

# Analog Transmission of Vocoder Features over Radio Channels

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Given a vector of vocoder features  $\mathbf{f}$ , use an autoencoder  $E$  to map them to a dimension  $d$  latent vector  $\mathbf{z}$  where  $d$  is even. Unlike digital modulation, each element  $z_i$  of  $\mathbf{z}$  is continuously valued and not constrained to a discrete set of points. For bandwidth efficient transmission over the channel the elements of  $\mathbf{z}$  are mapped to  $d/2$  complex symbols  $\mathbf{q}$ . Compared to classical digital modulation, the elements of  $\mathbf{z}$  can be considered BPSK symbols (continuously valued, analog bits), and the elements of  $\mathbf{q}$  analog QPSK symbols.

Our goal is to determine if reasonable speech quality can be obtained over a channel of bandwidth  $B < 3000$  Hz and SNR (measured in  $B = 3000$  Hz) of between 0 and 6dB, roughly the lower limit of Single Side Band (SSB) - a common power and bandwidth efficient form of analog radio communication.

## 1 Simulation of AWGN Channels

The autoencoder output  $\mathbf{z}$  is updated every  $T_z = 1/R_z$  seconds, giving a BPSK symbol rate of:

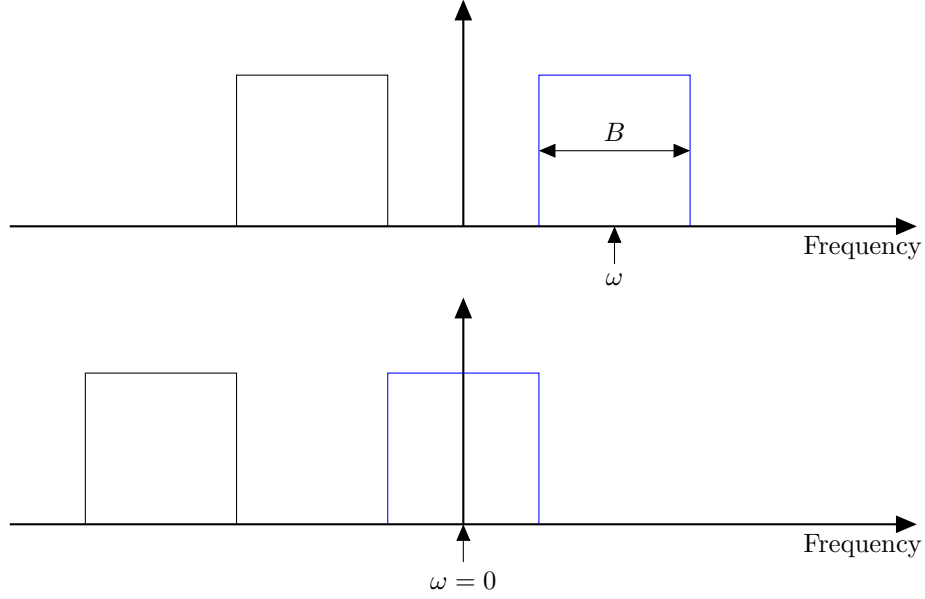
$$R_b = d/T_z \tag{1}$$

For example with  $T_z = 0.04$ ,  $d = 80$ ,  $R_b = 2000$  symbols/s. The QPSK symbol rate is given by:

$$R_q = \frac{d}{2T_z} \tag{2}$$

For example with  $T_z = 0.04$ ,  $d = 80$ ,  $R_q = 1000$  symbols/s.

Figure 1: Real sampled off-air signal. We are interested in the blue bandpass interval of bandwidth  $B$ , which is single sided and hence complex valued. After shifting to baseband, it's power is unchanged, and it remains complex valued.



We wish to simulate an AWGN channel with a user-defined  $E_b/N_0$ , where  $E_b$  is the energy of each BPSK symbol, and  $N_0$  is the noise power per unit bandwidth. Consider a real valued signal sampled off air (Figure 1). We will follow convention and define signal and noise power in the “single sided” bandpass interval of the frequency spectrum with bandwidth  $B$  centered on  $\omega$ . As the interval is single sided, we must use complex valued quantities to represent it.

We wish to simulate a bandpass AWGN channel at baseband ( $\omega = 0$ ). This implies a frequency shift of the complex valued signal, but the signal remains complex valued and it's power is unchanged. The negative frequency component on the LHS of Figure 1 is redundant and after frequency shifting can be removed by filtering.

Note that even at baseband we must use complex valued quantities for the signal and noise to represent a bandpass signal of bandwidth  $B$ . For example, given a fixed sample rate  $B$  and noise power  $N$ , a real valued noise sequence can only represent a bandwidth of  $B/2$  which results in doubling the noise density  $N_0 = N/(B/2) = 2N_0$  compared to a complex valued noise sequence with the same power.

