```
clear all
sympref('FloatingPointOutput', false)
```

```
ans = logical
```

# **Table of Contents**

Problem 2	
Part A	1
Part B	3
Problem 3	4
Part A	4
Controllability Gramian	5
Evaluate at the time values and determine wether or not are convergent	5
Which States Are Most Controllable?	8
Observability Gramian	g
Evaluate at the time values and determine wether or not are convergent	
Which States Are Most Observable?	
Part B	13
Three Linear Quadratic Regulators	13
Simulate the Full State Feedback Controllers from	
Plot results	15
Discussion	18
Part C	
Simulate Fuel Optimal Control Law	19
Plot Results	
Discussion	

# **Problem 2**

# Part A

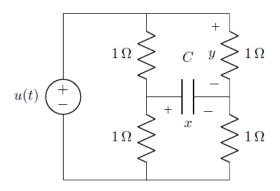


Figure 1: Capacitive bridge.

```
syms i_1 i_2 i_3 u x x_dot y C
%Loop 1 equation
lleqn = i_1 + i_2 == u
```

```
l1eqn = i_1 + i_2 = u
```

12eqn =  $-x + y - i_1 = 0$ 

n2eqn =  $-y + i_3 = C \dot{x}$ 

13eqn =  $x - i_2 + i_3 = 0$ 

eqns = [l1eqn;n1eqn;l2eqn;n2eqn;l3eqn]

eqns =

$$i_{1} + i_{2} = u$$

$$i_{1} - i_{2} = C \dot{x}$$

$$-x + y - i_{1} = 0$$

$$-y + i_{3} = C \dot{x}$$

$$x - i_{2} + i_{3} = 0$$

```
state_eqn = 0 == eliminate(eqns, [i_1 i_2 i_3 y]);
state_eqn = isolate(state_eqn, x_dot)
```

state\_eqn =

$$\dot{x} = -\frac{x}{C}$$

output\_eqn = 0 == eliminate(eqns, [i\_1 i\_2 i\_3 x\_dot])

 $output_eqn = 0 = x - 2y + u$ 

output\_eqn = isolate(output\_eqn, y)

output\_eqn =

$$y = \frac{x}{2} + \frac{u}{2}$$

# Part B

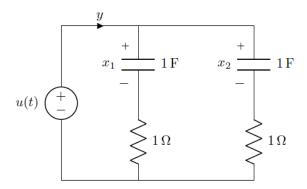


Figure 2: Parallel circuit.

```
syms x_1 x_2 x_dot_1 x_dot_2
%Loop 1 equation
lleqn = x_1 + i_1 - u == 0
```

```
l1eqn = x_1 - u + i_1 = 0
```

```
%Loop 2 equation
12eqn = x_2 + i_2 - u == 0
```

12eqn = 
$$x_2 - u + i_2 = 0$$

```
%Node 1 equation
n1eqn = y == x_dot_1 + x_dot_2
```

n1eqn =  $y = \dot{x}_1 + \dot{x}_2$ 

```
%Node 2 equation
n2eqn = i_1 == x_dot_1
```

