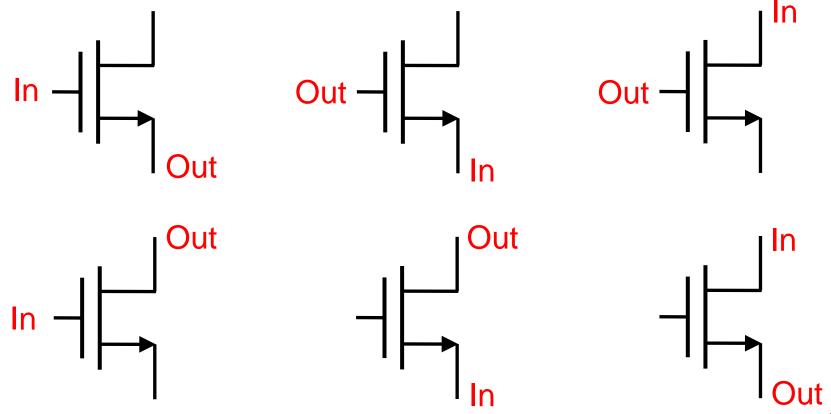
Lecture21: CMOS amplifiers (5)

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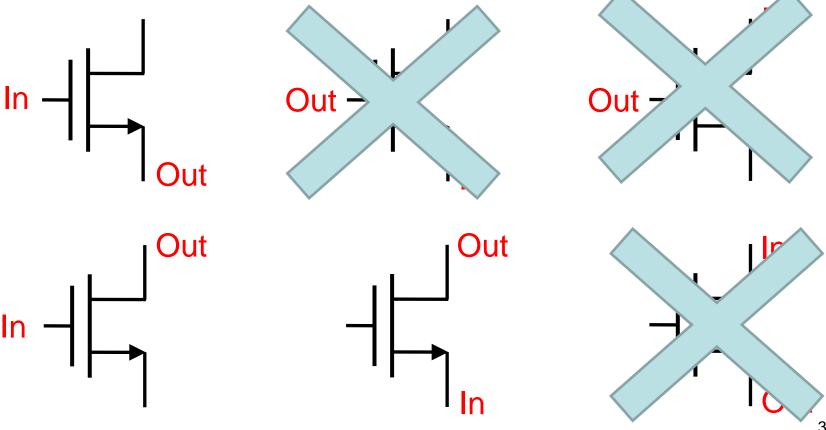
CMOS amplifiers (1/2)

- Select one input. Then, select one output.
 - What are possible topologies?



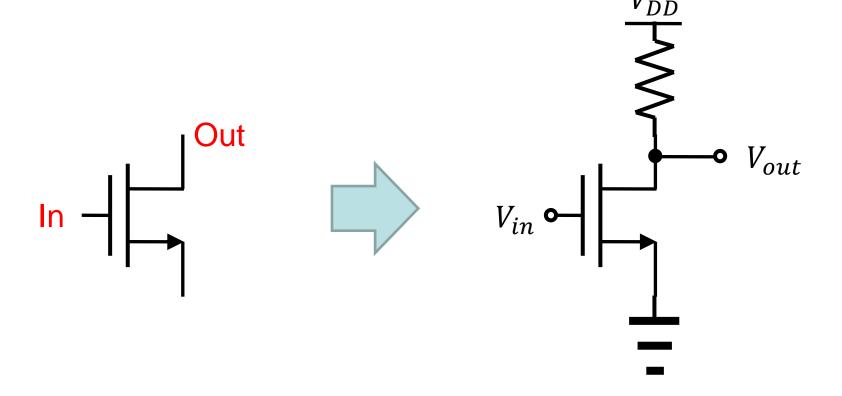
CMOS amplifiers (2/2)

- Only three are possible.
 - Each of them has own name.



