

# Parameterised Modelling of Antenna Beams for Global 21cm Experiments

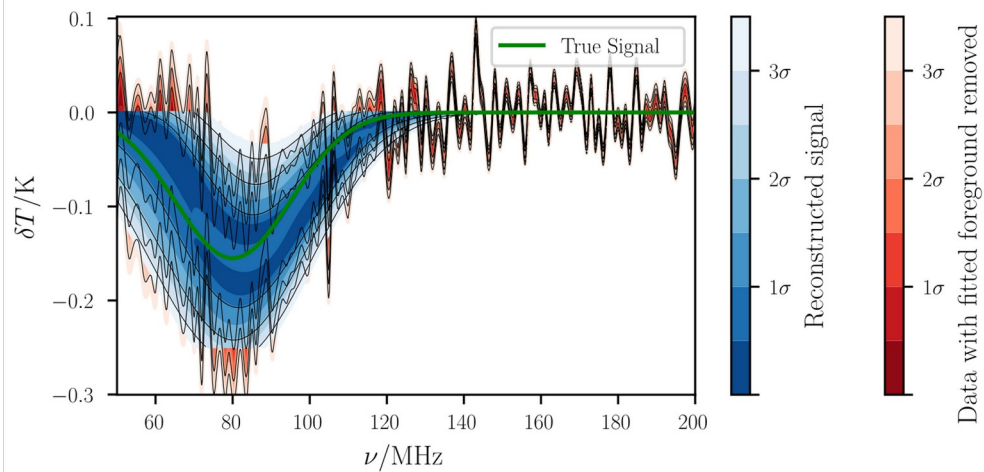
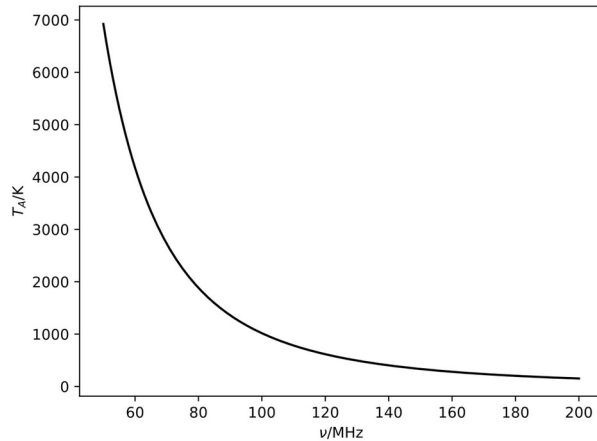
Dominic Anstey | 5<sup>th</sup> Global 21cm Workshop



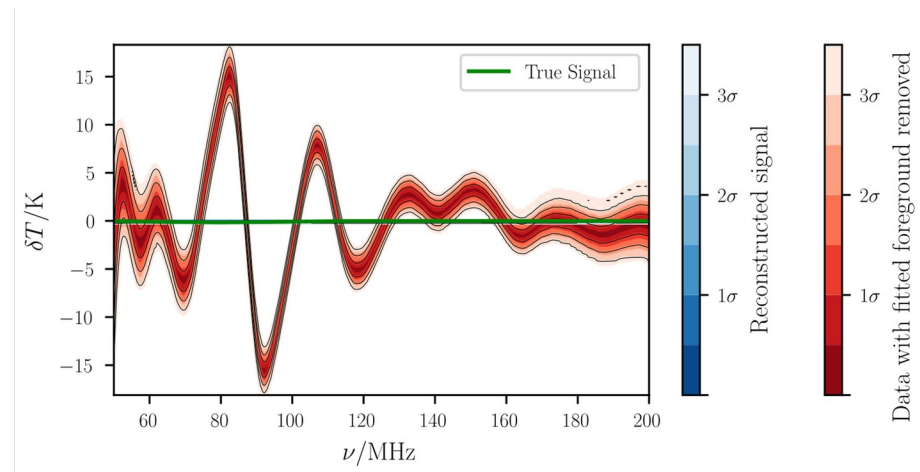
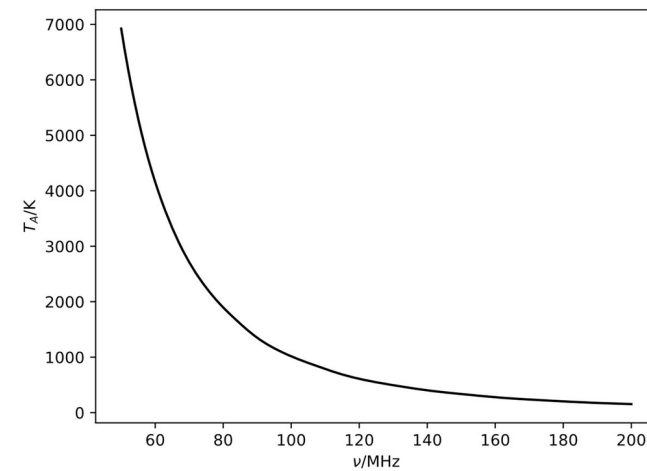
On behalf of the  
REACH collaboration

