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## Research paper

Thermal stability of FeSi as barrier layer in high-performance  $\text{Mg}_2\text{Si}_{0.3}\text{Sn}_{0.7}$  thermoelectric deviceShanshan Hu <sup>a,1</sup>, Chen Huang <sup>b,1</sup>, Changyuan Li <sup>a</sup>, Long Yang <sup>a</sup>, Zhiwei Chen <sup>a</sup>,  
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## ABSTRACT

Thermal stability of thermoelectric devices plays a pivotal role in their practical applications. Chemical reaction/diffusion between thermoelectric materials and electrodes is one of the primary factors contributing to the degradation/failure of device performance at elevated temperatures. Introducing barrier layers to impede the behavior of chemical reactions has emerged as an effective approach for averting the failure of these devices. In this work, the FeSi is revealed to be a potent material of barrier layer in high-performance  $\text{Mg}_2\text{Si}_{0.3}\text{Sn}_{0.7}$  thermoelectric material based on the considerations of interfacial reaction energy and sinterability. The well-established bond in  $\text{Mg}_2\text{Si}_{0.3}\text{Sn}_{0.7}/\text{FeSi}$  joint results in a low contact resistivity of  $\sim 20 \mu\Omega\text{-cm}^2$  and a conversion efficient of  $\sim 6.5\%$  for the  $\text{Mg}_2\text{Si}_{0.3}\text{Sn}_{0.7}$  single-leg device is achieved at a temperature difference of  $\sim 290$  K. Long-term measurements of the device at a hot-side temperature of 600 K reveal that the performance remains nearly invariable as time further increases, which suggests that the FeSi layer retards the chemical reaction/diffusion.

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## 1. Introduction

The majority of energy production and conversion processes are based on thermal engineering, which often results in significant carbon emissions. In the pursuit of sustainable development and carbon neutrality, thermoelectric generators with their advantages of zero emissions and silent operation, stand out as a highly promising green technology [1–3]. The efficiency and power output of the generators are contingent upon the performance of thermoelectric materials, which is determined by the dimensionless figure of merit  $zT = S^2T/\rho(\kappa_E + \kappa_L)$  and the power factor  $\text{PF} = S^2/\rho$ , respectively ( $S$ ,  $\rho$ ,  $T$ ,  $\kappa_E$  and  $\kappa_L$  are the Seebeck coefficient, electrical resistivity, absolute temperature, electronic and thermal conductivities, respectively) [4,5].

So far research efforts concerning materials have primarily focused on enhancing the performance of existing thermoelectric

materials and uncovering high-performance novel thermoelectric candidates. Band convergence, which involves increasing the band degeneracy ( $N_v$ ), has emerged as a prominent strategy for enhancing both PF and  $zT$ , enabling breakthroughs in a variety of thermoelectric materials, including PbTe [6], GeTe [7], SnTe [8], SnSe [9], CoSb<sub>3</sub> [10], (Bi,Sb)<sub>2</sub>Te<sub>3</sub> [11],  $\text{Mg}_2(\text{Si},\text{Sn})$  [12], half-Heusler [13] and Zintl phases [14]. Alternatively, the introduction of diverse defects to further scatter phonons and thereby reducing  $\kappa_L$  [15–17], acts as an indispensable pathway for maximizing the  $zT$ . Furthermore, the features of complex crystal structure, soft chemical bonding and intrinsic vacancy generally accompany with an inherently low  $\kappa_L$ . These characteristics serve as a guiding principle for exploring novel high-performance thermoelectric materials, such as argyrodite compounds [18,19],  $\text{Cu}_2\text{SnSe}_4$  [20,21] and  $\text{Ag}_5\text{Te}_3$  [22].

Advancements in material performance have increased the demand for fabricating efficient and sustainable thermoelectric devices. Interfacial contacts between thermoelectric materials and electrodes, characterized by low electrical conductivity, high thermal conductivity, strong bonding and thermal stability, play as a critical role in determining the durability of the devices [23–25]. Note that the typical weldable electrodes of Cu and Ag, usually being the efficient dopants in many thermoelectric materials, are reactive to form internal compounds at elevated temperatures and

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thereby result in the invalidation of the devices [26–29]. The implementation of barrier layers has been extensively showcased as a proficient means to hinder chemical diffusion/reaction at the interfaces [30].

Mg<sub>2</sub>Si has attracted widespread attention in the field of thermoelectric applications owing to its low density, non-toxicity, elemental abundance and exceptional thermoelectric performance [31,32]. The controllable manipulation of the conduction band through Mg<sub>2</sub>Sn alloying facilitates an PF of ~42  $\mu\text{W}/(\text{cm}\cdot\text{K}^2)$  and an average  $zT_{\text{ave}}$  of ~1.03 within 300–675 K for Mg<sub>2</sub>Si<sub>0.3</sub>Sn<sub>0.7</sub> alloy with the additional help of  $\kappa_{\text{L}}$ -reduction [33]. These results ensure the achievement of high power output and conversion efficiency for the devices. However, establishing a robust interfacial contact remains a significant challenge due to the pronounced chemical reactivity of Mg and Si elements towards the electrode materials including Cu, Ag and Ni [34–36]. Hence, the quest for a suitable barrier layer that exhibits inertness to both thermoelectric materials and the electrodes, becomes an urgent concern that needs to be addressed immediately.