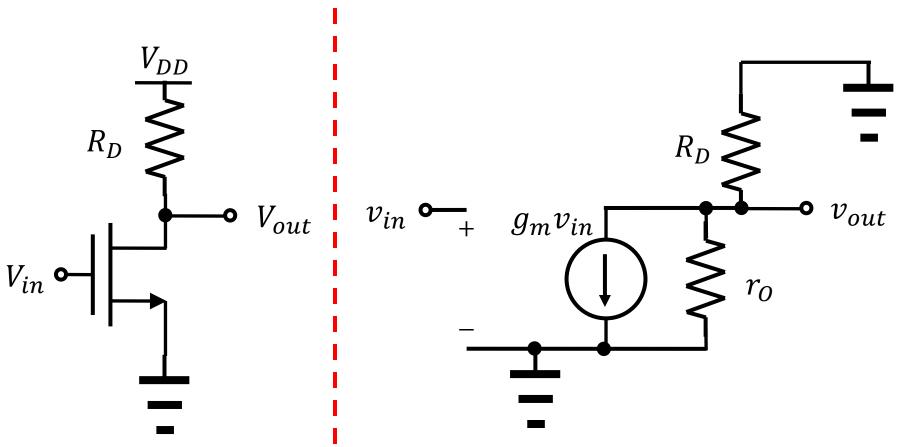
Common-source

Source terminal is grounded.



Small-signal model

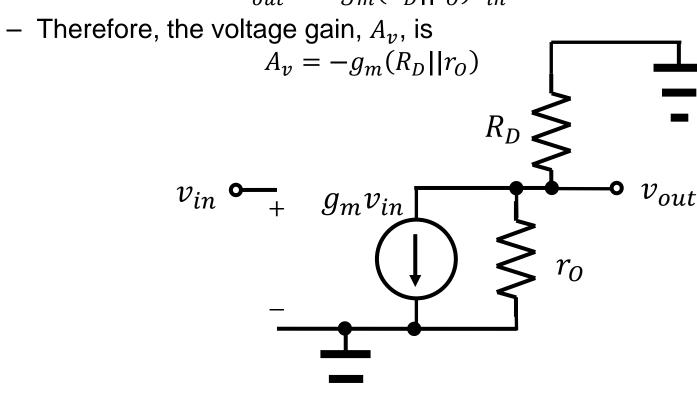
Let's draw the small-signal model together!



Gain

- Now, calculate the v_{out} .
 - KCL for the v_{out} node gives

$$v_{out} = -g_m(R_D||r_0)v_{in}$$

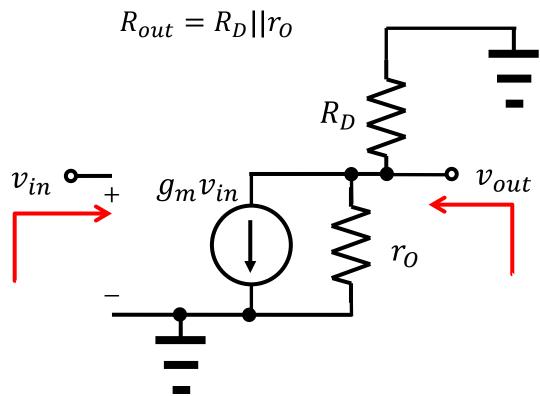


Input/output impedances

Input impedance

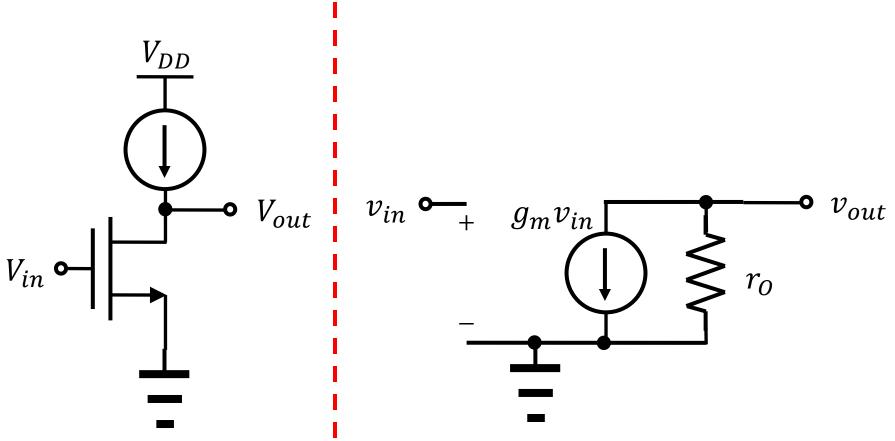
$$R_{in} = \infty$$

Output impedance



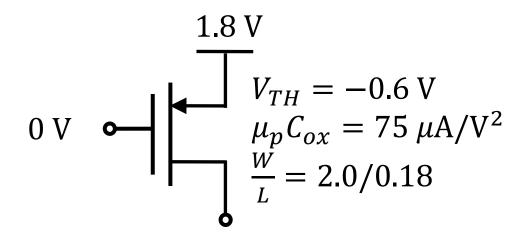
Current-source load

- When $R_D \to \infty$,
 - The gain can be maximized.



