

Types of AM

- Conventional/Full AM
 - Analog broadcast radio
 - DSB Suppressed-Carrier AM
 - Satellite Communications
 - Single Sideband AM
 - Long distance telephone links
 - Vestigial Sideband AM
 - Analog broadcast TV
 - Quadrature AM
 - PC modem, wireless LAN, digital TV
- } See Section 3.5 on pages 88-91

Conventional AM

- Consider a sinusoidal carrier wave given by $A_c \cos(2\pi f_c t)$.
Let $m(t)$ denote the modulating signal (i.e., message).

The full AM is given by

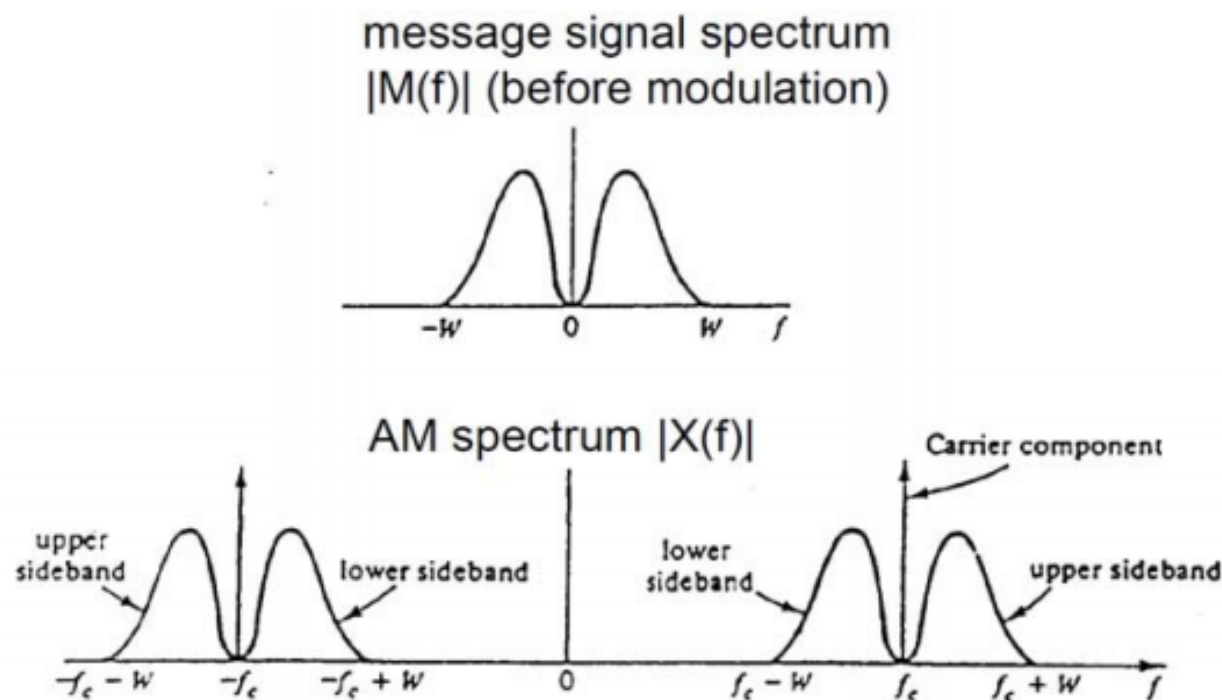
$$\begin{aligned} x(t) &= A_c [1 + \boxed{k_a} m(t)] \cos 2\pi f_c t \\ &= \underbrace{A_c \cos 2\pi f_c t}_{\text{carrier}} + \underbrace{A_c k_a m(t) \cos 2\pi f_c t}_{\text{sidebands}} \end{aligned}$$

Amplitude sensitivity, a constant (1/volt)

- Fourier transform of $x(t)$:

$$\begin{aligned} X(f) &= \frac{A_c}{2} [\delta(f - f_c) + \delta(f + f_c)] \\ &\quad + \frac{k_a A_c}{2} [M(f - f_c) + M(f + f_c)] \end{aligned}$$