In this work, transition metal silicides exhibiting metallic conduction behavior are proposed as potential barrier materials. The positive values for the interfacial reaction energy indicate their inertness towards high-performance Mg<sub>2</sub>Si<sub>0.3</sub>Sn<sub>0.7</sub> thermoelectric material, thereby theoretically demonstrating the chemical stability of the interfaces. Further considering the sinterability, a well-bonding Mg<sub>2</sub>Si<sub>0.3</sub>Sn<sub>0.7</sub>/FeSi joint with a low contact resistivity of ~20  $\mu\Omega\cdot\text{cm}^2$  is obtained, even though a small amount of Mg diffusion in FeSi is observed. As a result, a conversion efficiency of 6.5% was realized for the Mg<sub>2</sub>Si<sub>0.3</sub>Sn<sub>0.7</sub> single-leg device at a temperature difference of ~290 K.

## 2. Experimental section

Polycrystalline Mg<sub>2.03</sub>(Si<sub>0.3</sub>Sn<sub>0.7</sub>)<sub>0.993</sub>Bi<sub>0.007</sub> samples were synthesized by melting stoichiometric high-purity (>99.99%) elements (Mg, Si, Sn and Bi) in sealed tantalum tubes in quartz ampoules at 1330 K for 7 h, followed by quenching in cold water and annealing at 973 K for 72 h. The resulting ingots were manually ground into fine powders for phase composition analysis using X-ray diffraction (XRD) and pellet preparation through hot-pressing. Dense pellets (>98%) with a diameter of ~12 mm were sintered for transport property measurements by hot pressing at 973 K for 60 min under a uniaxial pressure of ~110 MPa.

Transport properties of the Hall coefficient ( $R_{\text{H}}$ ), resistivity ( $\rho$ ) and Seebeck coefficient ( $S$ ) were simultaneously measured under helium (He) atmosphere. The  $R_{\text{H}}$  and  $\rho$  were measured using the Van der Pauw method. The  $S$  was determined from the slope of thermopower versus temperature difference within the range of 0–5 K. Thermal diffusivity ( $D$ ) was measured using the laser flash technique, and thermal conductivity ( $\kappa$ ) was determined by  $\kappa = dC_{\text{p}}D$ , where  $d$  is the density measured using the mass and geometric volume and the specific heat ( $C_{\text{p}}$ ) was measured using a differential scanning calorimetry (DSC). The measurement uncertainties of  $R_{\text{H}}$ ,  $\rho$ ,  $S$  and  $D$  were about 5%.

FeSi ingots were synthesized by the arc melting of stoichiometric high-purity (>99.99%) elements (Fe and Si), which were then ground into powders using a high-energy ball mill at 500 r/min for 12 h. The bulks of Cu/FeSi/Mg<sub>2.03</sub>(Si<sub>0.3</sub>Sn<sub>0.7</sub>)<sub>0.993</sub>Bi<sub>0.007</sub>/FeSi/Cu were fabricated by one-step hot pressing using powders of FeSi, Cu and Mg<sub>2.03</sub>(Si<sub>0.3</sub>Sn<sub>0.7</sub>)<sub>0.993</sub>Bi<sub>0.007</sub>. The process was performed at a temperature of 933 K under a uniaxial pressure of ~110 MPa for 60 min. The bulks were then cut into the legs with size of ~1.3 mm  $\times$  1.3 mm  $\times$  5.5 mm for the measurements of interfacial contact resistance ( $R_{\text{c}}$ ) and efficiency ( $\eta$ ), and the estimation of thermal stability after aging at 550 K for different times.

The  $R_{\text{c}}$  was measured using the four-probe technique. The  $\eta$  of the single-leg devices was measured by a home-made efficiency system, where the legs were loaded between the heater and the heat-flow meter using liquid metals. Two K-type thermocouples, labeled as  $T_1$  and  $T_2$ , were embedded at two sides of the leg to measure both the temperature difference and the output voltage. The copper bar (cross-sectional area of 3 mm  $\times$  3 mm) was used as a heat-flow meter and two K-type thermocouples ( $T_3$  and  $T_4$ ) with a small diameter of 0.06 mm were embedded to determine the temperature difference. The output current was measured through the metal heater block and heat-flow meter.