Biasing of PMOS devices

- Use a PMOS as a current source
 - The amount of "gate overdrive" is 1.2 V.
 - It is not 0.6 V.

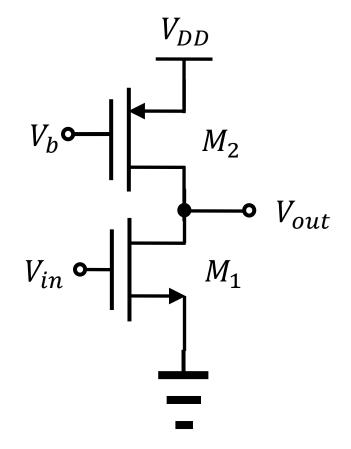


Real current-source load

- Use a PMOS as a current source.
 - It is not an ideal current source.

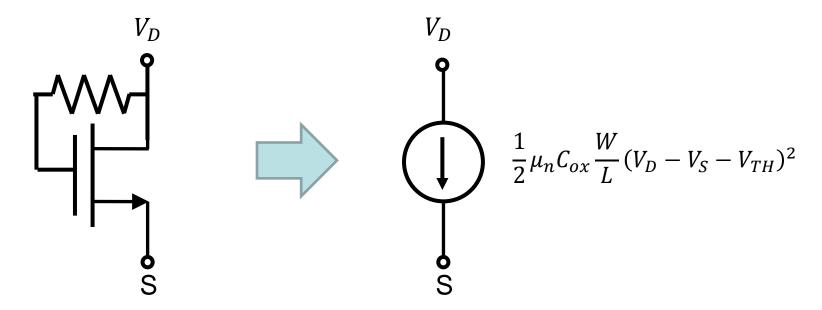
$$v_{out} = -g_{m1}(r_{01}||r_{02})v_{in}$$

$$A_{v} = -g_{m1}(r_{01}||r_{02})$$



Self-biasing

- Already covered in Example 6.13.
 - Always in the saturation region.



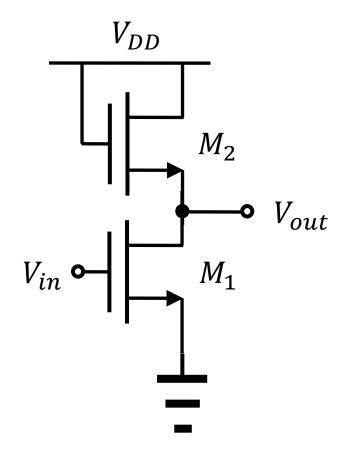
Gate and drain are tied.

In this case,

- Use a diode-connected load.
 - It is not an ideal current source.

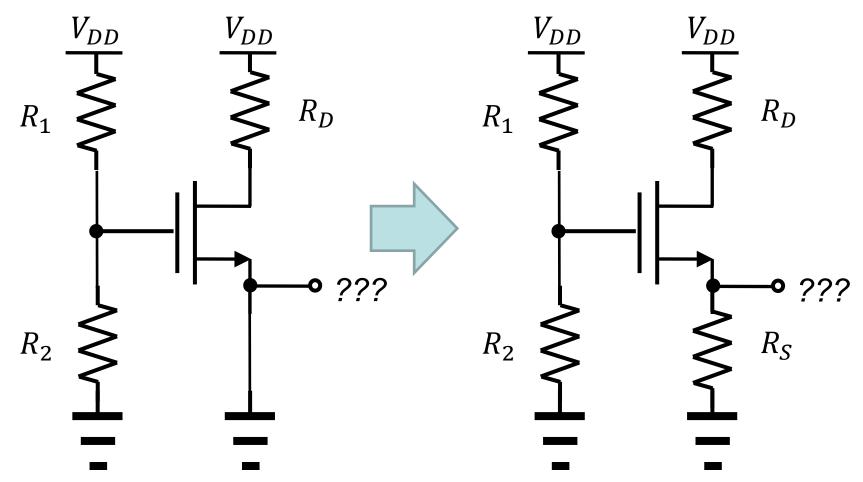
$$v_{out} = -g_{m1} \left(r_{O1} || \frac{1}{g_{m2}} || r_{O2} \right) v_{in}$$