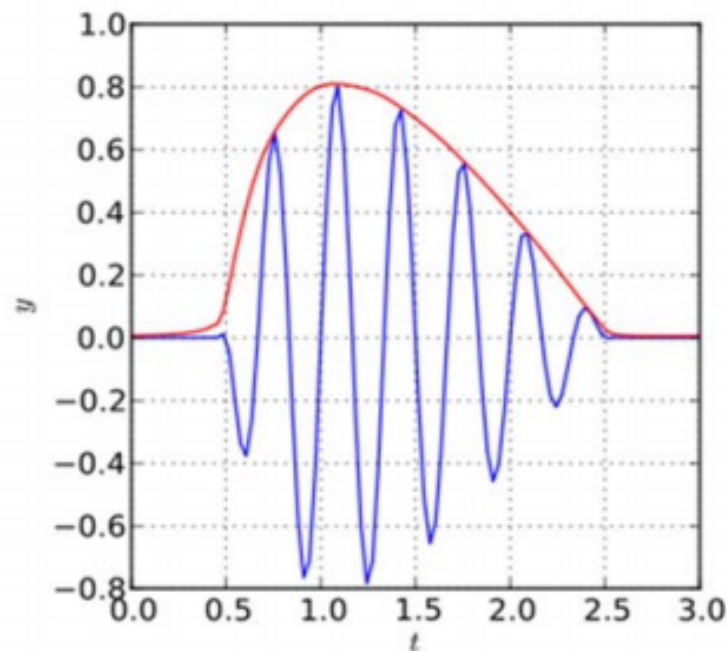
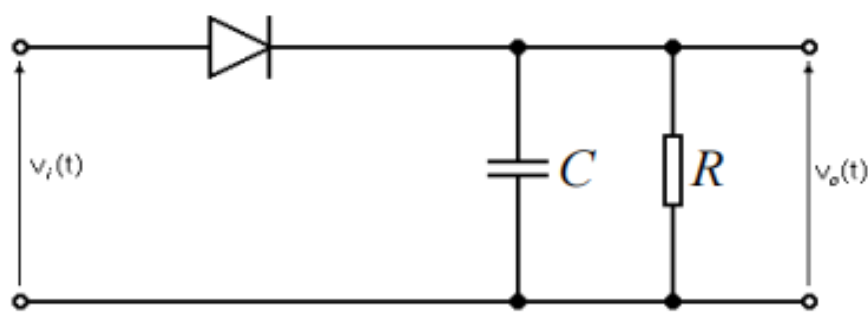
Spectrum of Conventional AM



- Upper sideband and lower sideband are symmetrical.
- $f_c > W$ to ensure the sidebands do not overlap.
- Transmission bandwidth of a conventional AM is exactly twice the message bandwidth W , that is, $2W$.

Envelope Detection

- The simplest form of **envelope detector** is the **diode detector**:

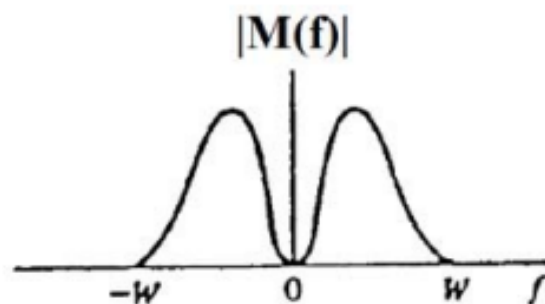


- In order for this diode detector to work, it is required that $\frac{1}{f_c} \ll RC \ll \frac{1}{W}$.