# The Issue of Chromaticity

Achromatic antenna



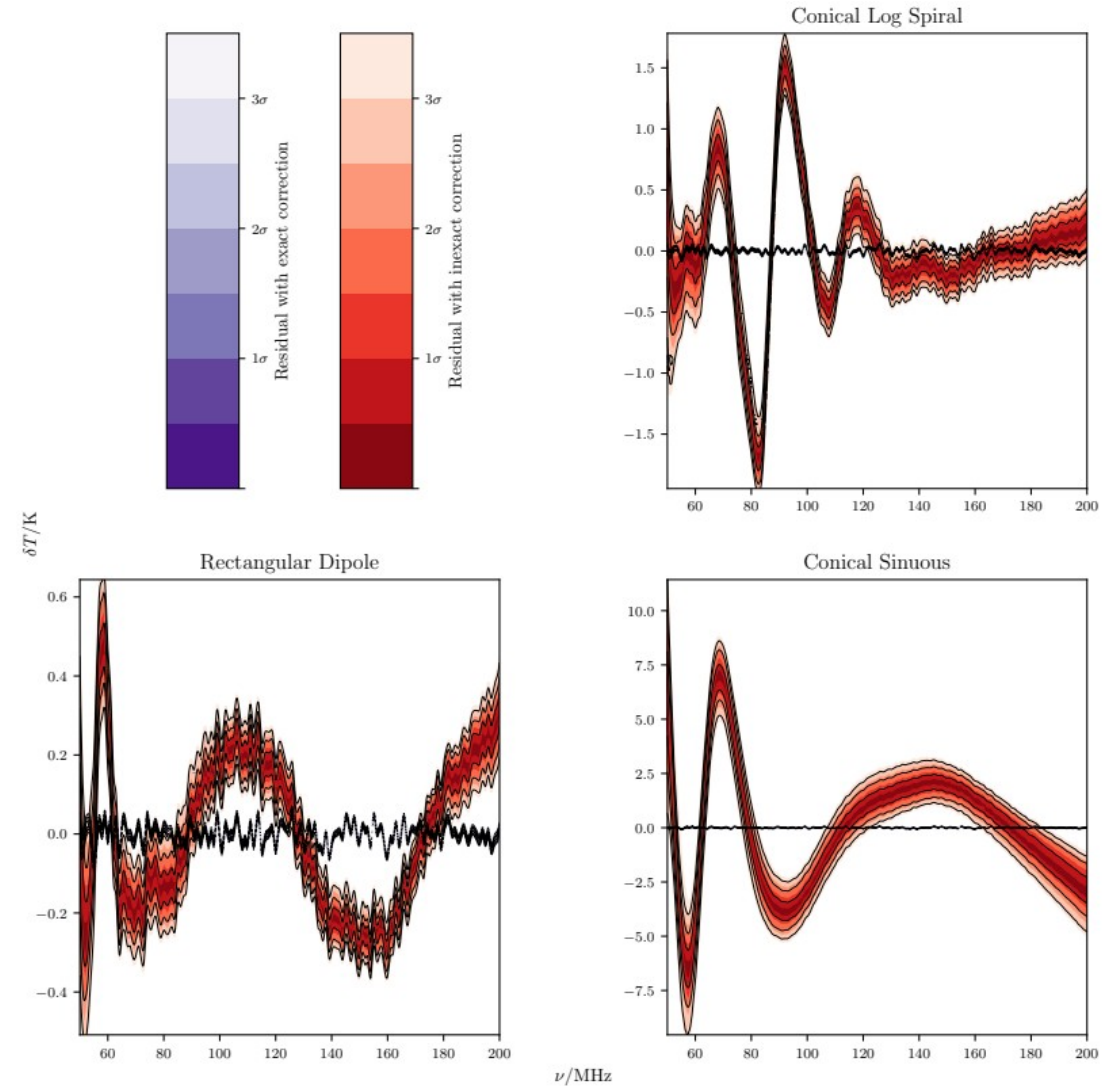
Chromatic antenna



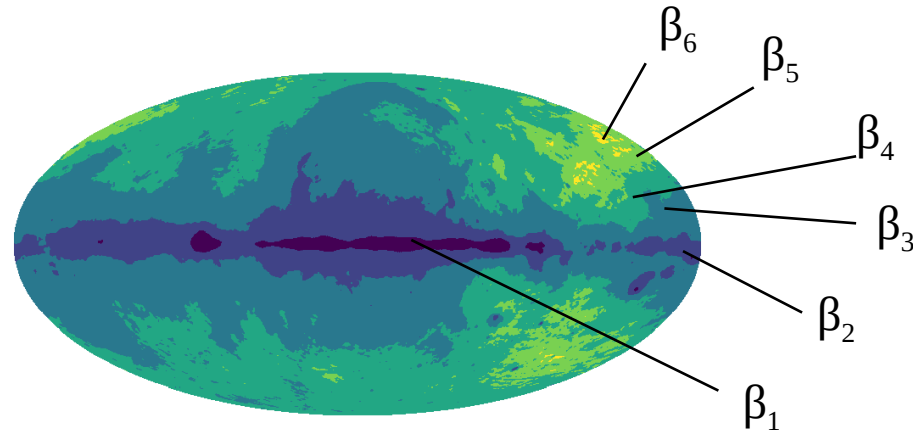
# The Issue of Chromaticity

$$B_{\text{factor}}(\nu, t) = \frac{\int D(\Omega, \nu) T_{\text{sky}}(\Omega, t) d\Omega}{\int D(\Omega, \nu_{\text{ref}}) T_{\text{sky}}(\Omega, t) d\Omega}$$

e.g. Mozdzen et al. (2019)  
Murray et al. (2022)



# Summary of REACH Pipeline



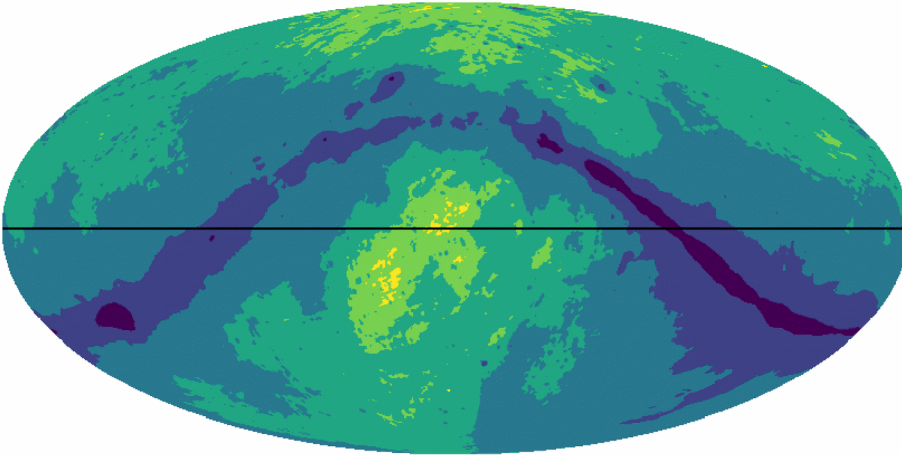
$$T_F(\nu, \theta_F) = \frac{1}{4\pi} \int_0^{4\pi} D(\theta, \phi, \nu) \times \int_{t_{\text{start}}}^{t_{\text{end}}} \sum_{i=1}^N M_i(\theta, \phi) (T_{230}(\theta, \phi) - T_{\text{CMB}}) \left(\frac{\nu}{230}\right)^{-\beta_i} dt d\Omega + T_{\text{CMB}}$$

$$\log \mathcal{L} = \sum_i -\frac{1}{2} \log(2\pi\sigma_n^2) - \frac{1}{2} \left( \frac{T_{\text{data}}(\nu_i) - (T_F(\nu_i, \theta_F) + T_S(\nu_i, \theta_S))}{\sigma_n} \right)^2$$

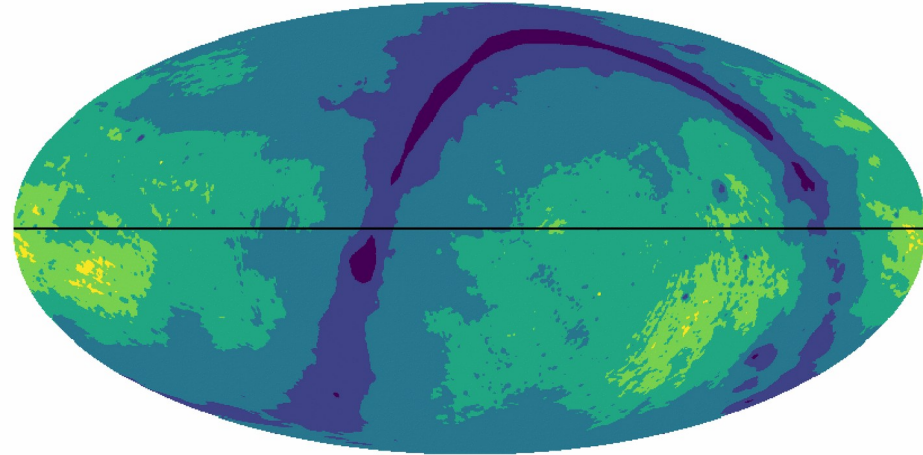
# Time-Separated Fitting

$$\log \mathcal{L} = \sum_i -\frac{1}{2} \log (2\pi\sigma_n^2) - \frac{1}{2} \left( \frac{\frac{1}{n_j} \sum_j [T_{\text{data}}(\nu_i, t_j)] - \left( \frac{1}{n_j} \sum_j [T_{\text{F}}(\nu_i, t_j, \theta_{\text{F}})] + T_{\text{S}}(\nu_i, \theta_{\text{S}}) \right)}{\sigma_n} \right)^2$$

