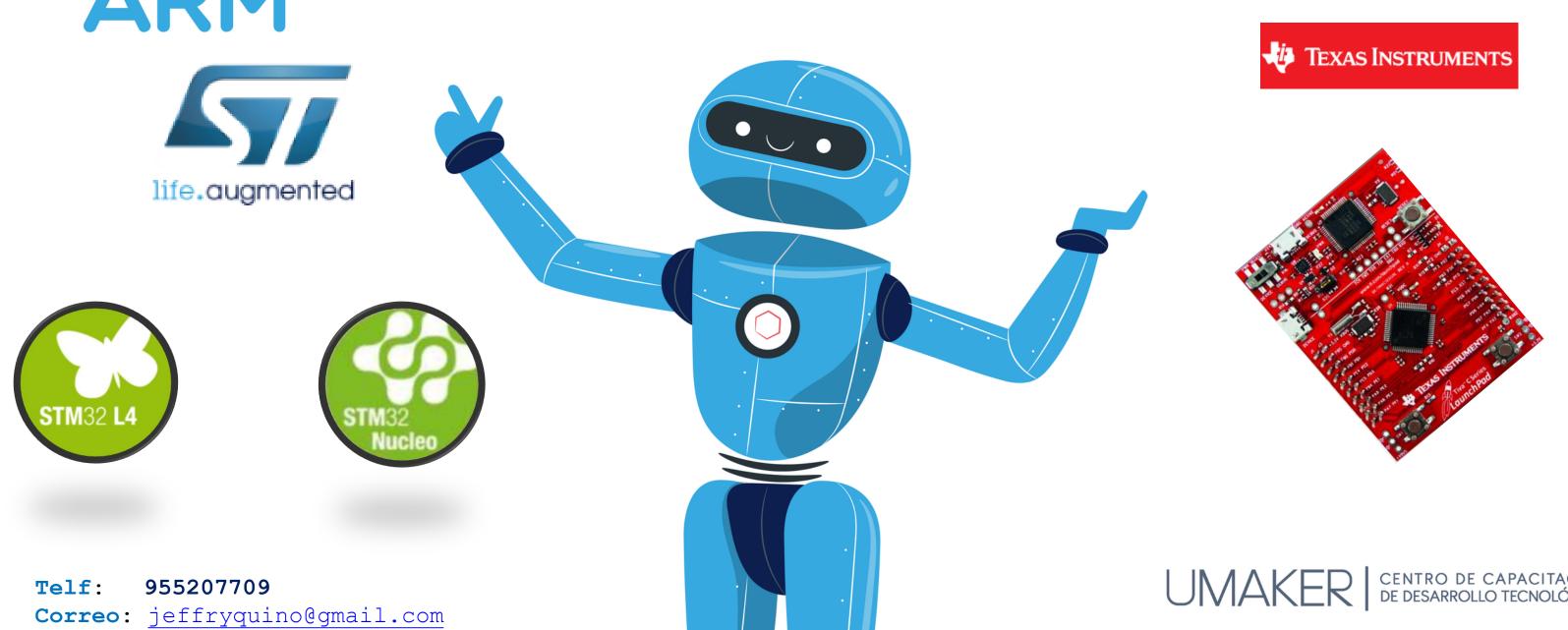
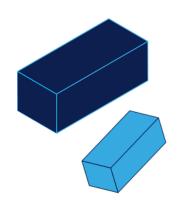
DISEÑO DE CONTROLADOR PID Y IMPLEMENTACION EN MICROCONTROLADORES ARM