$$A_v = -g_{m1} \left(r_{01} || \frac{1}{g_{m2}} || r_{02} \right)$$



Source degeneration (1/2)

A resistor placed in series with the source terminal



Source degeneration (2/2)

- Now we have to find the source voltage.
 - (Saturation current of the MOSFET) = (Current flowing through R_S)
 - After a simple manipulation, we can find

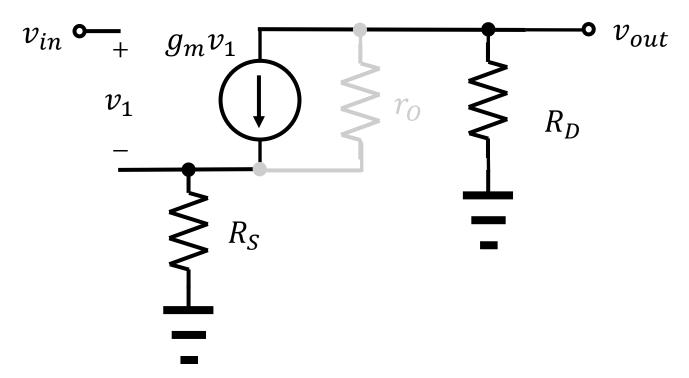
$$V_S = V_G + V_1 - V_{TH} - \sqrt{V_1^2 + 2(V_G - V_{TH})V_1}$$

Here,

$$V_1 = \frac{1}{\mu_n C_{ox} \frac{W}{L} R_s}$$

Effect of R_S (1/2)

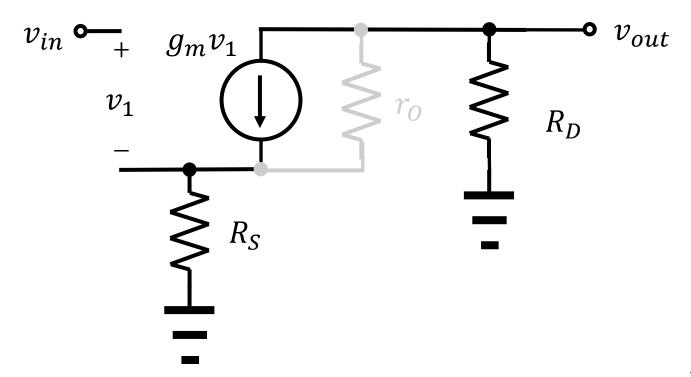
- Reduction of the gate-source voltage
 - Therefore, also reduction of the gain.
- For a while, neglect the channel-length modulation.



Effect of R_S (2/2)