n2eqn =  $i_1 = \dot{x}_1$ 

```
%Node 3 equation
n3eqn = i_2 == x_dot_2
```

n3eqn =  $i_2 = \dot{x}_2$ 

```
eqns = [l1eqn;l2eqn;n1eqn;n2eqn;n3eqn]
```

eqns =

```
\begin{bmatrix} x_1 - u + i_1 = 0 \\ x_2 - u + i_2 = 0 \\ y = \dot{x}_1 + \dot{x}_2 \\ i_1 = \dot{x}_1 \\ i_2 = \dot{x}_2 \end{bmatrix}
```

```
solved\_state\_eqns = eliminate(eqns, [i\_1 i\_2 y])
solved\_state\_eqns = [-x_2 - \dot{x}_2 + u, x_1 - x_2 + \dot{x}_1 - \dot{x}_2]
solved\_state\_eqns = [0;0] == [solved\_state\_eqns(1); solved\_state\_eqns(2)];
solved\_state\_eqns = [solved\_state\_eqns(1) - solved\_state\_eqns(2); solved\_state\_eqns(1)];
solved\_state\_eqns = [isolate(solved\_state\_eqns(1), x\_dot\_1); isolate(solved\_state\_eqns(2), x\_dot\_1);
solved\_state\_eqns = [\dot{x}_1 = -x_1 + u]
\dot{x}_2 = -x_2 + u
solved\_output\_eqn = 0 == eliminate(eqns, [i\_1 i\_2 x\_dot\_1 x\_dot\_2]);
solved\_output\_eqn = isolate(solved\_output\_eqn, y)
solved\_output\_eqn = y = -x_1 - x_2 + 2u
```

# **Problem 3**

# Part A

State space model of spring mass system:

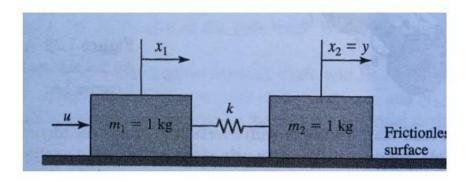


Figure 3: Two-mass-spring system. Assume a frictionless surface. Source: [Za] Fig. 1.31.

Here, the state space model is  $\dot{x} = Ax + Bu$  where  $x = [x_1 \ x_2 \ \dot{x}_1 \ \dot{x}_2]$ 

```
0 0 0 1

-k/m1 k/m1 0 0

k/m2 -k/m2 0 0];

B = [ 0

0

1/m1

0 ];

C = [ 0 1 0 0];

D = 0;

sys = ss(A,B,C,D);
```

# Controllability Gramian $W_c$

$$W_c(t) = \int_0^t e^{A\tau} B B^T e^{A^T \tau} d\tau$$

```
syms Tau t n
```

Symbolic Integrand for  $W_c$ 

```
Wc_integrand = expm(A*Tau)*(B*B.')*expm(A.'*Tau);
```

Symbolically Integrate (too large to display)

```
Wc(t) = int(Wc_integrand, Tau, 0, t);
```

Evaluate  $W_c$  at the time values  $t_1 = 10$ ,  $t_2 = 20$ , and  $t_3 = 100$  and determine wether or not  $W_c(t_1)$ ,  $W_c(t_2)$ ,  $W_c(t_3)$  are convergent.

Via a proof shown in the hand calculations, any real diagonalizable matrix is convergent if and only if all of its eigenvalues are less than 1. The controllability grammians of this system are all real and diagonalizable and are shown to each have at least one eigenvalue greater than 1.

```
t1 = 10;
t2 = 20;
t3 = 100;
Wc1 = double(Wc(t1))
Wc1 = 4 \times 4
   84.1477
            82.7081
                      14.3302
                                10.9210
   82.7081
            83.7694
                      13.9540
                                10.7948
   14.3302
            13.9540
                       4.1031
                                 1.2504
   10.9210
            10.7948
                       1.2504
                                 3.3960
Wc2 = double(Wc(t2))
```

```
Wc2 = 4 \times 4
  672.9142 665.4171 49.9649
                                   50.5351
                       49.4649
  665.4171 662.9182
                                   50.0351
   49.9649
            49.4649
                         7.4974
                                    2.4991
   50.5351 50.0351
                         2.4991
                                    7.5044
Wc3 = double(Wc(t3))
Wc3 = 4 \times 4
10<sup>4</sup> ×
    8.3365
              8.3327
                       0.1249
                                    0.1251
```