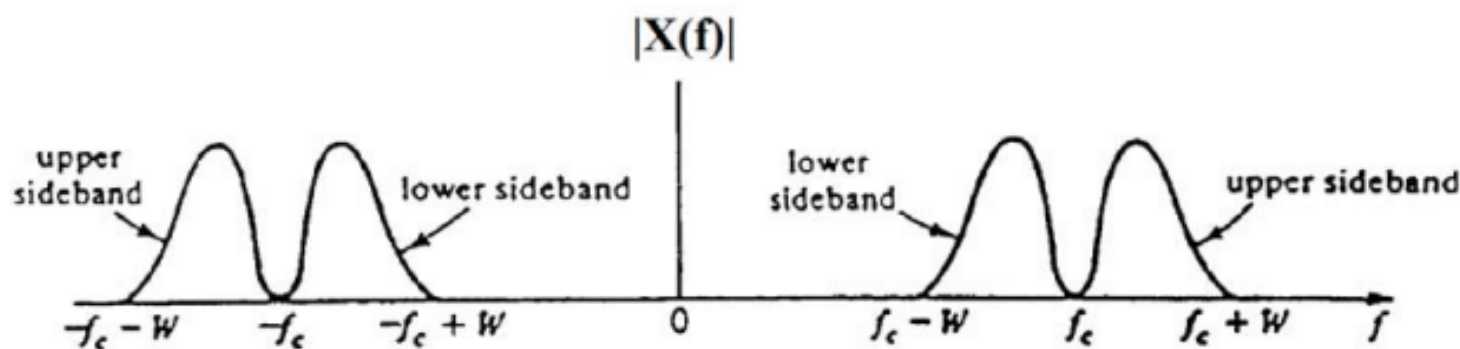
Expression & Spectrum of DSBSC-AM

- The DSBSC AM modulated signal $x(t)$ is
$$x(t) = m(t) \cdot A_c \cos 2\pi f_c t$$
- The signal spectrum is obtained as

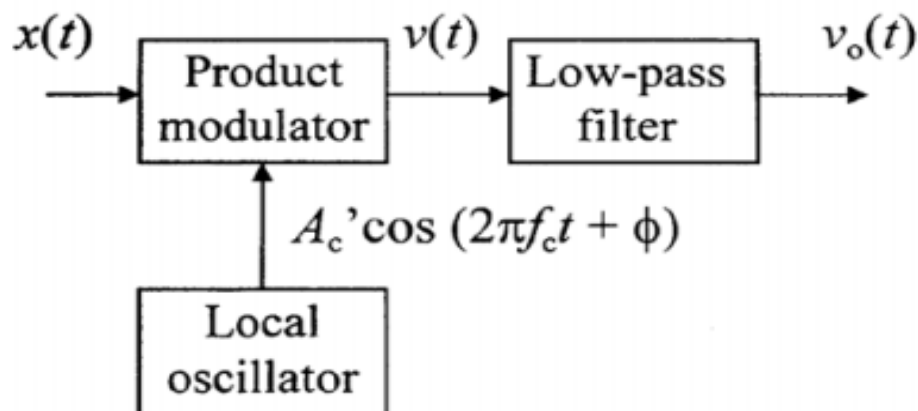
$$X(f) = \frac{A_c}{2} [M(f - f_c) + M(f + f_c)]$$



Note: DSBSC-AM shifts the center freq. from 0 to $\pm f_c$, and doubles the BW, while maintaining the spectral shape