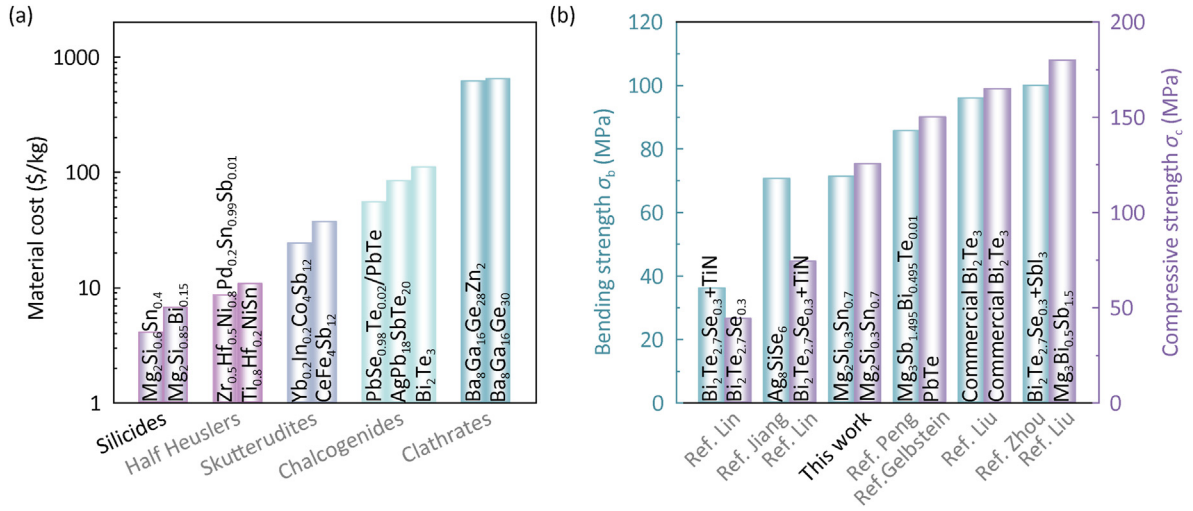
Microstructures and compositions were analyzed using a scanning electron microscope (SEM) equipped with an energy dispersive spectrometer (EDS). Optical reflectance was measured by a Fourier transform infrared spectrometer equipped with a diffuse reflectance attachment. Samples with the size of 2.5 mm  $\times$  1.0 mm  $\times$  10.0 mm, 3 mm  $\times$  3 mm  $\times$  6 mm were used for three-point bending and compressive tests by a micro-computer controlled electronic universal test machine with a loading rate of 0.03 mm/min and 0.5 mm/min, respectively.

## 3. Results and discussions

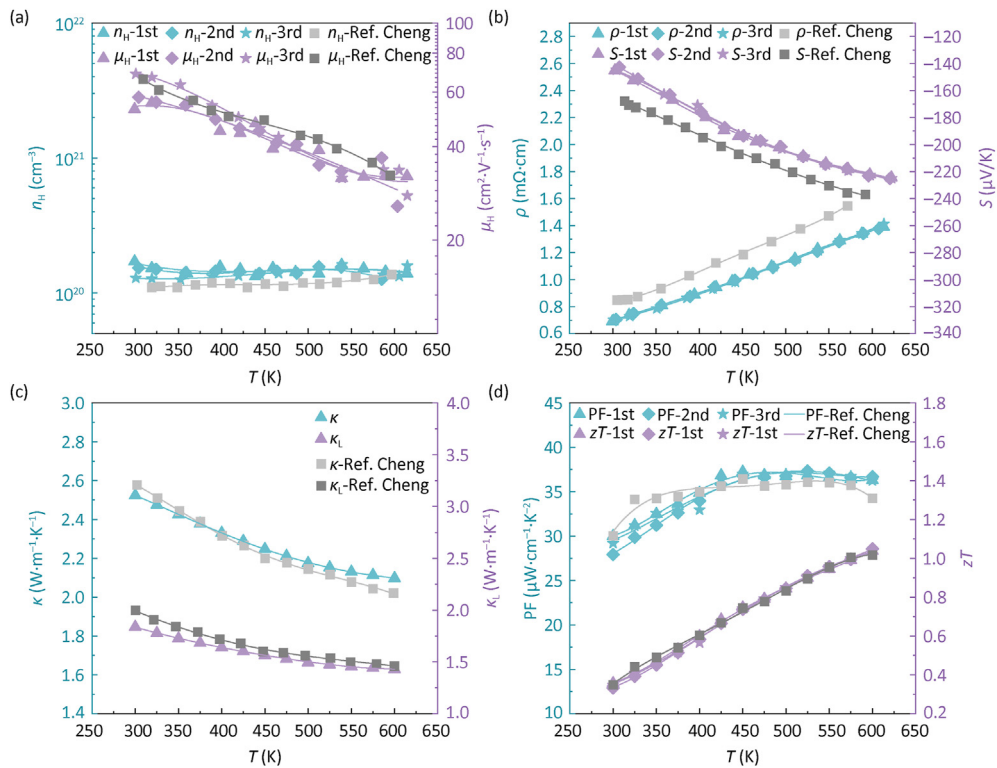
Thermoelectric technique as a sustainable remedy for the energy crisis and environmental issues, proposes the demand for low cost and eco-friendly thermoelectric materials. Non-toxic Mg<sub>2</sub>Si<sub>0.3</sub>Sn<sub>0.7</sub> not only possesses exceptional thermoelectric performance [37], but also boasts the most cost-effective nature among the existing n-type thermoelectric materials [38] (Fig. 1a). Moreover, this compound exhibits mechanical properties comparable to those of the renowned high-performance thermoelectric materials [39–45], as shown in Fig. 1b and Fig. S1. All these results prompt this work to be dedicated to search for effective barrier materials to promote practical applications of Mg<sub>2</sub>Si<sub>0.3</sub>Sn<sub>0.7</sub>-based thermoelectric devices.