#### t1 = 10 sec

t2 = 20 sec

8.3327

0.1249

0.1251

8.3315

0.1251

0.1249

0.1249

0.0037

0.0012

0.1251

0.0012

0.0038

```
% V is the matrix of eigenvectors and D is a diagonal matrix of eigenvalues
[V1, Wc_bar_1] = eig(Wc1);
%Make sure they are ordered from largest to smallest
[eigvals1,ind1] = sort(diag(Wc_bar_1), 'descend');
disp(["Reordered Eigenvalue of Wc1 = " + eigvals1 "Index = " + ind1]);
```

```
"Reordered Eigenvalue of Wc1 = 170.5095" "Index = 4" "Reordered Eigenvalue of Wc1 = 2.458196" "Index = 3" "Reordered Eigenvalue of Wc1 = 1.456741" "Index = 2" "Reordered Eigenvalue of Wc1 = 0.9917897" "Index = 1"
```

```
Wc_bar_s1 = Wc_bar_1(ind1,ind1)
```

Since the matrix  $\overline{W}_{c_1}$ , which is in the eigenbasis of  $W_{c_1}$ , has at least one eigenvalue greater than 1,

 $\lim_{n \to \infty} W_{c_1}^{\ \ n} \neq \widetilde{0}$  . I.e.  $W_{c_1}$  does not converge (see hand calculations for proof).

```
%Reordered Eigenvectors
Vs1 = V1(:,ind1)
Vs1 = 4 \times 4
   0.7000
             0.0540
                     -0.4444
                              -0.5565
   0.6981
            -0.0605
                     0.5900
                                0.4011
   0.1195
            0.6300
                     -0.4824
                                0.5967
   0.0917
           -0.7723
                    -0.4708
                                0.4164
```

```
% V is the matrix of eigenvectors and D is a diagonal matrix of eigenvalues
[V2, Wc_bar_2] = eig(Wc2);
%Make sure they are ordered from largest to smallest
[eigvals2,ind2] = sort(diag(Wc_bar_2), 'descend');
disp(["Reordered Eigenvalue of Wc2 = " + eigvals2 "Index = " + ind2]);
```

```
"Reordered Eigenvalue of Wc2 = 1340.8664" "Index = 4" "Reordered Eigenvalue of Wc2 = 5.0021324" "Index = 3" "Reordered Eigenvalue of Wc2 = 2.6068916" "Index = 2" "Reordered Eigenvalue of Wc2 = 2.3587624" "Index = 1"
```

```
Wc_bar_s2 = Wc_bar_2(ind2,ind2)
```

Since the matrix  $\overline{W}_{c_2}$ , which is in the eigenbasis of  $W_{c_2}$ , has at least one eigenvalue greater than 1,

 $\lim_{n \to \infty} W_{c_2}^{\quad n} \neq \widetilde{0}$  . I.e.  $W_{c_2}$  does not converge (see hand calculations for proof).

```
%Reordered Eigenvectors
Vs2 = V2(:,ind2)
Vs2 = 4×4
```

```
0.7078 -0.0006 0.4551 0.5403
0.7025 0.0017 -0.5345 -0.4699
0.0527 -0.7181 0.4948 -0.4866
0.0533 0.6959 0.5122 -0.5005
```

#### t3 = 100 sec

```
% V is the matrix of eigenvectors and D is a diagonal matrix of eigenvalues
[V3, Wc_bar_3] = eig(Wc3);
%Make sure they are ordered from largest to smallest
[eigvals3,ind3] = sort(diag(Wc_bar_3), 'descend');
disp(["Reordered Eigenvalue of Wc3 = " + eigvals3 "Index = " + ind3]);
```

```
"Reordered Eigenvalue of Wc3 = 166704.1732" "Index = 4"

"Reordered Eigenvalue of Wc3 = 25.00875972" "Index = 3"

"Reordered Eigenvalue of Wc3 = 12.61979239" "Index = 2"

"Reordered Eigenvalue of Wc3 = 12.36925083" "Index = 1"
```

# Wc\_bar\_s3 = Wc\_bar\_3(ind3,ind3)

Since the matrix  $\overline{W}_{c_3}$ , which is in the eigenbasis of  $W_{c_3}$ , has at least one eigenvalue greater than 1,

