

Chemical Reaction Engineering—Homework #9

Due: Online submission on Canvas as PDF, **Wednesday, April 8, 2020 at 11:59pm.**

No late submissions will be accepted.

Problems that require a numeric answer should have 3 significant figures.

Units, where required, are shown in blue. Please use these units.

Problem 1: Non-ideal reactors

Experiments are being performed using a reactor with non-ideal flow. The exit concentration in response to a pulse input with an inlet volumetric flow rate of 0.1 L/s is given below.

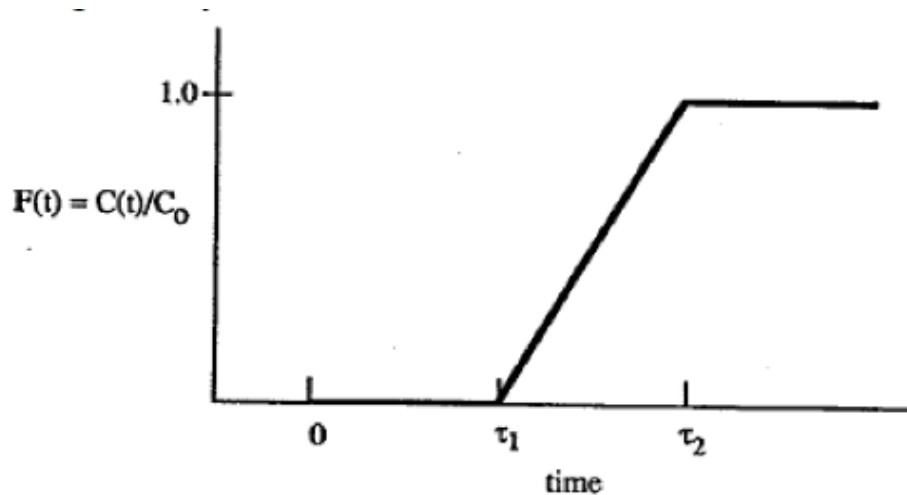
$$\begin{array}{ll} C = 0 & \text{for } t < 3 \text{ s} \\ C = 0.5t - 1.5 & \text{for } 3\text{s} < t < 5\text{s} \\ C = -t + 6 & \text{for } 5\text{s} < t < 6\text{s} \\ C = 0 & \text{for } t > 6\text{s} \end{array}$$

C has units of mol/L.

- What is the total amount of tracer fed at $t = 0$? **[0.15 mol]**
- Find an algebraic expression for the residence time distribution function $E(t)$ and graph this as a function of time.
- Plot $F(t)$ of this reactor to a step change in inlet concentration from 0 to 1 mol/L at $t = 0$.
- What is the mean residence time in this reactor? **[4.5 s]** What is the volume of this reactor? **[0.45 L]**
- Using the segregation model of mixing, what is the mean conversion for the second order reaction $A \rightarrow B$ with $k = 0.5 \text{ L}/(\text{mol}\cdot\text{s})$, and $C_{A0} = 1 \text{ mol/L}$? **[0.7]**
How does this compare to the conversions achieved in a CSTR and a PFR operating at the same residence time?

Problem 2: Writing $E(t)$ from $F(t)$

The response of an isothermal tubular reactor to a step change in concentration at $t = 0$ is given by the following graph.



- Write an expression for $E(t)$ and sketch the predicted response of this reactor to a pulse input.
- Calculate the conversion of A in this reactor using a segregated model for this non-ideal tubular reactor for the liquid phase reaction. The experimental conversion is 35%. [0.35]

