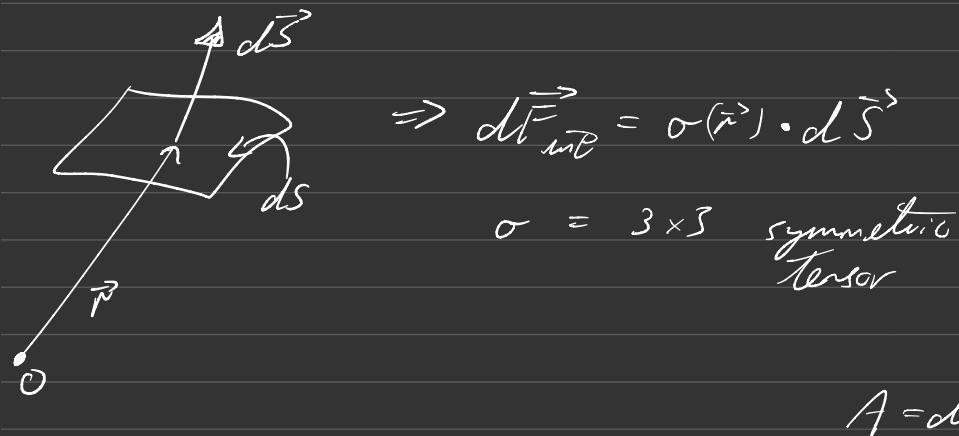


# Lamé stress tensor

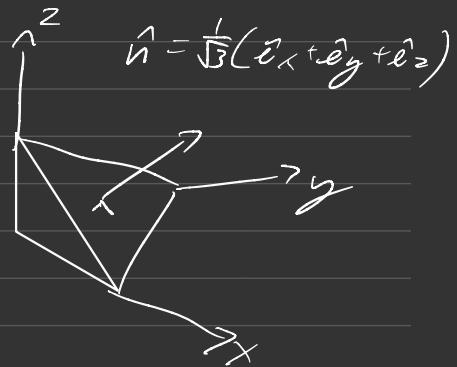
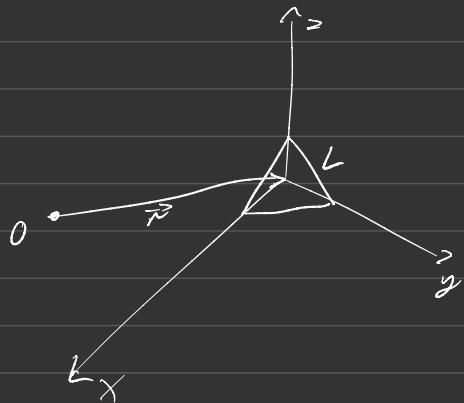


$$\begin{aligned}
 d\vec{F}_{int} &= \vec{G}(\vec{r}, \hat{n}, A) \\
 &= \vec{G}(\vec{r}, \hat{n}, 0) + \frac{\partial \vec{G}}{\partial A}(\vec{r}, \hat{n}, 0) dS \\
 &\quad + \frac{1}{2} \frac{\partial^2 \vec{G}}{\partial A^2}(\vec{r}, \hat{n}, 0) dS^2 + \dots
 \end{aligned}$$

$$= \frac{\partial \vec{G}}{\partial A}(\vec{r}, \hat{n}, 0) dS + O(dS^2)$$

$$\frac{d\vec{F}_{int}}{dS} = \underbrace{\frac{\partial \vec{G}}{\partial A}(\vec{r}, \hat{n}, 0)}_{\vec{H}(\vec{r}, \hat{n})}$$

$$d\vec{F}_{int} = H(\vec{r}, \hat{n}, 0) dS$$



$$\begin{aligned}
 (\vec{dF}_{int})_A &= \vec{H}(\vec{r} + \frac{L}{3}(e_x + e_z), -\hat{e}_y) \pm L^2 \sqrt{3} n_y \\
 &\quad + \vec{H}(\vec{r} + \frac{L}{3}(e_x + \hat{e}_y), -\hat{e}_z) \pm L^2 \sqrt{3} n_z \\
 &\quad + \vec{H}(\vec{r} + \frac{L}{3}(\hat{e}_y + e_z), -\hat{e}_x) \pm L^2 \sqrt{3} n_x \\
 &\quad + \vec{H}(\vec{r} + \frac{L}{2}(e_x + \hat{e}_y + \hat{e}_z), \hat{n}) \pm \frac{\sqrt{3}}{2} L^2
 \end{aligned}$$

$$\begin{aligned}
 \vec{dF}_{int} &= \left\{ \vec{H}(\vec{r}, -\hat{e}_x) n_x + \vec{H}(\vec{r}, \hat{e}_y) n_y \right. \\
 &\quad \left. + \vec{H}(\vec{r}, -\hat{e}_z) + \vec{H}(\vec{r}, \hat{n}) \right\} \frac{\sqrt{3}}{2} L^2 + O(L^3) \\
 &= (\text{mass insides the tetrahedron}) \times (\text{acceleration})
 \end{aligned}$$

$$= \rho(\vec{r}) \frac{1}{6} L^3 \vec{a}$$

$$\left\{ \vec{H}(\vec{r}, -\hat{e}_x) n_x + \vec{H}(\vec{r}, -\hat{e}_y) n_y + \vec{H}(\vec{r}, -\hat{e}_z) n_z \right. \\ \left. + \vec{H}(\vec{r}, \vec{n}) \right\} \frac{\sqrt{3}}{2} + O(\cancel{\vec{e}}^0) = \cancel{\frac{1}{6} \rho \vec{a} \sum}$$

$$\vec{H}_c(\vec{r}, \vec{n}) = - \sum_{j=1}^3 H_j(\vec{r}, -\hat{e}_j) n_j$$

$$\text{Define } \sigma_{ij}(\vec{r}) = -H_i(\vec{r}, -\hat{e}_j)$$

$$H_i = \sum_{j=1}^3 \sigma_{ij} n_j$$

$$\vec{H} = \sigma \cdot \hat{n} \Rightarrow d\vec{F}_{int} = \sigma \cdot \hat{n} dS = \sigma d\vec{S}$$

$$\vec{F}_{int} = \oint_{\Sigma} \sigma \cdot d\vec{S} \\ = \int_{\Omega} \vec{\nabla} \sigma dV \quad (\vec{\nabla} \sigma)_i = \sum_j \frac{\partial \sigma_{ij}}{\partial x_i}$$

$$d\vec{F}_{int} = \left\{ \begin{array}{l} \sigma \cdot d\vec{S} \\ \vec{\nabla} \sigma dV \end{array} \right.$$

$$d\vec{v} = \vec{r} \times d\vec{F}$$

$$= \begin{cases} \vec{r} \times (\sigma \cdot d\vec{s}) \\ r \times (\nabla \sigma) d\vec{s} \end{cases}$$

$$\oint_{\Sigma} r \times (\sigma \cdot d\vec{s}) = \int_S r \times (\nabla \sigma) dV$$

$$\epsilon_{ijk} = \begin{cases} +1 & jk = 123, 231, 312 \\ -1 & jk = 321, 213, 132 \\ 0 & \text{any two are the same} \end{cases}$$

$$(\vec{A} \times \vec{B})_i = \sum_{j,k} \epsilon_{ijk} A_j B_k$$

$$\oint_{\Sigma} [\vec{r} \times (r \cdot d\vec{s})]_i = \oint_{\Sigma} \epsilon_{ijk} \times_j (\sigma \cdot d\vec{s})_k$$

$$= \oint_{\Sigma} (\epsilon_{ijk} \times_j \sigma_{ik}) dS_i$$

$$= \int \frac{\partial}{\partial x_i} (\epsilon_{ijk} \times_j \sigma) dV$$

$$\left[ \oint_{\Sigma} r \times (\sigma \cdot d\vec{s}) \right]_i = \int_S \frac{\partial}{\partial x_i} (\epsilon_{ijk} \times_j \sigma_{ik}) dV$$

$$= \int_{\Omega} \varepsilon_{ijk} \left[ \delta_{ij} \sigma_{kk} + \delta_{ij} \frac{\partial \sigma_{kl}}{\partial x^l} \right] dV$$

$$= \int_{\Omega} \varepsilon_{ijk} \left[ \sigma_{kj} + x_j (\nabla \sigma)_k \right] dV$$

$$= \int_{\Omega} \varepsilon_{ijk} \sigma_{kj} dV + \left[ \int_{\Omega} n^j x_j (\nabla \sigma) dV \right]_i$$

$$= \left[ \int_{\Omega} n^j x_j (\nabla \sigma) dV \right]_i$$

$$= \int_{\Omega} \varepsilon_{ijk} \sigma_{kj} dV = 0$$

$$\sum_{j,k} \varepsilon_{ijk} \sigma_{kj} = 0$$

$$i = 1 (x), \quad \sum_{jk} \varepsilon_{ijk} \sigma_{kj} = \varepsilon_{123} \sigma_{21} + \varepsilon_{132} \sigma_{23}$$

$$\Rightarrow \sigma_{23} - \sigma_{32} = 0$$

## Example

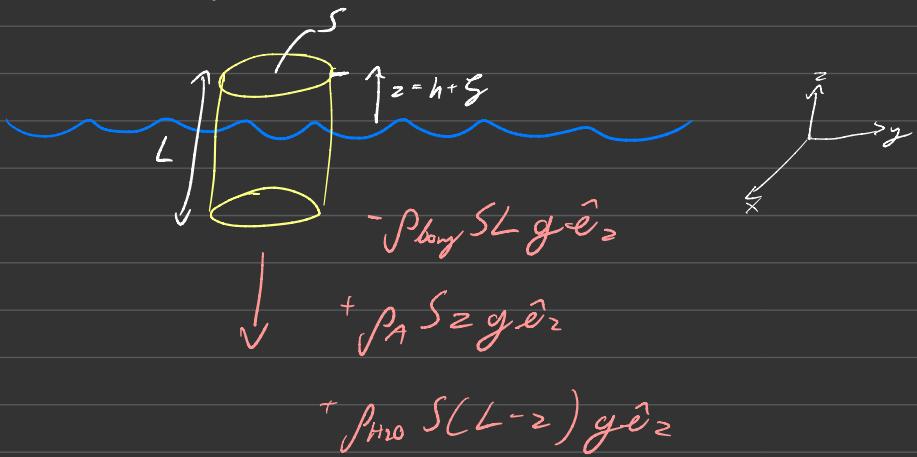
$$\rho \vec{F} - \vec{\nabla} P = \vec{0}$$

$\Rightarrow$  Archimedes Principle

$$\vec{F}_{\text{buoy}} = \rho_0 g V_{\text{obj}} \hat{e}_z$$

$\rho_{\text{buoy}}$   
 $V_{\text{obj}}$   
 $\rho_{H_2O}$

Buoy



$$\vec{F} = [(\rho_{H_2O} - \rho_{\text{buoy}})L - (\rho_{H_2O} - \rho_{A_{ir}})z] S g \hat{e}_z$$

$h$  = ~~equation~~ of height of top of box

$$h = \left( \frac{\rho_{H_2O} - \rho_{\text{buoy}}}{\rho_{H_2O} - \rho_{A_{ir}}} \right) L \approx \left( 1 - \frac{\rho_{\text{buoy}}}{\rho_{H_2O}} \right) L$$

specific gravity

$$\rho_{\text{buoy}} \approx 0.7 \rho_{\text{air}}$$

$$h \approx 0.3L$$

$$\vec{F}(g) = [(p_{\text{H}_2\text{O}} - \rho_{\text{buoy}})L - (p_{\text{air}} - p_{\text{atm}})(h + g)]S_g \hat{e}_z$$

$$= -(p_{\text{H}_2\text{O}} - p_{\text{air}}) S_g S \hat{e}_z$$

= Hooke's Law!