 $\lim_{n\to\infty}W_{c_3}{}^n\neq\widetilde{0}$  . I.e.  $W_{c_3}$  does not converge (see hand calculations for proof).

```
%Reordered Eigenvectors
Vs3 = V3(:,ind3)
```

```
Vs3 = 4 \times 4
   0.7071
              0.0000
                        0.4870
                                 -0.5126
   0.7069
            -0.0000
                       -0.5023
                                   0.4979
   0.0106
              0.7080
                         0.5045
                                   0.4940
   0.0106
             -0.7062
                         0.5059
                                   0.4952
```

#### Which States Are Most Controllable?

The degree of controllability of any state in this system is determined, roughly, by how much of the eigenvector associated with the dominant eigenvalue lies in the direction of that state. Since for each of these controllibility Gramian matrices, there is one eigenvalue that is orders of magnitude larger than the others, this is a good criteria.

For  $t_1 = 10s$ , the dominant eigenvector is:

```
Vs1(:,1)

ans = 4×1
0.7000
0.6981
0.1195
0.0917
```

Which has the associated eigenvalue:

```
disp(eigvals1(1))
170.5095
```

The eigenvalue points largely in the directions of  $x_1$  and  $x_2$ , but is slightly more in  $x_1$  than it is in  $x_2$ . These states are the most controllable.

For  $t_2 = 20s$ , the dominant eigenvector is:

```
Vs2(:,1)

ans = 4×1
0.7078
0.7025
0.0527
0.0533
```

Which has the associated eigenvalue:

```
disp(eigvals2(1))
1.3409e+03
```

The eigenvalue points largely in the directions of  $x_1$  and  $x_2$ , but is slightly more in  $x_1$  than it is in  $x_2$ . These states are the most controllable.

For  $t_3 = 100s$ , the dominant eigenvector is:

```
Vs3(:,1)

ans = 4×1
0.7071
0.7069
0.0106
0.0106
```

Which has the associated eigenvalue:

```
disp(eigvals3(1))
```

1.6670e+05

The eigenvalue points largely in the directions of  $x_1$  and  $x_2$ , but is slightly more in  $x_1$  than it is in  $x_2$ . These states are the most controllable.

The clear trend is that the position states tend to be much more controllable than the velocity states and  $x_1$ , where the input most directly affects the mass, is slightly more controllable than  $x_2$ .

Observability Gramian  $W_o$ 

$$W_o(t) = \int_0^t e^{A^T \tau} C^T C e^{A\tau} d\tau$$

Symbolic Integrand for  $W_o$ 

```
Wo_integrand = expm(A'*Tau)*(C'*C)*expm(A*Tau);
```

Symbolically Integrate (too large to display)

```
Wo(t) = int(Wo_integrand, Tau, 0, t);
```

Evaluate  $W_o$  at the time values  $t_1 = 10$ ,  $t_2 = 20$ , and  $t_3 = 100$  and determine wether or not  $W_o(t_1)$ ,  $W_o(t_2)$ ,  $W_o(t_3)$  are convergent.

Via a proof shown in the hand calculations, any real diagonalizable matrix is convergent if and only if all of its eigenvalues are less than 1. The observability grammians of this system are all real and diagonalizable and are shown to each have at least one eigenvalue greater than 1.

```
Wo1 = double(Wo(t1))

Wo1 = 4×4
3.3960 1.2504 10.7948 10.9210
```

```
1.2504 4.1031 13.9540
                           14.3302
  10.7948 13.9540 83.7694
                           82.7081
  10.9210
           14.3302 82.7081
                           84.1477
Wo2 = double(Wo(t2))
Wo2 = 4\times4
          2.4991 50.0351
   7.5044
                           50.5351
   2.4991 7.4974 49.4649 49.9649
  50.0351 49.4649 662.9182 665.4171
  50.5351 49.9649 665.4171 672.9142
Wo3 = double(Wo(t3))
Wo3 = 4\times4
10<sup>4</sup> ×
   0.0038
          0.0012 0.1251
                             0.1251
   0.0012 0.0037 0.1249
                             0.1249
   0.1251 0.1249 8.3315
                             8.3327
   0.1251 0.1249 8.3327
                              8.3365
```