DISEÑO DE CONTROLADOR PID

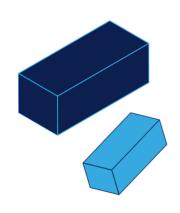


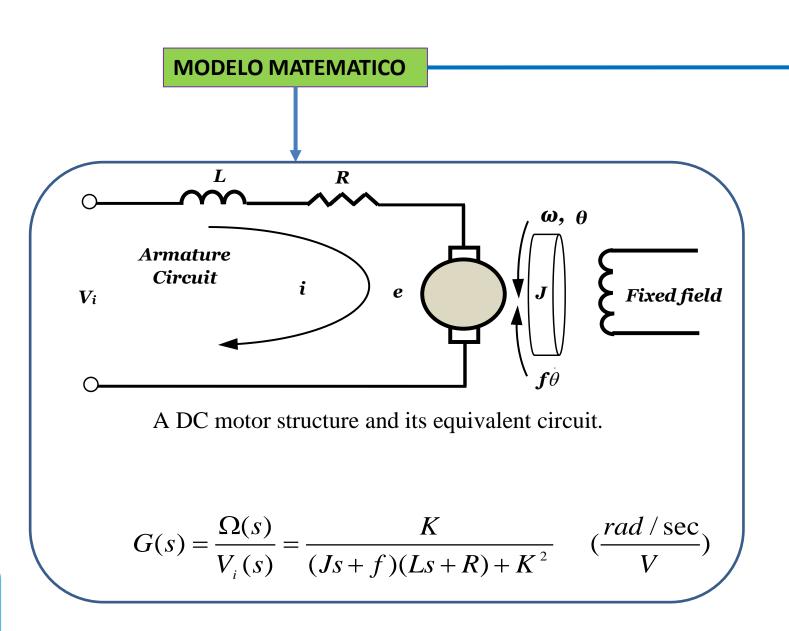
Telf: 955207709

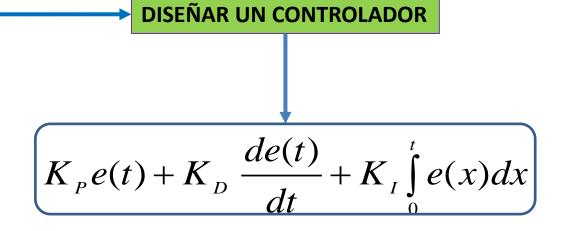


MODELO MATEMATICO MOTOR DC

Modelo matemático consiste en utilizar ecuaciones matemáticas para definir la relación entrada-salida de un sistema de control, de la forma más completa y precisa posible.







MODELO ESTIMADO A PARTIR DE DATOS EXPERIMENTALES

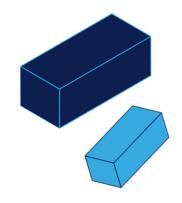
$$G(s) = \frac{20100}{s^2 + 51.9s + 913.3}$$