The energy of each BPSK symbol  $E_b$  is the signal power  $S$  divided by the symbol rate  $R_b = 1/T_b$ . The noise per unit bandwidth is the total noise power  $N$  divided by the bandwidth  $B$  of the system. If we are simulating at one sample per symbol,  $B = R_b$ :

$$\begin{aligned}\frac{E_b}{N_0} &= \frac{S/R_b}{N/R_b} \\ &= \frac{S}{N} \\ &= \frac{A^2}{\sigma^2}\end{aligned}\tag{3}$$

where  $A$  is the amplitude of each BPSK symbol and  $\sigma^2 = N$  is the variance of the complex valued noise (mean noise energy per sample). Given a set point  $E_b/N_0$ :

$$\sigma = \frac{A}{\sqrt{E_b/N_0}}\tag{4}$$

The complex noise sample  $r_i$  can be generated as:

$$r_i = \frac{\sigma}{\sqrt{2}}(\mathcal{N}_{2i}(0, 1) + j\mathcal{N}_{2i+1}(0, 1))\tag{5}$$

where  $\mathcal{N}_i(0, 1)$  is the  $i$ -th sample of a unit variance, zero mean, real Gaussian noise source. Note the noise power is split evenly between the real and imaginary arms. Our symbols passing through an AWGN channel can be simulated at complex baseband as:

$$\begin{aligned}\hat{z}_i &= z_i + r_i \\ \hat{q}_i &= q_i + r_i\end{aligned}\tag{6}$$

If the noise is zero mean, we can estimate  $\sigma^2$  over  $K$  noise samples  $r_i$  as:

$$\sigma^2 = E[|r_i|^2] = \frac{1}{K} \sum_{i=0}^{K-1} |r_i|^2\tag{7}$$

## 1.1 SNR Measurement

In order to compare with other methods of speech communication that have varying bandwidths  $B$ , it is useful to formulate expressions for estimating SNR from the BPSK and QPSK symbols. The Signal to Noise ratio (SNR) is given by:

$$\begin{aligned}\frac{S}{N} &= \frac{E_b R_b}{N_0 B} \\ &= \frac{E_q R_q}{N_0 B}\end{aligned}\tag{8}$$

A noise bandwidth  $B$  needs to be selected; common choices are  $B = R_b$ , in which case  $S/N = E_b/N_0$ ; for HF radio  $B = 3000$  Hz to compare with existing analog and digital voice waveforms; or  $B = 1$  to obtain a normalised  $C/N_0$  carrier power to noise density ratio - useful for comparing waveforms with different bandwidths.

At one sample per symbol, the power, the mean energy of each QPSK symbol over a window of  $K$  samples is given by:

$$E_q = E[|q_i|^2] = \frac{1}{K} \sum_{i=0}^{K-1} |q_i|^2 \quad (9)$$

Note the variance function should not be used to calculate  $E_q$ , as we cannot guarantee  $q_i$  is zero mean. As each QPSK symbol contains 2 BPSK symbols, the energy is split evenly:

$$E_b = E_q/2 \quad (10)$$

For example if the symbol amplitude is  $A = 1$ ,  $E_b = A^2 = 1$ , then  $E_q = 1+1 = 2$ .

To model transmission over multipath channels using OFDM we arrange the QPSK symbols as  $N_c$  parallel carriers, each running at a symbol rate of  $R_s = R_q/N_c$  symbols/s, where  $R_s$  is chosen based on delay spread considerations. Typical values for HF modems are  $N_c = 20$  and  $R_s = 50$  Hz. However the OFDM carriers are arranged such that the total symbol rate over the channel remains constant. So for a given signal power  $E_q$  and  $E_b$  remain constant (Table 1).

Waveform	$N_c$	$R_s$	$R_q$	$R_b$	$E_q$	$E_b$
Single Carrier BPSK	1	-	-	2000	-	$S/2000$
Single Carrier QPSK	1	-	1000	2000	$S/1000$	$S/2000$
OFDM QPSK	20	50	1000	2000	$S/1000$	$S/2000$

Table 1:  $E_b$  and  $E_q$  examples for single and multi-carrier OFDM waveforms for constant carrier power  $S$

## 1.2 Calibration and Testing

In order to evaluate the ML system early in the development process it is important to ensure the noise is correctly calibrated. The expressions above can be used to check the noise injection process:

1. Set a target  $E_b/N_0$  for the simulation run, and calculate  $\sigma$  using (4).
2. Establish the equivalent target SNR from (8) evaluated using the target  $E_b/N_0$ .
3. After the simulation run measure  $E_q = E[|q_i|^2]$  over a sample of transmitted symbols. Note that in general  $E_q \neq 2$  as the encoder outputs continuous values.