#### t1 = 10 sec

```
"Reordered Eigenvalue of Wo1 = 0.9917897" "Index = 1"
Wo_bar_s1 = Wo_bar_1(ind1,ind1)
```

```
Wo_bar_s1 = 4\times4

170.5095 0 0 0

0 2.4582 0 0

0 0 1.4567 0

0 0 0.9918
```

Since the matrix  $\bar{W}_{o_1}$ , which is in the eigenbasis of  $W_{o_1}$ , has at least one eigenvalue greater than 1,

 $\lim_{n\to\infty}W_{o_1}^n\neq\widetilde{0}$  . I.e.  $W_{o_1}$  does not converge (see hand calculations for proof).

#### t2 = 20 sec

% V is the matrix of eigenvectors and D is a diagonal matrix of eigenvalues

```
[V2, Wo_bar_2] = eig(Wo2);
%Make sure they are ordered from largest to smallest
[eigvals2,ind2] = sort(diag(Wo_bar_2), 'descend');
disp(["Reordered Eigenvalue of Wo2 = " + eigvals2 "Index = " + ind2]);
   "Reordered Eigenvalue of Wo2 = 1340.8664"
                                            "Index = 4"
                                            "Index = 3"
   "Reordered Eigenvalue of Wo2 = 5.0021324"
                                            "Index = 2"
   "Reordered Eigenvalue of Wo2 = 2.6068916"
                                            "Index = 1"
   "Reordered Eigenvalue of Wo2 = 2.3587624"
Wo_bar_s2 = Wo_bar_2(ind2,ind2)
Wo_bar_s2 = 4 \times 4
10<sup>3</sup> ×
      109 0 0
0 0.0050 0
   1.3409
                                   0
                                   0
       0 0.0026
```

Since the matrix  $\overline{W}_{o_2}$ , which is in the eigenbasis of  $W_{o_2}$ , has at least one eigenvalue greater than 1,

 $\lim_{n\to\infty}W_{o_2}^{n}\neq\widetilde{0}$  . I.e.  $W_{o_2}$  does not converge (see hand calculations for proof).

#### t3 = 100 sec

```
Wo_bar_s3 = 4×4

10<sup>5</sup> ×

1.6670 0 0 0

0 0.0003 0 0

0 0 0.0001 0

0 0 0 0.0001
```

Since the matrix  $\overline{W}_{o_3}$ , which is in the eigenbasis of  $W_{o_3}$ , has at least one eigenvalue greater than 1,

 $\lim_{n\to\infty}W_{o_3}^{\quad n}\neq\widetilde{0}$  . I.e.  $W_{o_3}$  does not converge (see hand calculations for proof).

#### Which States Are Most Observable?

The degree of observability of any state in this system is determined, roughly, by how much of the eigenvector associated with the dominant eigenvalue lies in the direction of that state. Since for each of these observability Gramian matrices, there is one eigenvalue that is orders of magnitude larger than the others, this is a good criteria.

For  $t_1 = 10s$ , the dominant eigenvector is:

```
Vs1(:,1)

ans = 4×1
0.0917
0.1195
0.6981
0.7000
```

Which has the associated eigenvalue:

```
disp(eigvals1(1))
170.5095
```

The eigenvalue points largely in the directions of  $\dot{x}_1$  and  $\dot{x}_2$ , but is slightly more in  $\dot{x}_2$  than it is in  $\dot{x}_1$ . These states are the most observable.

For  $t_2 = 20s$ , the dominant eigenvector is:

```
Vs2(:,1)

ans = 4×1
0.0533
0.0527
0.7025
0.7078
```

Which has the associated eigenvalue:

```
disp(eigvals2(1))
1.3409e+03
```

The eigenvalue points largely in the directions of  $\dot{x}_1$  and  $\dot{x}_2$ , but is slightly more in  $\dot{x}_2$  than it is in  $\dot{x}_1$ . These states are the most observable.

