# Adjoint formulation for manifold-reduced system

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#### Original governing equation

We refer to the original governing equation as a priori projected system:

$$\frac{d\mathbf{x}}{dt} = \mathbf{P}(\mathbf{x}; \theta) \cdot \mathbf{F}(\mathbf{x}; \theta)$$

$$\mathbf{P}(\mathbf{x}; \theta) = \mathbf{I} - \mathbf{V}_f \mathbf{U}_f$$

$$\mathbf{J} = \nabla_x \mathbf{F} = \begin{bmatrix} \mathbf{V}_s & \mathbf{V}_f \end{bmatrix} \begin{bmatrix} \Lambda_{ss} & 0 \\ 0 & \Lambda_{ff} \end{bmatrix} \begin{bmatrix} \mathbf{U}_s \\ \mathbf{U}_f \end{bmatrix}$$
(1)

where  $\theta \in \mathbb{R}^{N_c}$  is the control parameter. For other notations, refer to the original document.

## Observable and its sensitivity

We have the observable as a functional of state variable  $\mathbf{x}$ :

$$\mathcal{O}[\mathbf{x}] = \int_0^T o(\mathbf{x}) dt,$$

and we would like to measure its sensitivity to control parameters,

$$\nabla_{\theta} \mathcal{O} = \int_{0}^{T} \nabla_{x} o \cdot \nabla_{\theta} \mathbf{x} \, dt + \int_{0}^{T} \nabla_{\theta} o \, dt$$
$$= \langle \nabla_{x} o, \nabla_{\theta} \mathbf{x} \rangle + \int_{0}^{T} \nabla_{\theta} o \, dt,$$
(2)

where the inner product is defined on  $\mathbb{R}^N$ ,

$$\langle \mathbf{a}, \mathbf{b} \rangle = \int_0^T a_i b_i \ dt$$

with Einstein notation for indices.

## Sensitivity equation

To obtain the sensitivity (2), the sensitivity of the solution  $\nabla_{\theta} \mathbf{x}$  needs to be computed. It can be obtained by solving the linearized equation from (1). From now on the equations are expressed in index notation to avoid the ambiguity.

- i, j, k: the index on  $\mathbb{R}^N$  space
- c: the index on control space  $\mathbb{R}^{N_c}$
- l: the index on fast manifold space  $\mathbb{R}^{N_f}$

$$\frac{d}{dt}\partial_{c}x_{i} = \partial_{c}\left(P_{ij}F_{j}\right)$$

$$= \partial_{k}\left(P_{ij}F_{j}\right)\partial_{c}x_{k} + \partial_{c}\left(P_{ij}F_{j}\right)$$

$$= \left[\partial_{k}P_{ij} \cdot F_{j} + P_{ij} \cdot \partial_{k}F_{j}\right]\partial_{c}x_{k} + \partial_{c}P_{ij}F_{j} + P_{ij}\partial_{c}F_{j}$$
(3)

$$\partial_k P_{ij} = -\partial_k V_{il} U_{lj} - V_{il} \partial_k U_{lj}$$
  
$$\partial_c P_{ij} = -\partial_c V_{il} U_{lj} - V_{il} \partial_c U_{lj}$$
(4)

# Adjoint formulation

We define a constraint functional  $\mathcal{H}$  as the inner product of adjoint variable and (3),

$$\mathcal{H} = \left\langle \mathbf{x}^{\dagger}, \frac{d}{dt} \partial_c x_i - \left[ \partial_k P_{ij} \cdot F_j + P_{ij} \cdot \partial_k F_j \right] \partial_c x_k - \partial_c P_{ij} F_j - P_{ij} \partial_c F_j \right\rangle$$

$$= 0$$
(5)

Since  $\mathcal{H}$  is always equivalent to 0 as (3) holds, we add (5) to the sensitivity (2),

$$\nabla_{\theta} \mathcal{O} = \langle \nabla_x o, \nabla_{\theta} \mathbf{x} \rangle + \int_0^T \nabla_{\theta} o \ dt = \langle \nabla_x o, \nabla_{\theta} \mathbf{x} \rangle + \mathcal{H} + \int_0^T \nabla_{\theta} o \ dt$$

which can be expressed in index-wise notation,

$$\nabla_{\theta} \mathcal{O} = \langle \nabla_{x} o, \nabla_{\theta} \mathbf{x} \rangle + \mathcal{H} + \int_{0}^{T} \nabla_{\theta} o \, dt$$

$$= \langle \partial_{i} o, \partial_{c} x_{i} \rangle + \left\langle x_{i}^{\dagger}, \frac{d}{dt} \partial_{c} x_{i} \right\rangle - \left\langle x_{i}^{\dagger}, [\partial_{k} P_{ij} \cdot F_{j} + P_{ij} \cdot \partial_{k} F_{j}] \partial_{c} x_{k} \right\rangle$$

$$- \left\langle x_{i}^{\dagger}, \partial_{c} P_{ij} F_{j} \right\rangle - \left\langle x_{i}^{\dagger}, P_{ij} \partial_{c} F_{j} \right\rangle + \int_{0}^{T} \partial_{c} o \, dt$$