Coherent/Synchronous Demodulation

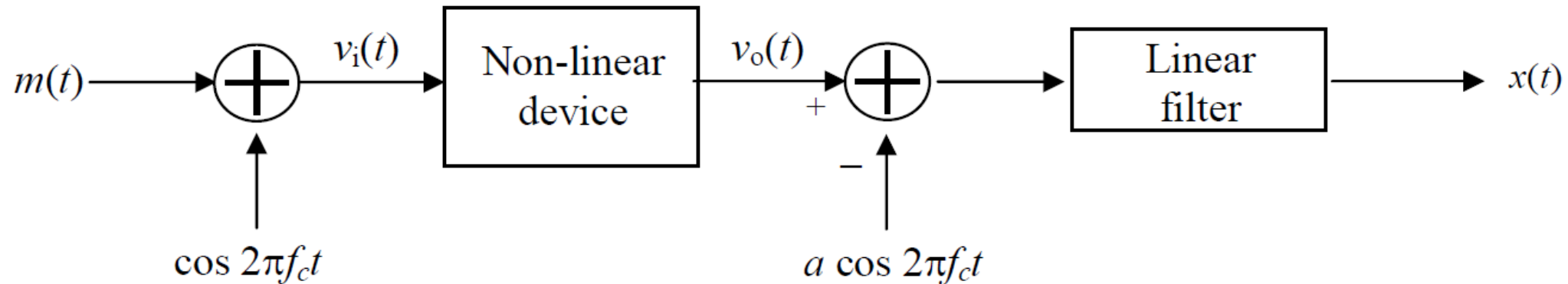


The job of demodulation is to recover the message $m(t)$ from the DSBSC-AM signal $x(t)$.

$$\cos x \cos y = \frac{1}{2} [\cos(x - y) + \cos(x + y)]$$

1. Input (DSBSC): $x(t) = m(t) \cdot A_c \cos 2\pi f_c t$
 2.
$$v(t) = A_c' \cos(2\pi f_c t + \phi) \cdot m(t) \cdot A_c \cos 2\pi f_c t$$
$$= \frac{1}{2} A_c' A_c m(t) \cos \phi + \frac{1}{2} A_c' A_c m(t) \cos(4\pi f_c t + \phi)$$
 3.
$$v_o(t) = \frac{1}{2} A_c' A_c m(t) \cos \phi = \text{constant} \times m(t)$$
- ✓ The output contains a phase error, ϕ . Output = 0 if $\phi = \pm\pi/2$. Output is max if $\phi = 0$, i.e., the local oscillator has the same frequency & phase (**synchronized, coherent**) as the carrier component in the AM signal.

1. The message signal $m(t) = 3 \cos(2\pi 70t) + 4 \sin(2\pi 70t)$ is input to the system shown below to generate a DSBSC-AM signal $x(t)$. Assume that $v_o(t) = a v_i(t) + b v_i^2(t)$ where a and b are constants, and the carrier frequency $f_c \gg 70\text{Hz}$.
- (a) Sketch the amplitude spectrum of the filter input
 - (b) Determine the center frequency and bandwidth of the filter in this modulator
 - (c) Determine the minimum value of f_c permitted for this modulator



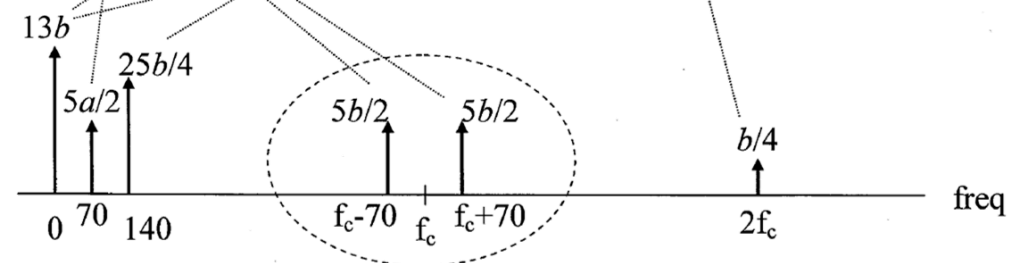
Solution of (a)

$$\begin{aligned}
 v_o(t) &= av_i(t) + bv_i^2(t) \\
 &= a[m(t) + \cos(2\pi f_c t)] + b[m(t) + \cos(2\pi f_c t)]^2 \\
 &= am(t) + bm^2(t) + 2bm(t)\cos(2\pi f_c t) + a\cos(2\pi f_c t) + \underbrace{b\cos^2(2\pi f_c t)}_{\frac{b}{2} + \frac{b}{2}\cos(4\pi f_c t)}
 \end{aligned}$$

$$\begin{aligned}
 m(t) &= 3\cos(2\pi 70t) + 4\sin(2\pi 70t) = 5\cos(2\pi 70t - \theta) \leftarrow \text{from Trigo Table} \\
 m^2(t) &= \frac{25}{2} + \frac{25}{2}\cos(2\pi 140t - 2\theta) \text{ where } \theta = \tan^{-1} \frac{4}{3}
 \end{aligned}$$