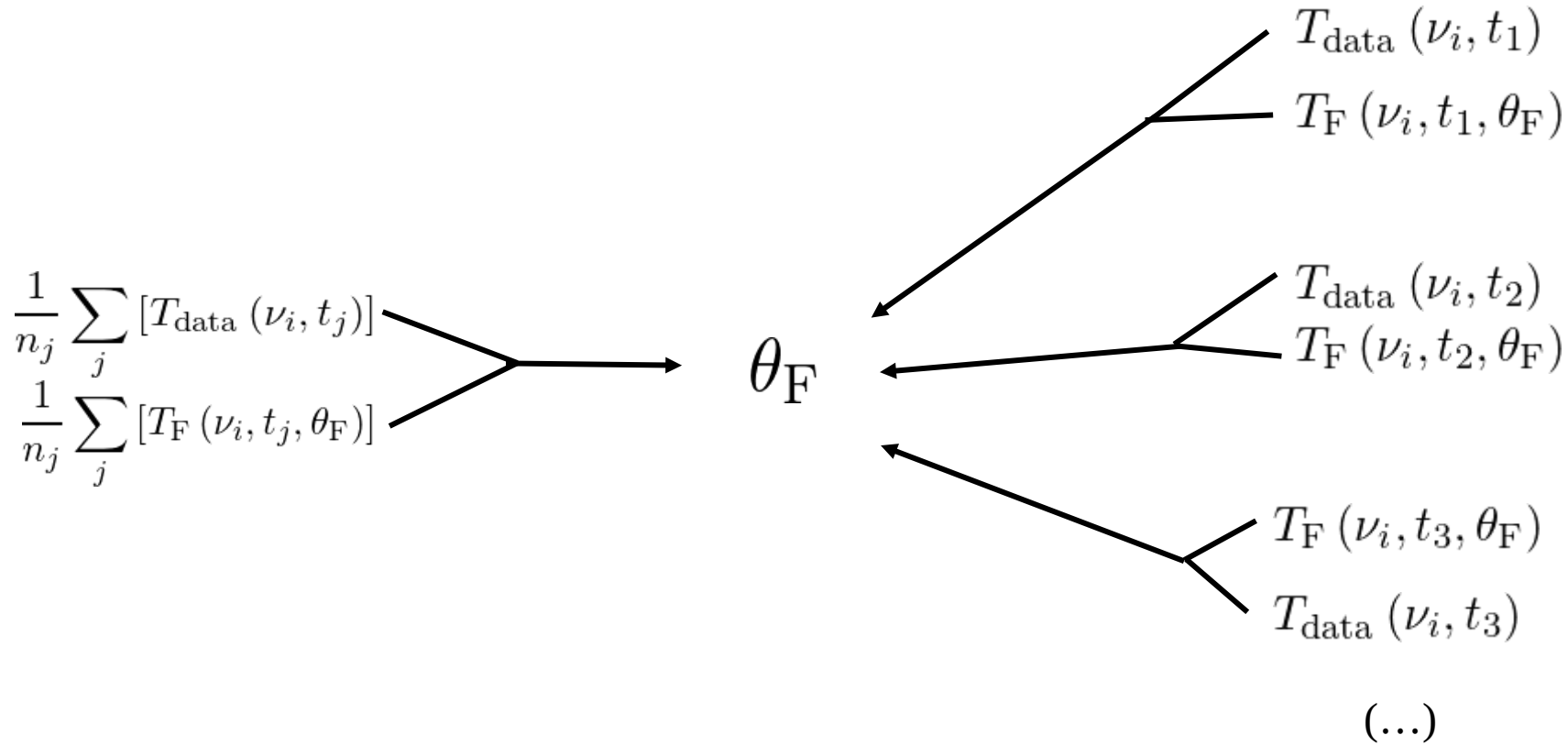
6 Regions LST=0hr



6 Regions LST=12hr



# Time-Separated Fitting



$$\log \mathcal{L} = \sum_i \sum_j -\frac{1}{2} \log (2\pi\sigma_n^2) - \frac{1}{2} \left( \frac{T_{\text{data}}(\nu_i, t_j) - (T_F(\nu_i, t_j, \theta_F) + T_S(\nu_i, \theta_S))}{\sigma_n} \right)^2$$

Anstey et al. (preprint  
arXiv:2210.04707)

# Antenna Beam Modelling

The antenna beam pattern may not be known exactly in practice:

- Soil permittivity
- Horizon effects
- Imperfections in construction
- Uncertainties in EM solver
- Etc.

# Impact of Uncertainties

	Ax	Bx	By	Cx	Cy	Dx	Dy	Ex	gap	h	groundplane_size	R_L	I_x	I_o
Beam A	17.956	78.147	565.57	271.74	454.42	724.74	415.64	894.35	11.208	694.9	14196	29.694	485.65	433.16
Beam B	18	79	566	271	454	725	415	895	11	700	14250	30	486	433
Difference	0.044	0.853	0.43	0.74	0.42	0.26	0.64	0.65	0.208	5.1	54	0.306	0.35	0.16

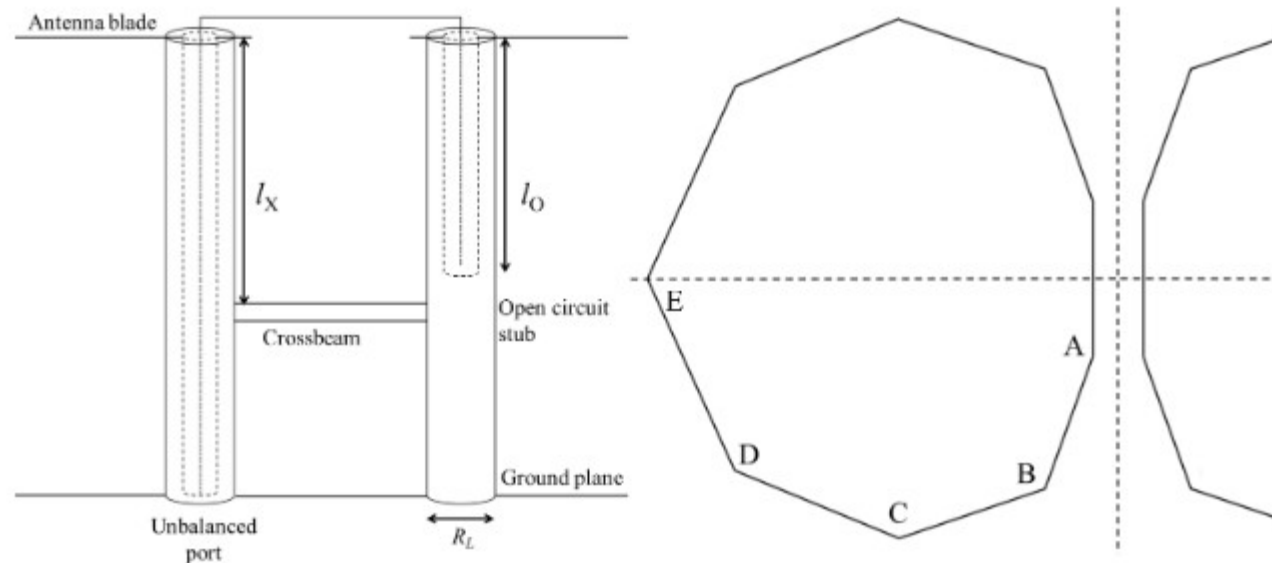
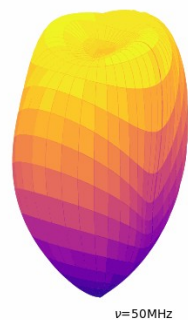