After a simple manipulation,

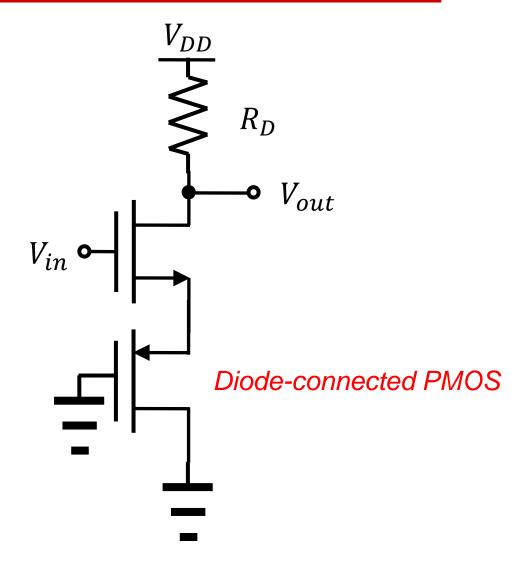
$$A_v = -\frac{g_m R_D}{1 + g_m R_S}$$



Example 17.20

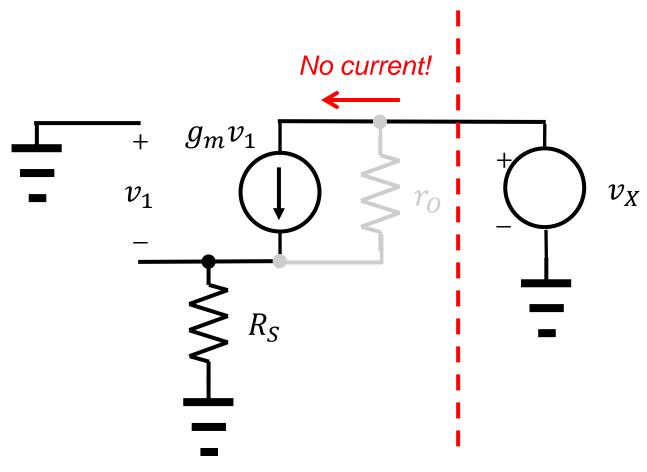
CS with degeneration

$$A_{v} = -\frac{R_{D}}{\frac{1}{g_{m1}} + \frac{1}{g_{m2}}}$$



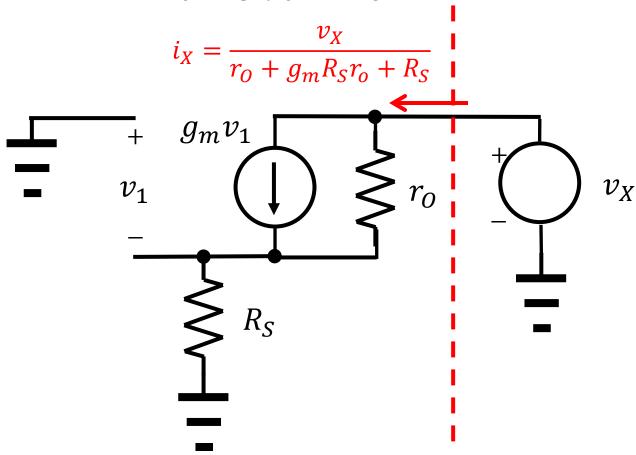
Output impedance of CS (1/2)

- Still neglecting the channel-length modulation
 - No current!



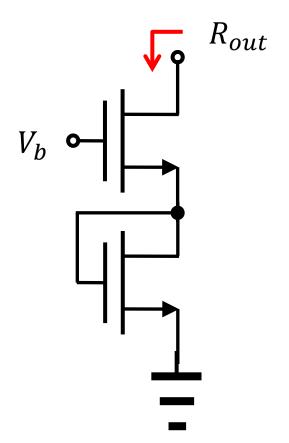
Output impedance of CS (2/2)

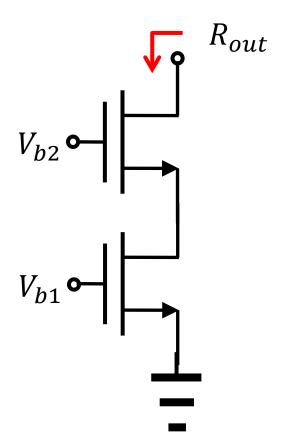
- Now considering the channel-length modulation
 - Output resistance is $r_0 + (g_m r_0 + 1)R_S$.



Examples 17.23 and 17.24

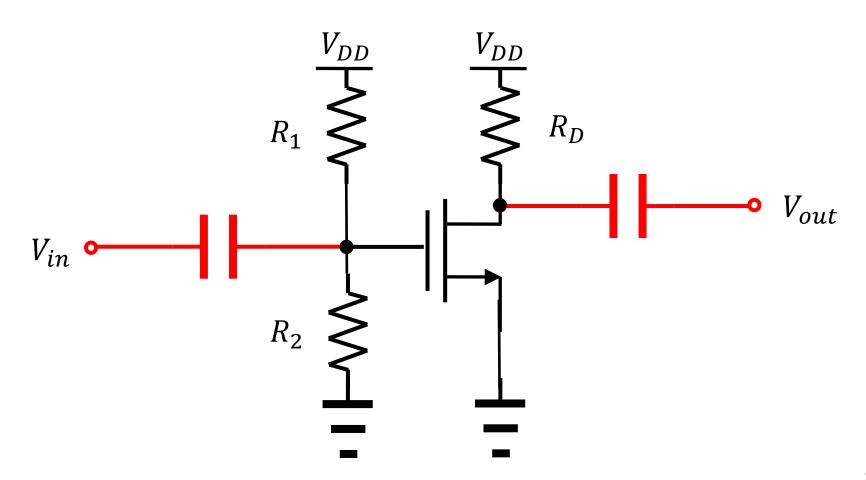
- Compute the output resistance.
 - What is the difference?





