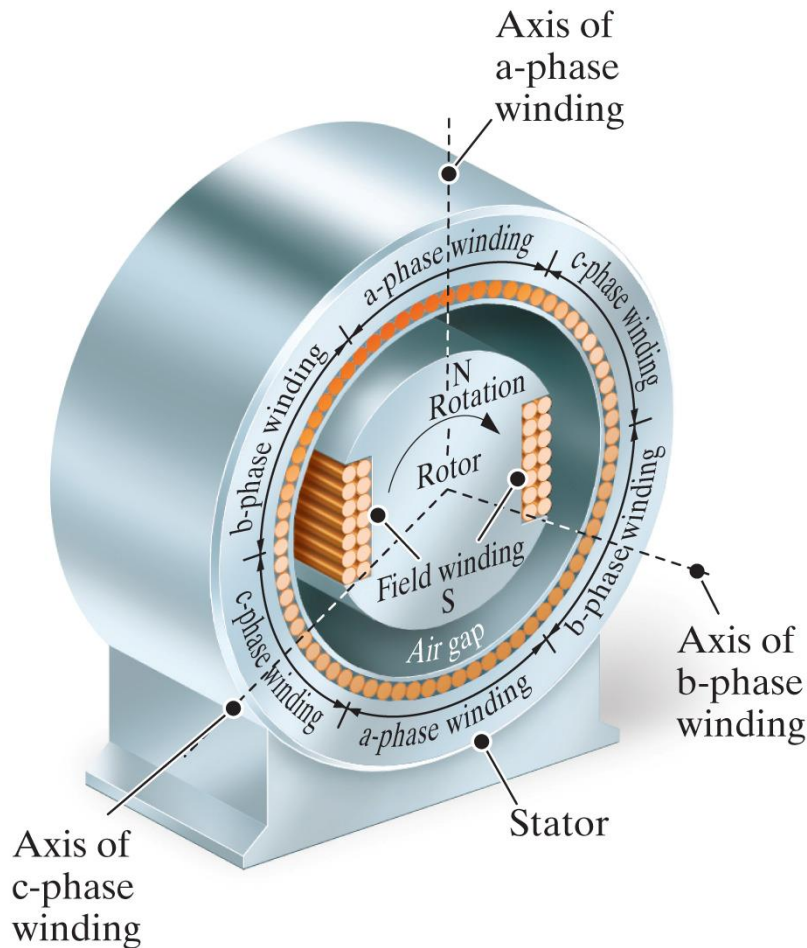


# Three-phase systems



- Source-load can be connected in four configurations: Y-Y, Y-Δ, Δ-Y, Δ-Δ.
- It's sufficient to analyze Y-Y, while the others can be treated by Δ-Y and Y-Δ transformations.

# Balanced Three-phase Voltages



A three-phase voltage source is a generator with **three separate windings** distributed around the periphery of the stator.

Each winding comprises one phase of the generator.

The **rotor of the generator is an electromagnet** driven at synchronous speed by a prime mover, such as a **steam or gas turbine**.

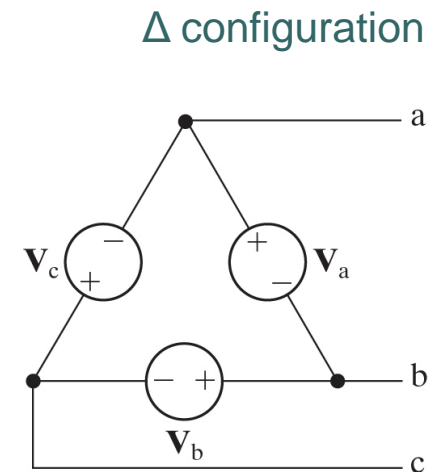
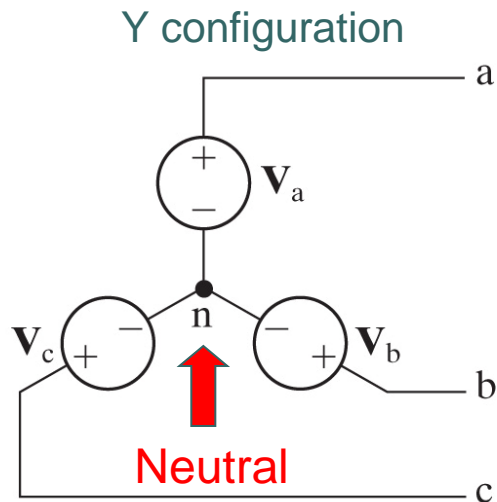
Rotation of the electromagnet induces a sinusoidal voltage in each winding.

The phase windings are designed so that the sinusoidal voltages induced in them are **equal in amplitude and out of phase with each other by  $120^\circ$** .

The phase windings are stationary with respect to the rotating electromagnet, so the frequency of the voltage induced in each winding is the same.

# Balanced Three-phase Voltages

- Ideal Y- and  $\Delta$ -connected voltage sources
- There are two ways of interconnecting the separate phase windings to form a three-phase source:



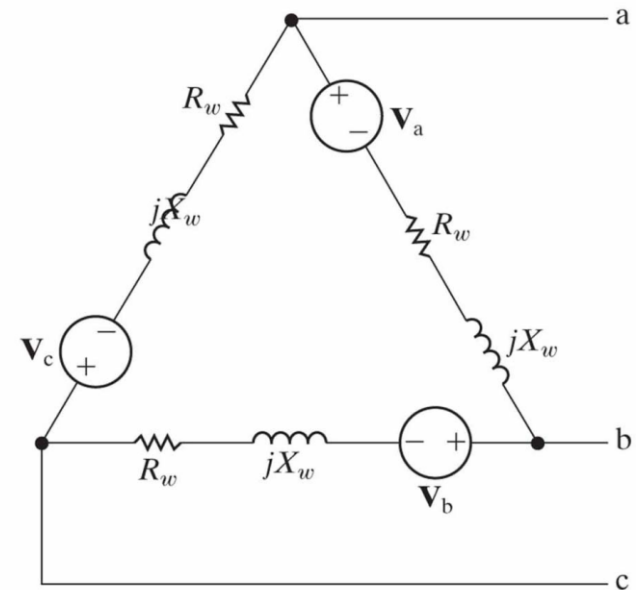
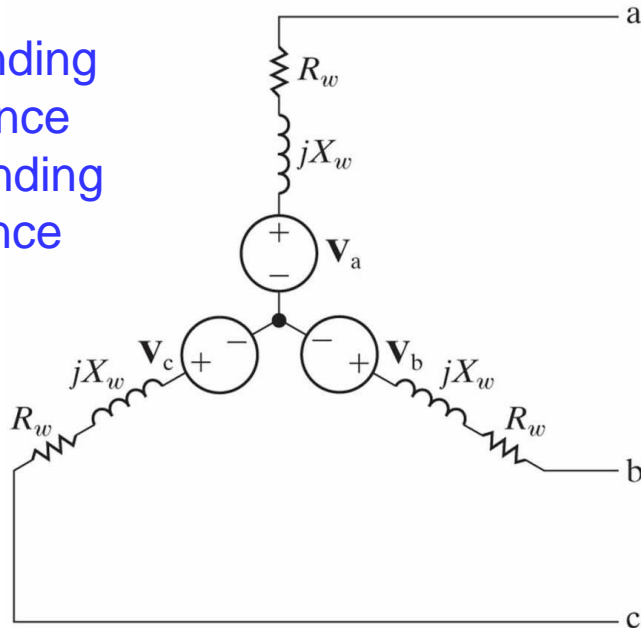
$n$  is the neutral terminal of the source. The neutral terminal may or may not be available for external connections

# Balanced Three-phase Voltages

Real Y- and  $\Delta$ -connected voltage sources

- Three-phase sources and loads can be either Y or  $\Delta$ -connected, therefore, there are 4 different configuration between source and load: Y – Y, Y –  $\Delta$ ,  $\Delta$  – Y,  $\Delta$  –  $\Delta$ .