The XRD pattern of Mg<sub>2.03</sub>(Si<sub>0.3</sub>Sn<sub>0.7</sub>)<sub>0.993</sub>Bi<sub>0.007</sub> is shown in Fig. S2a, suggesting the formation of a single phase. This is further confirmed by the absence of impurities and the homogeneous elemental distribution as revealed by SEM observation and the corresponding EDS analysis (Fig. S2c). The optical band gap ( $E_{\text{g}}$ ) for the obtained material is estimated to be ~0.41 eV (Fig. S2b), which is in well agreement with the literature result (~0.46 eV)<sup>33</sup>.

The transport properties for Mg<sub>2.03</sub>(Si<sub>0.3</sub>Sn<sub>0.7</sub>)<sub>0.993</sub>Bi<sub>0.007</sub> are shown in Fig. 2. The obtained sample in this work displays a Hall carrier concentration ( $n_{\text{H}}$ ) of  $\sim 1.4 \times 10^{20} \text{ cm}^{-3}$ , approaching its maximum [33], and a Hall mobility ( $\mu_{\text{H}}$ ) of ~60  $\text{cm}^2/(\text{V}\cdot\text{s})$  (Fig. 2a). As shown in Fig. 2b, the increases in both resistivity and Seebeck coefficient with increasing temperature illustrate the degenerate conduction behavior, which is in accordance with the Hall measurement results. The total thermal conductivity ( $\kappa$ , Fig. 2c) is calculated using the measured  $C_{\text{p}}$  (Fig. S3a). The determination of  $\kappa_{\text{L}}$  entails subtracting the electronic contribution ( $\kappa_{\text{E}}$ ), which is dictated by the Wiedemann-Franz law ( $\kappa_{\text{E}} = LT/\rho$ ), from the overall thermal conductivity ( $\kappa$ ) (Fig. 2c). Here, the Lorentz factor ( $L$ ) is ascertained using the single parabolic band (SPB) model, with acoustic phonon scattering being taken into account. As a result, a PF higher than ~37  $\mu\text{W}/(\text{cm}\cdot\text{K}^2)$  and a peak  $zT$  of ~1.0 are attained here. All the transport properties are comparable to those of the reported Mg<sub>2</sub>Si<sub>0.7</sub>Sn<sub>0.3</sub>-based thermoelectric material with a similar  $n_{\text{H}}$  [33]. Moreover, the repeated measurements elucidate the stability of the material when the temperature is lower than 600 K. When further compared to the n-type thermoelectric materials with high-performance in the temperature range of 300–600 K (Fig. 3), the Mg<sub>2</sub>Si<sub>0.7</sub>Sn<sub>0.3</sub> exhibits a leading  $PF_{\text{ave}}$ , ensuring superior power output of the related thermoelectric



**Fig. 1.** Cost [38] (a) and mechanical properties [39–45] (b) for  $\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})_{0.993}\text{Bi}_{0.007}$  with a comparison to those of ever-reported n-type thermoelectric materials.