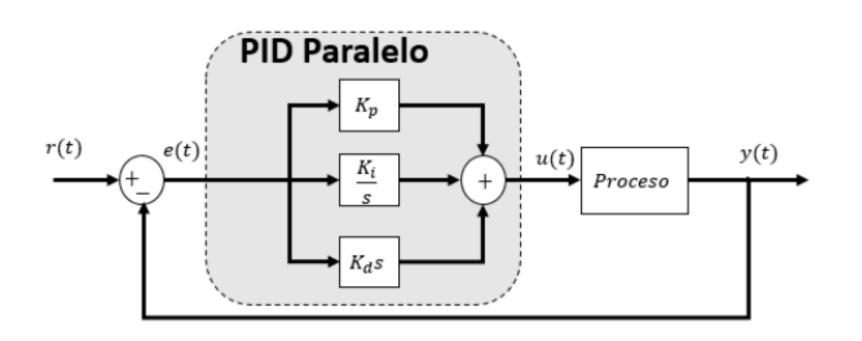


Telf: 955207709

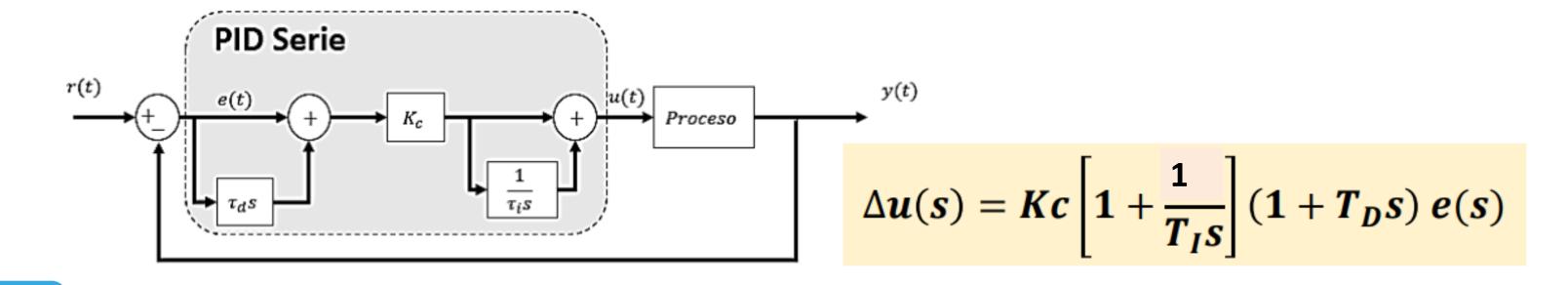


CONTROLADORES PID IDEALES





$$\Delta u(s) = Kc \left[1 + \frac{1}{T_I s} + T_D s \right] e(s)$$

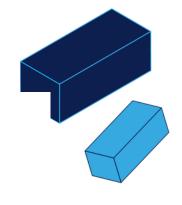


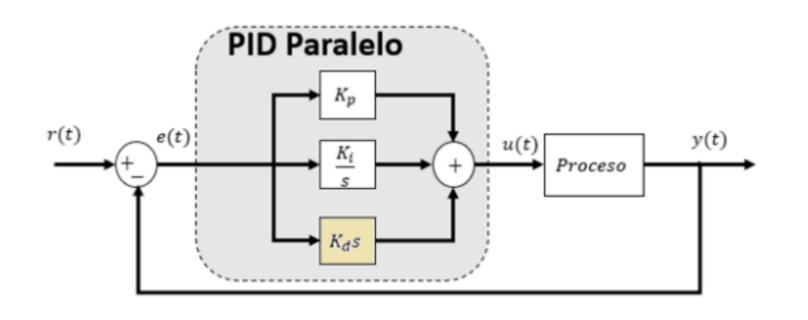


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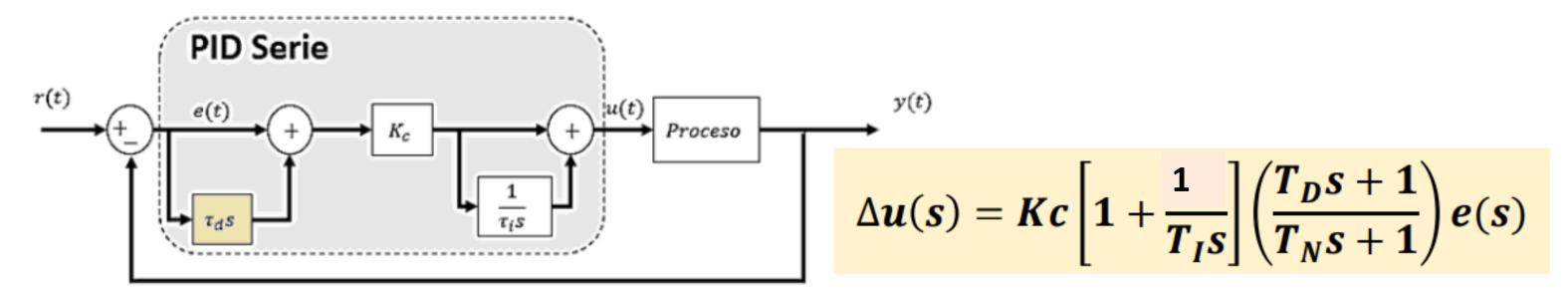


CONTROLADORES PID REALES





$$\Delta u(s) = Kc \left(1 + \frac{1}{Tis} + \frac{Tds}{T_N s + 1} \right) e(s)$$



$$\frac{T_N}{T_D} \approx 0.05 \ a \ 0.1$$

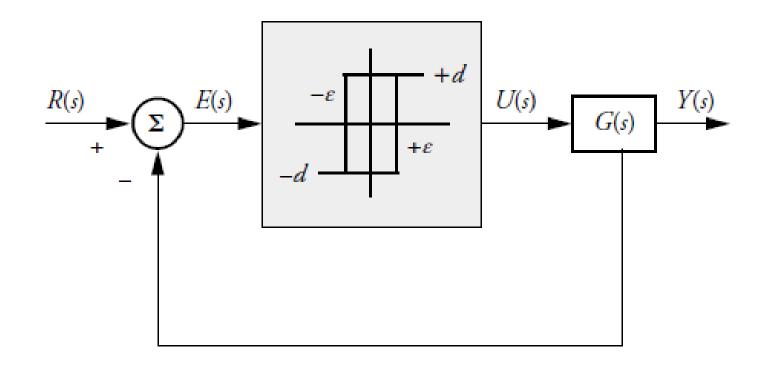


Telf: 955207709



SINTONIZACION DE CONTROLADORES PID

- Método de Ziegler-Nichols
- Método del relevador
- Método de Cohen-Coon
- Sintonización de controladores PID con criterios óptimos



Método	del	relevador
1100000	\sim \sim	TCTCVAACT

controlador	Parametros
БР	$K_c = \frac{1}{K_p} \frac{\alpha}{\tau} \left(1 + \frac{\tau}{3\alpha} \right)$
PI	$K_c = \frac{1}{K_p} \frac{\alpha}{\tau} \left(\frac{9}{10} + \frac{\tau}{12\alpha} \right)$ $T_i = \tau \frac{30 + 3\left(\frac{\tau}{\alpha}\right)}{9 + 20\left(\frac{\tau}{\alpha}\right)}$
PD	$K_{c} = \frac{1}{K_{p}} \frac{\alpha}{\tau} \left(\frac{5}{4} + \frac{\tau}{6\alpha} \right)$ $T_{d} = \tau \frac{6 - 2\left(\frac{\tau}{\alpha}\right)}{22 + 3\left(\frac{\tau}{\alpha}\right)}$
PID	$K_{c} = \frac{1}{K_{p}} \frac{\alpha}{\tau} \left(\frac{4}{3} + \frac{\tau}{4\alpha} \right)$ $T_{i} = \tau \frac{32 + 6\left(\frac{\tau}{\alpha}\right)}{13 + 8\left(\frac{\tau}{\alpha}\right)}$ $T_{d} = \tau \frac{4}{11 + 2\left(\frac{\tau}{\alpha}\right)}$