$R_w$ : winding  
resistance  
 $X_w$ : winding  
reactance

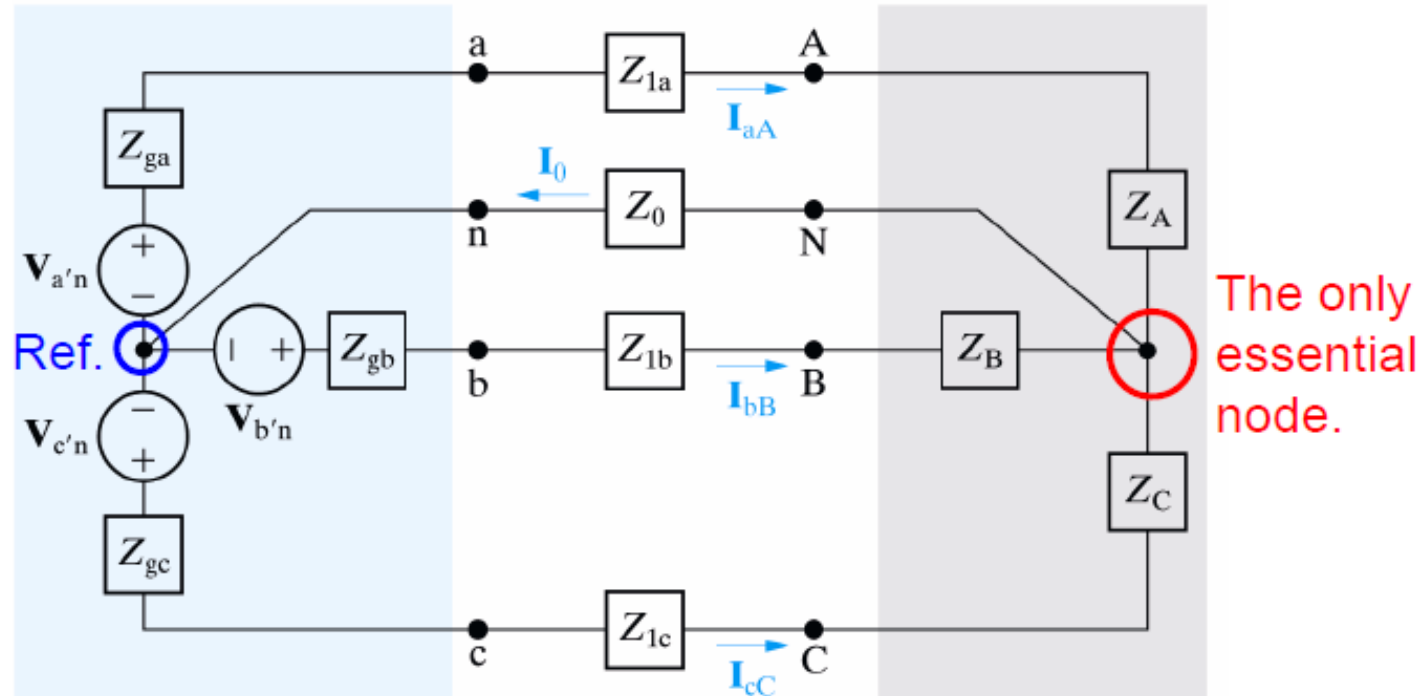


A model of a three-phase source with winding impedance

Internal impedance of a generator is usually **inductive** (due to the use of coils).

# Analysis of the Y-Y circuit

General Y-Y  
circuit model



$Z_{ga}$ ,  $Z_{gb}$ ,  $Z_{gc}$  : the internal impedance associated with each phase winding of the voltage generator.

$Z_{1a}$ ,  $Z_{1b}$ ,  $Z_{1c}$  : the impedance of the lines connecting a phase of the source to a phase of the load

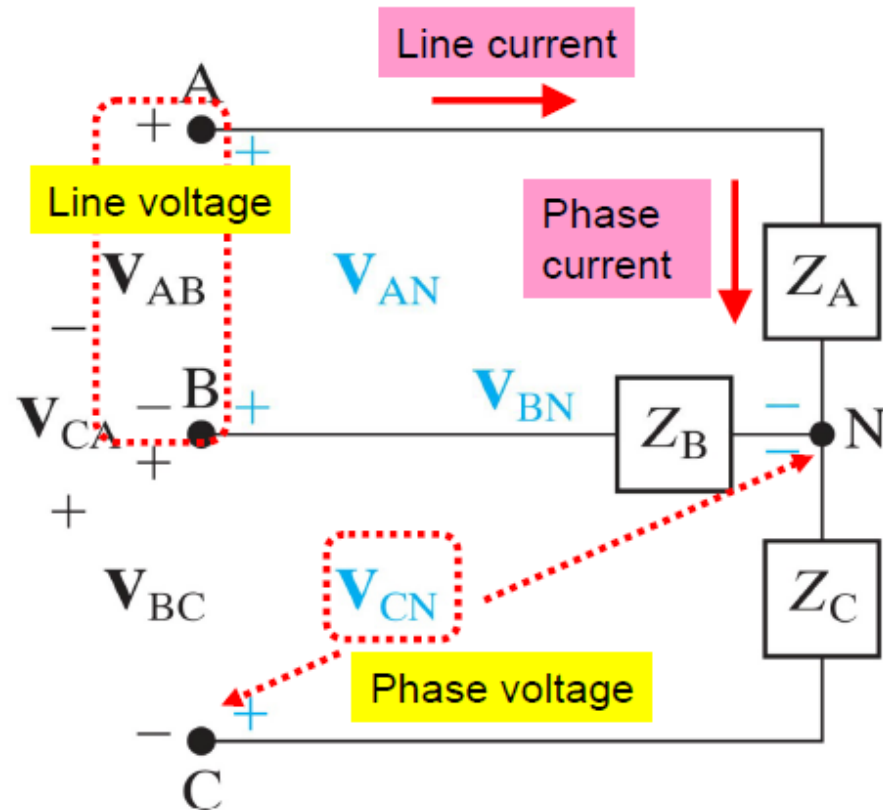
$Z_0$  : the impedance of the neutral conductor connecting the source neutral to the load neutral

$Z_A$ ,  $Z_B$ ,  $Z_C$  : the impedance of each phase of the load.

# Analysis of the Y-Y circuit

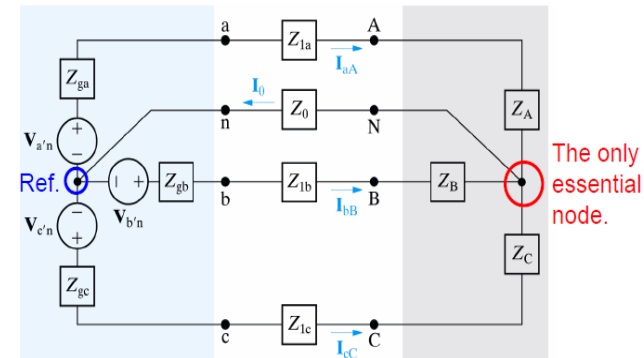
Unknowns to be solved

- Line (line-to-line) voltage: voltage across any pair of lines.
- Phase (line-to-neutral) voltage: voltage across a single phase.
- For Y-connected load, line current equals phase current.