Figure 24 from  
Cumner et al. 2022



# Impact of Uncertainties

Beam A



$\nu = 50\text{MHz}$

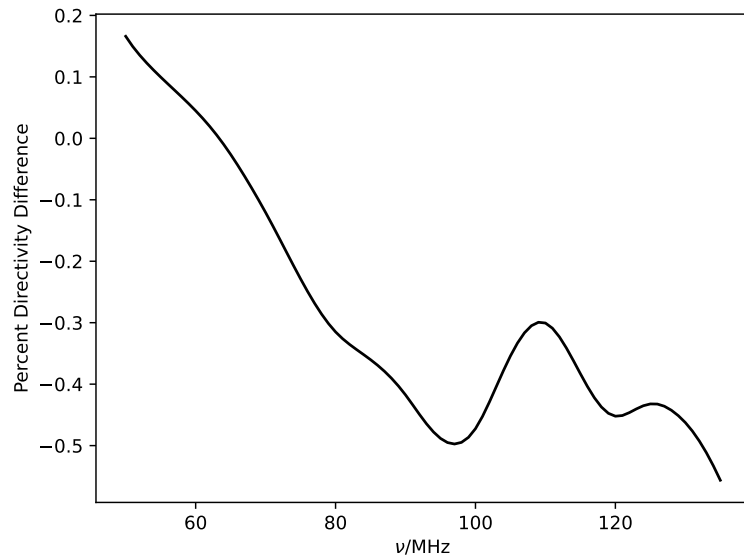
Difference

$\nu = 50\text{MHz}$



Beams simulated by  
John Cumner

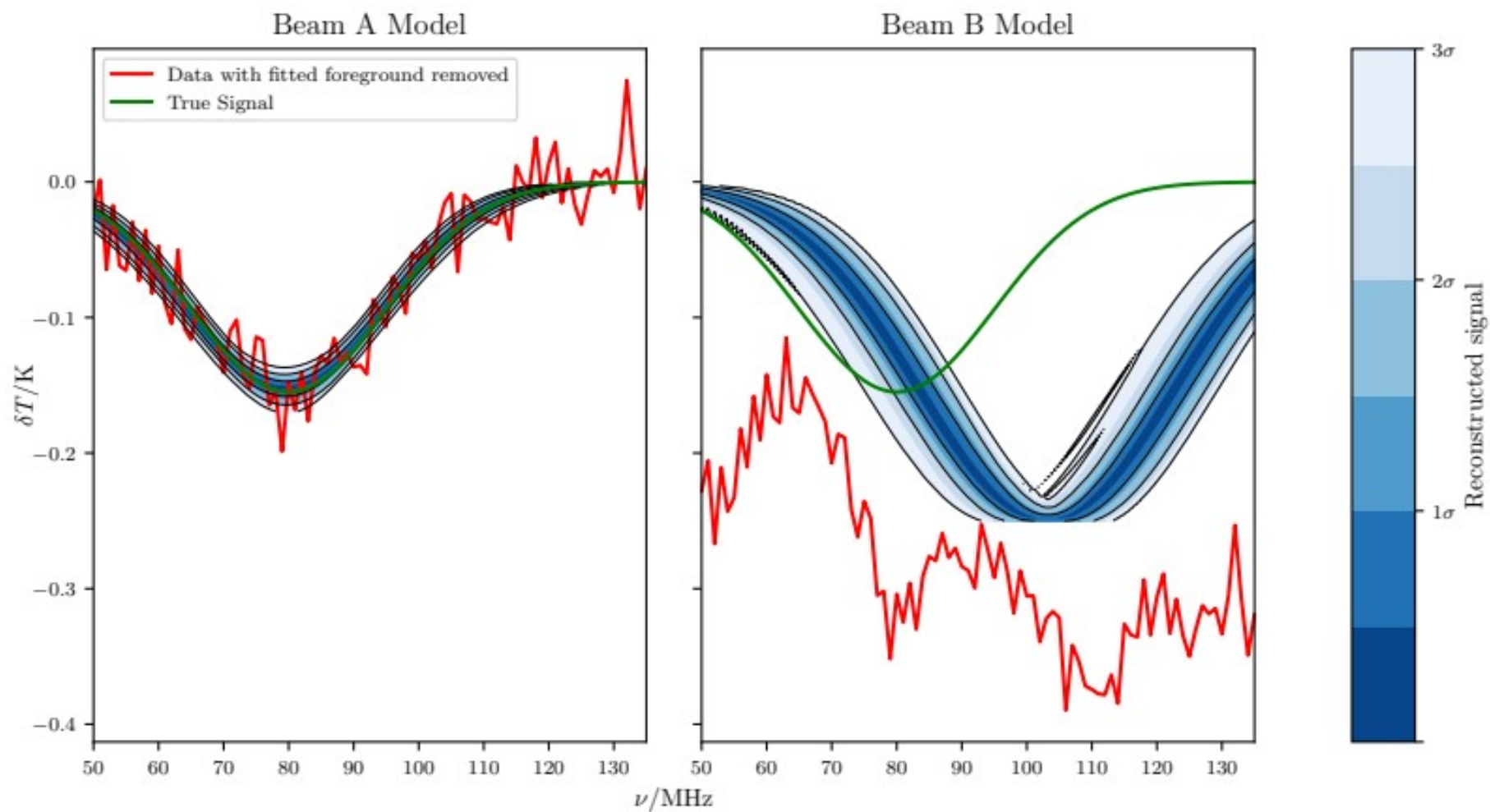
# Impact of Uncertainties



- Generate a simulated data set using Beam A
- Fit for the signal correcting for the chromaticity assuming Beam A
- Fit for the signal correcting for the chromaticity assuming Beam B