For  $t_3 = 100s$ , the dominant eigenvector is:

```
Vs3(:,1)

ans = 4×1
    0.0106
    0.7069
    0.7071
```

Which has the associated eigenvalue:

```
disp(eigvals3(1))
```

1.6670e+05

The eigenvalue points largely in the directions of  $\dot{x}_1$  and  $\dot{x}_2$ , but is slightly more in  $\dot{x}_2$  than it is in  $\dot{x}_1$ . These states are the most observable.

The clear trend is that the velocity states tend to be much more observable than the position states and  $\dot{x}_2$ , is slightly more observable than  $\dot{x}_1$ .

### Part B

# **Three Linear Quadratic Regulators**

Linear quadratic regulators are used to choose stabilizing k matrices for full state feedback. Bryson's rule for various values of the maximum acceptable state and input are utilized to get three different K matrices.

```
%Bryson's rule for xmax = 3 meters, x_dot_max = 10 m/s, and Umax = 2 newtons - because why %not?

Q1 = [1/3 0 0 0; 0 1/3 0 0; 0 0 1/10 0; 0 0 0 1/10];

R1 = 1/2;

[K1,S1,e1] = lqr(A,B,Q1,R1);

K1

K1 = 1×4

1.1488 0.0059 1.5804 0.9373
```

```
%Bryson's rule for xmax = 1 meters, x_dot_max = 15 m/s, and Umax = 20 newtons
Q2 = [1/1 0 0 0; 0 1/1 0 0; 0 0 1/15 0; 0 0 0 1/15];
R2 = 1/20;
[K2,S2,e2] = lqr(A,B,Q2,R2);
K2
```

```
K2 = 1×4
6.4807 -0.1562 3.7809 4.5822
```

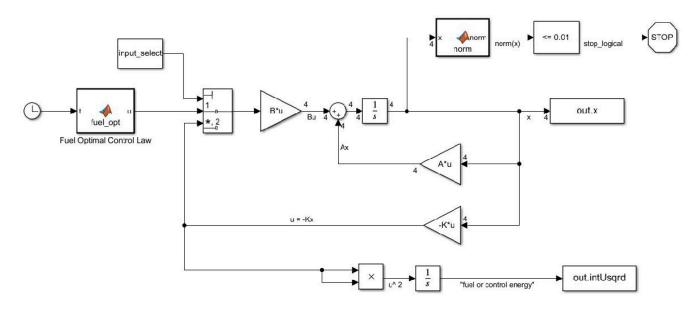
```
%Bryson's rule for xmax = .05 meters, x_dot_max = 2 m/s, and Umax = 3 newtons
Q3 = [1/.05 0 0 0; 0 1/.05 0 0; 0 0 1/2 0; 0 0 0 1/2];
R3 = 1/3;
[K3,S3,e3] = lqr(A,B,Q3,R3);
K3
```

```
K3 = 1×4
10.6433 0.3111 4.7735 7.8756
```

# Simulate the Full State Feedback Controllers from $\tilde{x}_0 = \begin{bmatrix} 1 & 0 & 2 & 0 \end{bmatrix}$

The full state feedback state space model was implemented in Simulink to allow for easy calculation of integrated controller fuel and determination of steady state from the euclidean norm of the state vector. The final simulation time is the time when the state vector enters a unit hypersphere of radius 0.01.

$$\dot{x} = (A - BK)x$$



Run 'initial' simulations and compare the energy cost and time to steady state

```
x0 = [1 0 2 0]'; %Initial state vector
tstop = 25;
input_select = 2; %Full state feedback input NOT fuel optimal control input
t_end = 3; %Not used now but need to initialize the variable so it's not undefined
Wc_sim = double(Wc(5)); %Grammian for 5 seconds
```

# LQR 1

```
K = K1;
out1 = sim('FSF');
x1 = out1.x;
tsim1 = out1.tout;
energy1 = out1.intUsqrd(end);
ss_time1 = tsim1(end);
```