Our purpose of adjoint formulation is to avoid calculation of  $\partial_c x_k$ . The adjoint formulation is required for first two terms of  $\mathcal{H}$ :

$$\bullet \left\langle x_i^{\dagger}, \frac{d}{dt} \partial_c x_i \right\rangle$$

$$\left\langle x_i^{\dagger}, \frac{d}{dt} \partial_c x_i \right\rangle = \int_0^T x_i^{\dagger} \frac{d}{dt} \partial_c x_i \, dt$$

$$= x_i^{\dagger} \partial_c x_i \Big|_0^T - \int_0^T \frac{d}{dt} x_i^{\dagger} \partial_c x_i \, dt$$

$$= x_i^{\dagger} \partial_c x_i \Big|_0^T - \left\langle \frac{d}{dt} x_i^{\dagger}, \partial_c x_i \right\rangle$$

$$\begin{array}{l} \bullet \ \left\langle x_i^\dagger, \left[\partial_k P_{ij} \cdot F_j + P_{ij} \cdot \partial_k F_j\right] \partial_c x_k \right\rangle \\ \\ \left\langle x_i^\dagger, \left[\partial_k P_{ij} \cdot F_j + P_{ij} \cdot \partial_k F_j\right] \partial_c x_k \right\rangle \\ \\ = \int_0^T x_i^\dagger \left[\partial_k P_{ij} \cdot F_j + P_{ij} \cdot \partial_k F_j\right] \partial_c x_k \ dt \\ \\ = \int_0^T x_k^\dagger \left[\partial_i P_{kj} \cdot F_j + P_{kj} \cdot \partial_i F_j\right] \partial_c x_i \ dt \\ \\ = \left\langle \left[\partial_i P_{kj} \cdot F_j + P_{kj} \cdot \partial_i F_j\right] x_k^\dagger, \partial_c x_i \right\rangle \end{aligned}$$

where nothing except the index exchange between i and k has been done, which corresponds to the transpose of the matrix  $\in \mathbb{R}^N \times \mathbb{R}^N$ .

Substituting these two terms, we obtain the dual expression for the sensitivity,

$$\nabla_{\theta} \mathcal{O} = \langle \nabla_{x} o, \nabla_{\theta} \mathbf{x} \rangle + \mathcal{H} + \int_{0}^{T} \nabla_{\theta} o \, dt$$

$$= \langle \partial_{i} o, \partial_{c} x_{i} \rangle + \left\langle x_{i}^{\dagger}, \frac{d}{dt} \partial_{c} x_{i} \right\rangle - \left\langle x_{i}^{\dagger}, [\partial_{k} P_{ij} \cdot F_{j} + P_{ij} \cdot \partial_{k} F_{j}] \partial_{c} x_{k} \right\rangle$$

$$- \left\langle x_{i}^{\dagger}, \partial_{c} P_{ij} F_{j} \right\rangle - \left\langle x_{i}^{\dagger}, P_{ij} \partial_{c} F_{j} \right\rangle + \int_{0}^{T} \partial_{c} o \, dt$$

$$= \langle \partial_{i} o, \partial_{c} x_{i} \rangle - \left\langle \frac{d}{dt} x_{i}^{\dagger}, \partial_{c} x_{i} \right\rangle - \left\langle [\partial_{i} P_{kj} \cdot F_{j} + P_{kj} \cdot \partial_{i} F_{j}] x_{k}^{\dagger}, \partial_{c} x_{i} \right\rangle$$

$$+ x_{i}^{\dagger} \partial_{c} x_{i} \Big|_{0}^{T} - \left\langle x_{i}^{\dagger}, \partial_{c} P_{ij} F_{j} \right\rangle - \left\langle x_{i}^{\dagger}, P_{ij} \partial_{c} F_{j} \right\rangle + \int_{0}^{T} \partial_{c} o \, dt$$

$$= \left\langle -\frac{d}{dt} x_{i}^{\dagger} - [\partial_{i} P_{kj} \cdot F_{j} + P_{kj} \cdot \partial_{i} F_{j}] x_{k}^{\dagger} + \partial_{i} o, \partial_{c} x_{i} \right\rangle$$

$$+ x_{i}^{\dagger} \partial_{c} x_{i} \Big|_{0}^{T} - \left\langle x_{i}^{\dagger}, \partial_{c} P_{ij} F_{j} \right\rangle - \left\langle x_{i}^{\dagger}, P_{ij} \partial_{c} F_{j} \right\rangle + \int_{0}^{T} \partial_{c} o \, dt$$