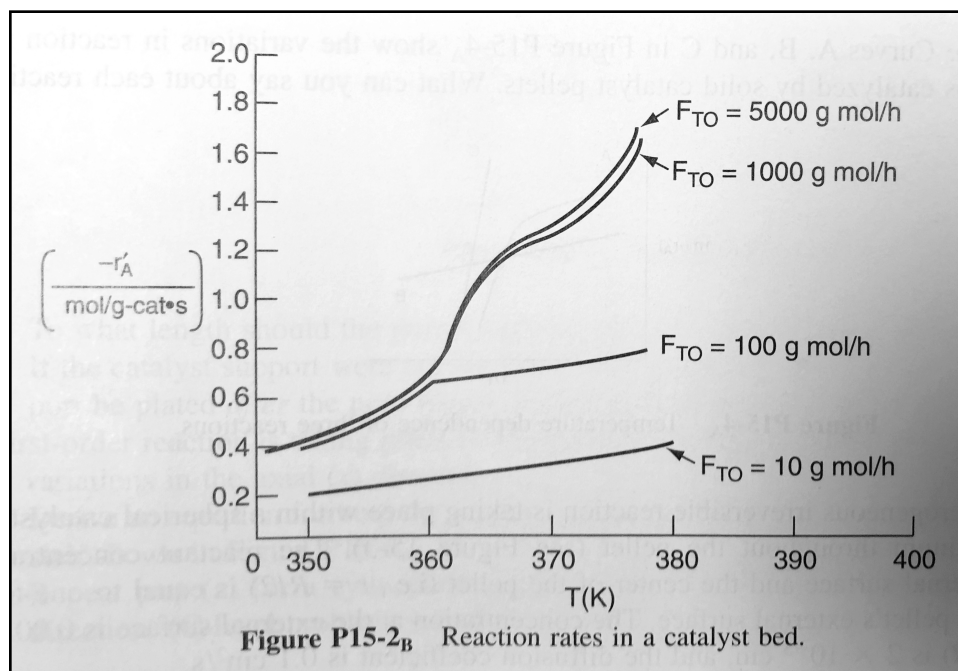


$$C_{A0} = 2C_{B0}$$

$$\tau_1 = 30\text{s}$$

$$kC_{A0} = 0.05\text{ s}^{-1}$$

$$\tau_2 = 50\text{ s}$$

Problem 3: Mass transfer limited or kinetically limited systems

Answer the following questions using the figure above from Fogler.

- Is the reaction limited by external diffusion?
- If your answer from part a was Yes, under what conditions (flow rate and temperature) is the reaction limited by external diffusion?
- Is the reaction “kinetically limited?”
- If your answer from part c was Yes, under what conditions (flow rate and temperature) is the reaction limited by the rate of chemical reaction?
- Is the reaction limited by internal diffusion?
- If your answer from part e was Yes, under what conditions (flow rate and temperature) is the reaction limited by internal diffusion?

Problem 4: Concentration gradients and internal effectiveness factor

Consider an irreversible first-order heterogeneous reaction inside a porous spherical pellet that is coated on the inside with platinum. Let the reactant concentration halfway between the external surface and the center of the pellet ($r = R/2$) be equal to one-tenth of the concentration of the pellet's external surface. At the external surface, the concentration is 0.001 mol/L, the effective diffusion coefficient is 0.1 cm²/s, and the diameter is 0.002 cm. Assume that the pellet is isothermal.

- a. At a radial distance of 0.0003 cm inside from the external pellet surface, what is the concentration of the reactant? $[2 \times 10^{-4} \text{ M}]$
- b. What diameter of particle must be used to have an effectiveness factor of 0.8? $[7 \times 10^{-4} \text{ cm}]$

Problem 5: Sizing a reactor with internal mass transfer limitations

The second order, ideal gas phase decomposition reaction of $A \rightarrow B$ is carried out isothermally and isobarically in a tubular reactor packed with catalyst pellets 0.4 cm in diameter. These large pellets are used to make pressure drop negligible, but as a consequence, the reaction becomes internal mass transfer limited. Pure A enters the reactor at a superficial velocity of 3 m/s, temperature of 250 degrees C and a pressure of 5 kPa. The reaction rate constant is $k'' = 0.0005 \text{ m}^4/(\text{mol}\cdot\text{s})$. Assume that the forced axial convection term in the mole balance is much larger than axial diffusion.

Calculate the length of the bed necessary to achieve 80% conversion with the 0.4 cm diameter pellets. $[0.04 \text{ m}]$

Additional information:

Effective diffusivity: $2.66(10^{-8}) \text{ m}^2/\text{s}$

Bed void fraction: 0.4

Pellet density $2(10^6) \text{ g}/\text{m}^3$

Internal surface area: $400 \text{ m}^2/\text{g}$