Tipo de

Método de Cohen-Coon



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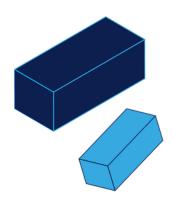


CONTROLADOR PID POR UBICACIÓN DE POLOS

Tomando en cuenta la configuración en paralelo

$$K_{P}e(t) + K_{D} \frac{de(t)}{dt} + K_{I} \int_{0}^{t} e(x)dx$$

$$G_p(s) = \frac{20100}{s^2 + 51.9s + 913.3}$$



La función de transferencia de | controlador PID en tiempo continuo viene dada por:

$$G_c(s) = \frac{U(s)}{E(s)} = \frac{K_p(T_d s^2 + s + 1/T_i)}{s}$$

Por consiguiente, la función de transferencia directa viene expresada por:

$$G_c(s)G_p(s) = \frac{20100K_p(T_ds^2 + s + \frac{1}{T_i})}{S^3 + 51.9s^2 + 913.3s}$$

Función de transferencia en lazo cerrado:

$$\mathsf{G}\left(s\right) = \frac{20100K_{p}(T_{d}s^{2} + s + \frac{1}{T_{i}})}{s^{3} + (51.9 + 20100T_{d}K_{p})s^{2} + (913.3 + 20100K_{p})s + 20100K_{p}/T_{i}}$$

La ecuación característica:

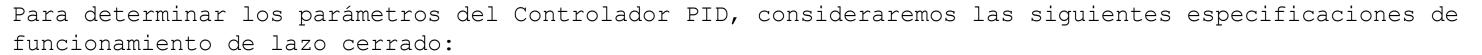
$$S^{3} + (51.9 + 20100T_{d}K_{p})s^{2} + (913.3 + 20100K_{p})s + \frac{20100K_{p}}{T_{i}} = 0$$

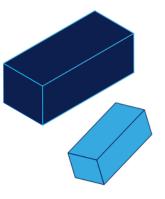


Telf: 955207709



CONTROLADOR PID POR UBICACIÓN DE POLOS





$$t_s = 0.4 \, \mathrm{Seg}$$
 $\zeta = 0.8$

Por lo que considerando el criterio de error de | 2%, obtendremos:

$$t_s = \frac{4}{\zeta w_n} \qquad w_n = 12.5 \frac{\text{rad}}{s}$$

Para que la respuesta del sistema en lazo cerrado se aproxime a la respuesta de un sistema de segundo orden, elegimos gl tercer polo ubicado a 5 veces la parte real de los polos dominantes, por lo que

$$p = 5(\zeta w_n)$$

En consecuencia la ecuación característica deseada de lazo cerrado, viene representada por:

$$(s^{2} + 2\zeta w_{n} + w_{n}^{2})(s+p) = 0$$

$$s^3 + 70s^2 + 1156.5s + 7825 = 0$$

Igualando las ecuaciones se obtiene los parámetros necesarios para el PID:

$$K_p = 0.0121$$

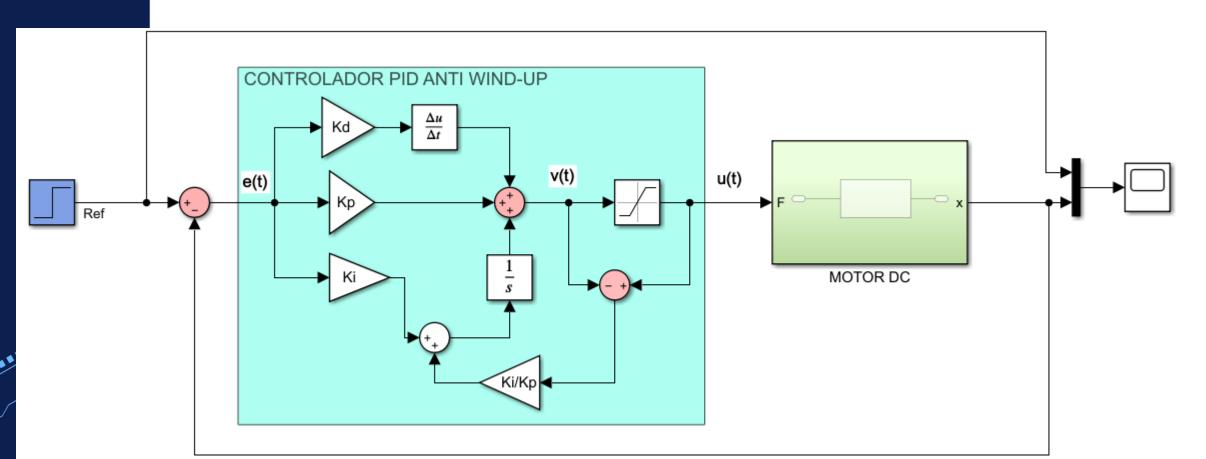
$$K_i = 0.39$$

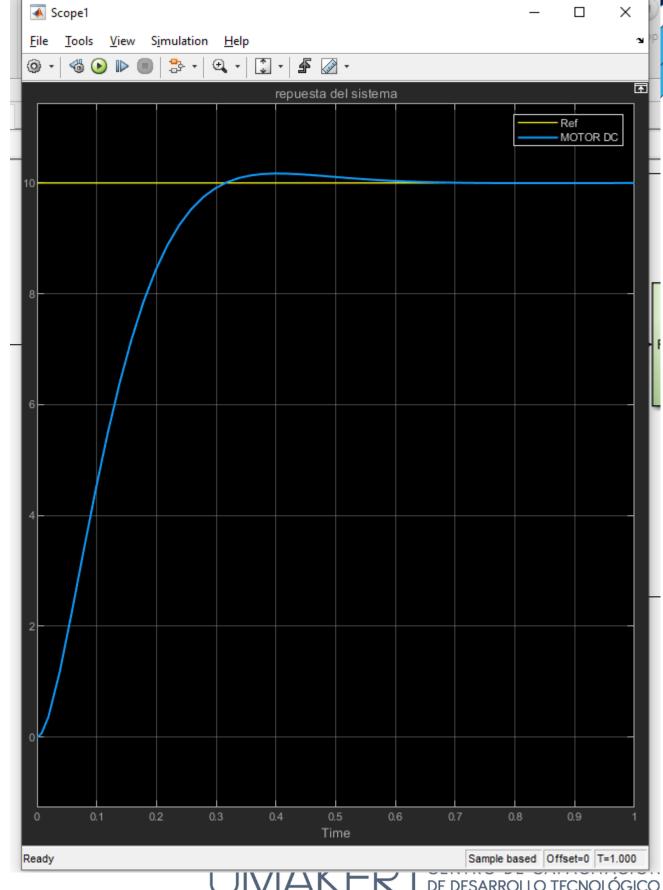
$$K_d = 8.95 * 10^{-4}$$

$$\Delta u(s) = 0.0121 \left(1 + \frac{1}{0.031s} + 0.074s \right) e(s)$$



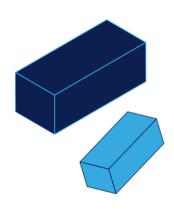
CONTROLADOR PID POR UBICACIÓN DE POLOS





MICRO-CONTRO-LADORES ARM

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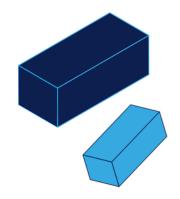


