

①

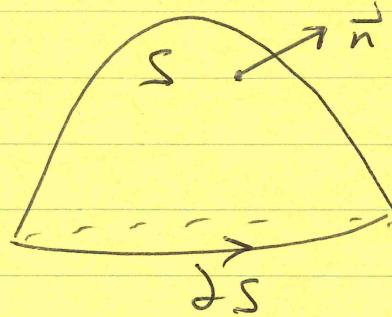
16.8 STOKES' THM

Let S be an oriented surface with positively oriented unit normal $\nabla F \vec{n}$.

Suppose S has a boundary curve, ∂S .

Ex $S = \text{Northern Hemisphere}$
outward normal.

$\partial S = \text{Equator}$



We choose the orientation for ∂S (direction to go around curve ∂S) as follows:

~~Walk around ∂S with your head pointing in direction of \vec{n} . in the direction which~~

The direction you should walk around ∂S is the one such that if your head points in direction of \vec{n} , the the surface will be on your left.

STOKES' THM Let $S, \partial S$ be as above. Let \vec{F} be ∇F on \mathbb{R}^3 . Then

$$\iint_S (\nabla \times \vec{F}) \cdot d\vec{S} = \oint_{\partial S} \vec{F} \cdot d\vec{r}$$

(2)

NOTES

① If $S = D$ is region in plane \mathbb{R}^2 ~~in~~
and \vec{F} is a VF on \mathbb{R}^2 ($\vec{F} = P\hat{i} + Q\hat{j}$) Then
Stokes Thm becomes Green's Thm !!

$$\textcircled{2} \quad \iint_S (\nabla \times \vec{F}) \cdot \hat{n} dS = \oint_C (\vec{F} \cdot \vec{T}) ds$$

Surface Integral of normal cpt of $\nabla \times \vec{F}$
over S

= Line Integral around ∂S of tangential cpt of \vec{F} .

EX

① Let S be sphere, \vec{F} any VF.

Then

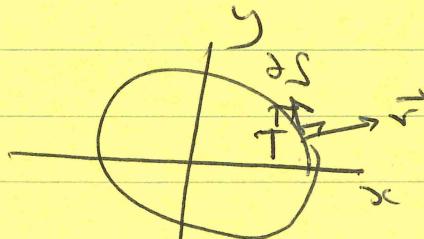
$$\iint_S (\nabla \times \vec{F}) \cdot d\vec{S} = 0 \quad \text{as } \partial S = \emptyset.$$

② Let S be northern hemisphere and let
 $\vec{F}(x, y, z) = x\hat{i} + y\hat{j} + z\hat{k}$.

Then

$$\iint_S (\nabla \times \vec{F}) \cdot d\vec{S} = \oint_C (\vec{F} \cdot \vec{T}) ds$$

on ∂S we have ~~$\vec{T} = f(x, y)\hat{i} + g(x, y)\hat{j}$~~
 $\vec{T} = f(x, y)\hat{i} + g(x, y)\hat{j}$



(3)

On ∂S , $z \rightarrow \infty$

$$\vec{F}(x, y, z) = xi + yj + zk = \vec{r}$$

and $\vec{n} \cdot \vec{r} = 0$.

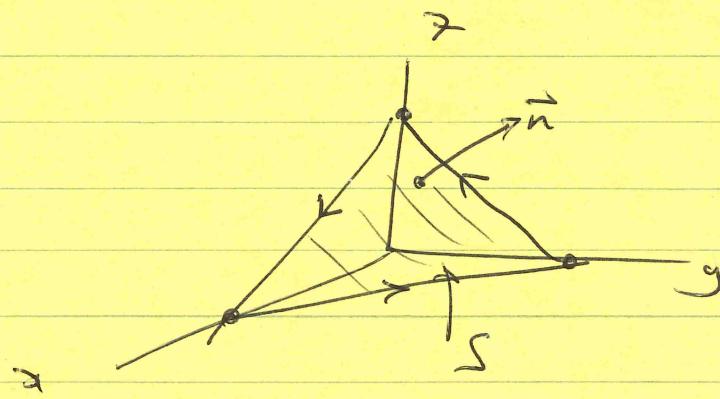
So, $\int_{\partial S} (\vec{F} \cdot \vec{r}) ds = 0$.

(3) $\vec{F}(x, y, z) = (x+y^2)i + (y+z^2)j + (z+x^2)k$.

C = Triangle Vertices $(1, 0, 0)$, $(0, 1, 0)$, $(0, 0, 1)$
oriented in that order.

Find $\int_C \vec{F} \cdot d\vec{r}$.

$C = \partial S$



where S is shaded Δ .

$$\nabla \times \vec{F} = \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ xy^2 & y+z^2 & z+x^2 \end{vmatrix}$$

$$= -2z\vec{i} - 2x\vec{j} - 2y\vec{k}$$

$$= -2(z\vec{i} + x\vec{j} + y\vec{k})$$

(4)

Parameterize S as follows.