Foreground known exactly:  
GSM base map scaled by -2.55  
spectral index

# Impact of Uncertainties



# Antenna Beam Modelling

$$D(\Omega, \nu, \bar{\theta}) = \sum_{j=1}^M \theta_j X_j(\Omega, \nu)$$

$$D(\Omega, \nu, \bar{\theta}) = \sum_{j=1}^M \Gamma(\nu, \bar{\theta}_j) Y_j(\Omega)$$

$$T_F(\nu, \theta_F) = \frac{1}{4\pi} \int_0^{4\pi} D(\theta, \phi, \nu) \times \int_{t_{\text{start}}}^{t_{\text{end}}} \sum_{i=1}^N M_i(\theta, \phi) (T_{230}(\theta, \phi) - T_{\text{CMB}}) \left(\frac{\nu}{230}\right)^{-\beta_i} dt d\Omega + T_{\text{CMB}}$$



$$T_F(\nu, \theta_F, \theta_A) = \frac{1}{4\pi} \int_0^{4\pi} \sum_{j=1}^M \Gamma(\nu, \theta_A) Y_j(\theta, \phi) \times \int_{t_{\text{start}}}^{t_{\text{end}}} \sum_{i=1}^N M_i(\theta, \phi) (T_{230}(\theta, \phi) - T_{\text{CMB}}) \left(\frac{\nu}{230}\right)^{-\beta_i} dt d\Omega + T_{\text{CMB}}$$

# Beam Normalisation

$$T_{\text{F}}(\nu) = \frac{1}{4\pi} \int_0^{4\pi} D(\Omega, \nu) \int_{t_{\text{start}}}^{t_{\text{end}}} (T_{\text{base}}(\Omega) - T_{\text{CMB}}) \left( \frac{\nu}{\nu_{\text{base}}} \right)^{-\beta(\Omega)} dt d\Omega + T_{\text{CMB}}$$

Provided basis functions are all normalised, can use polynomials

0<sup>th</sup> order coefficients of all basis functions sum to 1

$$\sum_{j=1}^M \theta_{j,0} = 1$$

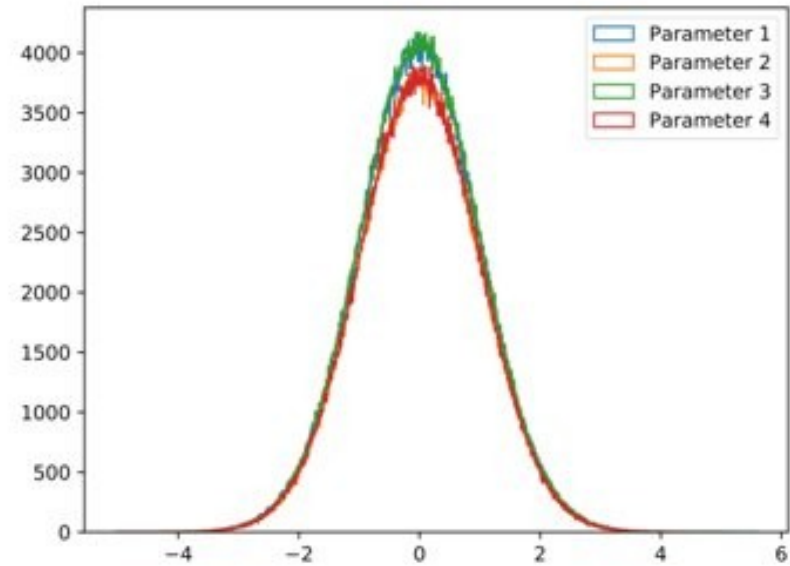
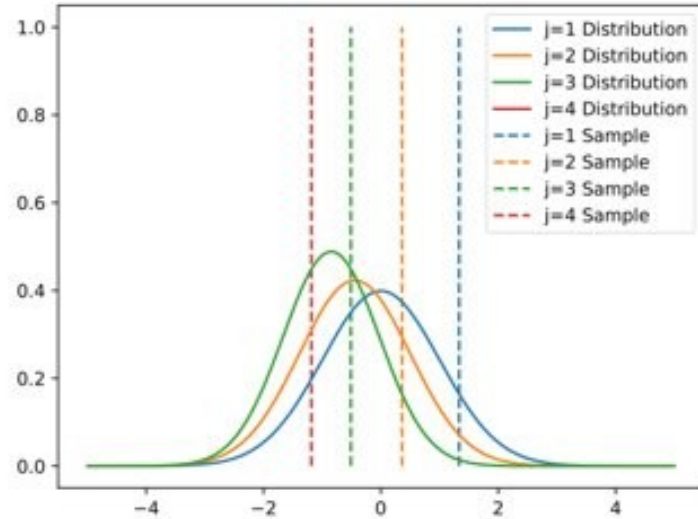
For every other order, coefficients of each basis function must sum to zero