# Analysis of the Y-Y circuit

Solution to general three-phase circuit



No matter it's **balanced or imbalanced** three- phase circuit, KCL leads to one equation:

$$\mathbf{I}_0 = \mathbf{I}_{aA} + \mathbf{I}_{bB} + \mathbf{I}_{cC}, \Rightarrow$$

$$\frac{\mathbf{V}_N}{Z_0} = \frac{\mathbf{V}_{a'n} - \mathbf{V}_N}{Z_{ga} + Z_{1a} + Z_A} + \frac{\mathbf{V}_{b'n} - \mathbf{V}_N}{Z_{gb} + Z_{1b} + Z_B} + \frac{\mathbf{V}_{c'n} - \mathbf{V}_N}{Z_{gc} + Z_{1c} + Z_C} \dots (1),$$

↓

Impedance  
of neutral  
line.

↓

Total  
impedance  
along line aA.

↓

Total  
impedance  
along line bB.

↓

Total  
impedance  
along line cC.

which is sufficient to solve  $\mathbf{V}_N$  (thus the entire circuit).

# Analysis of the Y-Y circuit

Solution to “balanced” three-phase circuit

■ For balanced three-phase circuits,

1.  $\{V_{a'n}, V_{b'n}, V_{c'n}\}$  have equal magnitude and  $120^\circ$  relative phases;

2.  $\{Z_{ga} = Z_{gb} = Z_{gc}\}$ ,  $\{Z_{1a} = Z_{1b} = Z_{1c}\}$ ,  $\{Z_A = Z_B = Z_C\}$ ;  
 $\Rightarrow$  total impedance along any line is the same

$$Z_{ga} + Z_{1a} + Z_A = \dots = Z_\phi.$$

■ Eq. (1) becomes: 
$$\frac{V_N}{Z_0} = \frac{V_{a'n} - V_N}{Z_\phi} + \frac{V_{b'n} - V_N}{Z_\phi} + \frac{V_{c'n} - V_N}{Z_\phi},$$

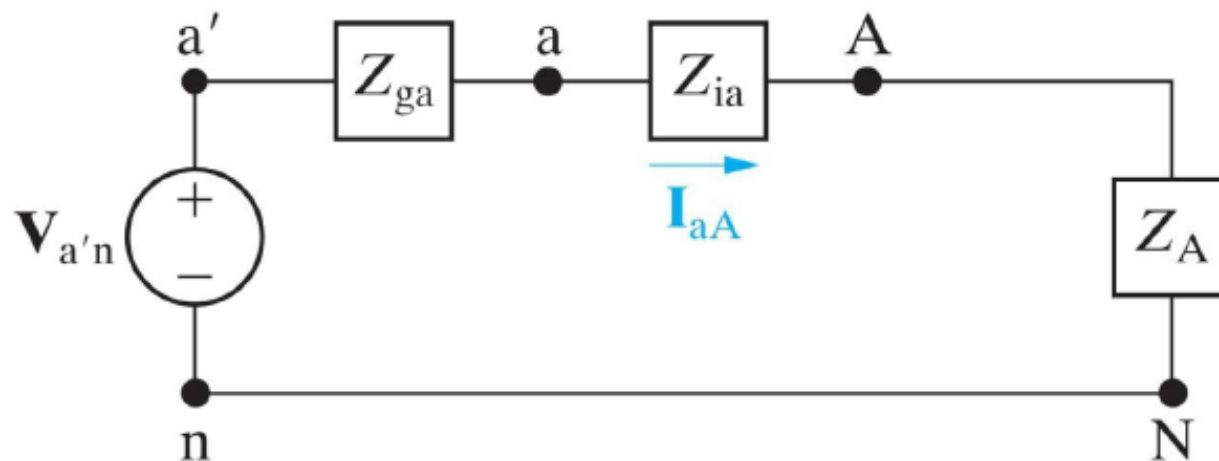
$$\Rightarrow V_N \left( \frac{1}{Z_0} + \frac{3}{Z_\phi} \right) = \frac{\vec{V}_{a'n} + \vec{V}_{b'n} + \vec{V}_{c'n}}{Z_\phi} = 0, \quad V_N = 0.$$



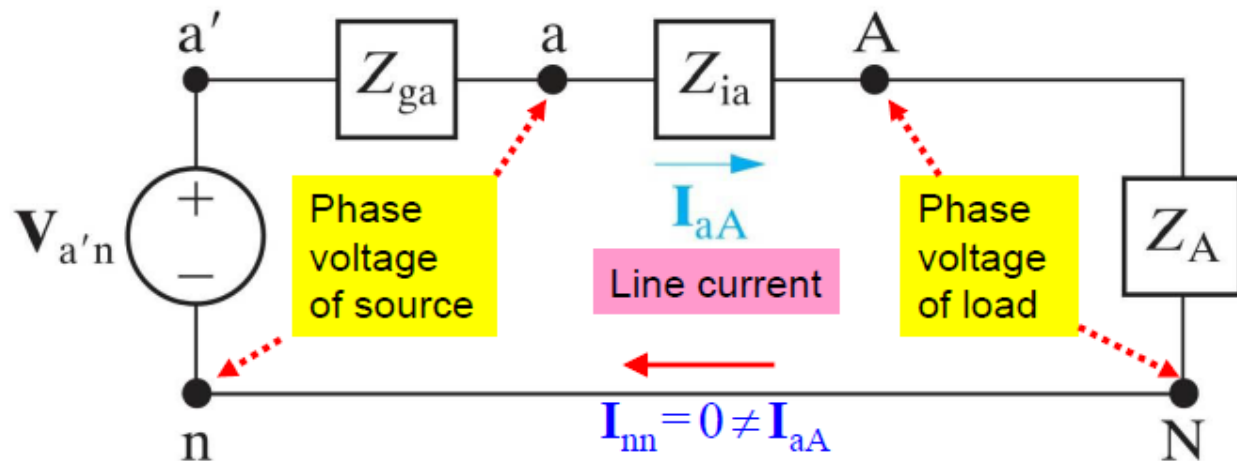
## Analysis of the Y-Y circuit

### Meaning of the solution

- $V_N = 0$  means no voltage difference between nodes  $n$  and  $N$  in the presence of  $Z_0$ .  $\Rightarrow$  Neutral line is **both short** ( $v = 0$ ) and **open** ( $i = 0$ ).
- The three-phase circuit can be separated into 3 one-phase circuits (open), while each of them has a short between nodes  $n$  and  $N$ .



## Equivalent one-phase circuit



- Directly giving the line current & phase voltages:

$$I_{aA} = \frac{V_{a'n} - \cancel{V_N}}{(Z_{ga} + Z_{ia} + Z_A) = Z_\phi}, \quad V_{AN} = I_{aA} Z_A, \quad V_{an} = I_{aA} (Z_{ia} + Z_A).$$