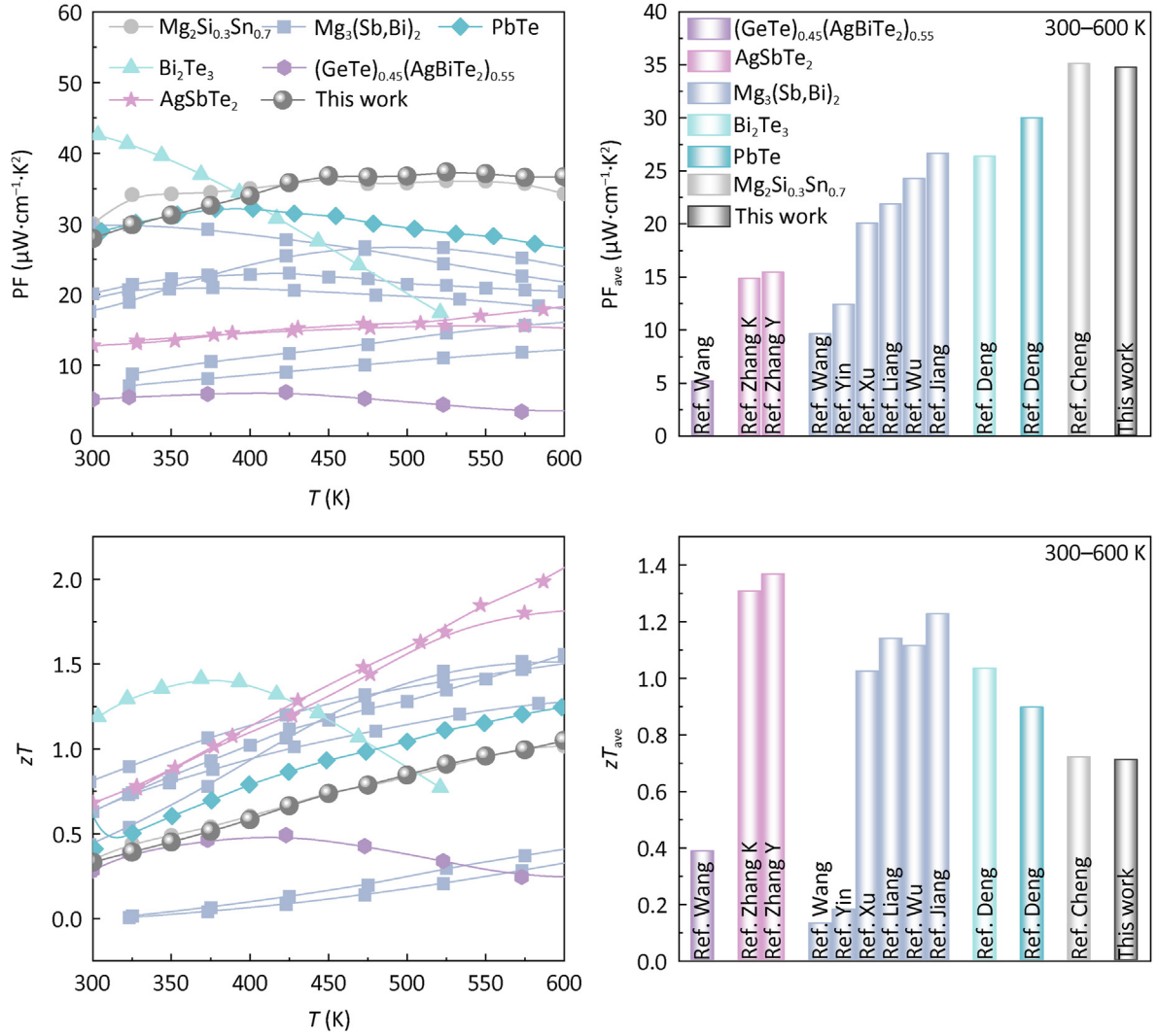


**Fig. 2.** Temperature dependent Hall carrier concentration ( $n_H$ ) and Hall mobility ( $\mu_H$ ) (a), resistivity ( $\rho$ ) and Seebeck coefficient ( $S$ ) (b), total ( $\kappa$ ) and lattice ( $\kappa_L$ ) thermal conductivities (c) and power factor (PF) and figure of merit ( $zT$ ) (d) for  $\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})_{0.993}\text{Bi}_{0.007}$  with a comparison to those of literatures [33].

devices. However, its average  $zT_{\text{ave}}$  is found to be lower than that of  $\text{AgSbTe}_2$ - [1,55],  $\text{Mg}_3(\text{Sb}, \text{Bi})_2$ - [46–51],  $\text{Bi}_2\text{Te}_3$ - [53], and  $\text{PbTe}$ -based [54] thermoelectric materials.

In addition to the superior thermoelectric performance, the robust interfacial contact also acts as a crucial factor in determining the performance and durability of the devices. Owing to the chemical activity of Mg and Si, the transition metal silicides including MnSi, FeSi, CoSi and NiSi that exhibit metallic conduction behavior are considered as potential barrier materials here. The interfacial reaction energy ( $E_{\text{IR}}$ ) between  $\text{Mg}_2\text{Si}/\text{Mg}_2\text{Sn}$  and these

silicides is calculated based on their formation energy at 0 K, which is obtained by the first-principles calculations (Tables S1–S2). The formation energy at 0 K serves as a straightforward and rapid indication on the reactivity of the considered compounds, but the calculation of Gibbs free energy needs to be done for accurate predictions. As shown in Fig. 4a, the positive values of the calculated reaction energy suggest the inertness of the barrier materials with respect to  $\text{Mg}_2\text{Si}$  and  $\text{Mg}_2\text{Sn}$ . The formation energy between FeSi and  $\text{Mg}_2\text{Sn}$  exhibits the highest positive value, indicating that FeSi can be prioritized as the barrier layer for device preparation



**Fig. 3.** Comparison of temperature-dependent and average PF (a, b) and  $zT$  (c, d) for  $\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})_{0.993}\text{Bi}_{0.007}$  to those of the ever-reported n-type thermoelectric materials [1,33,46–55].