### LQR 2

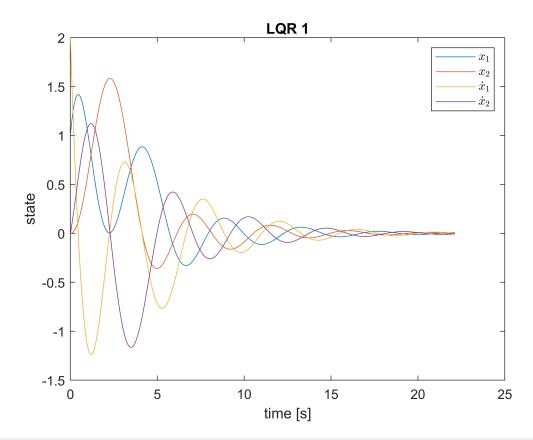
```
K = K2;
out2 = sim('FSF');
x2 = out2.x;
tsim2 = out2.tout;
energy2 = out2.intUsqrd(end);
ss_time2 = tsim2(end);
```

# LQR3

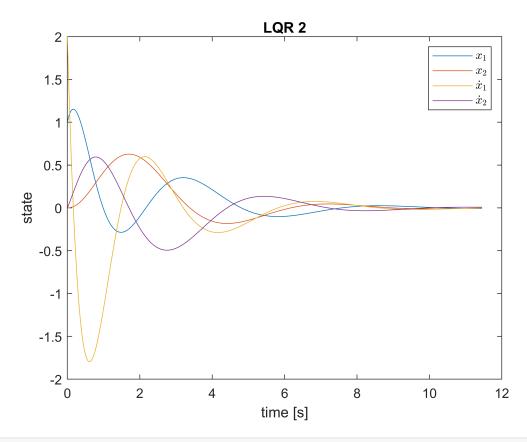
```
K = K3;
out3 = sim('FSF');
x3 = out3.x;
tsim3 = out3.tout;
energy3 = out3.intUsqrd(end);
ss_time3 = tsim3(end);
```

### Plot results

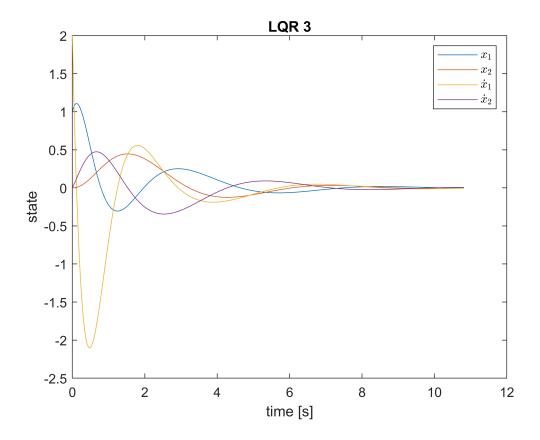
```
figure
plot(tsim1,x1)
legend('$x_1$','$x_2$', '$\dot{x}_1$','$\dot{x}_2$','interpreter','latex')
xlabel('time [s]')
ylabel('state')
title('LQR 1')
```



```
figure
plot(tsim2,x2)
legend('$x_1$','$x_2$', '$\dot{x}_1$','$\dot{x}_2$','interpreter','latex')
xlabel('time [s]')
ylabel('state')
title('LQR 2')
```



```
figure
plot(tsim3,x3)
legend('$x_1$','$x_2$', '$\dot{x}_1$','$\dot{x}_2$','interpreter','latex')
xlabel('time [s]')
ylabel('state')
title('LQR 3')
```



### **Discussion**

Controller 1 utilized the least energy but took the most amount of time. Controller 3 utilized the most energy but took the least amount of time. Controller 2 landed between those two scenarios.

```
disp("Energy cost controller 1 was " + num2str(energy1,2) + ".")
Energy cost controller 1 was 6.9.

disp("Time to steady state controller 1 was " + num2str(ss_time1,3) + " seconds.")

Time to steady state controller 1 was 22.1 seconds.

disp("Energy cost controller 2 was " + num2str(energy2,3) + ".")
Energy cost controller 2 was 31.2.

disp("Time to steady state controller 2 was " + num2str(ss_time2,3) + " seconds.")

Time to steady state controller 3 was " + num2str(energy3,3) + ".")
Energy cost controller 3 was 51.1.

disp("Time to steady state controller 3 was " + num2str(ss_time3,3) + " seconds.")

Time to steady state controller 3 was 10.8 seconds.
```