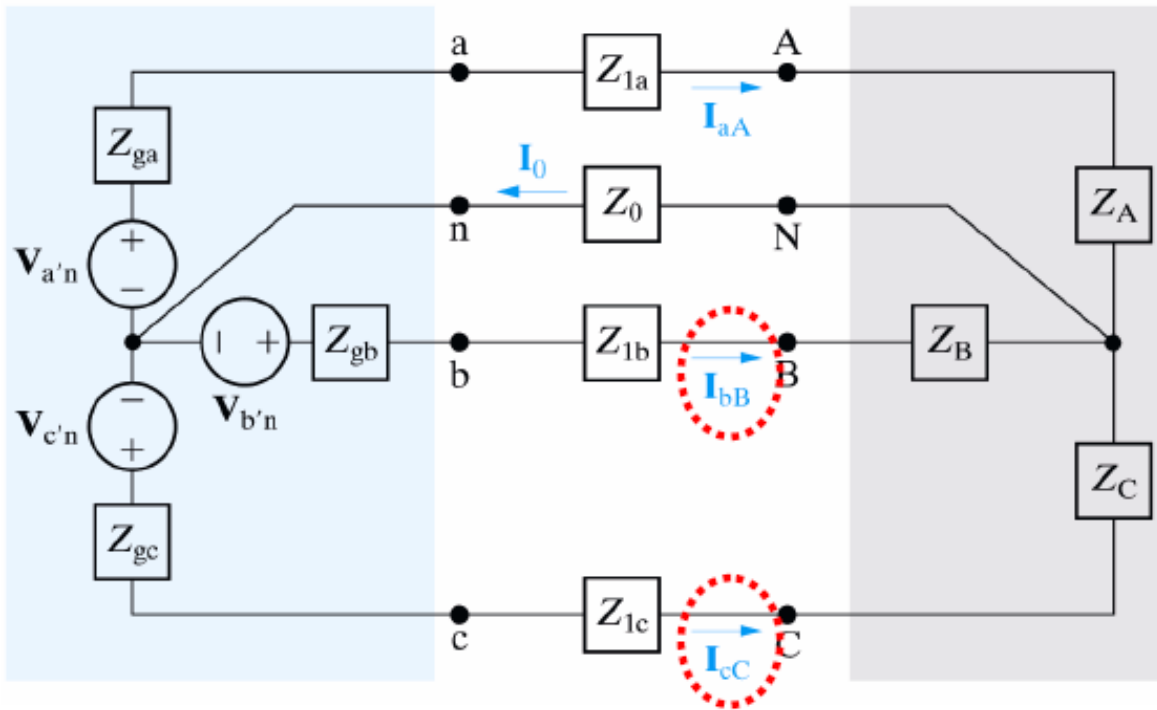
- Unknowns of phases b, c can be determined by the fixed (abc or acb) **sequence relation**.

## Analysis of the Y-Y circuit

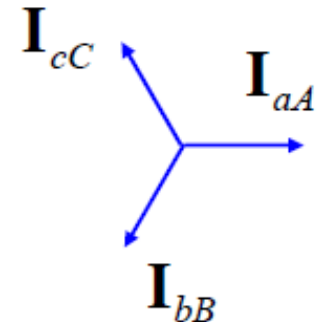
The 3 line and phase currents in abc sequence

Given  $\mathbf{I}_{aA} = \mathbf{V}_{a'n} / Z_\phi$ , the other 2 line currents are:

$$\mathbf{I}_{bB} = \frac{\mathbf{V}_{b'n}}{Z_\phi} = \mathbf{I}_{aA} \angle -120^\circ, \quad \mathbf{I}_{cC} = \frac{\mathbf{V}_{c'n}}{Z_\phi} = \mathbf{I}_{aA} \angle 120^\circ,$$



which still follow the abc sequence relation.



# Analysis of the Y-Y circuit

The phase & line voltages of the load in **abc seq.**

$$\mathbf{V}_{AN} = \mathbf{V}_{a'n} \frac{Z_A}{Z_\phi}, \mathbf{V}_{BN} = \mathbf{V}_{b'n} \frac{Z_B}{Z_\phi} = \mathbf{V}_{AN} \angle -120^\circ, \mathbf{V}_{CN} = \mathbf{V}_{AN} \angle 120^\circ.$$

$$\mathbf{V}_{AB} = \mathbf{V}_{AN} - \mathbf{V}_{BN}$$

$$= \mathbf{V}_{AN} - (\mathbf{V}_{AN} \angle -120^\circ)$$

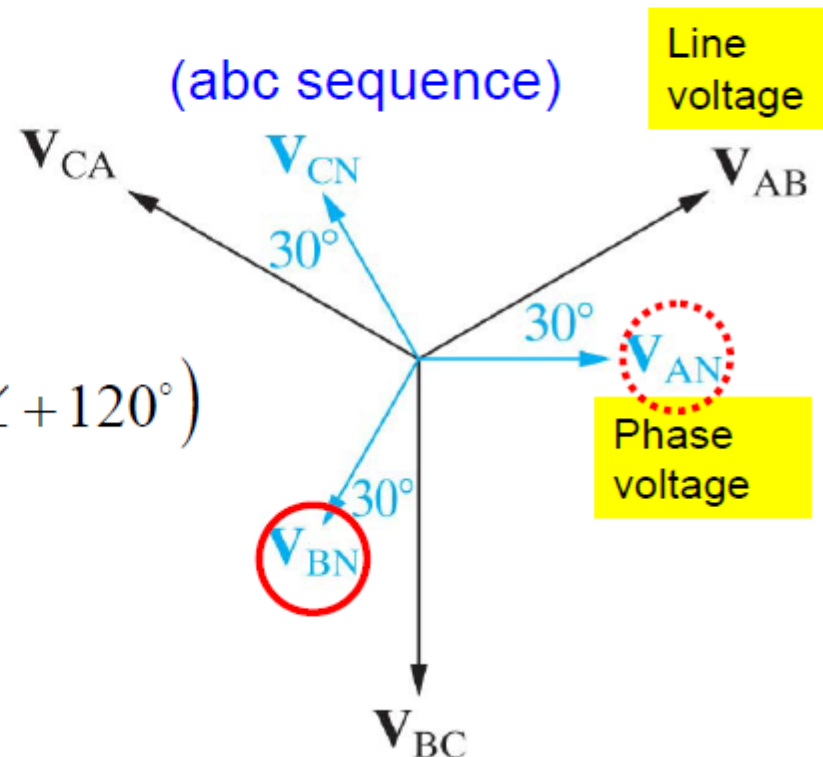
$$= \sqrt{3} \mathbf{V}_{AN} \angle +30^\circ,$$

$$\mathbf{V}_{BC} = (\mathbf{V}_{AN} \angle -120^\circ) - (\mathbf{V}_{AN} \angle +120^\circ)$$

$$= \sqrt{3} \mathbf{V}_{AN} \angle -90^\circ,$$

$$\mathbf{V}_{CA} = (\mathbf{V}_{AN} \angle +120^\circ) - \mathbf{V}_{AN}$$

$$= \sqrt{3} \mathbf{V}_{AN} \angle +150^\circ.$$



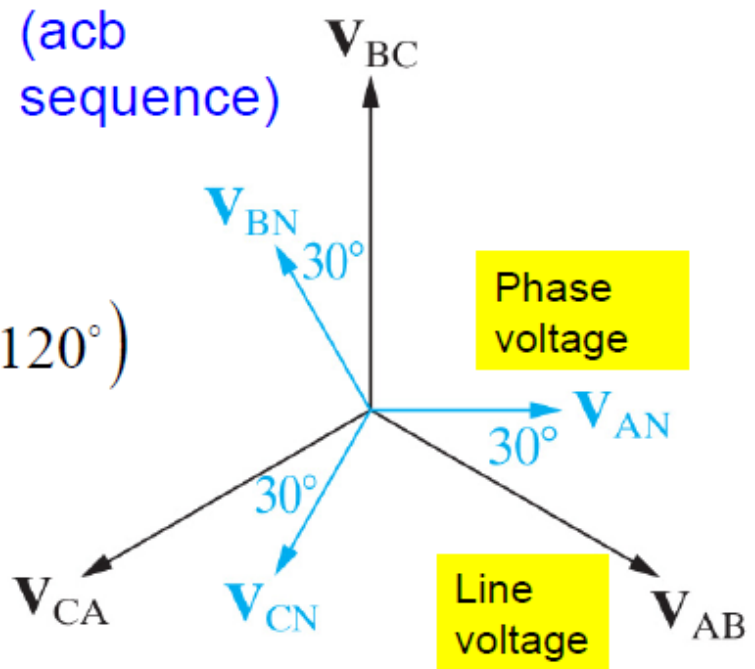
# Analysis of the Y-Y circuit

The phase & line voltages of the load in **acb seq.**

$$\begin{aligned}V_{AB} &= V_{AN} - V_{BN} \\&= V_{AN} - (V_{AN} \angle +120^\circ) \\&= \sqrt{3} V_{AN} \angle -30^\circ,\end{aligned}$$

$$\begin{aligned}V_{BC} &= (V_{AN} \angle +120^\circ) - (V_{AN} \angle -120^\circ) \\&= \sqrt{3} V_{AN} \angle +90^\circ,\end{aligned}$$

$$\begin{aligned}V_{CA} &= (V_{AN} \angle -120^\circ) - V_{AN} \\&= \sqrt{3} V_{AN} \angle -150^\circ.\end{aligned}$$



- Line voltages are  $\sqrt{3}$  times bigger, leading (abc) or lagging (acb) the phase voltages by  $30^\circ$ .