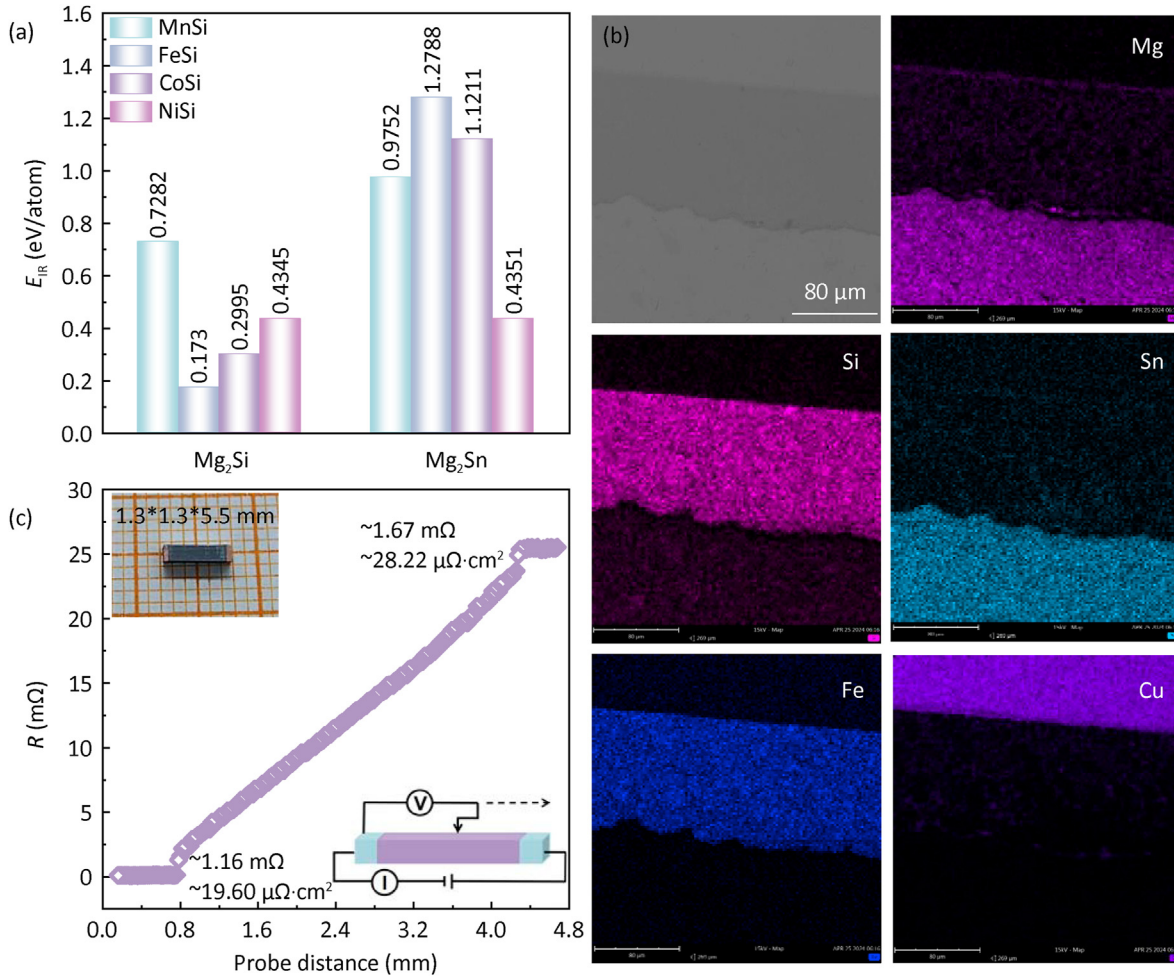
and research. For FeSi, the formation energy and the Gibbs free energy are both positive due to the negative entropy difference, thus inertness at all temperatures is expected. Additionally, under suitable fabrication conditions, other silicides may also serve as potential barrier layers for further investigation.

The strong bonds that facilitate excellent electrical and thermal conductivity between thermoelectric material and electrode is imperative for the thermoelectric devices. The successful fabrication of  $\text{Cu}/\text{FeSi}/\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})_{0.993}\text{Bi}_{0.007}$  bulks via one-step hot pressing further drives the current work to concentrate on the thermal stability of FeSi (Fig. S3b) as the barrier layer. The schematic of the bulk preparation is shown in Fig. S4a. The legs with a size of  $1.3\text{ mm} \times 1.3\text{ mm} \times 5.5\text{ mm}$  are cut from the bulks for interface characterization, and interfacial contact resistance and conversion efficiency measurements. The specific interfaces are characterized by the SEM observation and EDS analysis, as shown in Fig. 4b. The boundaries without voids illustrate the well-established bonding of  $\text{Cu}/\text{FeSi}$  and  $\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})_{0.993}\text{Bi}_{0.007}/\text{FeSi}$  joints. The chemical inertness is reliably demonstrated by the impeded diffusion or reaction. The aging of the legs is carried out at 550 K to further identify the element diffusions. The SEM

observations (Fig. S5) qualitatively verify that the introduction of FeSi barrier layer remains a passivation strategy for extending the service life of the  $\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})$ -based device. The electrical contact resistance ( $R_c$ ) for the joint is measured by a four-probe technique and the measurement schematic is shown in the inset of Fig. 4c. The  $R_c$  is found to be 1.16 m $\Omega$  and 1.67 m $\Omega$  at both ends of the leg, which correspond to the electrical contact resistivities ( $\rho_c$ ) of 19.6  $\mu\Omega\cdot\text{cm}^2$  and 28.2  $\mu\Omega\cdot\text{cm}^2$ , respectively. The obtained  $\rho_c$  is found to be lower than that of  $\text{Mg}_2\text{Cu}$  barrier material [33], which firmly reveals FeSi as a promising barrier candidate for  $\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})_{0.993}\text{Bi}_{0.007}$  thermoelectric.