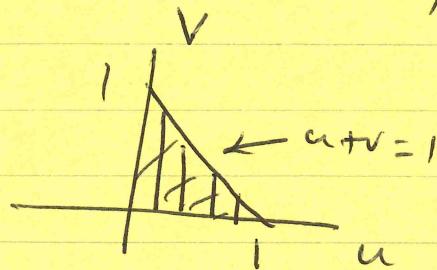
$S \approx$ part of plane $x+y+z=1$. (3 vertices
3 points lie on this plane)

Use

$$x = u$$

$$y = v$$

$$z = 1 - u - v$$



$$0 \leq u \leq 1$$

$$0 \leq v \leq 1-u$$

$$\vec{r}(u,v) = (u, v, 1-u-v)$$

$$\vec{r}_u \times \vec{r}_v = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ 1 & 0 & -1 \\ 0 & 1 & -1 \end{vmatrix} = \vec{i} + \vec{j} + \vec{k}$$

(Agrees w/ \vec{n} from plane)
outward/upward //

So

$$\int_C \vec{F} \cdot d\vec{r} = \iint_S (\nabla \times \vec{F}) \cdot d\vec{S}$$

$$= -2 \int_{u=0}^1 \int_{v=0}^{1-u} (1-u-v, u, v) \cdot (1, 1, 1) dv du$$

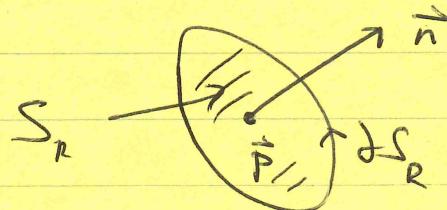
$$= -2 \int_{u=0}^1 \int_{v=0}^{1-u} 1 dv du = -2 \text{Area}(\triangle) = -2 \cdot \frac{1}{2} \cdot 1 \cdot 1 = -1$$

(5)

MORE ON PHYSICAL MEANING OF CURL

Let \vec{F} be velocity VF of fluid in \mathbb{R}^3 .

Let $\vec{p} \in \mathbb{R}^3$ and let \vec{n} be a vector at \vec{p} .



Let S_R be disc center \vec{p}_1 , normal \vec{n} , radius R .

Orient the circle ∂S_R as in Stokes' Thm.

The Angular Velocity around ∂S_R is defined to be

$$\frac{\text{Component of } \vec{F} \text{ tangent to } \partial S_R}{R} \quad [\omega = \frac{v}{R}]$$

So Average Angular Velocity around ∂S_R

$$= \frac{1}{\text{Length}(\partial S_R)} \int_{\partial S_R} \frac{\vec{F} \cdot \vec{T}}{R} dS$$

$$= \frac{1}{2\pi R^2} \int_{\partial S_R} \vec{F} \cdot d\vec{r} = \frac{1}{2} \frac{\int_{\partial S_R} \vec{F} \cdot d\vec{r}}{\text{Area}(S_R)}$$

UNITS RAD/SEC.

(6)

THM

$$= \frac{1}{2} \underbrace{\iint_{S_R} (\nabla \vec{F}) \cdot d\vec{S}}_{\text{Area } (S_R)} = \text{by STOKES' THM}$$

$$\underset{\text{RSMTH}}{\approx} \frac{1}{2} \frac{(\nabla \vec{F}(\vec{p}) \cdot \vec{n}) \text{Area}(S_R)}{\text{Area}(S_R)}$$

Assuming
 $\nabla \vec{F}$ is approx
 const on S_R

$$= \frac{1}{2} (\nabla \vec{F}(\vec{p})) \cdot \vec{n}$$

TWO CASES

① If $(\nabla \vec{F})(\vec{p}) = \vec{0}$ Then fluid doesn't rotate

about \vec{p} , no matter what axis \vec{n} is chosen to measure angular velocity.

Say \vec{F} is IRROTATIONATE

② If $(\nabla \vec{F})(\vec{p}) \neq \vec{0}$ Then The axis \vec{n} for which Average Angular Velocity about that axis is LARGEST is given by

$$\vec{n} = \frac{(\nabla \vec{F})(\vec{p})}{|(\nabla \vec{F})(\vec{p})|}$$

(7)

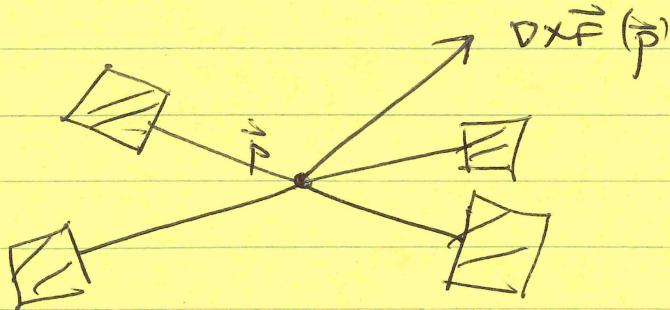
and Av. Angular Velocity about that axis is

$$\frac{1}{2} |(\nabla \times \vec{F})(\hat{p})|.$$

Physically Put Paddlewheel in fluid.

Axis will align with $(\nabla \times \vec{F})(\hat{p})$.

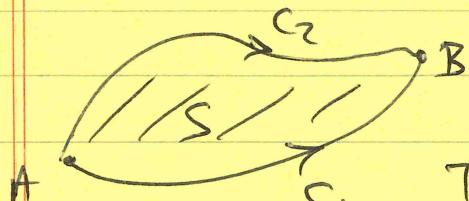
Angular Velocity of PW $\approx \frac{1}{2} |(\nabla \times \vec{F})(\hat{p})|$



APPLICATION TO CONSERVATIVE VFs

Suppose $\nabla \times \vec{F} = \vec{0}$. Then $\vec{F} = \nabla f$ is conservative
Reason $\int_C \vec{F} \cdot d\vec{r}$ is indept of path

Intuit



Let C_1, C_2 be 2 curves from A, B and S surface wth $\partial S = C_1 - C_2$ (as in picture).

$$0 = \iint_S (\nabla \times \vec{F}) \cdot d\vec{S} = \int_{C_1} \vec{F} \cdot d\vec{r} - \int_{C_2} \vec{F} \cdot d\vec{r}$$