# Analysis of the Y-Y circuit

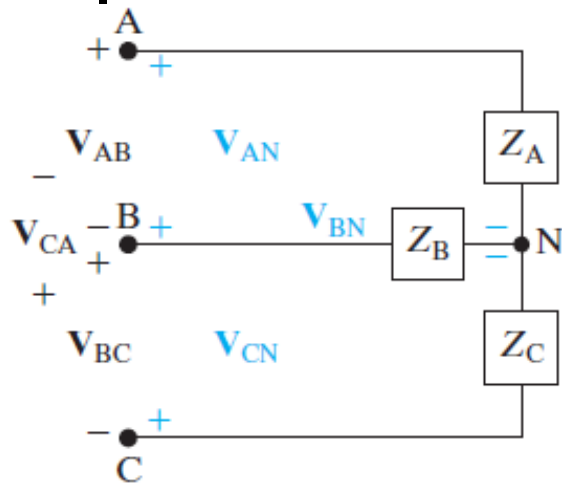
Load balance  $V_N=0$

$$I_{aA} = \frac{V_{a'n} - V_N}{Z_A + Z_{1a} + Z_{ga}} = \frac{V_{a'n}}{Z_\phi}$$

$$I_{bB} = \frac{V_{b'n} - V_N}{Z_B + Z_{1b} + Z_{gb}} = \frac{V_{b'n}}{Z_\phi}$$

$$I_{cC} = \frac{V_{c'n} - V_N}{Z_C + Z_{1c} + Z_{gc}} = \frac{V_{c'n}}{Z_\phi}$$

# Line-to-line and line-to-neutral voltages

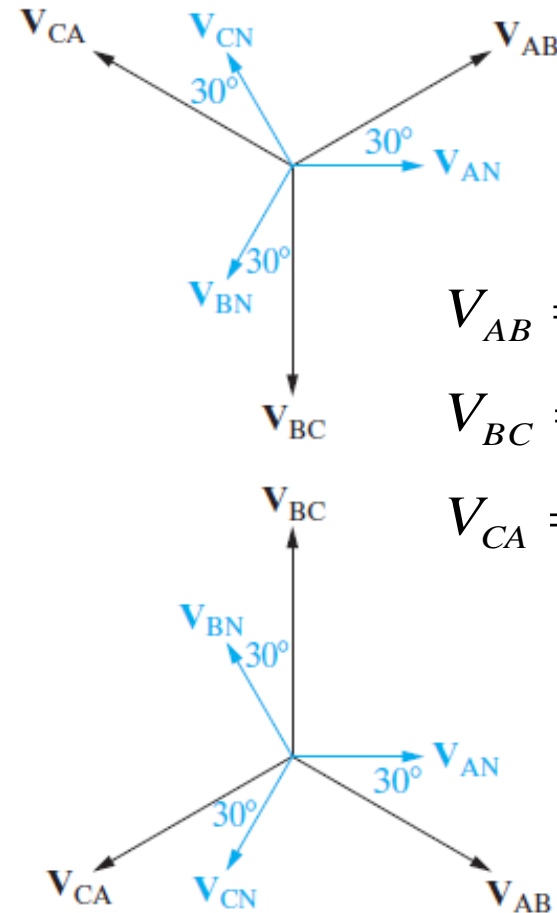


**Figure 11.8** ▲ Line-to-line and line-to-neutral voltages.

$$V_{AB} = V_{AN} - V_{BN}$$

$$V_{BC} = V_{BN} - V_{CN}$$

$$V_{CA} = V_{CN} - V_{AN}$$



$$V_{AB} = \sqrt{3}V_{\phi} \angle 30^{\circ}$$

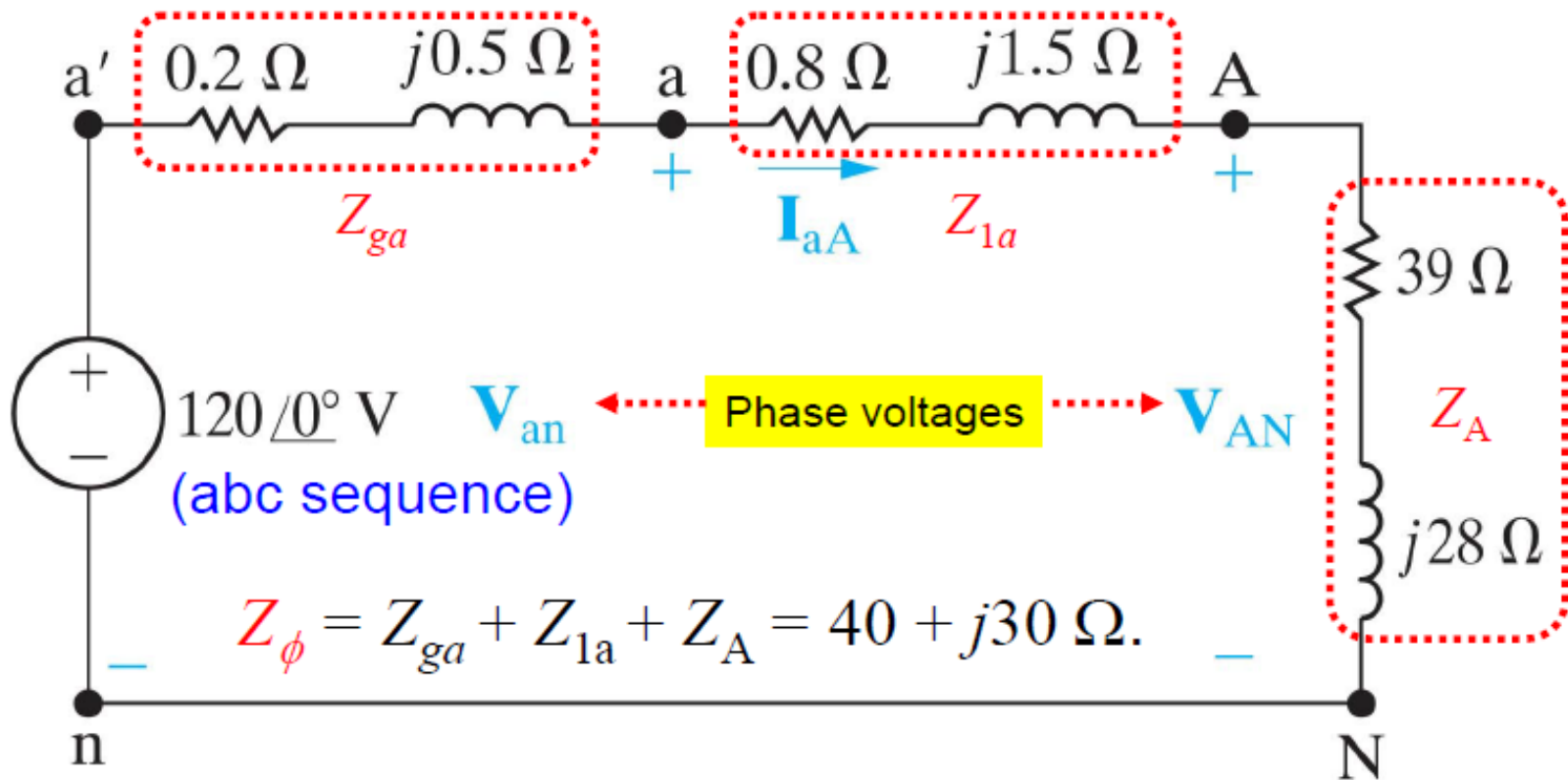
$$V_{BC} = \sqrt{3}V_{\phi} \angle -90^{\circ}$$