$$\sum_{j=1}^M \theta_{j,k \neq 0} = 0$$

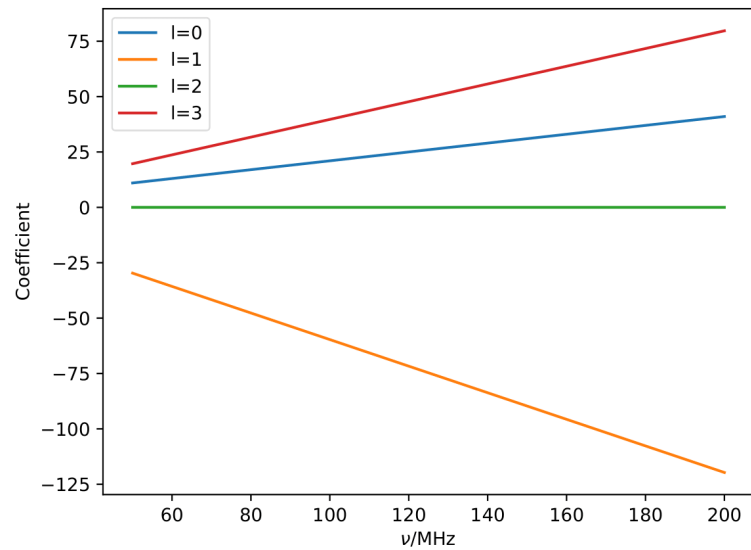
# Beam Normalisation

$$\mu_j = \frac{-\sum_{l=1}^j \theta_l}{N_{\text{basis}} - j + 1}$$

$$\sigma_j = \sigma \sqrt{1 - \frac{j-1}{(M-1)(M-j-1)'}}$$

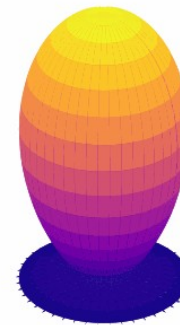


# Example Beam



	$l=0$	$l=1$	$l=2$	$l=3$
$a_0$	1.0	0.3	0.0	-0.3
$a_1$	0.2	-0.6	0.0	0.4

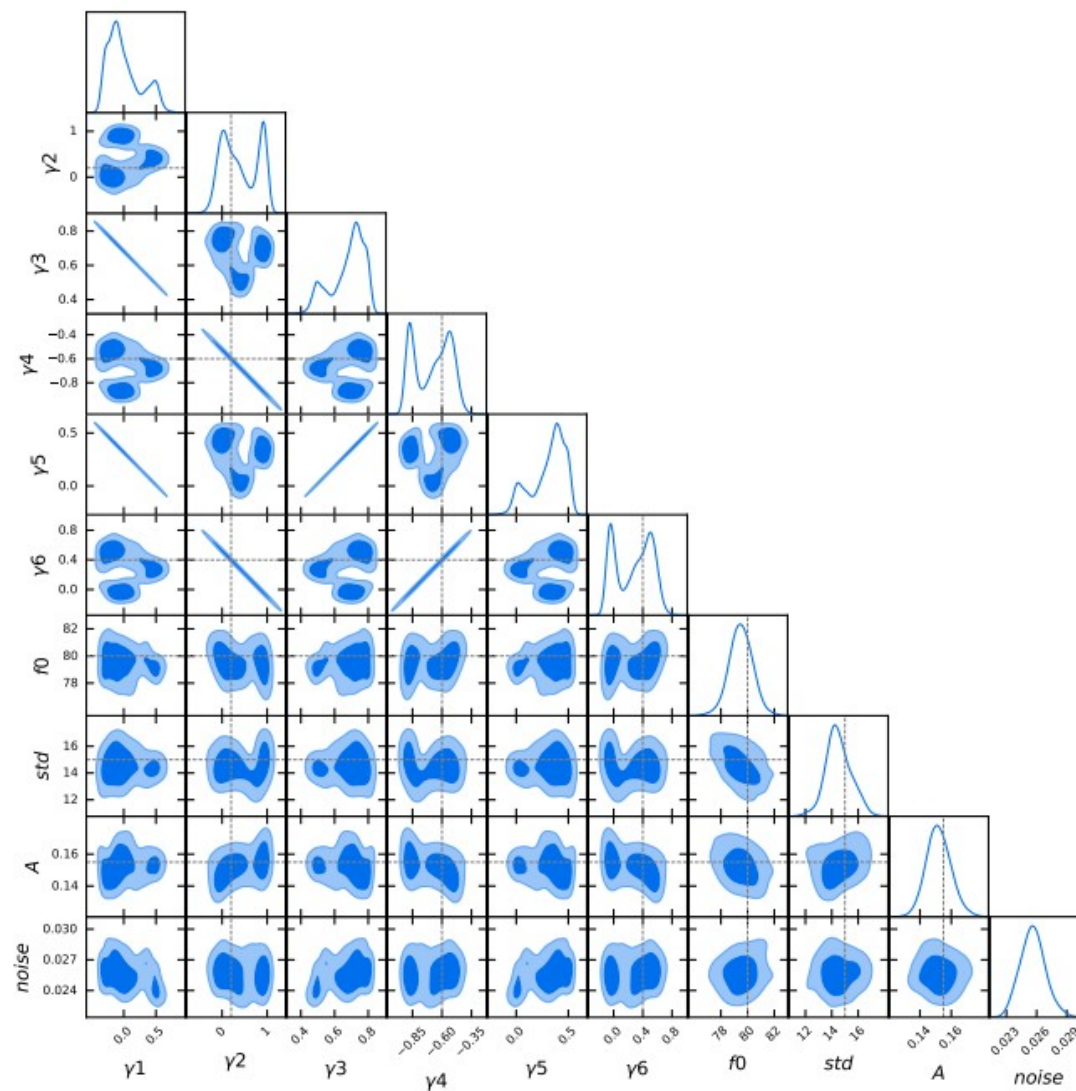
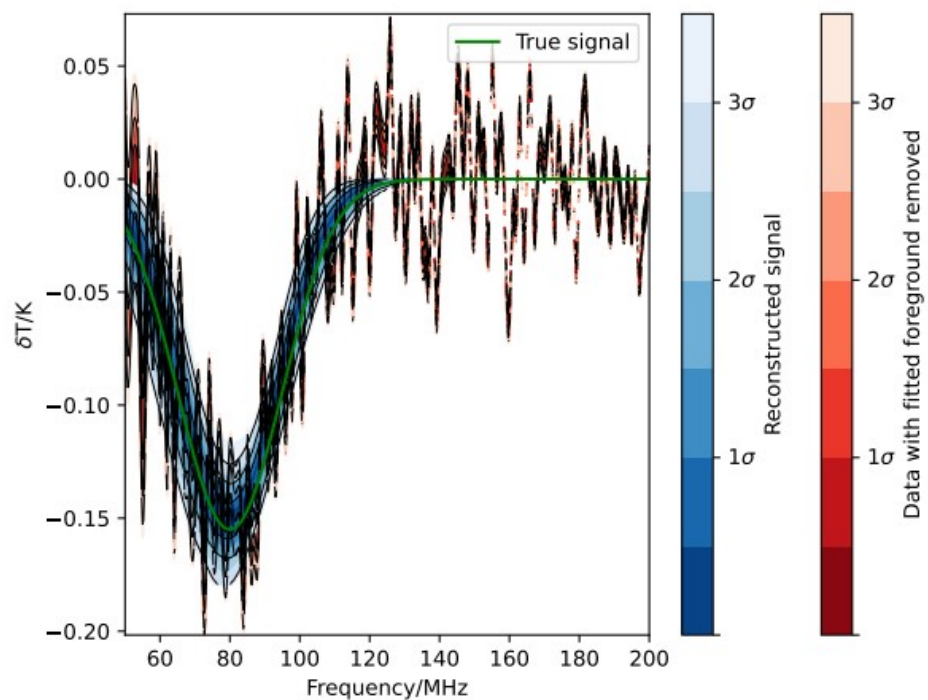
Artificial Beam



$\nu=50\text{MHz}$

# Example Beam Fitting Tests

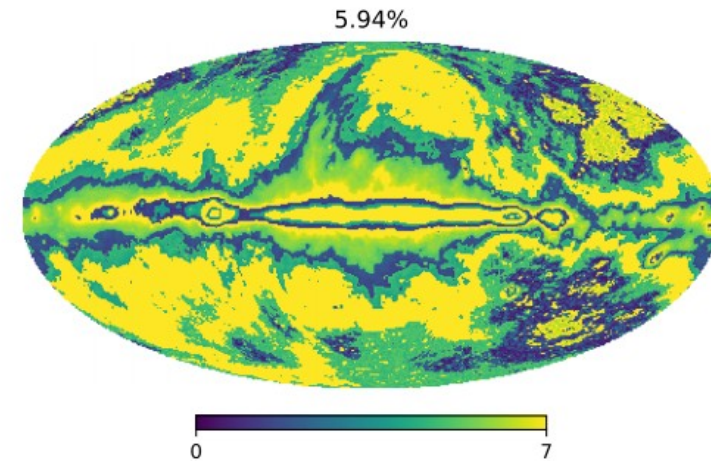
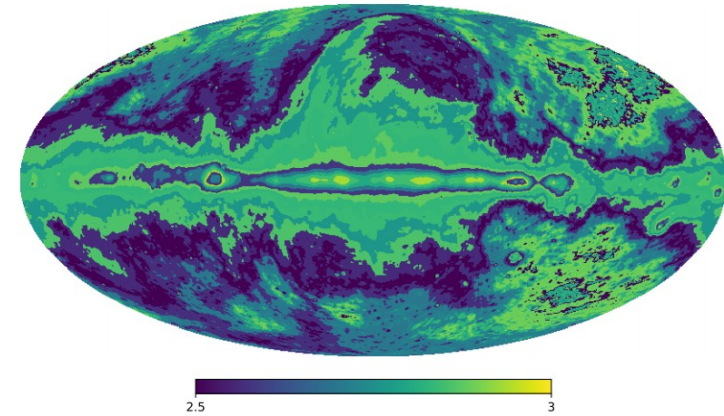
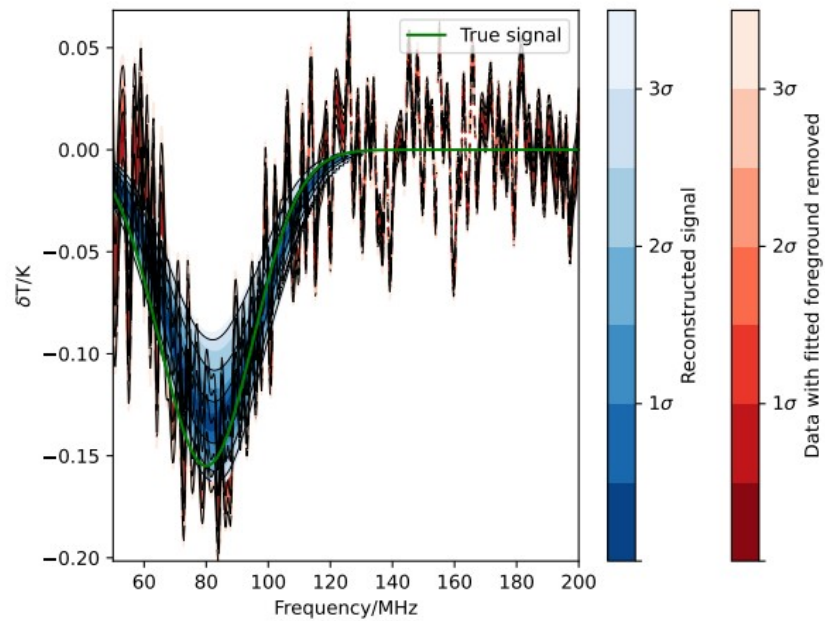
Foreground model fixed