### Part C

Control law is now the open loop law

$$u(t) = -B^T e^{A^T (t_1 - t)} W_c^{-1}(t_1) [e^{At} x_0 - x_1]$$

Instead of the closed loop law

$$u(t) = -Kx(t)$$

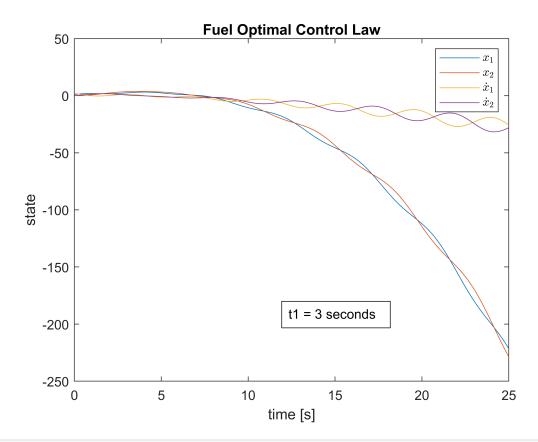
# **Simulate Fuel Optimal Control Law**

```
x0 = [1 0 2 0]'; %Initial state vector
tstop = 25;
input_select = 1; %Fuel optimal control law
%t1 from the control law (named differently because "t1" is already used elsewhere)
t_end = 3; %Not used now but need to initialize the variable so it's not undefined
Wc_sim = double(Wc(5)); %Grammian for 5 seconds

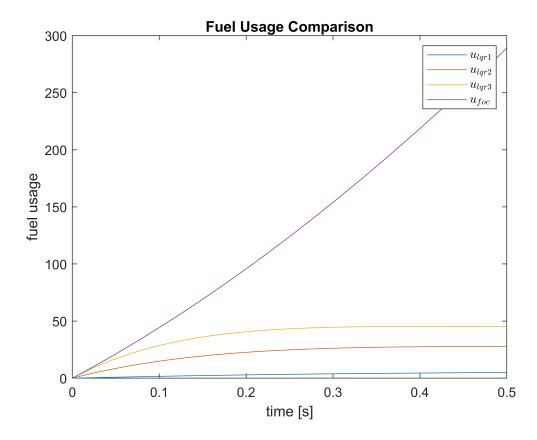
out4 = sim('FSF');
x4 = out4.x;
tsim4 = out4.tout;
energy4 = out4.intUsqrd(end);
ss_time4 = tsim4(end);
```

#### Plot Results

```
figure
plot(tsim4,x4)
legend('$x_1$','$x_2$', '$\dot{x}_1$','$\dot{x}_2$','interpreter','latex')
xlabel('time [s]')
ylabel('state')
title('Fuel Optimal Control Law')
annotation('textbox', [0.5, 0.2, 0.1, 0.1],'string', ['t1 = ' num2str(t_end) ' seconds'])
```



```
figure
plot(tsim1,out1.intUsqrd,tsim2,out2.intUsqrd,tsim3,out3.intUsqrd,tsim4,out4.intUsqrd)
legend('$u_{lqr1}$','$u_{lqr2}$', '$u_{lqr3}$','$u_{foc}$','interpreter','latex')
xlabel('time [s]')
ylabel('fuel usage')
title('Fuel Usage Comparison')
xlim([0 .5])
```



# **Discussion**

Since the system is not open loop stable, the fuel optimal control law u(t) does not take the state to zero let alone within time  $t_1$  in an energy minimizing manner - the system is actually unstable. The fuel consumption is plotted over a very small time interval to see where the unstable controller's fuel consumption diverges from the three stable controller's fuel consumption.