$$= \rho_{\text{buoy}} S L \vec{g} \hat{e}_z$$

$$\vec{g} = \frac{p_{\text{H}_2\text{O}} - p_{\text{air}}}{\rho_{\text{buoy}}} \frac{g}{L} \vec{g}$$

$$\vec{g} + \omega^2 \vec{g} = 0 \quad \omega = \sqrt{\frac{p_{\text{H}_2\text{O}} - p_{\text{air}}}{\rho_{\text{buoy}}} \frac{g}{L}}$$

$$T = \frac{2\pi}{\omega} = 2\pi \sqrt{\frac{\rho_{\text{buoy}}}{p_{\text{H}_2\text{O}} - p_{\text{air}}} \frac{L}{g}}$$

$$\approx 2.45$$

$$\rho \vec{f} = \vec{\nabla} P$$

$\rho, P$  are unknown if compressible

equation of state

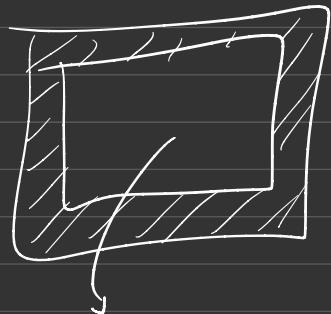
$$P = P(\rho)$$

Example

$$PV = Nk_B T$$

$$\Rightarrow P(\rho) = \frac{k_B T_0}{m} \rho$$

$$P(\rho, z) = \frac{k_B T(z)}{m} \rho$$



$$\text{entropy} = \text{constant} \Rightarrow PV^\gamma = \text{const}$$

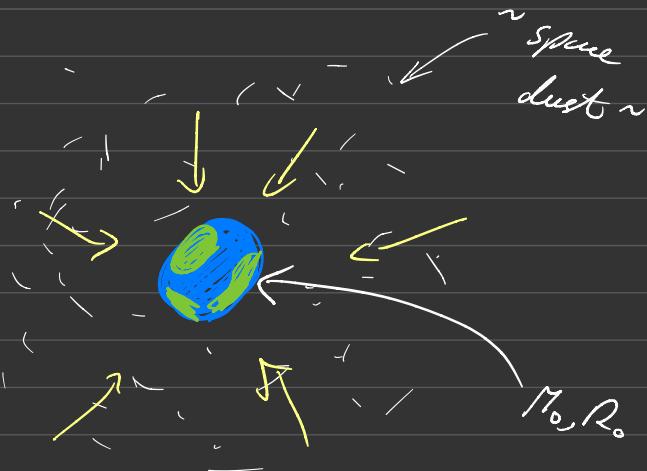
adiabatic equation of state

$$\gamma = \frac{C_p}{C_v}$$

$$\rho \propto \frac{1}{V}$$

$$\rho \propto \left(\frac{1}{V}\right)^\gamma \propto V^{-\gamma}$$

$$P(r) = K \rho r \quad K > 0$$



$$\vec{F} = -\frac{G M_0}{r^2} \hat{e}_r$$

$$-\frac{G M_0}{r^2} \hat{e}_r = \vec{\nabla} P$$

$$= \vec{\nabla} (\kappa \rho r)$$

$$= \gamma K \rho^{r-1} \vec{V} \rho$$

$$\int \gamma K \rho^{r-1} \frac{\partial \rho}{\partial r} = - \frac{G M_0}{r^2} \rho$$

$$\gamma K \rho^{r-1} \frac{1}{r} \frac{\partial \rho}{\partial \theta} = 0$$

$$\gamma K \rho^{r-1} \frac{1}{r \sin \theta} \frac{\partial \rho}{\partial \phi} = 0$$

$$v^{r-2} \frac{dp}{dr} = - \frac{G M_0}{\gamma K} \frac{1}{r^2}$$

$$-\frac{1}{\gamma^{-1}} \rho^{r-1} = \frac{G M_0}{\gamma K} \frac{1}{r} + C$$

$$m_{\text{gas}} = \int_{R_0}^{\infty} \rho dV = \int_{R_0}^{\infty} 4\pi r^2 \rho(r) dr$$

$$\rho(r) \rightarrow 0 \quad \text{as } r \rightarrow \infty \quad \Rightarrow \quad C = 0$$

$$\frac{1}{\gamma^{-1}} \rho^{r-1} = \frac{G M_0}{\gamma K} \frac{1}{r}$$

$$\rho(r) = \left( \frac{(\gamma-1) G M_0}{\gamma K r} \right)^{\frac{1}{\gamma-1}}$$

$$m_{gas} = \int_{r_0}^{\infty} 4\pi r^2 \left( \frac{(\gamma-1) G M_0}{\gamma K r} \right)^{\frac{1}{\gamma-1}} dr$$

$$= 4\pi \left( \frac{(\gamma-1) G M_0}{\gamma K} \right)^{\frac{1}{\gamma-1}} \int_{r_0}^{\infty} r^{\frac{2\gamma-3}{\gamma-1}} dr$$

$$= 4\pi \left( \frac{(\gamma-1) G M_0}{\gamma K} \right)^{\frac{1}{\gamma-1}} \frac{1}{\left( \frac{3\gamma-4}{\gamma-1} \right)} r^{\frac{3\gamma-4}{\gamma-1}} \Big|_{r_0}^{\infty}$$

$$\frac{3\gamma-4}{\gamma-1} \geq 0 \Rightarrow \gamma \geq \frac{4}{3}$$

$$\left. \begin{aligned} C_p &= \left( \frac{\gamma+2}{2} \right) N k_B \\ C_V &= \frac{\gamma}{2} N k_B \end{aligned} \right\} \quad \frac{C_p}{C_V} = 1 + \frac{2}{\gamma}$$

$$1 + \frac{2}{\gamma} \leq \frac{4}{3}$$

$$\frac{2}{\gamma} \leq \frac{1}{3} \Rightarrow \boxed{\gamma \geq 6}$$

Monatomic:  $\gamma = 3$

Diatomic:  $\gamma = 5 \text{ or } 6$

Polyatomic:  $H_2O, CO_2$   
 $\gamma = 9 \quad \gamma = 7$



$$\vec{F} = -\frac{G M(r) \hat{e}_r}{r^2}$$

$$M(r) = M_0 + \int_{R_0}^r 4\pi r'^2 \rho(r') dr'$$

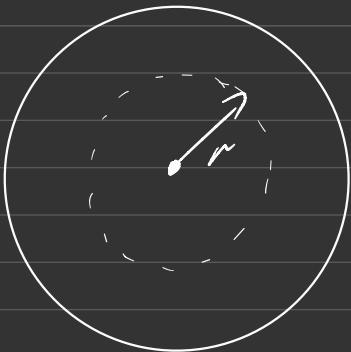
$$\rho \vec{J} = \vec{\nabla} P$$

$$\frac{dM(r)}{dr} = 4\pi r^2 \rho(r)$$

$$-\frac{G M(r)}{r^2} \rho(r) = \frac{dP(r)}{dr}$$

$$\rho(r), P(r), M(r)$$

Equations of state



$$P(\rho) = \frac{K_B T_0}{m} \rho$$

$$-\frac{GM\rho}{r^2} = \frac{K_B T_0}{m} \frac{dp}{dr}$$

$$M = -\frac{K_B T_0}{GM} \frac{r^2}{\rho} \frac{dp}{dr}$$

$$-\frac{K_B T_0}{GM} \frac{d}{dr} \left( \frac{r^2}{\rho} \frac{dp}{dr} \right) = 4\pi r^2 \rho$$

$$\frac{r^2}{\rho} \frac{d^2 p}{dr^2} + \frac{2r}{\rho} \frac{dp}{dr} - \frac{r}{\rho} \left( \frac{dp}{dr} \right)^2 + \frac{4\pi G m r^3 \rho}{K_B T_0} = 0$$

$$\text{Try } \rho^{(n)} = A r^\alpha$$

$$\underbrace{\alpha(\alpha-1) + 2\alpha - \alpha^2}_{\alpha} + \frac{4\pi G m}{K_B T_0} A r^{\alpha+2} = 0$$

$$= -2 + \frac{4\pi G m A}{K_B T_0} = 0$$

$$\alpha = -2 \quad , \quad A = \frac{K_B T_0}{2\pi G m}$$

$$\rho(n) = \frac{K_B T_0}{2\pi G m} \frac{1}{n^2}$$

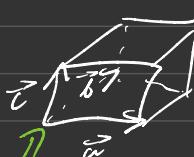
$$\int_0^{R_\odot} 4\pi r^2 \rho(n) dr = M_\odot$$
$$= \frac{K_B T_0 R_\odot}{2\pi G m}$$

$$m \approx 50 m_p$$

$$T_0 \approx 3.76 \times 10^5 K$$

$$\frac{d}{dt}(\Delta V_t) = (\vec{\nabla} \cdot \vec{u}) \Delta V_t$$

Parallelogram speed



$$\text{Volume} = \vec{u} \cdot (\vec{b} \times \vec{c}) = ((\vec{a} \times \vec{b}) \cdot \vec{c})$$

$$= \sum_{ijk} \epsilon_{ijk} a_i b_j c_k$$

$$r + \vec{u}(t, \vec{r}) \Delta t$$

$$\vec{u} + \vec{a}(t, \vec{r} + \vec{a}) \Delta t$$

$$\vec{a}^+ = \vec{u} + \vec{a}(t, \vec{r} + \vec{a}) - \vec{a}(t, \vec{r}) \Delta t$$

$$u_i(t, x^{tag}, y^{tag}, z^{tag})$$

$$\approx u_i(t, x, y, z) + a_x \frac{du}{dx} + a_y \frac{du}{dy}$$

$$\Delta V_t \rightarrow \epsilon_{ijk} (a_i + (\vec{a} \cdot \vec{\nabla}) a_i \Delta t + \dots)$$

$$(b_j + (\vec{b} \cdot \vec{\nabla}) a_j \Delta t + \dots)$$

$$(c_k + (\vec{c} \cdot \vec{\nabla}) a_k \Delta t + \dots)$$

$$= \varepsilon_{ijk} a_i b_j c_k$$

$$\tau \Delta t \varepsilon_{ijk} / a_i b_j (c \cdot \vec{\nabla}) w$$

$$+ a_i (b \cdot \vec{\nabla}) w b_j c_k$$

$$+ (\vec{w} \cdot \vec{\nabla}) w b_j c_k$$

$$\Delta V_{\text{test}} = \Delta V_t + \Delta t (\vec{\nabla} \cdot \vec{w}) \Delta V_t$$

$$\frac{d}{dt} (\Delta V_t) = (\vec{\nabla} \cdot \vec{w}) \Delta V_t$$

# Bernoulli's Principle (united, conservative body force)

incompressible  
steady flow

$$\frac{1}{2} |\vec{u}|^2 + \frac{\rho g}{\rho_0} = \text{constant on each pathline}$$

irrotational

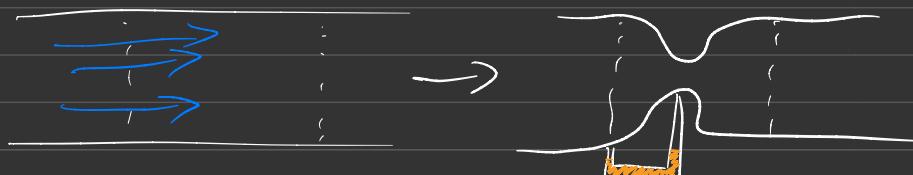
$$\vec{\nabla} \times \vec{u} = \vec{0}$$

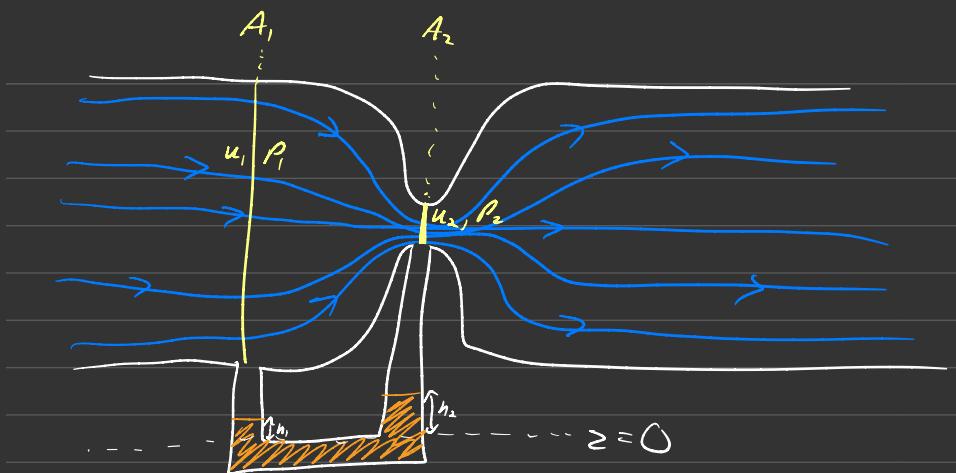
$$\vec{u} = \vec{\nabla} \phi$$

$$\frac{\partial \phi}{\partial t} + \frac{1}{2} |\vec{\nabla} \phi|^2 + \frac{\rho g}{\rho_0} + \int \frac{dP}{\rho} = C(t)$$

everywhere in the fluid

## Venturi meter





$$\frac{1}{2} u_1^2 + \frac{p_1}{\rho_0} \approx \frac{1}{2} u_2^2 + \frac{p_2}{\rho_0}$$