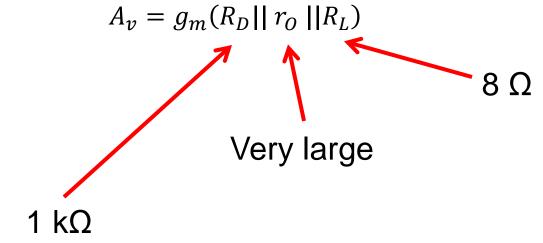
CS stage with biasing

We need capacitive coupling at the input and output.



Low load impedance

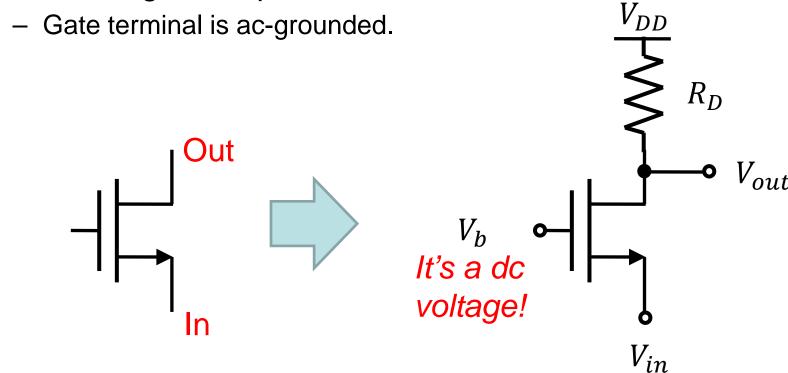
- Example 17.27
 - With the load impedance, R_L , the gain becomes



Low load impedance drops the gain drastically!

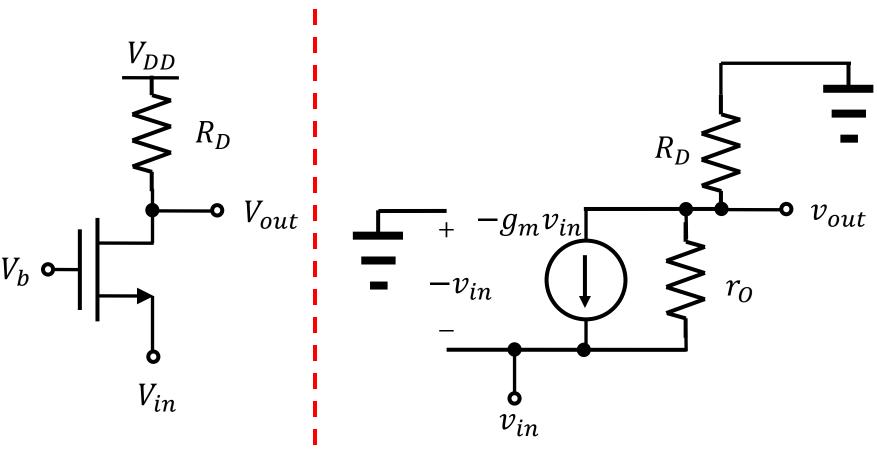
Common-gate amplifier

- Why do we study other amplification topologies?
 - Different circuit properties
- Common-gate amplifier



Small-signal model

Let's draw the small-signal model together!