The single-leg device with a size of  $1.3\text{ mm} \times 1.3\text{ mm} \times 5.5\text{ mm}$  is utilized for measuring the power output ( $P$ ) and efficiency ( $\eta$ ). Schematic of the measurement is shown in Fig. S4b and the corresponding results are shown in Fig. 5. The cold side temperature is fixed at 300 K to measure the performance of the devices. The output voltage ( $V$ ) versus current ( $I$ ) for  $\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})_{0.993}\text{Bi}_{0.007}$  single-leg device with FeSi barrier layers and Cu electrodes under different  $\Delta T$  is shown in Fig. 5a. The open circuit voltage ( $V_{oc}$ ) and the internal resistance ( $R_{in}$ ) can be determined by the intercepts and slopes of the linearly fitted  $V$ – $I$  curves, respectively. The rise in





**Fig. 4.** Calculated interfacial reaction energy ( $E_{IR}$ ) for Mg<sub>2</sub>Si and Mg<sub>2</sub>Sn thermoelectrics with the potential barrier materials (a). SEM image and corresponding EDS mapping (b) and room temperature interfacial contact resistance measured using a line scanning technique (c) for Mg<sub>2.03</sub>(Si<sub>0.3</sub>Sn<sub>0.7</sub>)<sub>0.993</sub>Bi<sub>0.007</sub>/FeSi/Cu joint.

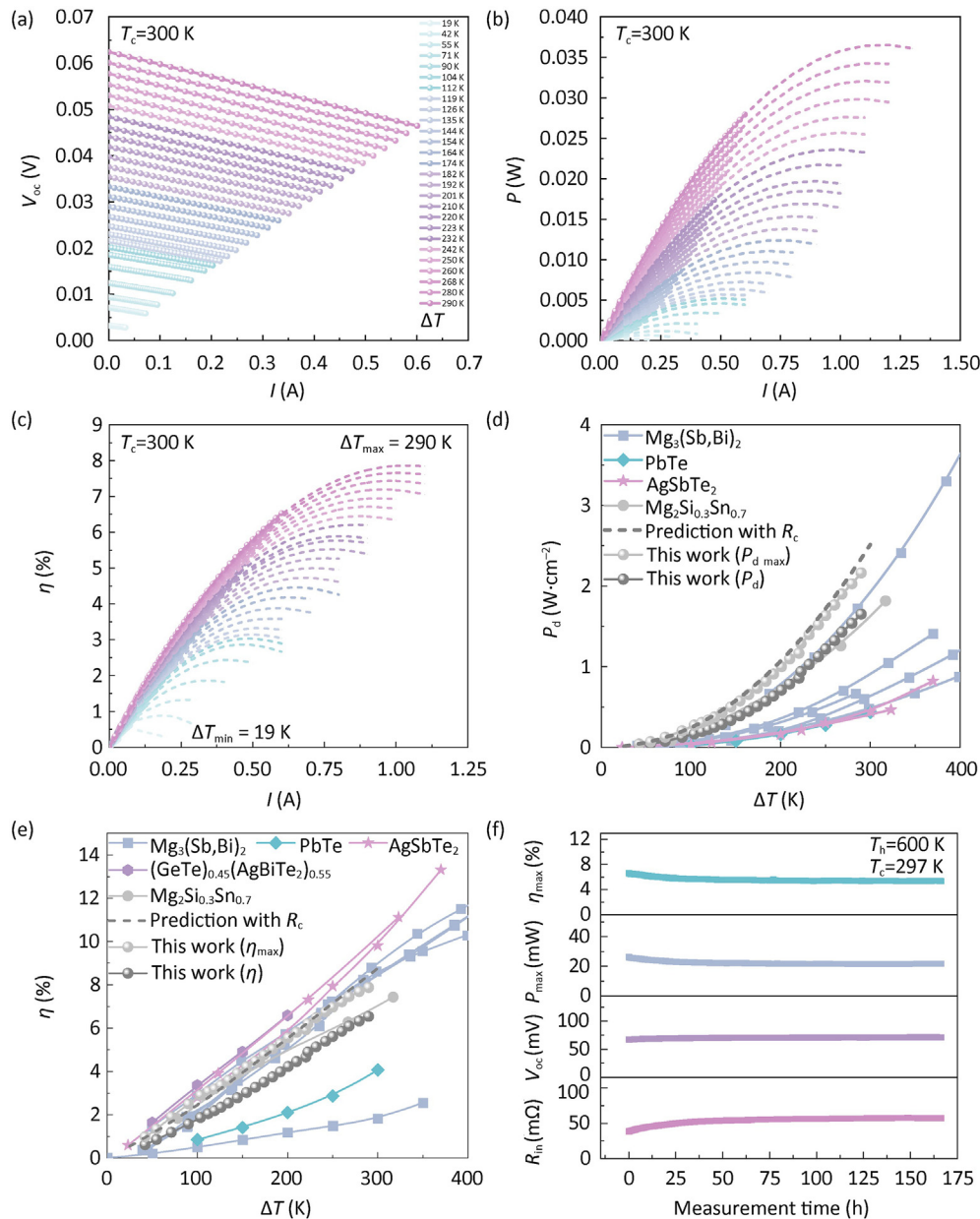
$V_{OC}$  with increasing  $\Delta T$  is attributed to the increased Seebeck coefficient at elevated temperatures. Moreover, the measured  $V_{OC}$  is close to the prediction based on the temperature-dependent Seebeck coefficient of thermoelectric material, as shown in Fig. S6a. While the  $R_{in}$  is found to be larger than that predicted using the material's resistivity (Fig. S6b), this discrepancy stems from the presence of interfacial contact resistance.