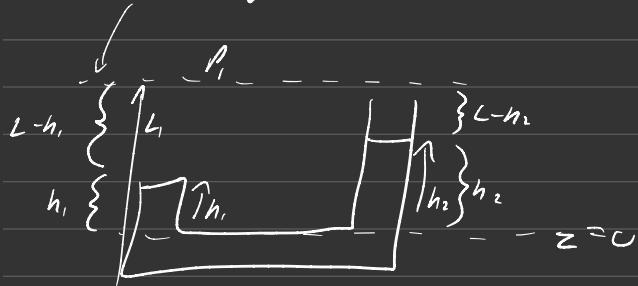
$$p_1 - p_2 = \frac{1}{2} \rho_0 (u_2^2 - u_1^2)$$

$$\frac{dm}{dt} = \rho_0 A_1 \frac{dx_1}{dt} = \rho_0 A_1 u_1 \\ = \rho_0 A_2 u_2$$

$$\Rightarrow A_1 u_1 = A_2 u_2 \quad , \quad u_2 = \frac{A_1}{A_2} u_1$$

$$\therefore p_1 - p_2 = \frac{1}{2} \rho_0 \left[ \frac{A_1^2}{A_2^2} - 1 \right] u_1^2$$

center of pressure



$$\rho_i + \rho_0(L - h_1)g + \rho_{H_2}h_1g$$

$$= \rho_i + (\rho_{H_2} - \rho_0)gh_1 + \rho_0 Lg$$

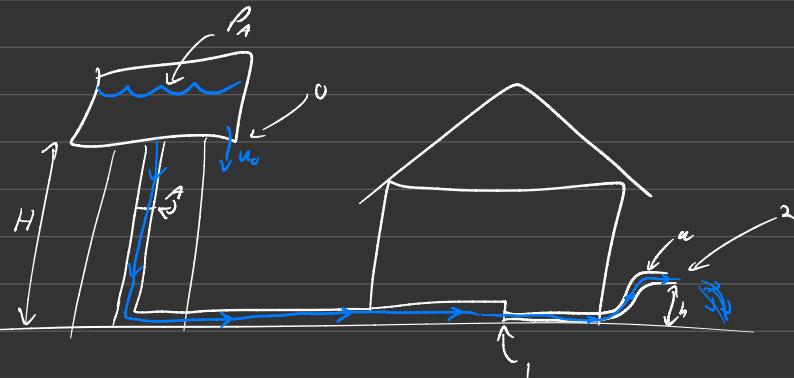
$$\rho_2 + (\rho_{H_2} - \rho_0)gh_2 + \rho_0 Lg$$

$$\rho_i + (\rho_{H_2} - \rho_0)gh_1 = \rho_2 + (\rho_{H_2} - \rho_0)gh_2$$

$$\rho_i - \rho_2 = (\rho_{H_2} - \rho_0)g(h_2 - h_1)$$

$$n_i = \sqrt{\frac{2(\rho_{H_2} - \rho_0)g(h_2 - h_1)}{\rho_0\left(\left(\frac{A_1}{A_2}\right)^2 - 1\right)}}$$

## Speed of water out of bore



$$\frac{1}{2} u_0^2 + gH + \frac{P_1}{\rho_0} = \frac{1}{2} u_2^2 + \frac{P_2}{\rho_0} = \frac{\bar{J}^2}{2A^2} + \frac{P_2}{\rho_0}$$

$\left. \begin{array}{l} \bar{J} = \text{water flux} = \text{volume per time} \\ \rho_0 A u_0 = \bar{J} \rho_0 \end{array} \right\}$

$$\bar{J} = A u_0$$

$$P_1 = \rho_0 g H + P_A - \frac{\bar{J}^2}{2A^2}$$

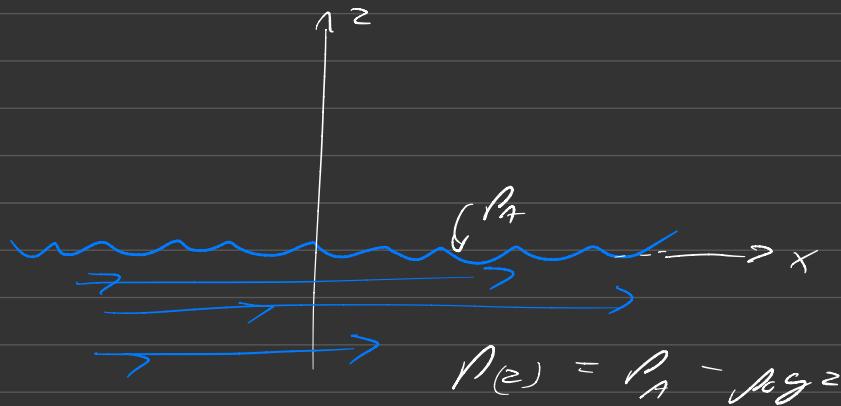
$$\left. \begin{array}{l} u_2 = \bar{J} \\ A \end{array} \right\}$$

$$\frac{1}{2} u_0^2 + \frac{P_1}{\rho_0} = \frac{1}{2} u_2^2 + g h + \frac{P_2}{\rho_0}$$

$$\underbrace{P_A + \rho_0 g H}_{P_A + \rho_0 g H / \bar{J}} = \frac{\bar{J}^2}{2A^2} + g h + \frac{P_2}{\rho_0}$$

$$\rho_2 = \rho_A + \rho_0 g (H - h) - \frac{\sigma^2}{2\alpha^2}$$

Example



$$\vec{w} = u_0 \hat{e}_x$$

$$\vec{\nabla} \times \vec{w} = \vec{0}$$

$$\vec{w} = \vec{\nabla} \varphi = \frac{\partial \varphi}{\partial x} \hat{e}_x + \frac{\partial \varphi}{\partial y} \hat{e}_y + \frac{\partial \varphi}{\partial z} \hat{e}_z$$

$$\varphi(t, x) = u_0 x + f(t)$$

$$\frac{d\varphi}{dt} = \frac{1}{2} |\vec{\nabla} \varphi|^2 + C(t)$$

$$\cancel{f(t)} + \frac{1}{2} \cancel{\dot{u}_0^2} + g^2 + \frac{P}{\rho_0} = C(t)$$

$$= f(t) + \frac{1}{2} \cancel{\dot{u}_0^2} + \frac{P_A}{\rho}$$

$$\Rightarrow P(z) = P_A - \rho_0 g z$$

wave

$$\mathcal{Q}(t, \vec{r}) \text{ and } \mathcal{Q}(t, \vec{r}) + f(t)$$

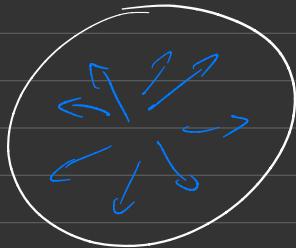
$$\frac{d\mathcal{Q}}{dt} = \frac{1}{2} |\vec{\nabla} \mathcal{Q}|^2 + 2E + \int \frac{dP}{\rho} = C(t)$$

$$\mathcal{Q} \rightarrow \mathcal{Q} + f(t)$$

$$\frac{d\mathcal{Q}}{dt} + f(t) + \frac{1}{2} |\vec{\nabla} \mathcal{Q}|^2 + 2E + \int \frac{dP}{\rho} = Q(t) E$$

pick  $f(t)$  such that  $f(t) = C(t) - E$

# Water balloon



$$\vec{u} = u(t, r) \hat{e}_r$$

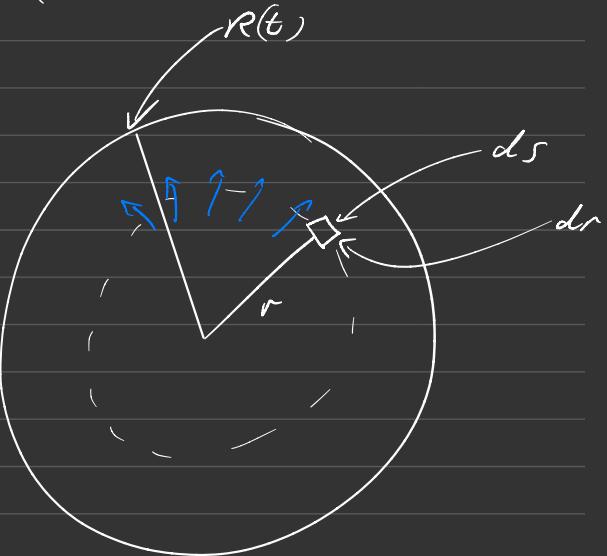
$$\bar{J}(t)$$

$$\rho_0 dS dr = \rho_0 \bar{J} dt$$

$$4\pi r^2 dr = \bar{J} dt$$

$$\bar{J} = 4\pi r^2 u$$

$$u(t, r) = \frac{\bar{J}(t)}{4\pi r^2}$$



$$\vec{u} = u \hat{e}_r = \frac{\bar{J}(t)}{4\pi r^2} \hat{e}_r$$

$$= \vec{\nabla} Q = \frac{\partial Q}{\partial r} \hat{e}_r$$

$$Q(t, r) = \frac{-\bar{J}(t)}{4\pi r} + f(t)$$

$$\frac{\partial \rho}{\partial t} + \frac{1}{2} \nabla \rho / \hat{r} + \frac{P}{\rho_0} = C(t)$$

$$-\frac{\dot{J}(t)}{4\pi r} + f + \frac{1}{2} \left( \frac{\dot{J}(t)}{4\pi r^2} \right)^2 + \frac{P(t, r)}{\rho_0} = C(t)$$

$$= -\frac{\dot{J}(t)}{4\pi R(t)} + f(t) + \frac{1}{2} \dot{R}(t)^2 + \frac{P_A}{\rho_0}$$

$$= -\frac{\dot{J}}{4\pi r} + \frac{1}{2} \left( \frac{\dot{J}}{4\pi r^2} \right)^2 + \frac{P}{\rho_0}$$

$$= -\frac{\dot{J}(t)}{4\pi R(t)} + \frac{1}{2} \dot{R}^2 + \frac{P_A}{\rho_0}$$

$$\dot{J}(t) = \frac{d}{dt} \left( \frac{4}{3} \pi R^3 \right)$$

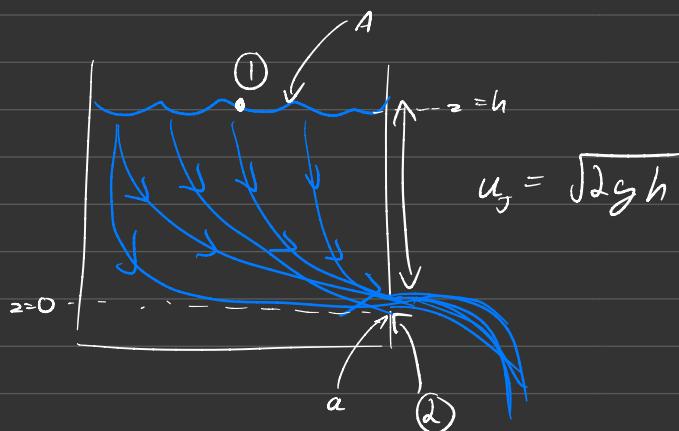
Cool Books

Landau and Lifshitz

Fluid Mechanics

## Torricelli's Law

inviscid  
steady  
incompressible



$$\frac{1}{2} \vec{u}^2 + \frac{P}{\rho_0} = \text{constant along each pathline}$$

$$\frac{1}{2} |u_s|^2 + gh + \frac{P_A}{\rho_0} = \frac{1}{2} |u_J|^2 + \frac{P_A}{\rho_0}$$

$$|u_J|^2 = |u_s|^2 + 2gh$$

$$u_J^2 = \frac{a^2}{A^2} u_s^2 + 2gh$$

$$\frac{dV}{dt} = \bar{J} = \alpha u_J = A u_s$$

$$\Rightarrow u_s = \frac{a}{A} u_J$$

$$u_J = \sqrt{\frac{2gh}{1 - \frac{a^2}{A^2}}}$$

$$\approx \sqrt{2gh}$$



$$h(t), \frac{dh}{dt} = -as, h(0) = H$$

$$= -\frac{a}{A} u_5$$

$$= -\frac{a}{A} \sqrt{\frac{2g}{1 - \frac{a^2}{A^2}}} \sqrt{h}$$

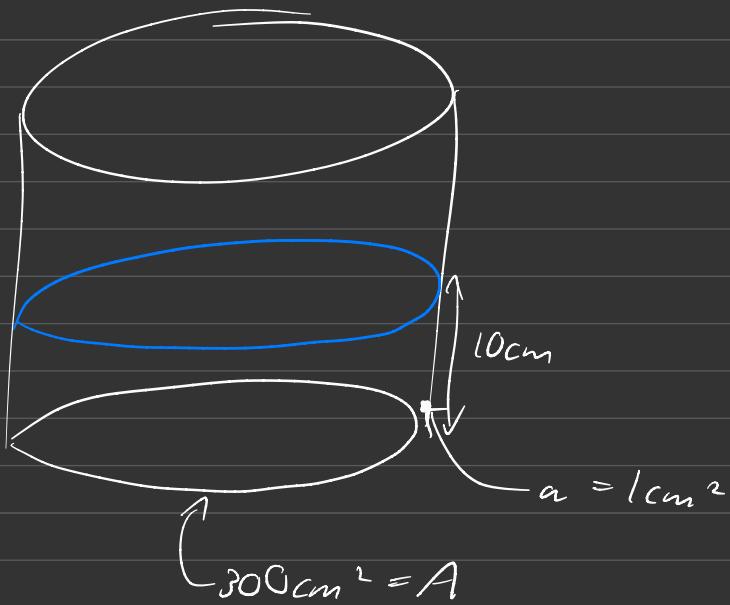
$$\frac{1}{\sqrt{h}} dh = -\frac{a}{A} \sqrt{\frac{2g}{1 - \frac{a^2}{A^2}}} dt$$

$$2\sqrt{h} = -\frac{a}{A} \sqrt{\frac{2g}{1 - \frac{a^2}{A^2}}} t + C$$

$$2\sqrt{h(t)} = 2\sqrt{H} - \frac{a}{A} \sqrt{\frac{2g}{1 - \frac{a^2}{A^2}}} t$$

$$h(t) = \left( \sqrt{H} - \frac{a}{2A} \sqrt{\frac{2g}{1 - \frac{a^2}{A^2}}} t \right)^2$$

$$h(T) = 0 \quad T = \frac{2\sqrt{H}A}{a} \sqrt{\frac{1 - \frac{a^2}{A^2}}{2g}}$$



$$T = \frac{2\sqrt{hA}}{a} \sqrt{\frac{1 - \frac{a^2}{A^2}}{2g}}$$

$$\times \frac{4}{a} \sqrt{\frac{2h}{2g}}$$

$$= \frac{300}{1} \sqrt{\frac{2 \cdot 0.1}{9.81}} = 135 \text{ s}$$

$\approx 2 \text{ mins}$

## Speed of Sound and Mach number

$$\rho(p) : c(p) = \sqrt{\rho'(p)}$$

$$M = \frac{|\vec{u}|}{c} \quad \left| \begin{array}{l} M \ll 1 \Rightarrow \text{approx incompressible} \end{array} \right.$$