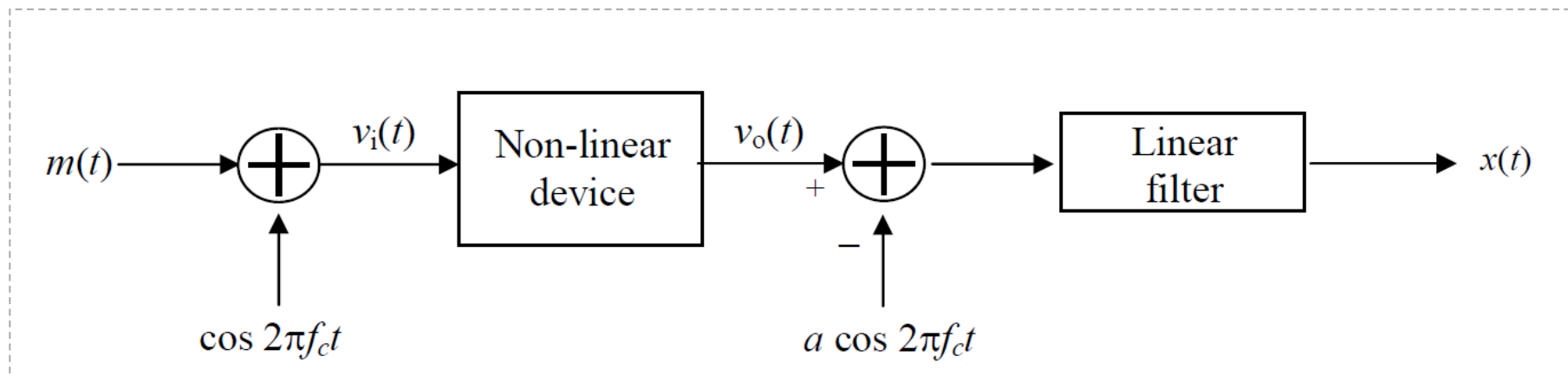
So,

$$\begin{aligned}
 \text{filter input} &= v_o(t) - a\cos(2\pi f_c t) \\
 &= 5a\cos(2\pi 70t - \theta) + \frac{25b}{2} + \frac{25b}{2}\cos(2\pi 140t - 2\theta) \\
 &\quad + 10b\cos(2\pi 70t - \theta)\cos(2\pi f_c t) + \frac{b}{2} + \frac{b}{2}\cos(4\pi f_c t)
 \end{aligned}$$



desired DSBSC-AM signal

傅里叶变换是对称的，所以可以只画单边频谱



Solution of (b)