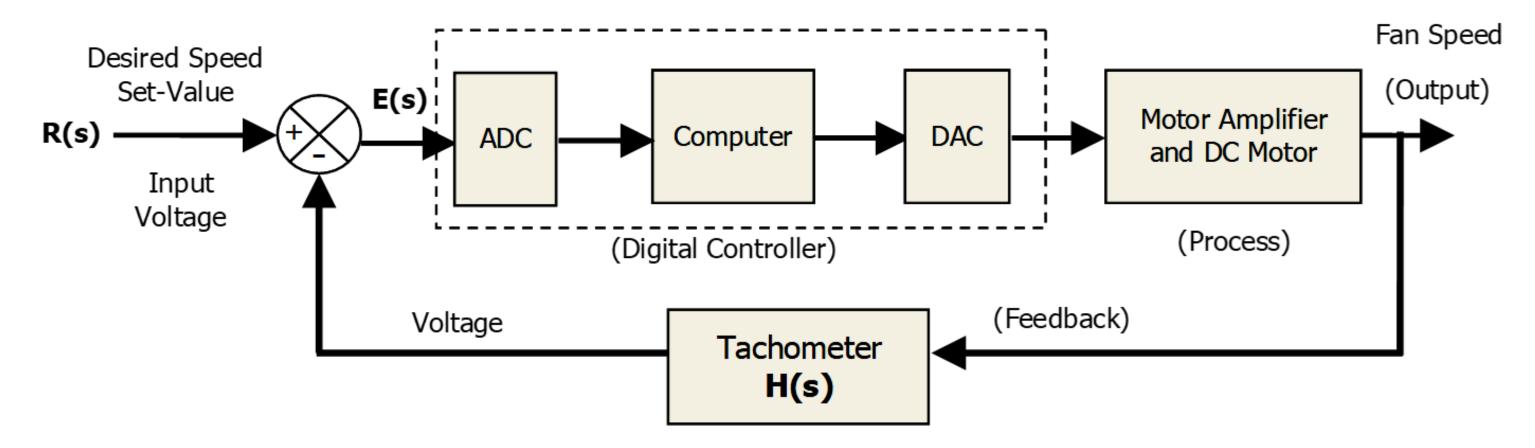
IMPLEMENTACION



Telf: 955207709





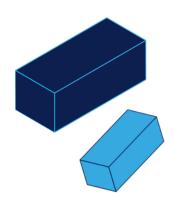


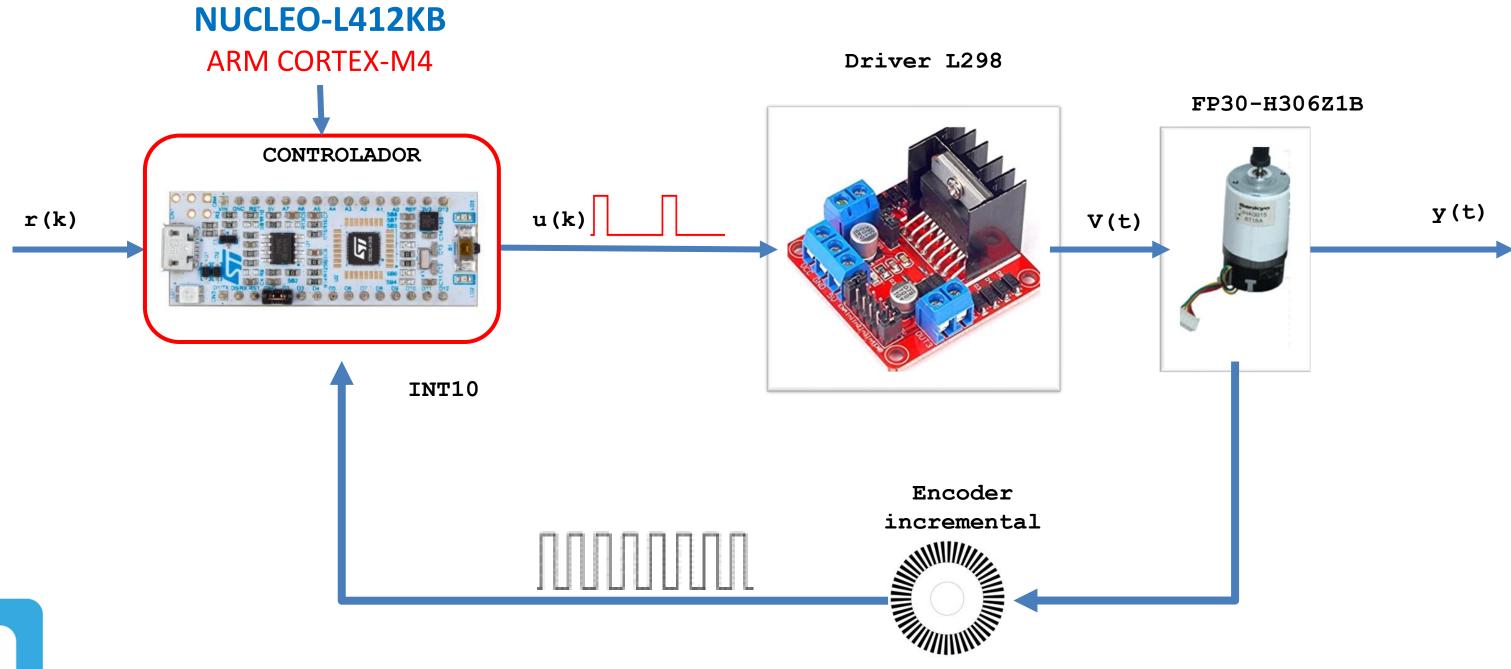
A complete closed-loop control system with a digital controller.