$$V_{CA} = \sqrt{3}V_{\phi} \angle 150^{\circ}$$

**Figure 11.9** ▲ Phasor diagrams showing the relationship between line-to-line and line-to-neutral voltages in a balanced system. (a) The abc sequence. (b) The acb sequence.

## Example

Q: What are the line currents, phase and line voltages of the load and source, respectively?





## Example

- The 3 **line currents** (of both load & source) are:

$$\mathbf{I}_{aA} = \frac{\mathbf{V}_{a'n}}{Z_{ga} + Z_{1a} + Z_A} = \frac{120 \angle 0^\circ}{40 + j30} = (2.4 \angle -36.87^\circ) \text{ A},$$

$$\mathbf{I}_{bB} = \mathbf{I}_{aA} \angle -120^\circ = (2.4 \angle -156.87^\circ) \text{ A},$$

$$\mathbf{I}_{cC} = \mathbf{I}_{aA} \angle +120^\circ = (2.4 \angle +83.13^\circ) \text{ A}.$$

- The 3 **phase voltages** of the **load** are:

$$\mathbf{V}_{AN} = \mathbf{I}_{aA} Z_A = (2.4 \angle -36.87^\circ)(39 + j28) = (115.22 \angle -1.19^\circ) \text{ V}.$$

$$\mathbf{V}_{BN} = \mathbf{V}_{AN} \angle -120^\circ = (115.22 \angle -121.19^\circ) \text{ V},$$

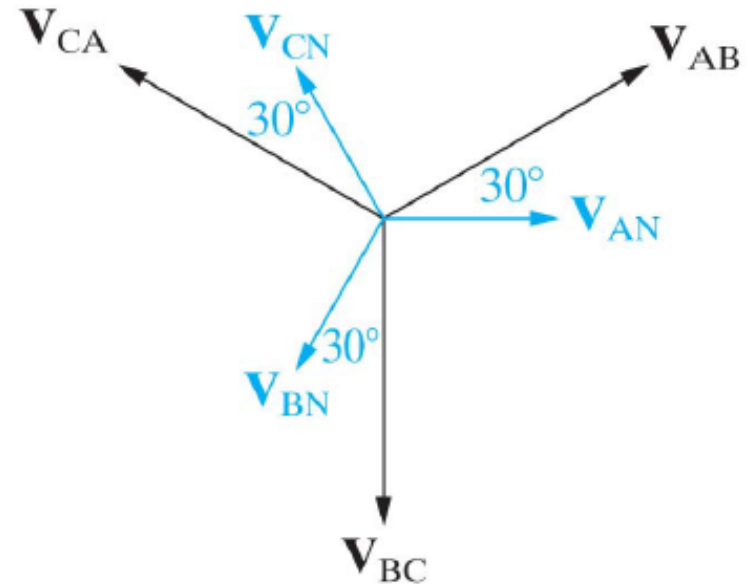
$$\mathbf{V}_{CN} = \mathbf{V}_{AN} \angle +120^\circ = (115.22 \angle +118.81^\circ) \text{ V}.$$

- The 3 line voltages of the load are:

$$\begin{aligned} \mathbf{V}_{AB} &= (\sqrt{3} \angle 30^\circ) \mathbf{V}_{AN} \\ &= (\sqrt{3} \angle 30^\circ) (115.22 \angle -1.19^\circ) \\ &= (199.58 \angle +28.81^\circ) \text{ V}, \end{aligned}$$

$$\begin{aligned} \mathbf{V}_{BC} &= \mathbf{V}_{AB} \angle -120^\circ \\ &= (199.58 \angle -91.19^\circ) \text{ V}, \end{aligned}$$

$$\begin{aligned} \mathbf{V}_{CA} &= \mathbf{V}_{AB} \angle +120^\circ \\ &= (199.58 \angle +148.81^\circ) \text{ V}. \end{aligned}$$



- 
- The 3 **phase voltages** of the **source** are:

$$\begin{aligned}V_{an} &= V_{a'n} - \mathbf{I}_{aA} Z_{ga} = 120 - (2.4 \angle -36.87^\circ)(0.2 + j0.5) \\&= (118.9 \angle -0.32^\circ) \text{V},\end{aligned}$$

$$V_{bn} = V_{an} \angle -120^\circ = (118.9 \angle -120.32^\circ) \text{V},$$

$$V_{cn} = V_{an} \angle +120^\circ = (118.9 \angle +119.68^\circ) \text{V}.$$

- The three **line voltages** of the **source** are:

$$\begin{aligned}V_{ab} &= (\sqrt{3} \angle 30^\circ) V_{an} = (\sqrt{3} \angle 30^\circ)(118.9 \angle -0.32^\circ) \\&= (205.94 \angle +29.68^\circ) \text{V},\end{aligned}$$

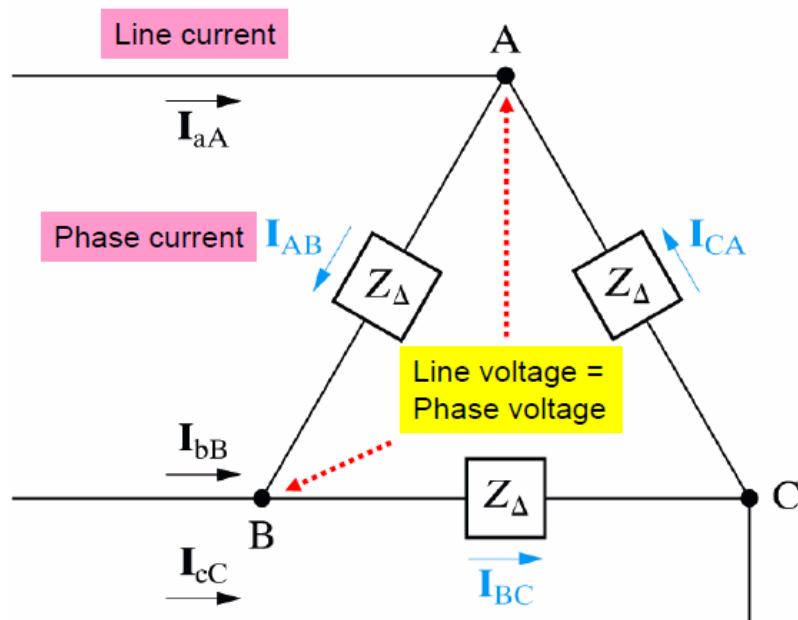
$$V_{bc} = V_{ab} \angle -120^\circ = (205.94 \angle -90.32^\circ) \text{V},$$