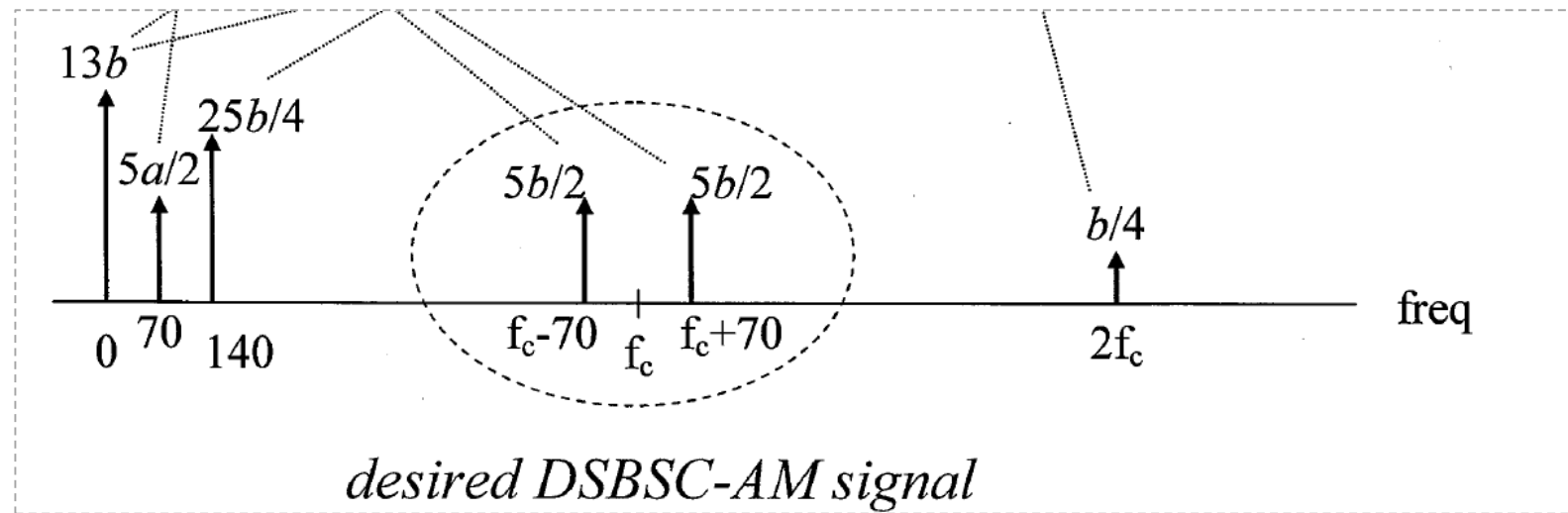
Since the message signal $m(t)$ is a $\cos(2\pi 70t - \theta)$ signal, its DSBSC-AM signal should be the $\cos(2\pi 70t - \theta) \cos(2\pi f_c t)$ term. Hence the linear filter should have center freq = f_c and bandwidth = 140Hz in order to separate it from the other unwanted signal components.

Solution of (c)

From the spectrum of part (a),

$$f_c - 70 > 140$$

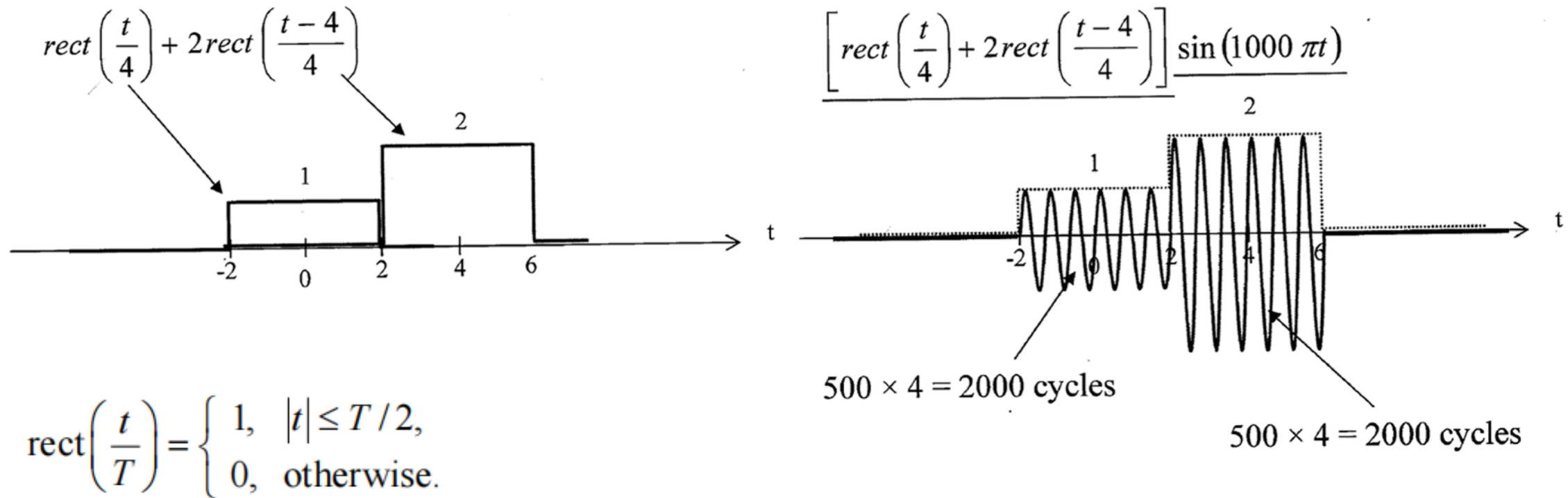
$$\Rightarrow f_c > 210, \text{ or } f_c > 3 \times \text{message bandwidth}$$