Telf: 955207709



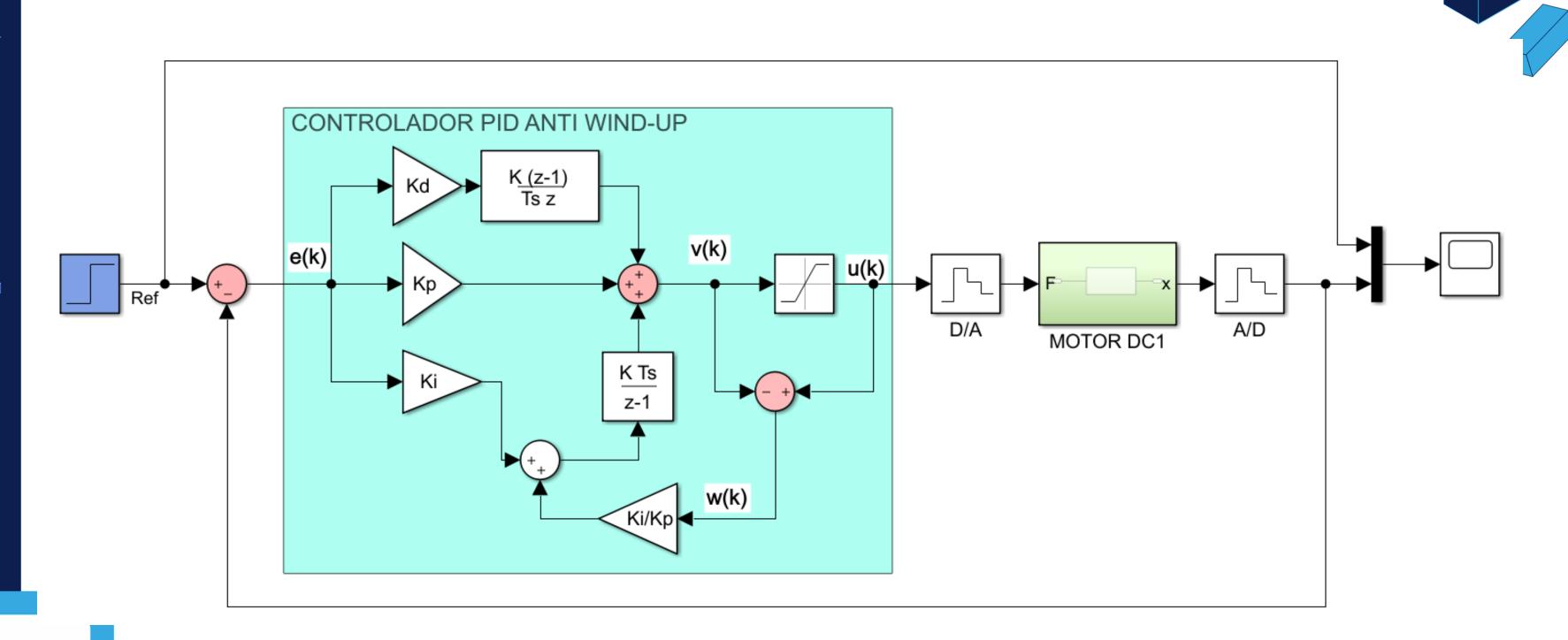




MICRO-CONTRO-LADORES ARM

Telf: 955207709

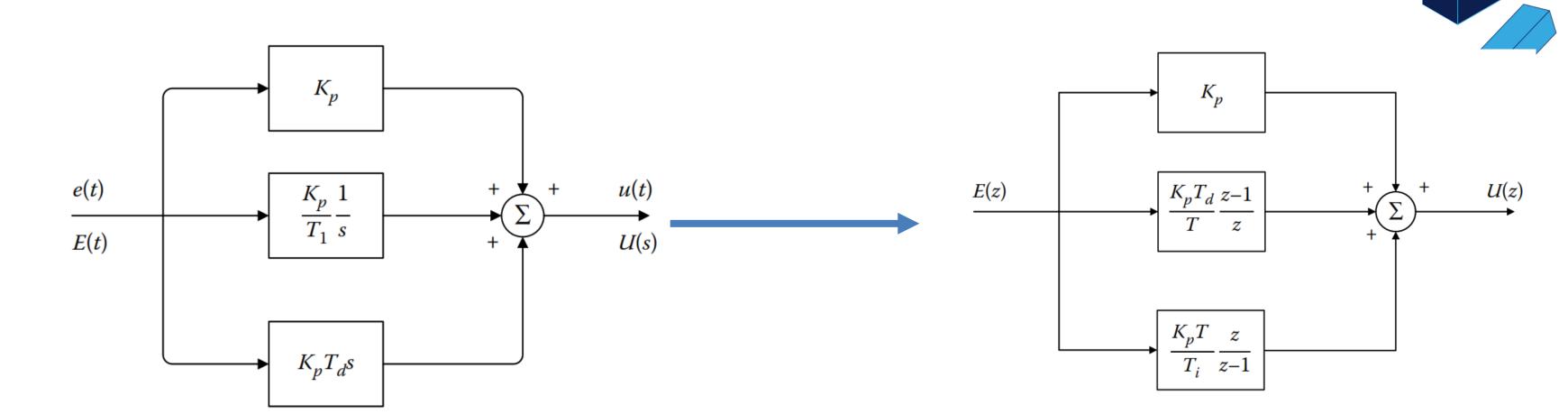




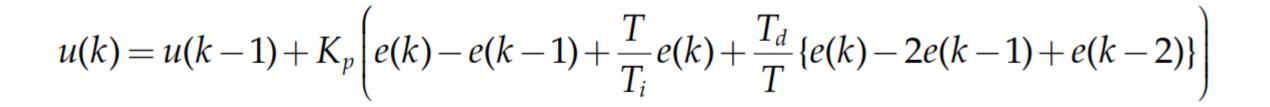


Telf: 955207709





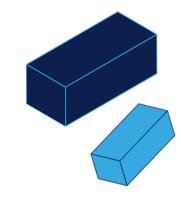
ECUACION DE DIFERENCIAS DEL CONTROLADOR PID





Telf: 955207709





PARTE PROPORCIONAL

$$P(k) = K_p e(k)$$

PARTE INTEGRAL

$$I(k) = I(k-1) + TK_ie(k) + TK_{aw}w(k)$$

PARTE DERIVATIVA

$$D(k) = \frac{K_d}{T}(e(k) - e(k-1))$$

$$V(k) = P(k) + I(k) + D(k)$$

SATURADOR

$$U(k) = egin{cases} U_{min} & , si \ V(k) < U_{min} \\ U_{max} & , si \ V(k) > U_{max} \\ V(k) & en \ otro \ caso \end{cases}$$

WIND UP

$$W(k) = U(k) - V(k)$$



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```
* @brief compute pid
|float PID_Compute(PID_Def_t *pidx, float Ref, float yk){
   float e_1 = pidx->e;
   float Uk;