Inviscid  
Irrotational  
No body force  
Steady

$$\frac{\partial \varphi}{\partial t} + \frac{1}{2} |\nabla \varphi|^2 + \cancel{\psi} + \int \frac{dp}{\rho} = c(t) = \epsilon$$

Bernoulli

$$\frac{1}{2} |\vec{u}|^2 + \int \frac{\rho'(p)}{\rho} dp = \epsilon$$

$$\frac{1}{2} M^2 c^2(p) + \int \frac{\rho'(p)}{\rho} dp = \epsilon$$

Example 1: Isothermal ideal gas

$$P(\rho) = \frac{k_B T}{m} \rho$$

$$c = \sqrt{P(\rho)} = \sqrt{\frac{k_B T}{m}} = c_0$$

$$\begin{aligned} \int \frac{d\rho}{\rho} &= \int \frac{P'(\rho) d\rho}{\rho} = \int \frac{\frac{k_B T}{m}}{\rho} d\rho \\ &= \frac{k_B T}{m} \ln \rho \end{aligned}$$

$$\frac{1}{2} \gamma^2 c_0^2 + c_0^2 \ln \rho = \epsilon$$

If  $m_0, \rho_0$  known at some point in  
the fluid

$$\frac{1}{2} \gamma^2 c_0^2 + c_0^2 \ln \rho = \frac{1}{2} \gamma_0^2 c_0^2 + c_0^2 \ln \rho_0$$

$$\rho(\gamma) = \rho_0 \exp\left(\frac{1}{2}(\gamma_0^2 - \gamma^2)\right)$$

$$= \rho_0 \exp\left(\frac{\gamma_0^2}{2}\right) \exp\left(-\frac{\gamma^2}{2}\right)$$

$$= \rho_0 \exp\left(\frac{\gamma_0^2}{2}\right) \left(1 - \frac{1}{2}\gamma^2 + \frac{1}{8}\gamma^4 - \dots\right)$$

Example 2 : Thermally insulated monoatomic gas

$$P(\rho) \propto \rho^{\frac{C_p}{C_V}}, \quad C_V = \frac{3}{2} Nk_B$$

$$P(\rho) = K \rho^{\frac{5}{3}} \quad C_p = \frac{5}{2} Nk_B$$

$$P'(\rho) = \frac{5K}{3} \rho^{\frac{2}{3}}$$

$$C(\rho) = \sqrt{\frac{5K}{3}} \rho^{\frac{1}{3}}$$

Suppose we have  $\rho_0, c_0$  at some point  
in the fluid

$$c_0 = \sqrt{\frac{5K}{3}} \rho_0^{\frac{1}{3}}, \quad K = \frac{3c_0^2}{5\rho_0^{\frac{2}{3}}}$$

$$C(\rho) = c_0 \left( \frac{\rho}{\rho_0} \right)^{\frac{1}{3}}$$

$$\rho(\rho) = \frac{3}{5} \rho_0 c_0^2 \left( \frac{\rho}{\rho_0} \right)^{\frac{5}{3}}$$

$$P'(\rho) = c_0^2 \left( \frac{\rho}{\rho_0} \right)^{\frac{2}{3}}$$

$$\int \frac{dP}{\rho} d\rho = \frac{c_0^2}{\rho_0^{\frac{2}{3}}} \int \rho^{\frac{2}{3}} d\rho$$

$$= \frac{3c_0^2}{2\rho_0^{\frac{2}{3}}} \rho^{\frac{2}{3}}$$

$$\frac{1}{2} w^2 + \frac{3c_0^2}{2} \left( \frac{\rho}{\rho_0} \right)^{\frac{2}{3}} = \mathcal{E}$$

$$\frac{1}{2} \gamma c_0^2 \left( \frac{\rho}{\rho_0} \right)^{\frac{2}{3}} + \frac{3}{2} c_0^2 \left( \frac{\rho}{\rho_0} \right)^{\frac{2}{3}} = \mathcal{E}$$

$$= \frac{1}{2} c_0^2 \left( \frac{\rho}{\rho_0} \right)^{\frac{2}{3}} (\gamma^2 + 3)$$

$$= \frac{1}{2} c_0^2 (\gamma_0^2 + 3)$$

$$\rho = \rho_0 \left( \frac{\gamma_0^2 + 3}{\gamma^2 + 3} \right)^{\frac{3}{2}}$$

$$\propto \rho_0 \left( 1 + \frac{\gamma_0^2}{3} \right)^{\frac{3}{2}} + O(\gamma^2)$$

$$\gamma \ll 1$$

$$\text{Thermal Physics stuff} \quad \left( \text{understanding} \right)$$

$$\int \frac{dP}{P} \Rightarrow \perp \vec{P} \quad \left( \int \frac{dt}{P} \right)$$

$$dU = TdS - PdV$$

$$H = \text{enthalpy} = U + PV$$

$$dH = dU + VdP + PdV$$

$$= TdS + VdP$$

$M$  = mass

$$\frac{dT}{M} = \frac{TdS}{M} + \frac{VdP}{M}$$

$$d\left(\frac{H}{M}\right) = Td\left(\frac{S}{M}\right) + \frac{dP}{P}$$

$$\text{specific enthalpy} = \frac{H}{m} = w$$

$$\text{specific entropy} = \frac{S}{M} = s$$

$$\Rightarrow dw = \vec{ds} + \int \frac{dP}{\rho}$$

If  $s = \text{const}$

$$dw = \frac{dP}{\rho}$$

$$\vec{D}w = \frac{\vec{D}\rho}{\rho}$$

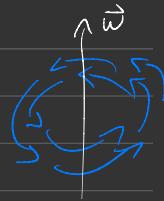
$$\vec{D} \left( \frac{\partial \varphi}{\partial t} + \frac{1}{2} |\vec{D}\varphi|^2 + \psi \right) = - \frac{1}{\rho} \vec{D}\rho$$

$$\int \frac{dP}{\rho} = \int_{r_0}^r \vec{D}\rho \cdot d\vec{r} = w$$

# A worked example

$$(\rho = \rho_0)$$

Inviscid, Incompressible, steady



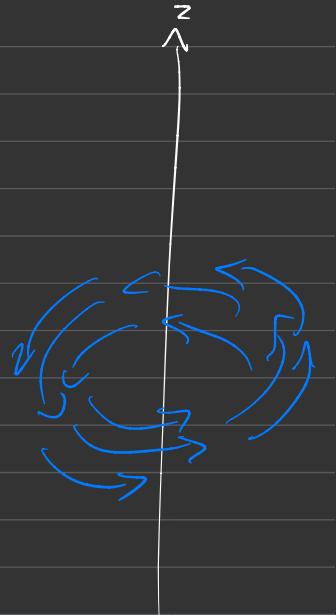
$$\vec{f} = -g\hat{e}_z$$

$$\nabla \cdot \vec{u} = 0$$

$$\rho_0 (\vec{u} \cdot \vec{\nabla}) \vec{u} = -\vec{\nabla} P - \rho_0 g \hat{e}_z$$

$$\vec{u} = u(r, \theta, z) \hat{e}_\theta$$

$$\vec{\nabla} \cdot \vec{u} = \frac{1}{r} \frac{\partial}{\partial r} (r u_r) + \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} + \frac{\partial u_z}{\partial z}$$



$$= \frac{1}{r} \frac{\partial u_r}{\partial \theta} = 0$$

$\Rightarrow u$  indep of  $\theta$

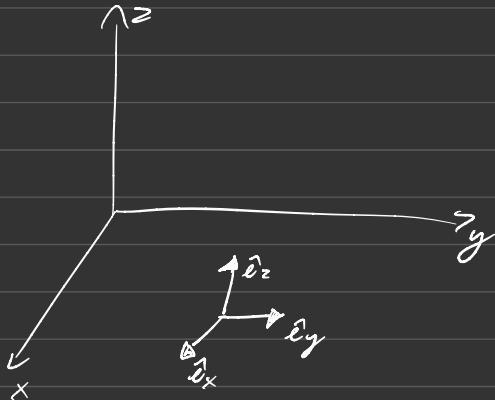
$$\vec{\nabla} = \hat{e}_r \frac{\partial}{\partial r} + \hat{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} + \hat{e}_z \frac{\partial}{\partial z}$$

$$\vec{u} \cdot \vec{\nabla} = u_r \frac{\partial}{\partial r} + \frac{u_\theta}{r} \frac{\partial}{\partial \theta} + u_z \frac{\partial}{\partial z}$$

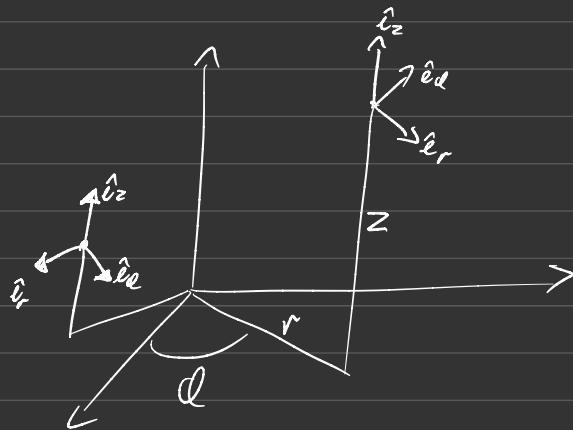
$$= \frac{u}{r} \frac{\partial}{\partial \theta}$$

$$(\vec{u} \cdot \vec{\nabla}) \vec{u} = \frac{u(r, z)}{r} \frac{\partial}{\partial \theta} [u(r, z) \hat{e}_\theta]$$

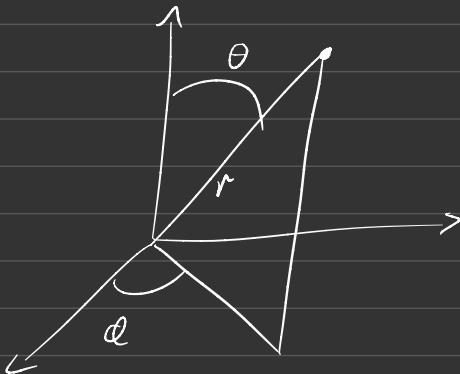
Cartesian



Cylindrical



# Spherical



$$\frac{\partial}{\partial r} \hat{e}_r = 0 = \frac{\partial}{\partial z} \hat{e}_r$$



$$\frac{\partial}{\partial r} \hat{e}_\phi = 0 = \frac{\partial}{\partial z} \hat{e}_\phi$$



$$\frac{\partial}{\partial \phi} \hat{e}_r = a \hat{e}_\phi$$



$$\frac{\partial}{\partial \phi} \hat{e}_\phi = -b \hat{e}_y$$

$$\frac{d}{d\phi} (\hat{e}_r \cdot \hat{e}_\phi) = 0$$

$$a \hat{e}_\phi \cdot \hat{e}_\phi + \partial_r \cdot (-b \hat{e}_r) = a - b = 0$$

$$\hat{e}_r = \cos\theta \hat{e}_x + \sin\theta \hat{e}_y$$

$$\hat{e}_\theta = -\sin\theta \hat{e}_x + \cos\theta \hat{e}_y$$

$$\hat{e}_z = \hat{e}_z$$

$$\frac{\partial \hat{e}_r}{\partial \theta} = -\sin\theta \hat{e}_x + \cos\theta \hat{e}_y = \hat{e}_\theta$$

$$\frac{\partial \hat{e}_\theta}{\partial \theta} = -\cos\theta \hat{e}_x - \sin\theta \hat{e}_y = -\hat{e}_r$$

$$\hat{e}_r = \sin\theta \cos\phi \hat{e}_x + \sin\theta \sin\phi \hat{e}_y + \cos\theta \hat{e}_z$$

$$\hat{e}_\theta = \cos\theta \cos\phi \hat{e}_x + \cos\theta \sin\phi \hat{e}_y - \sin\theta \hat{e}_z$$

$$\hat{e}_\phi = -\sin\phi \hat{e}_x + \cos\phi \hat{e}_y$$

$$\frac{\partial \hat{e}_r}{\partial \phi} = -\cos\phi \hat{e}_x - \sin\phi \hat{e}_y$$

$$\hat{e}_x = \sin\theta \cos\phi \hat{e}_r + \cos\theta \cos\phi \hat{e}_\theta - \sin\theta \hat{e}_z$$

$$\hat{e}_y = \sin\theta \sin\phi \hat{e}_r + \cos\theta \sin\phi \hat{e}_\theta + \cos\theta \hat{e}_z$$