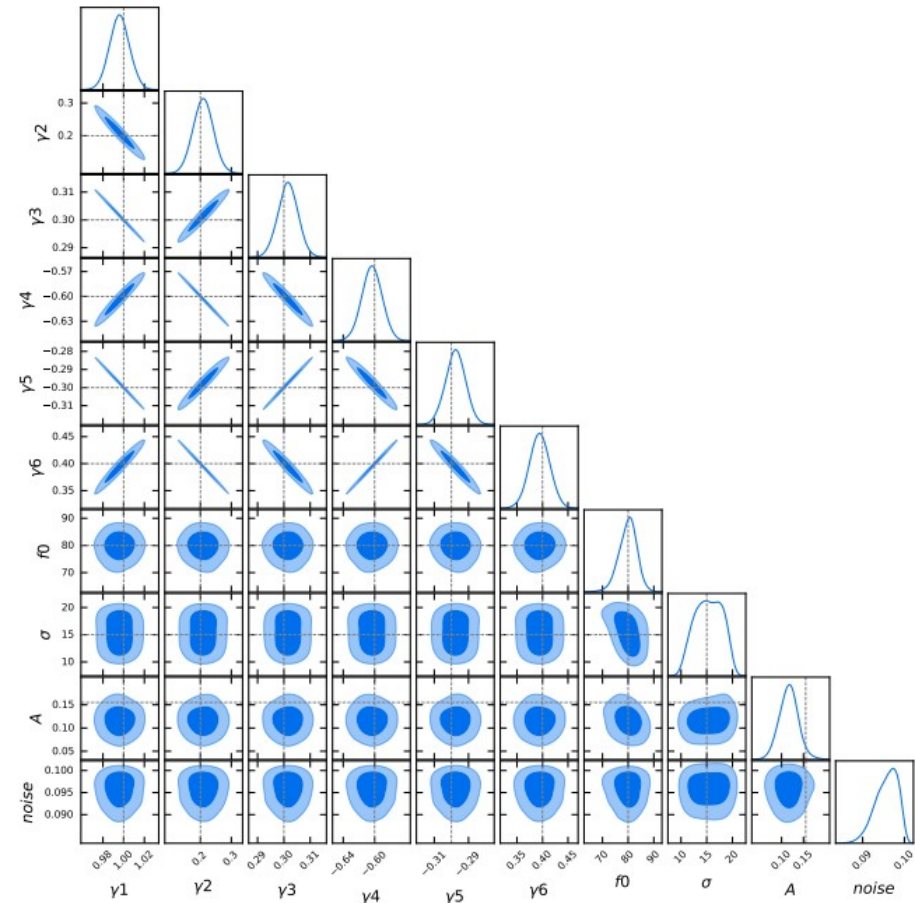
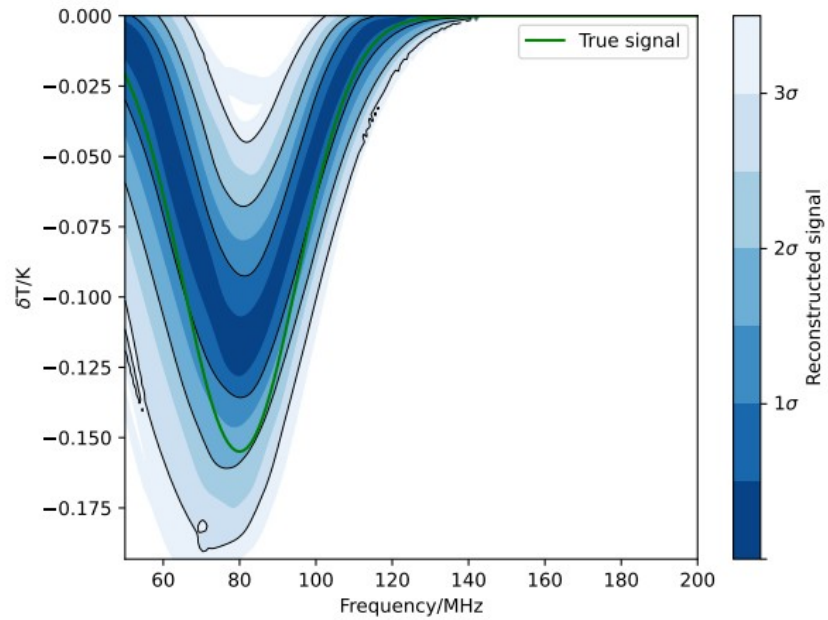
# Example Beam Fitting Tests