2. A suppressed-carrier AM signal $x_1(t)$ is generated by modulating

$$s_1(t) = \text{rect}\left(\frac{t}{4}\right) + 2\text{rect}\left(\frac{t-4}{4}\right) \text{ with } \sin(1000\pi t). \text{ Sketch the time waveform of } x_1(t).$$

Solution



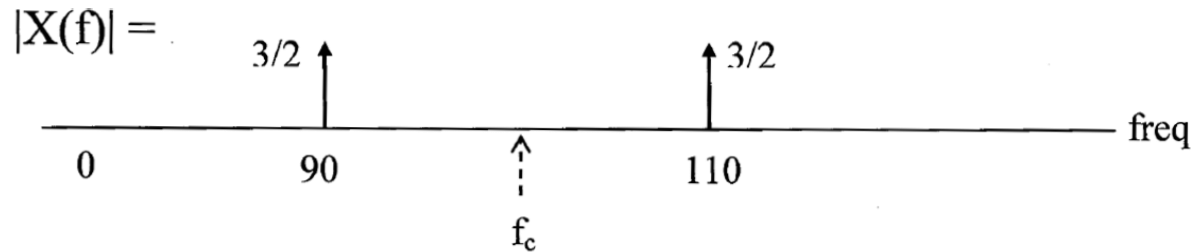
3. A DSBSC-AM signal is

$$x(t) = 3 \sin 180\pi t + 3 \sin 220\pi t$$

- (a) Sketch the amplitude spectrum of $x(t)$ to deduce the carrier frequency in $x(t)$
(b) Given that $x(t)$ was generated using a sine carrier signal with phase 0, demodulate $x(t)$.

Solution

$$x(t) = 3 \sin 180\pi t + 3 \sin 220\pi t$$



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Carrier freq = centre freq of AM spectrum $\Rightarrow f_c = 100\text{Hz}$

To demod $x(t)$, multiply it by $\sin(2\pi 100t)$ followed by LPF.

From $X(f)$, AM signal BW = $110 - 90 = 20\text{Hz}$.

LPF bandwidth = message signal BW = $\frac{1}{2} \times 20\text{Hz} = 10\text{Hz}$.

Demodulator output

$$\begin{aligned} &= [(3 \sin 180\pi t + 3 \sin 220\pi t) \sin 200\pi t]_{\text{LPF}} \\ &= 3 [\sin 180\pi t \sin 200\pi t + \sin 220\pi t \sin 200\pi t]_{\text{LPF}} \\ &= \frac{3}{2} [\cos(180-200)\pi t - \cos(180+200)\pi t \\ &\quad + \cos(220-200)\pi t - \cos(220+200)\pi t]_{\text{LPF}} \\ &= \frac{3}{2} [2 \cos 20\pi t - \cos 380\pi t - \cos 420\pi t]_{\text{LPF}} \\ &= 3 \cos 20\pi t \end{aligned}$$

Since the modulation process would halve the amplitude of message signal, a filter with a gain of 2 should be added into demodulator. Then we would have demodulator output as

$$6 \cos 20\pi t$$