$$(\vec{u} \cdot \vec{\nabla}) \vec{u} = \frac{u}{r} \frac{\partial}{\partial \theta} (\text{uice})$$

$$= \frac{u}{r} (-u \hat{e}_r)$$

$$= -\frac{u^2}{r} \hat{e}_r$$

$$\cancel{-\frac{\rho_0 u^2}{r}} \hat{e}_r = -\vec{\nabla} P + \rho_0 \vec{f}$$

$$= -\vec{\nabla} P - \rho_0 g \hat{e}_z$$

$$r : -\frac{\rho_0 u^2}{r} = -\frac{\partial P}{\partial r}$$

$$d : 0 = -\frac{1}{r} \frac{\partial P}{\partial \theta} \Rightarrow P \text{ independent of } \theta$$

$$z : 0 = -\frac{\partial P}{\partial z} - \rho_0 g = \frac{\partial}{\partial z} (P + \rho_0 g z)$$

$$\Rightarrow P + \rho_0 g z = f(r) \quad \swarrow$$

$$\rho = f(r) - \rho_0 g =$$

$$\frac{\rho_0 u(r)}{r} = f'(r)$$

$$\vec{\omega} = \vec{\nabla} \times \vec{u} = \hat{e}_r \left( \frac{\partial u_r}{\partial z} - \frac{1}{r} \frac{\partial u_z}{\partial \theta} \right)^0 + \hat{e}_{\theta} \left( \frac{\partial u_r}{\partial z} - \frac{\partial u_z}{\partial r} \right)^0 + \hat{e}_z \left( \frac{1}{r} \frac{\partial}{\partial r} (ru_{\theta}) - \frac{1}{r} \frac{\partial u_r}{\partial \theta} \right)^0$$

$$\vec{\omega} = \hat{e}_z \frac{1}{r} \frac{d}{dr} (ru_{\theta})$$

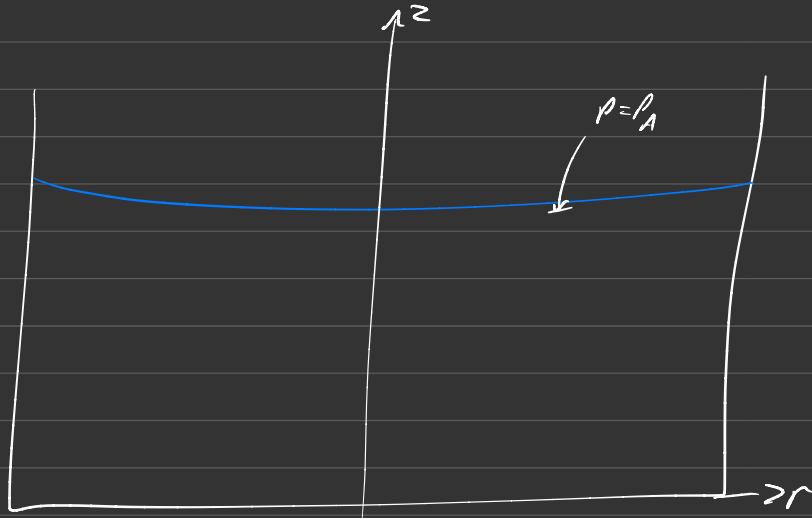
$$u(r) = \sqrt{2}r \quad (\vec{u} = \sqrt{2} \times \vec{r})$$

$$\vec{\omega} = 2\sqrt{2} \hat{e}_z$$

$$f'(r) = \mu_0 \sqrt{2}^2 r$$

$$f(r) = \frac{1}{2} \mu_0 \sqrt{2}^2 r^2 + \rho_0$$

$$P(r, \theta, z) = P_0 + \frac{1}{2} \rho_0 \sigma^2 r^2 - \rho_0 g z$$



$$P_A = P_0 + \frac{1}{2} \rho_0 \sigma^2 r^2 - \rho_0 g z(r)$$

$$z(r) = \frac{\sigma^2}{2g} r^2 + \text{constant}$$

So the surface  
of the spinning  
liquid is a  
parabola!

## Basisgrößen

$$P(\rho) \text{ or } \rho(P)$$

$$1\text{st Law: } dU = TdS - PdV$$

$$\Rightarrow U(S, V)$$

$\Rightarrow$  There is a relation  
between  $U, S, V$

$$H = U + PV$$

$$dH = TdS + VdP$$

$$F = U - TS$$

$$dF = -SdT - PdV$$

$$u = \frac{U}{N}, \quad s = \frac{S}{N}$$

$$du = Tds - \rho$$

$$= Tds + \frac{\rho}{\rho^2} d\rho$$

$$u(\rho, P) \quad s(\rho, P) \quad w(\rho, P) \quad T(\rho, P)$$

$\gamma = u \text{ or } s \text{ or } w \text{ or } T$

$$(\gamma, \rho, P)$$

$$\rho(p, \gamma)$$

$\gamma = \text{conserved}$

$$\gamma = \gamma_0$$

$$\rho(p, \gamma_0)$$

Sackur-Tetrode Entropy  
- monatomic ideal gas

$$S(U, V) = Nk_B \left\{ \ln \left[ \frac{V}{N} \left( \frac{4\pi U}{3Nh^2} \right)^{\frac{3}{2}} \right] + \frac{5}{2} \right\}$$

$$\frac{S}{N} = \frac{Nk_B}{Nm} \left\{ \ln \left[ \frac{V}{N} \left( \frac{2\pi PV}{Nh^2} \right)^{\frac{3}{2}} \right] + \frac{5}{2} \right\}$$
$$U = \frac{3}{2} Nk_B T = \frac{3}{2} PV$$

$$S = \frac{k_B}{m} \left\{ \ln \left[ \left( \frac{V}{N} \right)^{\frac{5}{2}} \left( \frac{2\pi P}{h^2} \right)^{\frac{3}{2}} \right] + \frac{3}{2} \right\}$$

$$= \frac{U_A}{m} \left\{ \ln \left[ \left( \frac{m}{V} \right)^{\frac{5}{2}} \left( \frac{2\pi\rho}{m^2} \right)^{\frac{3}{2}} \right] + \frac{5}{2} \right\}$$

$$S = S_0$$

$$\frac{\rho^{\frac{3}{2}}}{V^{\frac{5}{2}}} = \text{const}$$

$$\rho \propto V^{\frac{5}{3}}$$

$$PV = Nk_B T$$

$$\rho = \frac{U_A T}{m} \rho$$

$$\frac{\partial \varphi}{\partial t} = \frac{\partial \varphi}{\partial t} + (\vec{\omega} \cdot \vec{\nabla}) \varphi = 0$$

Biotropic is conserved quantity  $\varphi$ ,  
 inviscid, conservative local for  
 $\Rightarrow$  conserved quantity

$$\frac{\partial}{\partial t} \left( \frac{\vec{\omega} \cdot \vec{\nabla} \varphi}{\rho} \right) = 0$$

$$\vec{\nabla} \rho = \vec{\nabla} \int \frac{\rho'(\rho)}{\rho} d\rho$$

$$\frac{\partial \vec{u}}{\partial t} + \frac{1}{2} \vec{\nabla} |\vec{u}|^2 + \vec{u} \cdot \vec{\nabla} \vec{u} = - \vec{\nabla} \left( \frac{u^2}{2} + \int \frac{\rho g}{\rho} d\rho \right)$$

$$\frac{d\vec{u}}{dt} + (\vec{u} \cdot \vec{\nabla}) \vec{u}$$

$$= \frac{D\vec{u}}{Dt} = (\vec{u} \cdot \vec{\nabla}) \vec{u} - \vec{u} (\vec{\nabla} \cdot \vec{u})$$

$$\frac{D\vec{u}}{Dt} = (\vec{u} \cdot \vec{\nabla}) \vec{u} - \vec{u} (\vec{\nabla} \cdot \vec{u}) =$$

$$= (\vec{u} \cdot \vec{\nabla}) \vec{u} + \frac{1}{\rho} \frac{d\rho}{dt} \vec{u}$$

$$\frac{\partial f}{\partial t} + \vec{\nabla} \cdot (\rho \vec{u}) = \frac{Df}{Dt} + \rho (\vec{\nabla} \cdot \vec{u}) = 0$$

$$\frac{1}{\rho} \frac{D\vec{u}}{Dt} - \frac{\vec{u}}{\rho} \frac{D\rho}{Dt} = (\frac{\vec{u}}{\rho} \cdot \vec{\nabla}) \vec{u}$$

$$\underbrace{\frac{D}{Dt} \left( \frac{\vec{u}}{\rho} \right)}_{\left. \left( \sum_j \frac{\partial u_j}{\partial x_j} \frac{D}{Dt} \left( \frac{u_j}{\rho} \right) = \sum_j \left( \frac{\vec{u}}{\rho} \cdot \vec{\nabla} \right) u_j \frac{\partial u_j}{\partial x_j} \right) \right\}}$$

$$\frac{Dg}{Dt} = 0 = \frac{\partial g}{\partial t} + \sum_j u_j \frac{\partial g}{\partial x_j}$$

$$\begin{aligned}
 \frac{\partial}{\partial x_i} \left( \frac{\partial \varphi}{\partial t} \right) &= \frac{\partial}{\partial x_i} \left( \frac{\partial \varphi}{\partial t} \right) + \frac{\partial}{\partial x_i} \left( \sum_j u_j \frac{\partial \varphi}{\partial x_j} \right) \\
 &= \frac{\partial^2 \varphi}{\partial t \partial x_i} + \sum_j \left( \frac{\partial u_j}{\partial x_i} \frac{\partial \varphi}{\partial x_j} + u_j \frac{\partial^2 \varphi}{\partial x_i \partial x_j} \right) \\
 &= \frac{\partial}{\partial t} \left( \frac{\partial \varphi}{\partial x_i} \right) + \sum_j u_j \frac{\partial}{\partial x_j} \left( \frac{\partial \varphi}{\partial x_i} \right) + \sum_j \frac{\partial u_j}{\partial x_i} \frac{\partial \varphi}{\partial x_j} \\
 &= \frac{\partial}{\partial t} \left( \frac{\partial \varphi}{\partial x_i} \right) + \sum_j \frac{\partial u_j}{\partial x_i} \frac{\partial \varphi}{\partial x_j}
 \end{aligned}$$

$$\sum_i \frac{w_i}{\rho} \frac{\partial}{\partial t} \left( \frac{\partial \varphi}{\partial x_i} \right) = - \sum_j \frac{\partial u_j}{\partial x_i} \frac{\partial \varphi}{\partial x_j} \frac{w_i}{\rho}$$

$$\frac{\vec{w}}{\rho} \cdot \frac{\partial}{\partial t} (\vec{\nabla} \varphi) = - \sum_{ij} \frac{w_i}{\rho} \frac{\partial u_j}{\partial x_i} \frac{\partial \varphi}{\partial x_j}$$

$$\left\{ \left( \vec{\nabla} \varphi \cdot \frac{\partial}{\partial t} \left( \frac{\vec{w}}{\rho} \right) = \sum_i \frac{w_i}{\rho} \frac{\partial u_i}{\partial x_i} \frac{\partial \varphi}{\partial x_i} \right) \right. \\
 \left. \frac{\vec{w}}{\rho} \cdot \frac{\partial}{\partial t} (\vec{\nabla} \varphi) + (\vec{\nabla} \varphi) \cdot \frac{\partial}{\partial t} \left( \frac{\vec{w}}{\rho} \right) = 0 \right.$$

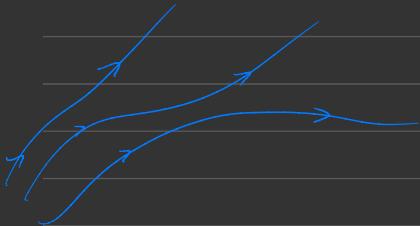
$$= \frac{\partial}{\partial t} \left( \frac{\vec{w} \cdot \vec{\nabla} \varphi}{\rho} \right) = 0$$