    pidx->e = Ref - yk;
   /*parte proporcional*/
    pidx->Pk = pidx->e * pidx->Kp;
   /*parte integral*/
    pidx->Ik += pidx->Ts*pidx->Ki*pidx->e + pidx->Ts*pidx->Kaw*pidx->Wk;
   /*parte derivativa*/
    pidx-Dk = (pidx-Kd/pidx-Ts)*(pidx-e - e_1);
   /*salida pid*/
    pidx-Vk = pidx-Pk + pidx-Ik + pidx-Dk;
   /*saturador*/
    if(pidx->Vk > pidx->Umax)
        Uk = pidx->Umax;
    else if(pidx->Vk < pidx->Umin)
        Uk = pidx->Umin;
    else
        Uk = pidx->Vk;
   /*error wind up*/
    pidx->Wk = Uk - pidx->Vk;
   /*se retorna la salida el valor calculado*/
    return Uk;
```

CONTRO-

LADORES ARM **Telf**: 955207709

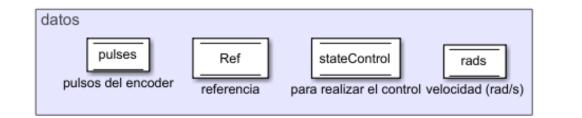




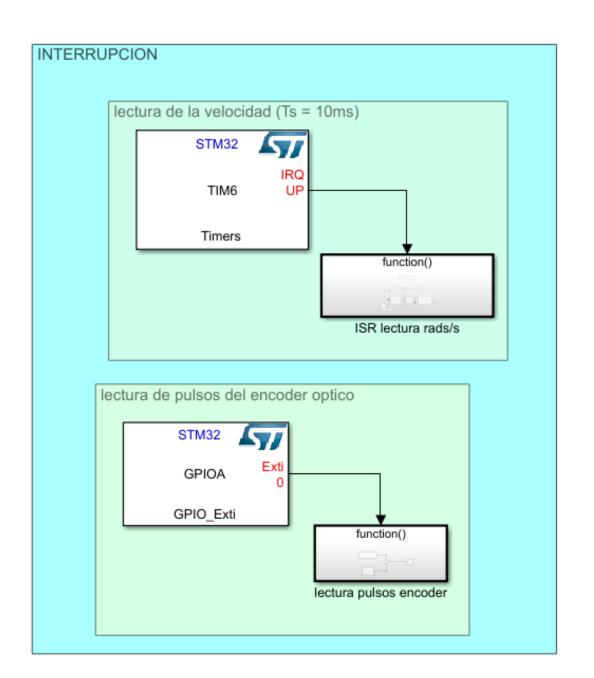
DISEÑO DEL CONTROLADOR PID- MOTOR DC

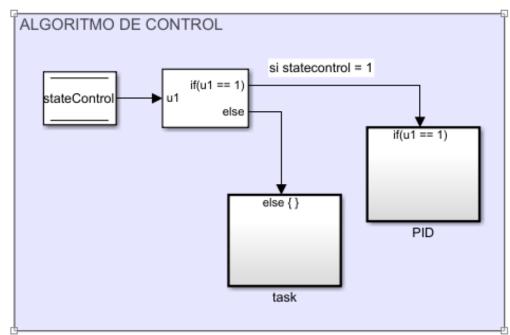
Embedded Coder - Simulink













Telf: 955207709