The  $V_{OC}$ ,  $P$ , and  $\eta$  under different temperature gradients ( $\Delta T$ ) are presented in Fig. 5a–c, respectively. A  $P$  of up to 28 mW is achieved at a  $\Delta T$  of  $\sim 290$  K (Fig. 5b), which corresponds to a power density ( $P_d$ ) of 1.65 W/cm<sup>2</sup>. Moreover, a conversion efficiency  $\eta$  of  $\sim 6.5\%$  is realized under  $\Delta T = 290$  K (Fig. 5c). Since the  $R_{in}$  for the single-leg device is smaller than the minimal  $R_{load}$  of the measurement system, the measured  $P$  and  $\eta$  are lower than their maximum in this work, where the maximum  $P_{max}$  of 36.5 mW and  $\eta_{max}$  of 7.9% are obtained through the extrapolation based on the measured results at each temperature gradient (Fig. 5b–c). The  $P_{max}$  and  $\eta_{max}$  extrapolated from the measured data are in agreement with the predictions based on the measured material and interface properties (Figs. S6c and S6d, where  $R_c$  is about 2.83 m $\Omega$ ). The predicted maximal  $P_d$  (Fig. 5d) and  $\eta_{max}$  for Mg<sub>2.03</sub>(Si<sub>0.3</sub>Sn<sub>0.7</sub>)<sub>0.993</sub>Bi<sub>0.007</sub> single-leg device in this work ranks the highest among the reported n-type thermoelectric single-leg devices at temperature below 600 K, while the predicted  $\eta_{max}$  (Fig. 5e) is slight lower than that of them.

These findings underline the potential of this material as a prominent n-type component for the thermoelectric generators to harness low-grade heat.

Meanwhile, an initial deterioration of  $\eta_{max}$  and  $P_{max}$  is observed during the long-term stability measurements at a hot-side temperature of 600 K as shown in Fig. 5f. The performance degradation can be attributed to the loss of Mg and Sn as well as the trace diffusion of Cu [34] due to the limited effectiveness of the FeSi barrier layer, leading to increased resistances at the interface and within the thermoelectric material. Consequently, optimizing the interface between the electrode and the Mg<sub>2</sub>(Si, Sn)-based thermoelectric material to enhance its thermal stability warrants further investigation.

The long-term measurements for the single-leg device are conducted at a hot-side temperature of 600 K to illustrate the thermal stability, and the corresponding results are shown in Fig. 5f. The deteriorations in  $\eta_{max}$  and  $P_{max}$  are observed initially for the single-leg device measured at 600 K, which then remain nearly constant. The degraded performance was associated with Mg and Sn loss as well as trace Cu diffuse [34], leading to the increased resistances of interface and thermoelectric material. Therefore, the optimization of the interface between electrodes and Mg<sub>2</sub>(Si, Sn)-based thermoelectric materials so as to enhance their thermal stability merits further exploration.



**Fig. 5.** Output voltage (a), output power (b) and conversion efficiency (c) versus current (the solid lines are the measured curves, and the dashed lines are the extrapolated curves), power density (d) and maximum conversion efficiency (e) versus temperature-difference for  $\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})_{0.993}\text{Bi}_{0.007}$  single-leg device with a comparison to the prediction and the literature results [1,33,46–55]. Maximum efficiency ( $\eta_{\max}$ ), maximum output power ( $P_{\max}$ ), open circuit voltage ( $V_{\text{oc}}$ ) and internal resistance ( $R_{\text{in}}$ ) for the device during the long-term measurements at the hot side temperature of 600 K (f).

#### 4. Conclusions

In summary, based on the calculated interfacial reaction energy and sinterability, FeSi is proposed as a potential barrier candidate for  $\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})_{0.993}\text{Bi}_{0.007}$  thermoelectric material. The firmly established bonding between the barrier layer and the thermoelectric material facilitates a low contact resistivity of  $\sim 20 \mu\Omega\text{-cm}^2$ , enabling a superior power output of  $\sim 28 \text{ mW}$  and an exceptional conversion efficiency of 6.5% at a temperature difference of 290 K. Although trace diffusions of Mg, Sn and Cu are observed, the device performance remains nearly constant as time increase for the long-term measurements at a hot-side temperature of 600 K, which indicates that the FeSi layer retards the chemical reaction/diffusion in  $\text{Mg}_{2.03}(\text{Si}_{0.3}\text{Sn}_{0.7})_{0.993}\text{Bi}_{0.007}$  single-leg device.

#### CRediT authorship contribution statement

**Shanshan Hu:** Writing – original draft, Investigation. **Chen Huang:** Software, Data curation. **Changyuan Li:** Software, Methodology. **Long Yang:** Methodology. **Zhiwei Chen:** Formal analysis. **Baisheng Sa:** Formal analysis. **Wen Li:** Writing – review & editing, Supervision. **Yanzhong Pei:** Supervision, Conceptualization.

#### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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## Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.jmat.2025.101044>.

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