First term in the equation above is now the new constraint functional, i.e. the adjoint equation, and the other three terms are equivalent to the sensitivity  $\nabla_{\theta}\mathcal{O}$ . As long as the adjoint equation equals to 0,  $\partial_c x_i$  needs not be computed. Regarding the second term  $x_i^{\dagger} \partial_c x_i$ , we don't really have the information about  $\partial_c \mathbf{x}$  at T, nor use the final condition of  $\mathbf{x}$  as a control parameter. This provides us with the final condition for  $\mathbf{x}^{\dagger}$ ,

$$\mathbf{x}^{\dagger} = 0$$
 at  $t = T$ 

Therefore, the sensitivity  $\nabla_{\theta} \mathcal{O}$  can be computed by solving the following adjoint system:

$$\frac{d}{dt}x_{i}^{\dagger} = -\left[\partial_{i}P_{kj} \cdot F_{j} + P_{kj} \cdot \partial_{i}F_{j}\right]x_{k}^{\dagger} + \partial_{i}o$$

$$\partial_{k}P_{ij} = -\partial_{k}V_{il}U_{lj} - V_{il}\partial_{k}U_{lj}$$

$$\mathbf{x}^{\dagger} = 0 \qquad \text{at } t = T$$

$$\partial_{c}\mathcal{O} = -x_{i}^{\dagger}\partial_{c}x_{i}\Big|_{t=0} - \left\langle x_{i}^{\dagger}, \partial_{c}P_{ij}F_{j}\right\rangle - \left\langle x_{i}^{\dagger}, P_{ij}\partial_{c}F_{j}\right\rangle + \int_{0}^{T}\partial_{c}o \, dt$$

$$\partial_{c}P_{ij} = -\partial_{c}V_{il}U_{lj} - V_{il}\partial_{c}U_{lj}$$

#### **Summary**

• Governing equation

$$\frac{d\mathbf{x}}{dt} = \mathbf{P}(\mathbf{x}; \theta) \cdot \mathbf{F}(\mathbf{x}; \theta)$$

$$\mathbf{P}(\mathbf{x}; \theta) = \mathbf{I} - \mathbf{V}_f \mathbf{U}_f$$

$$\mathbf{J} = \nabla_x \mathbf{F} = \begin{bmatrix} \mathbf{V}_s & \mathbf{V}_f \end{bmatrix} \begin{bmatrix} \Lambda_{ss} & 0 \\ 0 & \Lambda_{ff} \end{bmatrix} \begin{bmatrix} \mathbf{U}_s \\ \mathbf{U}_f \end{bmatrix}$$
(6)

• Observable and its sensitivity

$$\mathcal{O}[\mathbf{x}; \theta] = \int_0^T o(\mathbf{x}; \theta) dt$$

$$\nabla_{\theta} \mathcal{O} = \langle \nabla_x o, \nabla_{\theta} \mathbf{x} \rangle + \int_0^T \nabla_{\theta} o \, dt$$
(7)

• Adjoint equation

$$\frac{d}{dt}x_i^{\dagger} = -\left[\partial_i P_{kj} \cdot F_j + P_{kj} \cdot \partial_i F_j\right] x_k^{\dagger} + \partial_i o$$

$$\partial_k P_{ij} = -\partial_k V_{il} U_{lj} - V_{il} \partial_k U_{lj}$$

$$\mathbf{x}^{\dagger} = 0 \qquad \text{at } t = T$$
(8)

- -i, j, k: the index on  $\mathbb{R}^N$  space
- c: the index on control space  $\mathbb{R}^{N_c}$
- l: the index on fast manifold space  $\mathbb{R}^{N_f}$
- Adjoint-based sensitivity

$$\partial_c \mathcal{O} = -x_i^{\dagger} \partial_c x_i \bigg|_{t=0} - \left\langle x_i^{\dagger}, \partial_c P_{ij} F_j \right\rangle - \left\langle x_i^{\dagger}, P_{ij} \partial_c F_j \right\rangle + \int_0^T \partial_c o \, dt$$

$$\partial_c P_{ij} = -\partial_c V_{il} U_{lj} - V_{il} \partial_c U_{lj}$$

$$(9)$$

## Comments on solving the adjoint equation

In solving the adjoint equation (8), we may first think of the same manifold-reduction as we do for the governing equation. That is, we can decompose  $\mathbf{x}^{\dagger}$  into slow and fast manifolds according to the matrix

$$-\left[\partial_i P_{kj} \cdot F_j + P_{kj} \cdot \partial_i F_j\right],\,$$

and reduce the system onto slow manifolds.

Although, this procedure may not be necessary and rather redundant. On this matter you should have a better knowledge, but I guess manifold reduction is usually required for a nonlinear system which is very stiff until it reaches the slow manifolds. On the other hand, the adjoint system (8), although time-variant, it is basically a linear system. Of course I cannot guarantee that its stiffness is always smaller than that of the original nonlinear system. But I hope a direct time-integration for (8) may be possible in an efficient way, but simpler than just following the same decomposition for nonlinear systems.