Fitting foreground together with antenna



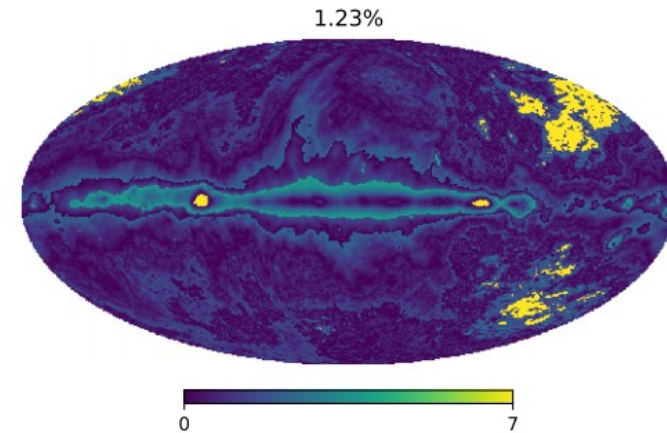
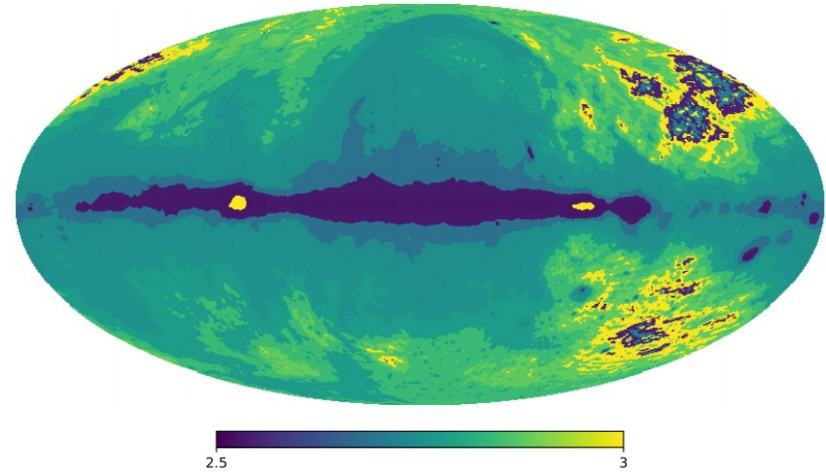
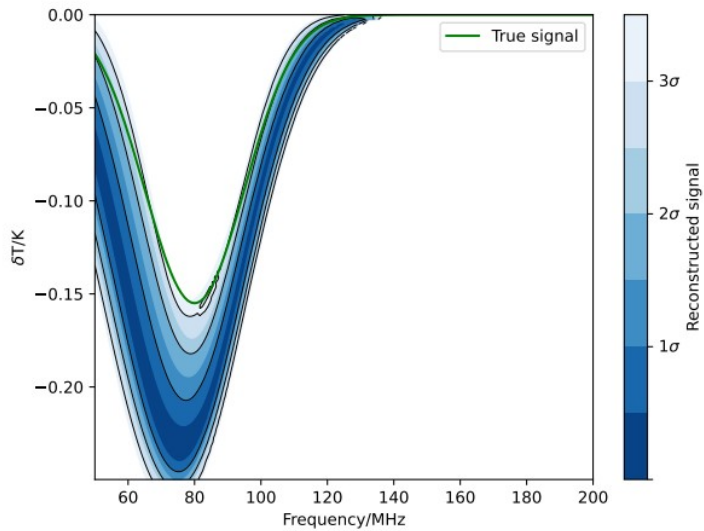
# Example Beam Fitting Tests

Foreground model fixed, 2 time bins



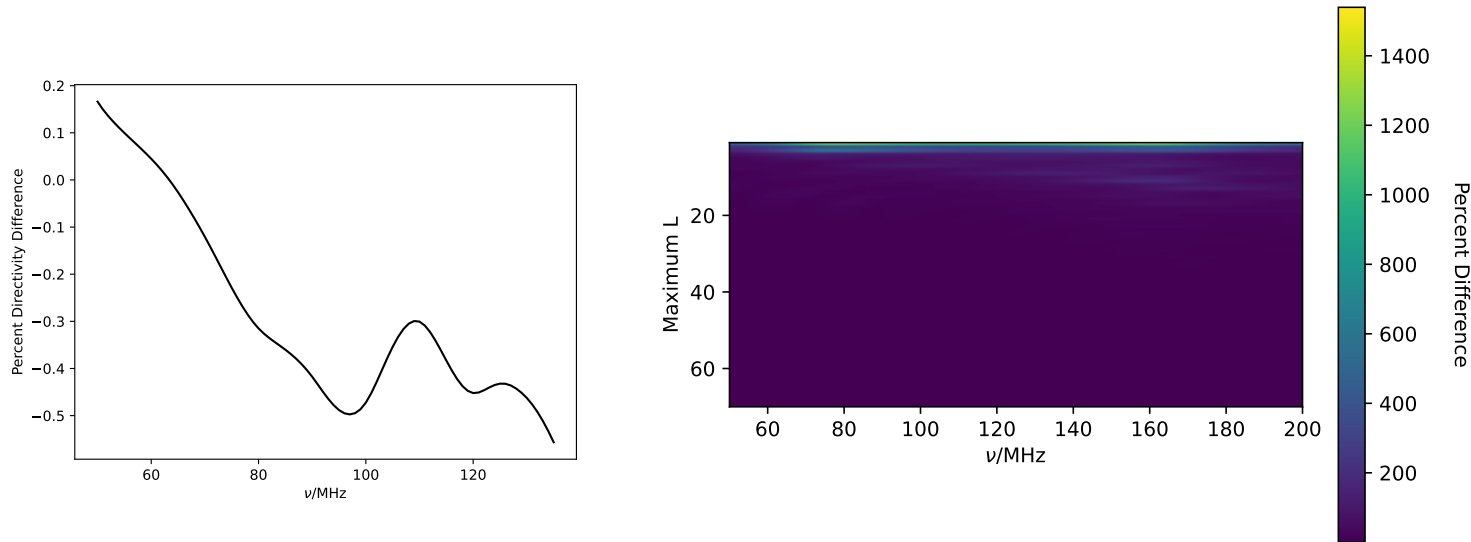
# Example Beam Fitting Tests

Fitting foreground together with antenna, 12 time bins



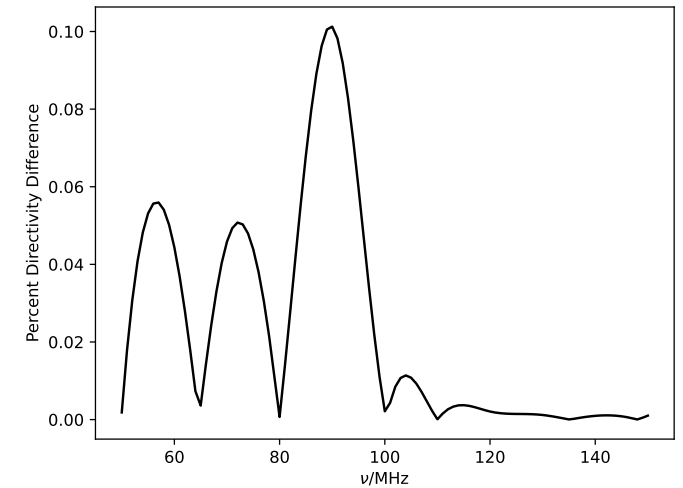
# Parameter Numbers

Spherical Harmonic basis functions



>2556 basis functions

Gram-Schmidt basis functions



21 basis functions

# Next Steps

- **Analytical Marginalisation of Linear Parameters**

e.g Tauscher et al. (2021), Murray et al. (2022)

- **Machine Learning**

# Conclusions

- Summarised current state of REACH pipeline
- Discussed the impact of beam uncertainties
- Showed how antenna beam modelling can be implemented in the REACH pipeline
- Discussed challenges with antenna beam modelling and how they can be addressed, in particular:
  - Beam normalisation
  - Parameter degeneracies