4. Calculate measured SNR using (8) and compare.

The calibration of the noise injection can be checked by replacing the encoder output  $z_i$  with discrete PSK symbols to create a digital modem, then measuring the BER at  $E_b/N_0$  points. The theoretical BER over an AWGN channel is:

$$BER = 0.5erfc(\sqrt{E_b/N_0}) \quad (11)$$

For a multipath channel:

$$BER = 0.5 \left( 1 - \sqrt{\frac{E_b/N_0}{E_b/N_0 + 1}} \right) \quad (12)$$

## 2 Comparison with Other Speech Waveforms

We wish to compare our radio autoencoder with existing waveforms used for speech transmission over radio channels. We start with the assumption that we have a transmitter of  $C$  watts, and an AWGN channel with a spectral noise density of  $N_0$  watts/Hz. As the speech waveforms being considered vary in bandwidth we will choose  $C/N_0$  as the SNR metric.

The  $C/N_0$  (in dBHz) at the demodulator input of a terrestrial radio receiver is given by:

$$\frac{C}{N_0} = P - PAPR - L_{path} - NF + 174 \quad (13)$$

where  $P$  is the maximum output power of the transmitter power amplifier,  $PAPR$  is the Peak to Average Power Ratio of the waveform,  $L_{path}$  is the path loss,  $NF$  is the noise figure of the receiver. For example consider a 400 MHz FM hand held radio over a 1km urban (non line of site) path. The radio has a 1W (30 dBm) power output,  $L_{path} = 120$  dB, with noise dominated by ambient EMI such that  $NF = 10$  dB.  $C/N_0 = 30 - 0 - 120 - 10 + 174 = 74$  dBHz, sufficient for good quality speech (Table 4).

Note that  $C/N_0$  in the demodulator is a function of PAPR. A high PAPR reduces the  $C/N_0$  at the receiver. We effectively “back off” the transmitter power from the maximum  $P$  by the PAPR. We assume the PA is capable of sustaining  $P$  watts indefinitely. As PAPR varies by waveform, it should be included in any metric for comparison of waveforms. We define  $P/N_0$  as:

$$P/N_0 = C/N_0 + PAPR \quad (14)$$

A waveform that delivers intelligible speech at a low  $P/N_0$  is the target. A low PAPR waveform has other desirable properties, such as greater PA efficiency, longer battery life, and low cost semiconductors.

Waveform	Threshold
Single Sideband	0dB SNR in a 3000 Hz, Tx speech compressor
Frequency Modulation	-120 dBm quoted for many NBFM radios, 54dB above thermal noise floor
FreeDV 700D	10% PER threshold at -2dB SNR in 3000 Hz
Radio Autoencoder	Intelligible speech at $E_b/N_0 = -8$ dB, $R_b = 2000$ Hz

Table 2: Thresholds for speech link closure for each waveform. The link is considered closed when the speech is barely intelligible to a trained listener.

Waveform	Abbr	Bandwidth	PAPR	$C/N_0$	$P/N_0$	$\Delta$
Single Sideband	SSB	2000	6	35	41	-15
Frequency Modulation	NBFM	16000	0	50	50	-24
FreeDV 700D	700D	1100	4	32	36	-10
Radio Autoencoder	radAE	1200	1	25	26	0

Table 3: Comparison of link closure by waveform over AWGN channels. Bandwidth refers to the RF bandwidth in Hz required over the radio channel.

Waveform	Audio BW	$C/N_0$	$P/N_0$	$\Delta$
Radio Autoencoder	8000	30	31	0
Frequency Modulation	3000	60	60	-29
Single Sideband	2000	55	62	-31

Table 4: Comparison of good quality “arm chair copy” by speech waveform over AWGN channels. They are ranked in terms of maximum achievable speech quality. FreeDV 700D has been omitted because of its low speech quality even in ideal channels. The radio autoencoder delivers wideband (8000 Hz) audio.

### 3 Over the Cable and Over the Air Tests

Impressive results have been obtained from the symbol rate simulations of an OFDM modem that assumed ideal synchronisation. Need to verify using real radio signals. This means building up a rate  $Fs_s$  system, and synchronisation subsystems. Choice was made to use classical DSP pilot symbol based synchronisation for the first pass, although we acknowledge potential for ML based synchronisation in future iterations.

Goal is to compare speech quality at  $E_b/N_0 = 0dB$  (approx -3dB SNR in 3000 Hz), and work through any issues that prevent the system working over real radio channels. A column of pilots between every  $N_s = 4$  pilots. Ref freedv low study, this is 0.96dB loss in SNR and increase in bandwidth. TODO calculations. Pilots used for coarse

Pilot based sync built up in PyTorch, used for coarse and fine timing, phase and amplitude equalisation. Unlike regular PSK, network is likely to be sensitive to amplitude variations. Phase equalisation allows small frequency offsets ( $\pm 2$  Hz) to be tracked.