$$V_{ca} = V_{ab} \angle +120^\circ = (205.94 \angle +149.68^\circ) \text{V}.$$

# Analysis of the Y-Δ Circuit

Δ-Y transformation for balanced 3-phase load

Load in Δ configuration



The impedance of each leg in Y-configuration ( $Z_Y$ ) is one-third of that in Δ-configuration ( $Z_\Delta$ ):

$$Z_1 = \frac{Z_b Z_c}{Z_a + Z_b + Z_c},$$

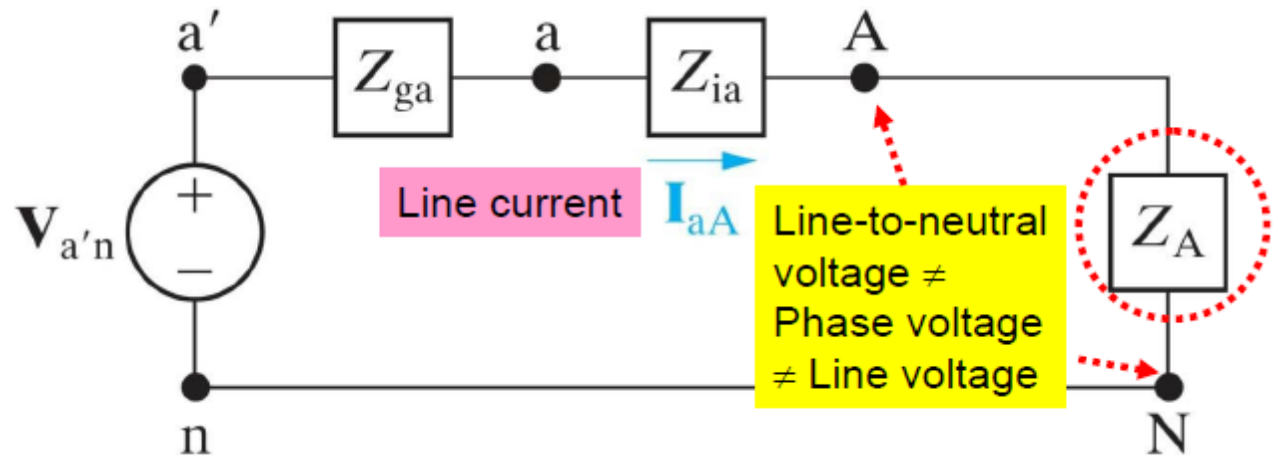
$$Z_2 = \frac{Z_c Z_a}{Z_a + Z_b + Z_c},$$

$$Z_3 = \frac{Z_a Z_b}{Z_a + Z_b + Z_c}.$$

$$\Rightarrow Z_Y = \frac{Z_\Delta Z_\Delta}{3Z_\Delta} = \frac{Z_\Delta}{3}.$$

# Equivalent one-phase circuit

The 1-phase equivalent circuit in Y-Y config. continues to work if  $Z_A$  is replaced by  $Z_{\Delta}/3$ :



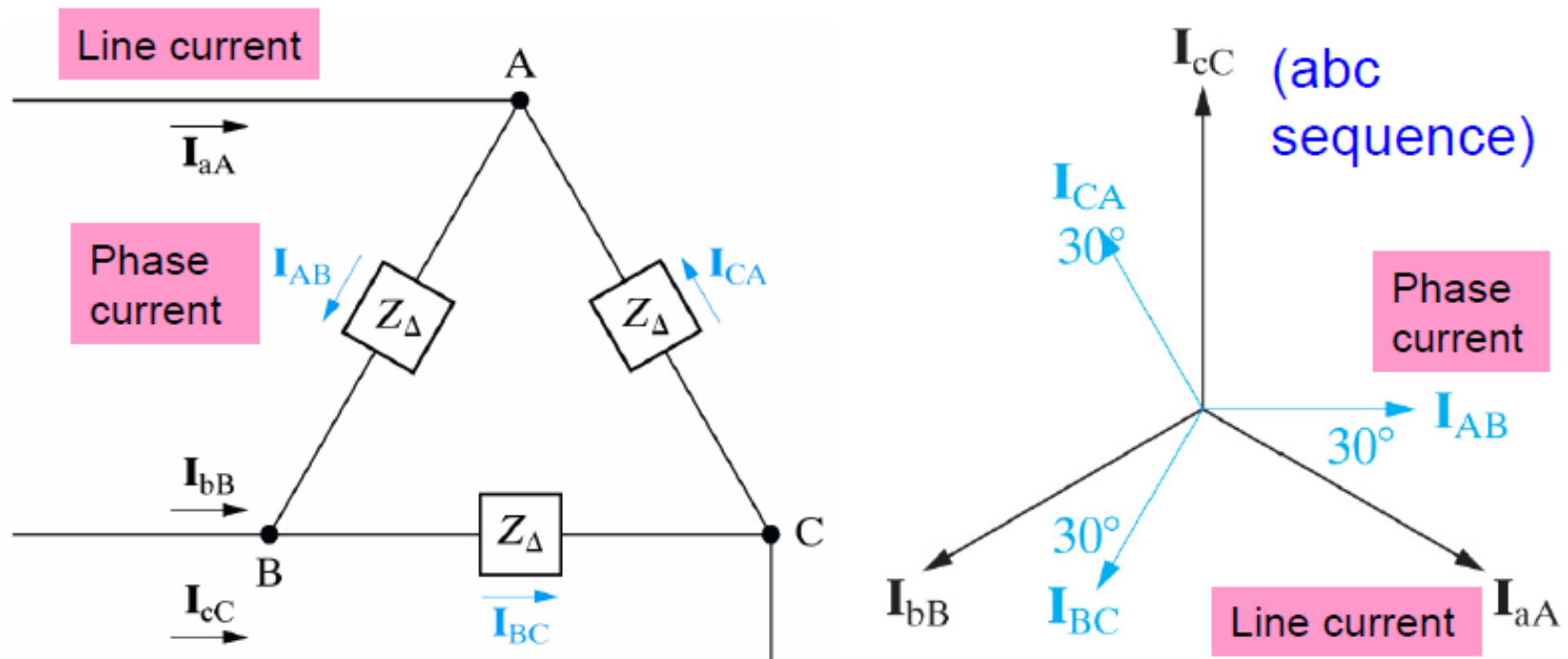
directly giving the line current: 
$$I_{aA} = \frac{V_{a'n}}{Z_{ga} + Z_{ia} + Z_A},$$

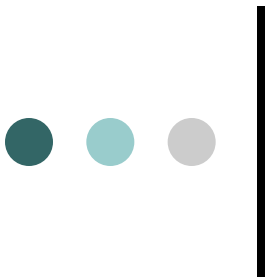
and line-to-neutral voltage: 
$$V_{AN} = I_{aA} Z_A.$$