## Pathlines

physical trajectories each bit  
of a fluid follows

$$t = t_0, \quad \vec{r} = \vec{r}_0$$

$$\frac{d\vec{r}(t)}{dt} = \vec{u}(t, \vec{r}(t))$$



## Streamlines

Snapshots of overall fluid flow at  
a fixed time

$$\text{pick } t: \vec{r}_t(\vec{r})$$

$$\frac{d\vec{r}_t}{d\vec{r}}(\vec{r}) = \vec{u}(t, \vec{r}_t(\vec{r}))$$



## Streaklines



$\frac{D}{Dt}$  : pathline

$\Psi$  : streamlines

22.2<sup>3</sup> fluids

$$W(z) = \varphi(x, y) + i\psi(x, y)$$

$$\text{and } \frac{\partial \varphi}{\partial t} + \frac{1}{2} |\vec{\nabla} \varphi|^2 + \Sigma + \frac{\rho}{\rho_0} = C(t)$$

$$z = x + iy$$

Suppose

$\kappa, u_0$  positive real constants

$$w(z) = \frac{u_0}{\kappa} \sin \kappa z$$

$$w(x+iy) = \frac{u_0}{\kappa} \sin(\kappa(x+iy))$$

$$= \frac{u_0}{\kappa} \frac{1}{2i} [e^{i\kappa(x+iy)} - e^{-i\kappa(x+iy)}]$$

$$= \frac{u_0}{2i\kappa} [e^{i(u_x - \kappa y)} - e^{-i(u_x + \kappa y)}]$$

$$= \frac{u_0}{2i\kappa} \left\{ [\cos(\kappa x) + i\sin(\kappa x)][\cosh(u_y) - i\sinh(u_y)] \right. \\ \left. - [\cosh(\kappa x) - i\sin(\kappa x)][\cosh(u_y) + i\sinh(u_y)] \right\}$$

$$= \frac{U_0}{\kappa} [\sinh(\kappa_x) \cosh(\kappa_y) + i \cos(\kappa_x) \sinh(\kappa_y)]$$

$$\vartheta(x, y) = \frac{U_0}{\kappa} \sin(\kappa_x) \cosh(\kappa_y)$$

$$\psi(x, y) = \frac{U_0}{\kappa} \cos(\kappa_x) \sinh(\kappa_y)$$

$$\frac{\partial \vartheta}{\partial x} = U_0 \cos(\kappa_x) \cosh(\kappa_y)$$

$$\frac{\partial \psi}{\partial y} = U_0 \cos(\kappa_x) \cosh(\kappa_y)$$

$$\frac{\partial \vartheta}{\partial y} = U_0 \sin(\kappa_x) \sinh(\kappa_y)$$

$$\frac{\partial \psi}{\partial x} = -U_0 \sin(\kappa_x) \sinh(\kappa_y)$$

$$\vec{u} = U_0 \cos(\kappa_x) \cosh(\kappa_y) \hat{e}_x + U_0 \sin(\kappa_x) \sinh(\kappa_y) \hat{e}_y$$

$$w'(z) = U_0 \cos(\kappa z)$$

$$= \frac{U_0}{2} [e^{i\kappa(x+y)} + e^{-i\kappa(x+y)}]$$

$$= U_0 \cos(k_x) \cosh(k_y) - i U_0 \sin(k_x) \sinh(k_y)$$

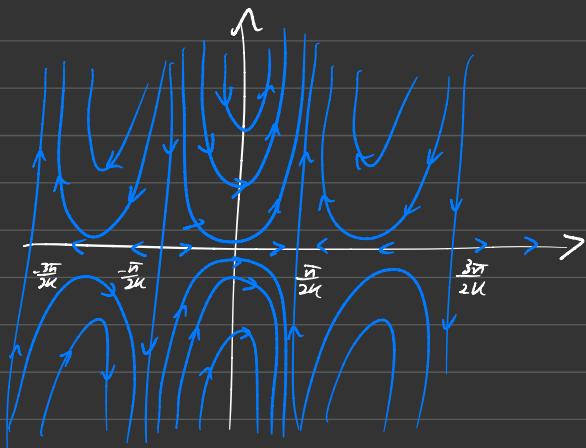
$$\frac{U_0 \cos(k_x) \sinh(k_y)}{k} = \text{const}$$

$$\cos(k_x) \sinh(k_y) = \alpha$$

$$\alpha = 0 : \cos(k_x) \sinh(k_y) = 0$$

$$\cos(k_x) = 0 \Rightarrow x = (2n+1)\frac{\pi}{2}, n \in \mathbb{Z}$$

$$\text{or } \sinh(k_y) = 0 \Rightarrow y = 0$$



$$\sinh(k_y) = \alpha \sec(k_x)$$

$$w = \sinh u$$

$$= \frac{1}{2}(e^u - e^{-u})$$

$$\Rightarrow e^u - 2w - e^{-u} = 0$$

$$(e^u)^2 - 2w(e^u) - 1 = 0$$

$$\Rightarrow e^u = \frac{2w \pm \sqrt{4w^2 + 4}}{2}$$

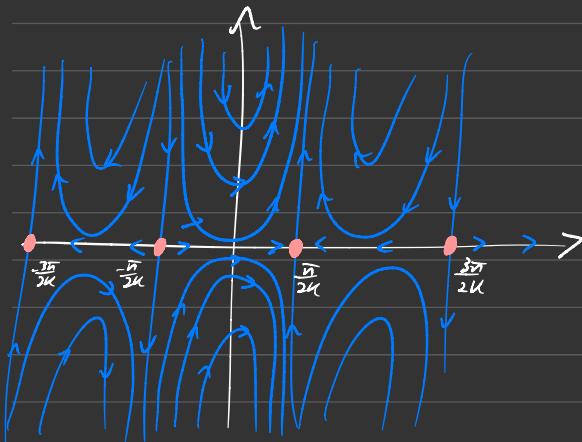
$$= w + \sqrt{w^2 + 1}$$

$$\Rightarrow u = \ln(w + \sqrt{w^2 + 1})$$

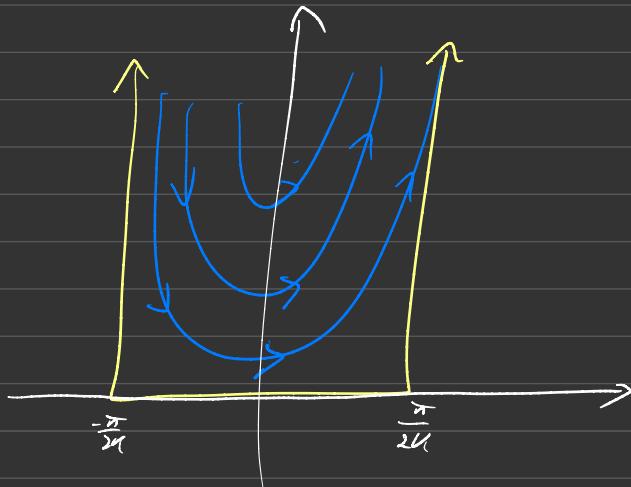
$$= \operatorname{arcsinh}(w)$$

$$y = \frac{1}{K} \ln \left[ 2 \sec(Kx) + \sqrt{2^2 \sec^2(Kx) + 1} \right]$$

"stagnation points"  $\vec{u} = \vec{0}$  at points  $\bullet$



infinitely tall rectangle boundary



$$\frac{1}{2} |\vec{u}|^2 + \frac{\rho}{\rho_0} = \epsilon$$

$$\Rightarrow \frac{1}{2} u_0^2 + \frac{\rho_0}{\rho_0} = \epsilon$$

$$P(x,0) = \rho_0 \Rightarrow \frac{1}{2} u_0^2 + \frac{\rho_0}{\rho_0} = \epsilon$$

$$\frac{u_0^2}{2} [\cos^2(k_x) \cosh^2(k_x) + \sin^2(k_x) \sinh^2(k_y)] + \frac{\rho_0(\epsilon_y)}{\rho_0} = \frac{1}{2} u_0^2 + \frac{\rho_0}{\rho_0}$$

$$P(x,0) = \frac{1}{2} u_0^2 (1 - \cos^2(k_x)) + \frac{\rho_0}{\rho_0}$$

$$= \frac{1}{2} U_0^2 \sin^2(\alpha x) + \frac{P_e}{\rho_0}$$

$$= \frac{1}{2} U_0^2 \sin^2 \left( \frac{\pi x}{a} \right) + \frac{P_e}{\rho_0}$$

$$\vec{F} = \int_{-\frac{a}{2}}^{\frac{a}{2}} P(x, 0) v dx (-\hat{e}_y)$$

$$= - P_{\text{wind}} \hat{e}_y - \frac{3}{4} \sigma_0 a U_0^2 \hat{e}_y$$

$$\sigma_0 = \rho_0 w$$

### Example

$$w(z) = U_0 \left( z + \frac{R^2}{z} \right) \quad 0 < U_0, R \in \mathbb{R}$$

$$w(x, y) = U_0 \left( x \hat{e}_x + \frac{R^2}{x^2 \hat{e}_y^2} \right)$$

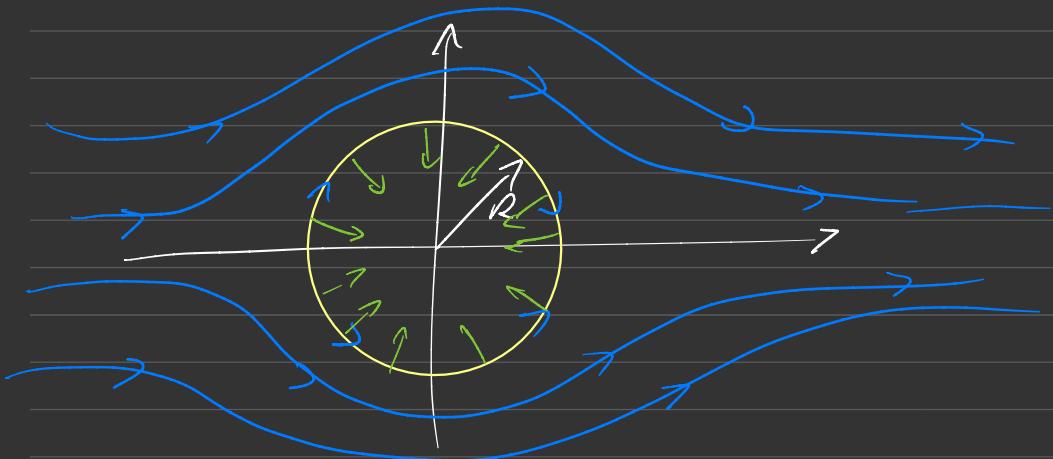
$$= U_0 \left( x \hat{e}_x + \frac{R(x \hat{e}_y)}{x^2 \hat{e}_y^2} \right)$$

$$d(x, y) = U_0 \left( 1 + \frac{R^2}{x^2 \hat{e}_y^2} \right) x$$

$$q(x, y) = U_0 \left( 1 - \frac{R^2}{x^2 \hat{e}_y^2} \right) y$$

$$\psi(x, y) = K \quad \text{constant}$$

$$\psi(x, y) = C : \quad y = 0, \quad x^2 + y^2 = R^2$$



$$u_x = U_0 \left[ 1 + \frac{R^2 (x^2 - y^2)}{(x^2 + y^2)^2} \right] = U_0 \left[ 1 + \frac{R^2 \cos 2\theta}{r^2} \right]$$

$$u_y = \frac{-2 U_0 R^2 x y}{(x^2 + y^2)^2} = \frac{U_0 R^2 \sin 2\theta}{r^2}$$

$$|\vec{v}| \rightarrow \infty \Rightarrow \vec{v} = U_0 \hat{e}_x$$

$$\frac{U_0^2}{2} \left[ 1 + \frac{2R^2}{r^2} \cos 2\theta + \frac{R^4}{r^4} \right] + \frac{\rho}{\rho_0} = \epsilon$$

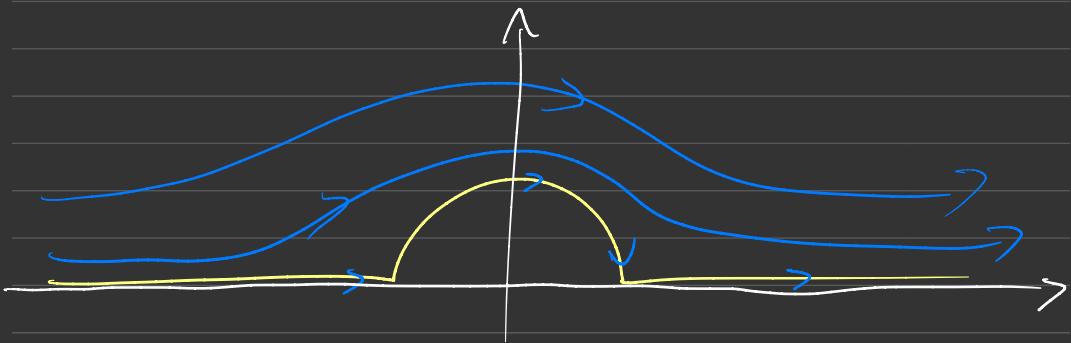
$$= \frac{U_0^2}{2} + \frac{\rho}{\rho_0}$$

$$\rho = \rho_\infty - \rho_0 \frac{U_0^2}{2} \left[ \frac{2R^2}{r^2} \cos 2\theta + \frac{R^4}{r^4} \right]$$

$$\vec{F} = \int_0^{2\pi} \rho(R, \theta) (\cos \theta \hat{x}_x - \sin \theta \hat{e}_y) \omega R d\theta$$

$$= \vec{0}$$

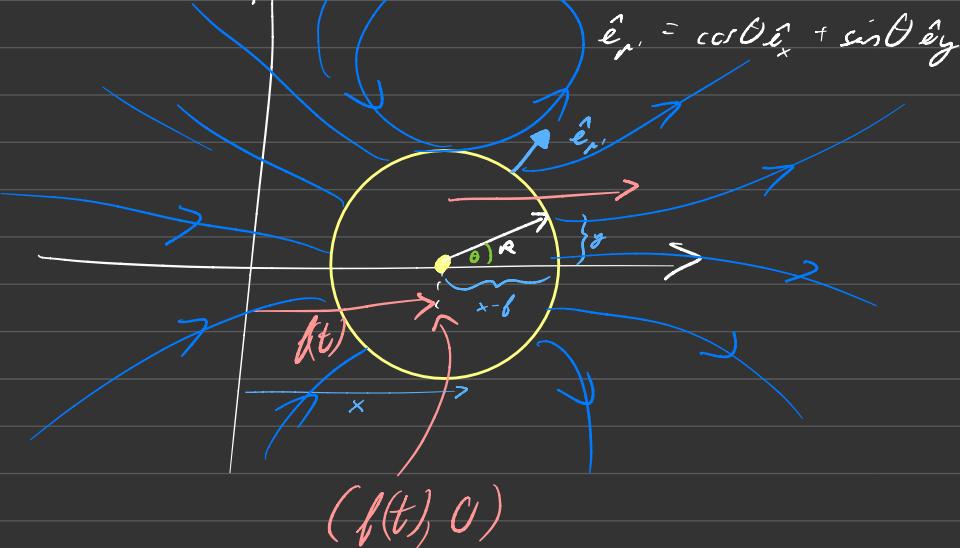
A truly inviscid fluid does not push the cylinder at all