Several phase estimators were prototyped. They were tested using BER measurements. Issues with maintaining low loss synchronisation at low  $E_b/N_0$ . Might be better to use lower dimension and higher  $E_b/N_0$ , which will allocate more power to pilots, less carriers. Using per-carrier phase estimation makes the system less dependant on fine timing and the ability to handle multipath, but has higher loss.

Figure 2: OFDM pilot based synchronisation algorithm performance, tested with digital PSK symbols on an AWGN channel. With ideal sync, intelligible speech is produced at  $E_b/N_0 = -6$  dB or BER=0.24.

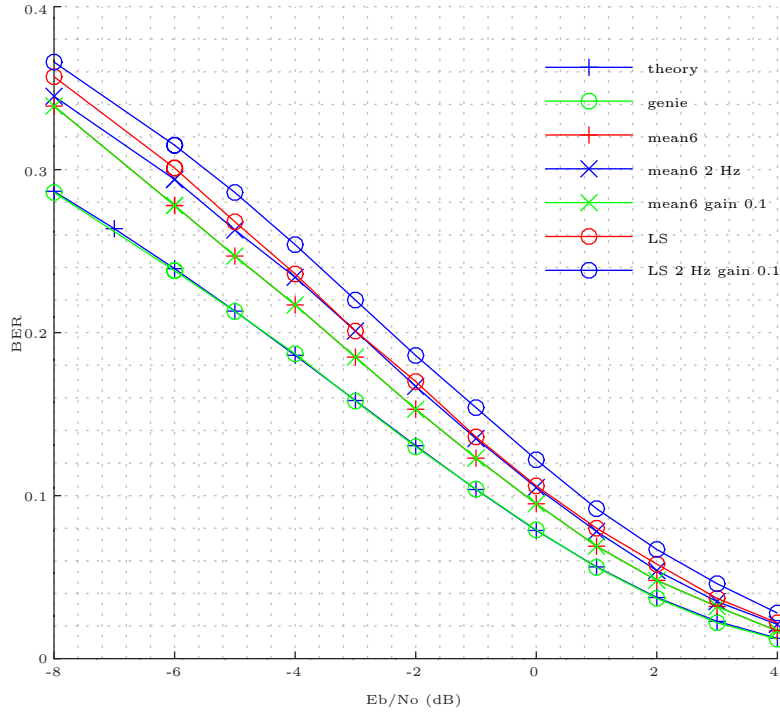


Figure 2 plots the performance of the OFDM pilot based synchronisation system used for the OTC/OTA tests on an AWGN channel. The unusually low  $E_b/N_0$  range we are considering is challenging. The *genie* curve is the

baseline rate  $F_s$  OFDM system with ideal sync, and matches the theoretical results. Using this system, we can obtain intelligible speech at  $E_b/N_0 = -6$ , or BER=0.24 in a digital system. We can use the BER=0.25 line to estimate the loss of the synchronisation based system at this operating point, which for the *mean6* and *LS* algorithms under realistic conditions is around 2dB.

No CP inserted at this time. TODO Figure of OFDM frame. TODO Figure of OTC tests TODO table/figure of sync results, discussion of issues

TODO further work, try lower dimension, higher Eb/No op point, put pilots in information sent to decoder, train with freq and phase offsets, train without pilots but phase/amp offsets, compare to classical DSP pilot losses.

## 4 Glossary

Symbol	Explanation	Units
$B$	noise or signal bandwidth	Hz
$C$	Carrier (transmitter) power $C = S$ for this study	
$C/N_0$	Carrier power/spectral noise density	
$d$	dimension of latent vector $\mathbf{z}$	
$E_b/N_0$	energy per BPSK symbol on spectral noise density	
$E_q/N_0$	energy per QPSK symbol on spectral noise density	
$N$	total noise power	Watts
$N_c$	Number of carriers	
$N_0$	Noise power in 1 Hz of bandwidth	
$P/N_0$	Peak trasnmmitter power/spectral noise density	
$\mathbf{q}$	vector of QPSK symbols	
$q_i$	single QPSK symbol, element of $\mathbf{q}$	
$R_b$	BPSK symbol rate	symbols/second
$R_q$	QPSK symbol rate	symbols/second
$R_s$	OFDM per carrier QPSK symbol rate	symbols/second
$R_z$	latent vector update rate	Hz
$SNR$	signal to noise Ratio	
$S$	total signal (carrier) power	Watts
$T_b$	BPSK symbol period	seconds
$T_q$	QPSK symbol period	seconds
$T_s$	OFDM per carrier QPSK symbol period	seconds
$T_z$	time between latent vector updates	seconds
$r_i$	noise sample	
$\mathbf{z}$	Autoencoder output latent vector	
$z_i$	single latent vector element of $\mathbf{z}$ , a BPSK symbol	

Table 5: Glossary of Symbols