## The 3 phase currents of the load in abc seq.

- Can be solved by 3 node equations once the 3 line currents  $\mathbf{I}_{aA}$ ,  $\mathbf{I}_{bB}$ ,  $\mathbf{I}_{cC}$  are known:

$$\mathbf{I}_{aA} = \mathbf{I}_{AB} - \mathbf{I}_{CA}, \quad \mathbf{I}_{bB} = \mathbf{I}_{BC} - \mathbf{I}_{AB}, \quad \mathbf{I}_{cC} = \mathbf{I}_{CA} - \mathbf{I}_{BC}.$$





$$I_{AB} = I_{\phi} \angle 0^{\circ}$$

$$I_{BC} = I_{\phi} \angle -120^{\circ}$$

$$I_{CA} = I_{\phi} \angle +120^{\circ}$$

$$I_{aA} = I_{AB} - I_{CA} = \sqrt{3}I_{\phi} \angle -30^{\circ}$$

$$I_{bB} = I_{BC} - I_{AB} = \sqrt{3}I_{\phi} \angle -150^{\circ}$$

$$I_{cC} = I_{CA} - I_{BC} = \sqrt{3}I_{\phi} \angle 90^{\circ}$$

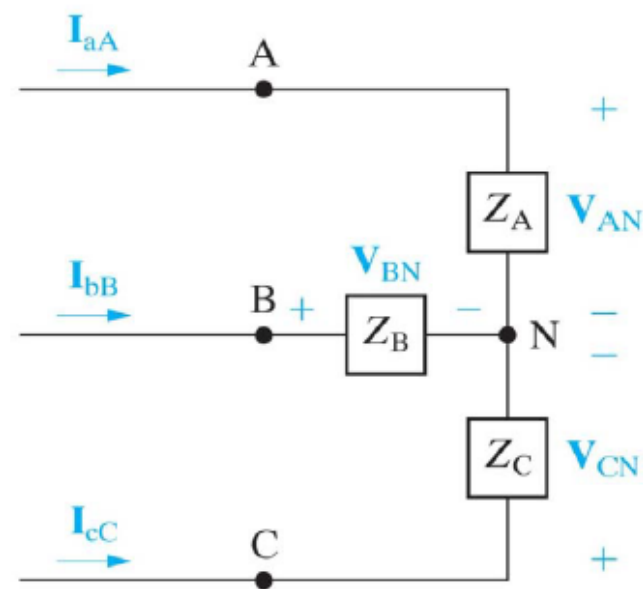
# Power Calculations in Balanced Three-Phase Circuits

## Average power of balanced Y-Load

- The average power delivered to  $Z_A$  is:

$$P_A = V_\phi I_\phi \cos \theta_\phi,$$

$$\begin{cases} V_\phi \equiv |\mathbf{V}_{AN}| = V_L / \sqrt{3}, \\ I_\phi \equiv |\mathbf{I}_{aA}| = I_L, \quad (\text{rms value}) \\ \theta_\phi \equiv \angle V_\phi - \angle I_\phi = \angle Z_A. \end{cases}$$



- The total power delivered to the Y-Load is:

$$P_{tot} = 3P_A = 3V_\phi I_\phi \cos \theta_\phi = \sqrt{3}V_L I_L \cos \theta_\phi.$$



# Power Calculations in Balanced Three-Phase Circuits

## Complex power of a balanced Y-Load

- The **reactive** powers of one phase and the entire Y-Load are:

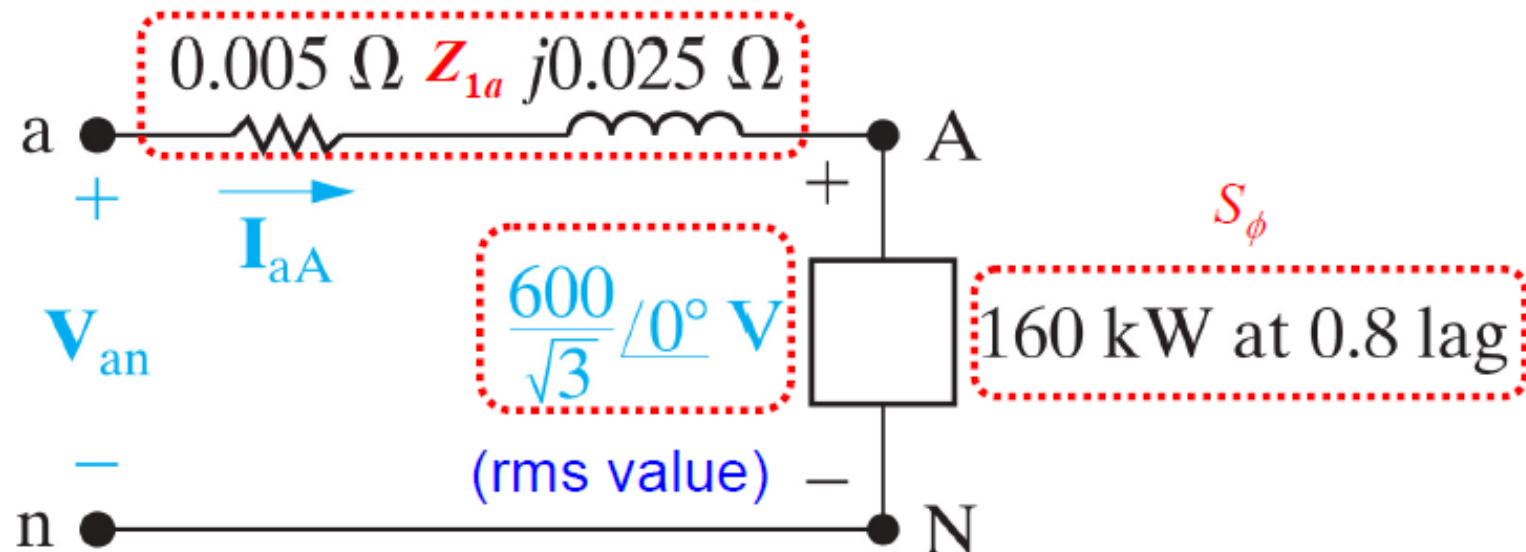
$$\begin{cases} Q_{\phi} = V_{\phi} I_{\phi} \sin \theta_{\phi}, \\ Q_{tot} = 3V_{\phi} I_{\phi} \sin \theta_{\phi} = \sqrt{3} V_L I_L \sin \theta_{\phi}. \end{cases}$$

- The **complex** powers of one phase and the entire Y-Load are:

$$\begin{cases} S_{\phi} = P_{\phi} + jQ_{\phi} = V_{\phi} I_{\phi} e^{j\theta_{\phi}} = \mathbf{V}_{\phi} \mathbf{I}_{\phi}^*; \\ S_{tot} = 3S_{\phi} = 3V_{\phi} I_{\phi} e^{j\theta_{\phi}} = \sqrt{3} V_L I_L e^{j\theta_{\phi}}. \end{cases}$$

## Example 2

- Q: What are the complex powers provided by the source and dissipated by the line of a-phase?
- The equivalent one-phase circuit in Y-Y configuration is:



## Example 2

- The line current of a-phase can be calculated by the complex power is:

$$S_{\phi} = \mathbf{V}_{\phi} \mathbf{I}_{\phi}^*, (160 + j120)10^3 = \frac{600}{\sqrt{3}} \mathbf{I}_{aA}^*, \quad (P/|S| = 0.8; Q = \text{SQRT}(|S|^2 - P^2))$$
$$\Rightarrow \mathbf{I}_{aA} = (577.35 \angle -36.87^{\circ}) \text{ A}.$$

- The a-phase voltage of the source is:

$$\begin{aligned} \mathbf{V}_{an} &= \mathbf{V}_{AN} + \mathbf{I}_{aA} Z_{1a} \\ &= 600/\sqrt{3} + (577.35 \angle -36.87^{\circ})(0.005 + j0.025) \\ &= (357.51 \angle 1.57^{\circ}) \text{ V}. \end{aligned}$$

## Example 2

- The complex power provided by the **source** of a-phase is:

$$\begin{aligned} S_{an} &= \mathbf{V}_{an} \mathbf{I}_{aA}^* = (357.51 \angle 1.57^\circ) (577.35 \angle 36.87^\circ) \\ &= (206.41 \angle 38.44^\circ) \text{ kVA.} \end{aligned}$$

- The complex power dissipated by the **line** of a-phase is:

$$\begin{aligned} S_{aA} &= |\mathbf{I}_{aA}|^2 Z_{1a} = (577.35)^2 (0.005 + j0.025) \\ &= (8.50 \angle 78.66^\circ) \text{ kVA.} \end{aligned}$$