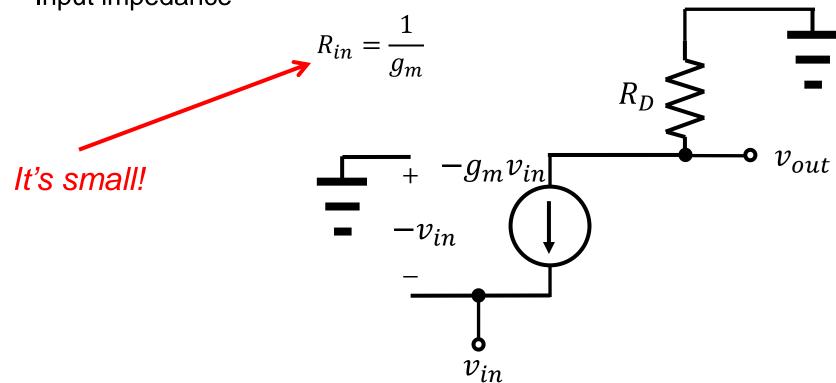


Gain and input impedance

- Neglect the output resistance, r_0 .
 - Voltage gain

$$A_v = +g_m R_D$$

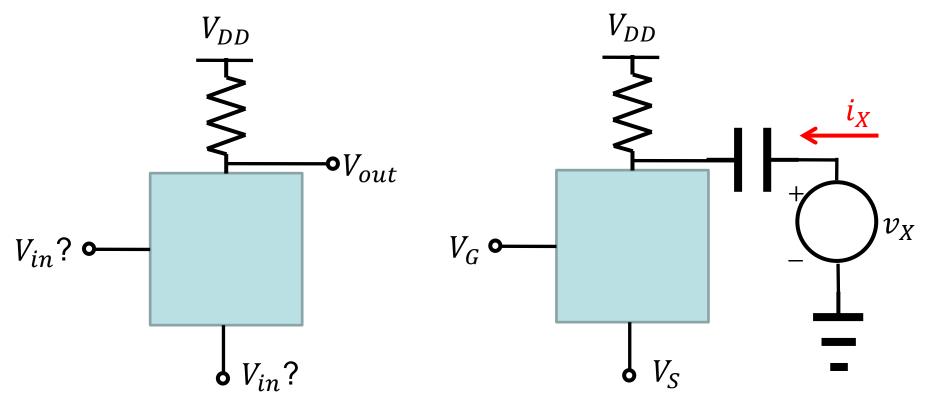
Input impedance



Output impedance

Same with the CS stage

$$R_{out} = r_O ||R_D|$$

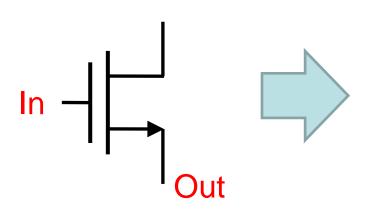


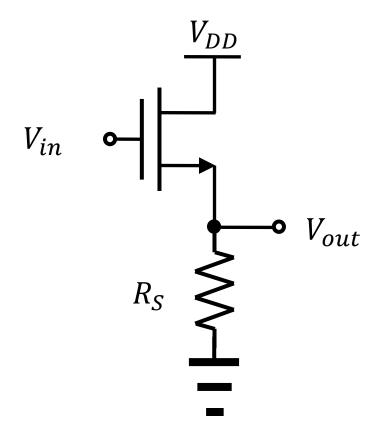
Generic form of CS and CG stages

Setting for calculating R_{out}

Source follower

- Also called the "common-drain" stage
 - The drain is ac ground.
- Wait a minute!
 - Is it a real amplifier?

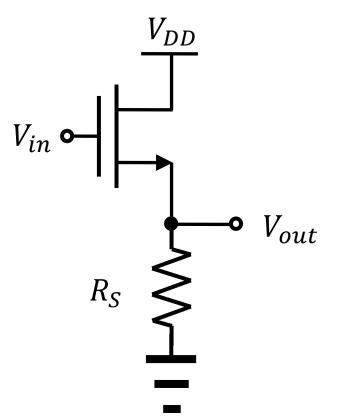




Its core

Gain is less than 1??

$$A_v = +\frac{g_m R_S}{1 + g_m R_S}$$



You should be able to draw the small-signal model.

Useless?

- Calculate the input and output impedances.
 - Since the gate is the input terminal, the input impedance is very high at low frequencies.
 - How about the output impedance?

$$R_{out} = \frac{1}{g_m} ||r_O||R_S$$

- It is relatively low.
- High input imp., low output imp.
 - They can serve as good "buffers."