$$\Rightarrow \vec{F} \neq \vec{0}$$

## Example

$2\omega I^2$



(i)  $u_r$  not match  $u_r$  of disc at boundary

(ii)  $|u| \rightarrow 0$  if  $|\vec{r}| \rightarrow \infty$

$$W(z) = -R^2 \frac{\dot{f}(t)}{z - f(t)}$$

$$W'(z) = \frac{R^2 \dot{f}(t)}{(z - f(t))^2}$$

$$= \frac{R^2 \dot{f}(t)}{(x^+, y - \dot{f}(t))^2} = \frac{R^2 \dot{f}(t)}{(x - f^+, y)^2}$$

$$= \frac{R^2 f(x - f - iy)}{(x - f - iy)^2}$$

$$= \frac{R^2 f [(x - f)^2 - y^2 - 2i(x - f)y]}{((x - f)^2 + y^2)^2}$$

$$\Rightarrow u_x(t, x, y) = \frac{R^2 f [(x - f)^2 - y^2]}{((x - f)^2 + y^2)^2}$$

$$u_y(t, x, y) = \frac{2R^2 f (x - f) y}{((x - f)^2 + y^2)^2}$$

$$u_x \Big|_{disc} = \frac{R^2 f (R^2 \cos^2 \theta - R^2 \sin^2 \theta)}{R^4}$$

$$= f \cos 2\theta$$

$$u_y \Big|_{disc} = \frac{2R^2 f R^2 \sin \theta \cos \theta}{R^4}$$

$$= f \sin 2\theta$$

$$\vec{u} \Big|_{disc} \cdot \hat{\vec{e}_r} = f \cos 2\theta \cos \theta + f \sin 2\theta \sin \theta$$

$$= \int \cos(2\theta - \theta)$$

$$= \int \cos \theta$$

$$\int \hat{e}_x \cdot \hat{e}_r = \int \cos \theta$$

$$V(x, y) = \frac{-R^2 \dot{\theta} (x - \theta)}{(x - \theta)^2 + y^2}$$

$$Q(t, x, y) = \frac{-R^2 \dot{\theta} (x - \theta)}{(x - \theta)^2 + y^2}$$

$$\Psi(t, x, y) = \frac{R^2 \dot{\theta} y}{(x - \theta)^2 + y^2}$$

$$\Psi(t, x, y) = C_t$$

$$C_t = 0 : y = 0$$

$$C_t \neq 0 : \frac{R^2 \dot{\theta} y}{(x - \theta)^2 + y^2} = C_t$$

$$\Rightarrow (x - \theta)^2 + y^2 = \frac{R^2 \dot{\theta} y}{C_t}$$

$$(x - \ell)^2 + y^2 - \frac{R^2 f}{C_t} y + \left(\frac{R^2}{2C_t}\right)^2 = \left(\frac{R^2}{2C_t}\right)^2$$

$$(x - \ell)^2 + \left(y - \frac{R^2 f}{2C_t}\right)^2 = \left(\frac{R^2}{2C_t}\right)^2$$

for pathline

$$\begin{cases} x(t), y(t) \\ \frac{dx}{dt} = u_x(t, x, y) \\ \frac{dy}{dt} = u_y(t, x, y) \end{cases}$$

$$\varPhi(t, x, y) = -\frac{R^2 f(x - \ell)}{(x - \ell)^2 + y^2}$$

$$\frac{\partial \varPhi}{\partial t} + \frac{1}{2} |\nabla \varPhi|^2 + \Psi + \int \frac{dP}{P} = C(t)$$

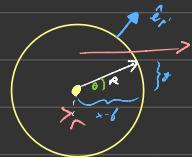
$$\frac{\partial \varPhi}{\partial t} = -\frac{R^2 f(x - \ell)}{(x - \ell)^2 + y^2} + \frac{R^2 f^2 y^2}{((x - \ell)^2 + y^2)^2}$$

$$\omega'(z) = u_x - i u_y$$

$$|\omega'(z)|^2 = |\vec{u}|^2$$

$$= \left| \frac{R^2 j}{(z-f)^2} \right|^2$$

$$= \frac{R^4 j^2}{((x-f)^2 + y^2)^2}$$



$$\vec{F} = \int_{disc} \rho_{disc} (-\hat{e}_r) dS$$



$$\frac{\partial \ell}{\partial t} + \frac{1}{2} |\nabla \ell|^2 + \frac{\rho}{\rho_0} = C(t)$$

$$\rho = \rho_0 C(t) - \frac{\partial \ell}{\partial t} - \frac{1}{2} |\nabla \ell|^2 \Big|_{disc}$$

$$= \rho_0 \left[ C(t) - \frac{1}{2} j^2 + R j \cos \theta - j \sin^2 \theta \right]$$

$$\vec{F} = - \int_{disc} \rho_{disc} \hat{e}_r dS$$

$$= -\rho_0 \int [R j \cos \theta - j \sin^2 \theta] [\cos \theta \hat{e}_x + \sin \theta \hat{e}_y] dS$$

$$\vec{F} = \mu_0 R^2 \vec{w} \int_0^{2\pi} \cos^2 \theta d\theta \hat{e}_x$$

$\int_0^{2\pi} \sin \theta d\theta = \int_0^{2\pi} \cos \theta d\theta$   
 $= \int_0^{2\pi} \sin \theta \cos \theta d\theta = \int_0^{2\pi} \sin^2 \theta d\theta$   
 $= \int_0^{2\pi} \sin^2 \theta d\theta = 0$

$$= -\mu_0 R^2 \vec{w} \cdot \hat{e}_x$$

$$= -\mu_0 R^2 \vec{w} \cdot \hat{e}_x$$

## Example

$$\rho \left[ \underbrace{\frac{d\vec{u}}{dt} + (\vec{u} \cdot \vec{\nabla}) \vec{u}}_{=0} \right] = \rho \vec{f} - \vec{\nabla} p + \cancel{2 \vec{\nabla} \vec{u}} \\ + \left( 5 + \frac{y}{3} \right) \vec{\nabla} (\vec{u} \cdot \vec{u})$$

Steady flow

Incompressible:  $\vec{\nabla} \cdot \vec{u} = 0$ ,  $\rho = \rho_0 \Rightarrow u(x, y)$

Unidirectional:  $\vec{\nabla} \cdot \vec{u} = \frac{\partial u}{\partial z}$

$$\vec{u} = u(x, y, z) \hat{e}_z$$

$$\Rightarrow (\vec{u} \cdot \vec{\nabla}) \vec{u} = u \frac{\partial}{\partial z} u \hat{e}_z = 0$$

The NS equation reduces to

$$\underbrace{\rho \vec{f} - \vec{\nabla} P + \rho \vec{\nabla}^2 \vec{u}}_{-\vec{\nabla}(\rho \Sigma + P)} = \vec{0}$$

Conservative body force:  $\vec{f} = -\vec{\nabla} \Sigma$

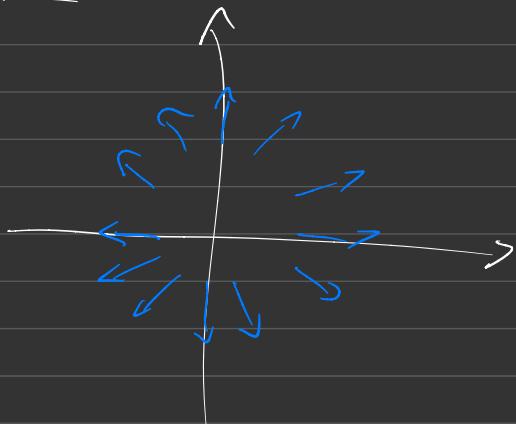
$$\vec{\nabla}(\rho \Sigma + P) = \rho \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) \hat{e}_z$$

$$\left. \begin{aligned} \frac{\partial}{\partial x} (\rho_0 \Sigma + P) &= 0 \\ \frac{\partial}{\partial y} (\rho_0 \Sigma + P) &= 0 \end{aligned} \right\} \Rightarrow \rho_0 \Sigma + P = f(z)$$

$$\frac{\partial}{\partial z} (\rho_0 \Sigma + P) = \rho \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right)$$

## Radial flow

(1) 2D



steady and incompressible

$$\vec{u} = u(r, \theta) \hat{e}_r$$

$$\vec{\nabla} \cdot \vec{u} = 0 = \frac{1}{r} \frac{\partial}{\partial r} (ru_r) + \frac{1}{r} \frac{\partial u_\theta}{\partial \theta}$$

$$= \frac{1}{r} \frac{\partial}{\partial r} (ru) \Rightarrow ru = A(\theta)$$

$$u(r, \theta) = \frac{A(\theta)}{r}$$

~~$$\rho_0 \left[ \frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \vec{\nabla}) \vec{u} \right] = \rho \vec{f} - \vec{\nabla} p + \gamma \nabla^2 \vec{u} + (g + \frac{u^2}{r}) \vec{\nabla} (\vec{\nabla} \cdot \vec{u})$$~~

$$\rho_0 (\vec{u} \cdot \vec{\nabla}) \vec{u} = -\vec{\nabla} (\rho \mp + p) + \gamma \nabla^2 \vec{u}$$

$$\hat{e}_r = \cos\theta \hat{e}_x + \sin\theta \hat{e}_y$$

$$\hat{e}_\theta = -\sin\theta \hat{e}_x + \cos\theta \hat{e}_y$$

$$(\vec{u} \cdot \vec{\nabla}) \vec{u} = \frac{A}{r} \frac{\partial}{\partial r} \left( \frac{A}{r} \hat{e}_r \right) = \frac{-A^2}{r^3} \hat{e}_r$$

$$\nabla^2 \vec{u} = \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial \vec{u}}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \vec{u}}{\partial \theta^2}$$

$$= \frac{1}{r} \frac{\partial}{\partial r} \left[ r \frac{\partial}{\partial r} \left( \frac{A}{r} \hat{e}_r \right) \right] + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} \left( \frac{A}{r} \hat{e}_r \right)$$

$$= \frac{A \hat{e}_r}{r} \left[ \frac{d}{dr} \left( r \frac{d}{dr} \frac{1}{r} \right) \right] + \frac{1}{r^3} \left[ \frac{d^2 A}{d\theta^2} \hat{e}_r + 2 \frac{dA}{d\theta} \frac{d\hat{e}_r}{d\theta} \right]$$

$$+ \frac{A d^2 \hat{e}_r}{d\theta^2}$$

$$= \cancel{\frac{A \hat{e}_r}{r^3}} + \frac{1}{r^3} \frac{d^2 A}{d\theta^2} \hat{e}_r + \frac{2}{r^3} \frac{dA}{d\theta} \hat{e}_\theta - \cancel{\frac{A \hat{e}_r}{r^3}}$$

$$\rho_0 (\vec{u} \cdot \vec{\nabla}) \vec{u} = -\vec{\nabla} (\rho_0 \underline{\Sigma} + P) + \nabla^2 \vec{u} = -\frac{\rho_0 A^2}{r^3} \hat{e}_r$$

$$= -\frac{2}{r^3} \left[ \rho_0 \underline{\Sigma} + P \right] \hat{e}_r - \frac{1}{r^2} \frac{\partial}{\partial \theta} \left[ \rho_0 \underline{\Sigma} + P \right] \hat{e}_\theta$$

$$+ \frac{4}{r^3} \frac{d^2 A}{d\theta^2} \partial_r + \frac{2g}{r^3} \frac{dA}{d\theta} \partial_\theta$$

$$r: -\rho_0 \frac{A^2}{r^3} = -\frac{\partial}{\partial r} (\rho_0 \Sigma + P) + \frac{4}{r^3} \frac{d^2 A}{d\theta^2}$$

$$\theta: 0 = -\frac{1}{r} \frac{\partial}{\partial \theta} (\rho_0 \Sigma + P) + \frac{2g}{r^3}$$

$$\frac{\partial}{\partial \theta} (\rho_0 \Sigma + P) = \frac{2g}{r^3} \frac{dA}{d\theta}$$

$$= \frac{\partial}{\partial \theta} \left( \frac{2g A}{r^2} \right)$$

$$\rho_0 \Sigma + P = \frac{2g A}{r^2} + g(r)$$

$$P(r, \theta) = -\rho_0 \Sigma + \frac{2g A(\theta)}{r^2} + g(r)$$

$$-\rho_0 \frac{A^2}{r^3} = \frac{4g A}{r^3} - g(r) + \frac{2}{r^3} \frac{d^2 A}{d\theta^2}$$

$$r^3 g'(r) = 2 \frac{d^2 A}{d\theta^2} + 4g A + \rho_0 A^2 = 1$$

(a constant)

$$g'(r) = \frac{1}{r^3} \Rightarrow g(r) = -\frac{1}{2r^2} + C$$

$$\frac{dA}{dr} + 4\gamma A + \rho_0 A^2 = 1$$

Assume cylindrical symmetry  $\Psi(r)$

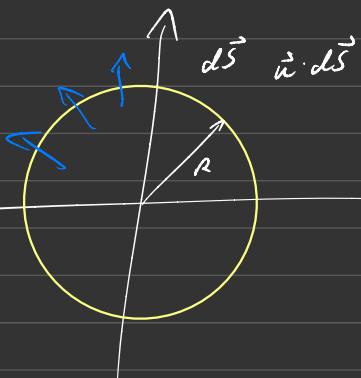
$$\Rightarrow A = \text{constant} \Rightarrow 4\gamma A + \rho_0 A^2 = 1$$

Then

$$\rho(r, d) = \rho(r) = -\rho_0 \Psi(r) - \frac{\rho_0 A^2}{2r^2} + C$$

$$\vec{u} = \frac{A}{r} \hat{e}_r \quad \text{(Axial flow)}$$

$$Q_2 = 2\pi R \cdot \frac{A}{R} = 2\pi A$$



$$A = \frac{Q}{2\pi} \quad \Downarrow$$

$$\left. \vec{u} = \frac{Q_2}{2\pi r} \hat{e}_r \right\}$$

$$\rho = C - \frac{\rho_0 Q^2}{8\pi^2 r^2} - \rho_0 \Psi$$

(2) 30

$$\rho_0 (\vec{u} \cdot \vec{\nabla}) \vec{u} = - \vec{\nabla} (\rho_0 \Sigma + P) + 2 \nabla^2 \vec{u}$$

$$\vec{u} = u(r, \theta, \varphi) \hat{e}_r$$

$$\begin{aligned} \vec{\nabla} \cdot \vec{u} &= 0 = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 u_r) + \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} + \frac{1}{r \sin \theta} \frac{\partial u_\varphi}{\partial \varphi} \\ &= \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 u) \end{aligned}$$

$$u = \frac{A(\theta, \varphi)}{r^2}$$

$$\begin{aligned} (\vec{u} \cdot \vec{\nabla}) \vec{u} &= \frac{A}{r^2} \frac{\partial}{\partial r} \left( \frac{A}{r^2} \right) \hat{e}_r \\ &= -\frac{2A}{r^5} \hat{e}_r \end{aligned}$$

$$\Sigma \quad \rho_0 (\vec{u} \cdot \vec{\nabla}) \vec{u} = -\frac{2A}{r^5} \hat{e}_r$$

$$\nabla^2 \vec{u} = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial \vec{u}}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial \vec{u}}{\partial r} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \vec{u}}{\partial \varphi^2}$$

*Note :*  $\vec{\nabla} \times (\vec{\nabla} \times \vec{u}) = \vec{\nabla}(\vec{\nabla} \cdot \vec{u}) - \nabla^2 \vec{u}$

$$\nabla^2 \vec{u} = \vec{\nabla}(\vec{\nabla} \cdot \vec{u}) - \vec{\nabla} \times (\vec{\nabla} \times \vec{u})$$

$$\nabla^2 \vec{u} = -\vec{\nabla} \times \vec{w}$$

$$\vec{w} = \frac{1}{r \sin \theta} \left[ \frac{\partial}{\partial \theta} \left( \sin \theta u_\varphi - \frac{\partial u_r}{\partial \varphi} \right) \hat{e}_r \right.$$

$$+ \left[ \frac{1}{r \sin \theta} \frac{\partial u_r}{\partial \varphi} - \frac{1}{r} \frac{\partial}{\partial r} (r u_\varphi) \right] \hat{e}_\theta$$

$$+ \frac{1}{r} \left[ \frac{\partial}{\partial r} (r u_\varphi) - \frac{\partial u_r}{\partial \varphi} \right] \hat{e}_\varphi$$

$$= \underbrace{\frac{1}{r^3 \sin \theta} \frac{\partial A}{\partial \varphi}}_{w_\theta} \hat{e}_\varphi - \underbrace{\frac{1}{r^3} \frac{\partial A}{\partial \theta}}_{w_\varphi} \hat{e}_\varphi$$

$$\vec{\nabla} \times \vec{w} = -\frac{1}{r^4} \left\{ \frac{1}{\sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial A}{\partial \theta} \right) + \frac{1}{\sin^2 \theta} \frac{\partial^2 A}{\partial \varphi^2} \right\} \hat{e}_r$$

$$- \frac{2}{r^4} \left( \frac{\partial A}{\partial \theta} \hat{e}_\theta + \frac{1}{\sin \theta} \frac{\partial A}{\partial \varphi} \hat{e}_\varphi \right)$$

$$\nabla^2 \vec{\omega} = -\vec{\nabla} \times \vec{\omega}$$

$$= \frac{1}{r^4} \left\{ \frac{1}{\sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial A}{\partial \theta} \right) + \frac{1}{\sin^2 \theta} \frac{\partial^2 A}{\partial \varphi^2} \right\} \hat{e}_r \\ + \frac{1}{r^4} \left( \frac{\partial A}{\partial \theta} \hat{e}_\theta + \frac{1}{\sin \theta} \frac{\partial A}{\partial \varphi} \hat{e}_\varphi \right)$$

$$\theta : 0 = -\frac{1}{r} \frac{\partial}{\partial \theta} (\rho_0 \Sigma + P)$$

$$+ \frac{\partial g}{r^4} \frac{\partial A}{\partial \theta}$$

$$\varphi : 0 = -\frac{1}{r \sin \theta} \frac{\partial}{\partial \varphi} (\rho_0 \Sigma + P)$$

$$+ \frac{\partial g}{r^4 \sin \theta} \frac{\partial A}{\partial \varphi}$$

$$\rho_0 \Sigma + P = \frac{2gA(\theta, \varphi)}{r^3} + g(r)$$

$$r! - \frac{2\rho_0 A}{r^5} = -\frac{2}{r^4} (\rho_0 \Sigma + P)$$

$$+ \frac{2}{r^4} \left\{ \frac{1}{\sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial A}{\partial \theta} \right) + \frac{1}{\sin^2 \theta} \frac{\partial^2 A}{\partial \varphi^2} \right\}$$

$$= \frac{6\gamma A}{r^4} - g'(r) + \frac{\kappa}{r^4} \left\{ \begin{array}{l} \theta, \alpha \end{array} \right\}$$

$$\frac{\partial}{\partial r} \left( \frac{-2\rho_0 A^2}{r} - G\gamma A + r^\alpha g'(r) \right) = 0$$

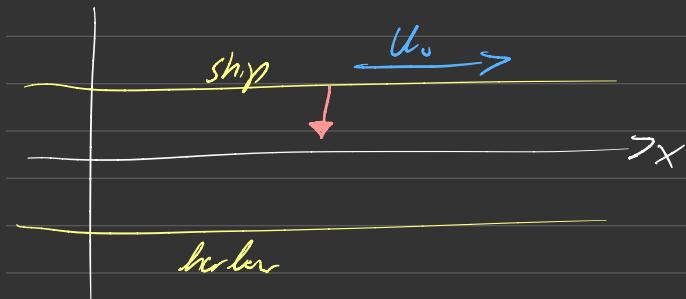
$$2\rho_0 A^2 + r^2 \frac{d}{dr} (r^\alpha g'(r)) = 0$$

$\Rightarrow A = \text{constant}$

$$\vec{u} = \frac{A}{r^2} \hat{e}_r$$

$$Q_3 = 4\pi A$$

## Ship in Harbor Example



$$\vec{u} = \left[ \frac{c}{2\gamma} \left( y^2 - \frac{\omega^2}{4} \right) + \frac{U_0}{w} \left( y + \frac{\omega}{2} \right) \right] e_x$$

$$\rho = -\rho_0 \Sigma + C_x + D$$

$$C=0$$

$$\vec{u} = \frac{U_0}{w} \left( y + \frac{\omega}{2} \right) e_x$$

$$\sigma_{ij} = -\rho \delta_{ij} + \eta \left[ \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} - \frac{2}{3} (\vec{\nabla} \cdot \vec{u}) \delta_{ij} \right]$$

$$+ \zeta (\vec{\nabla} \cdot \vec{u}) \delta_{ij}$$

$$\sigma = \begin{bmatrix} -\rho & \frac{\gamma u_0}{w} & 0 \\ \frac{\gamma u_0}{w} & -\rho & 0 \\ 0 & 0 & -\rho \end{bmatrix} \quad \sigma_{xy} = \sigma_{yx}$$

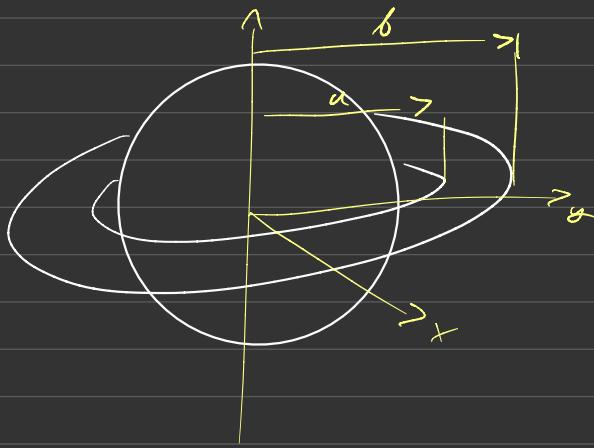
$$d\vec{F} = \begin{bmatrix} -\rho & \frac{\gamma u_0}{w} & 0 \\ \frac{\gamma u_0}{w} & -\rho & 0 \\ 0 & 0 & -\rho \end{bmatrix} \begin{bmatrix} 0 \\ -1 \\ 0 \end{bmatrix}$$

$$= \begin{bmatrix} -\frac{\gamma u_0}{w} \\ \rho \\ 0 \end{bmatrix} dS$$

$$dF_x = -\frac{\gamma u_0}{w} dS$$

Drag force

## Rings of Saturn



$$b \approx 140\,000 \text{ km}$$

$$a \approx 67\,000 \text{ km}$$

## Assumptions

- 2D
  - steady
  - circular
  - $\vec{f} = -\frac{GM}{r^2} \hat{e}_r$
  - constant density  $\rho_0$
- $\left. \begin{array}{l} \\ \\ \end{array} \right\} \vec{u} = u(r, \theta) \hat{e}_\phi$

$$\vec{\nabla} \cdot \vec{u} = 0$$

$$\rho_0 (\vec{u} \cdot \vec{\nabla}) \vec{u} = -\frac{GM}{r^2} \hat{e}_r - \vec{\nabla} p + \gamma \nabla^2 \vec{u}$$

$$\vec{\nabla} \cdot \vec{u} = \frac{1}{r} \frac{\partial u}{\partial \theta} = 0$$

$u$  is independent of  $\theta$

$$\rho_0 \frac{u}{r} \frac{\partial}{\partial \theta} (u \hat{e}_\theta) = - \frac{\rho_0 u^2}{r} \hat{e}_r$$

$$\vec{\nabla}^2 \vec{u} = \vec{\nabla}(\vec{\nabla} \cdot \vec{u}) - \vec{\nabla} \times (\vec{\nabla} \times \vec{u})$$

$$= - \vec{\nabla} \times \vec{u}$$

$$= \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial \vec{u}}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \vec{u}}{\partial \theta^2} + \frac{\partial^2 \vec{u}}{\partial z^2}$$

$$= \frac{1}{r} \frac{d}{dr} \left( r \frac{du}{dr} \right) \hat{e}_\theta - \frac{u}{r^2} \hat{e}_\phi$$

$$-\rho_0 \frac{u^2}{r} \hat{e}_r = -\frac{G M \rho_0}{r^2} \hat{e}_r - \frac{\partial P}{\partial r} \hat{e}_r - \frac{1}{r} \frac{\partial P}{\partial \theta} \hat{e}_\theta$$

$$+ 2 \left[ \frac{1}{r} \frac{d}{dr} \left( r \frac{du}{dr} \right) - \frac{u}{r^2} \right] \hat{e}_\theta$$

$$r : -\frac{\partial u^2}{r} = -\frac{6\gamma p_e}{r^2} - \frac{\partial P}{\partial r}$$

$$\partial : 0 = -\frac{1}{r} \frac{\partial P}{\partial \varphi} + \eta \left[ \frac{du^2}{dr^2} + \frac{1}{r} \frac{du}{dr} - \frac{u}{r^2} \right]$$

$$0 = \frac{\partial P}{\partial \vartheta} = \eta r \left[ \frac{d^2 u}{dr^2} + \frac{1}{r} \frac{du}{dr} - \frac{u}{r^2} \right]$$

$$\begin{aligned} \lambda \frac{\partial^2 P}{\partial \vartheta^2} = 0 &\Rightarrow P(r, \vartheta) = f(r) + g(r) \vartheta \\ &\Rightarrow P(r, \vartheta + 2\pi) = P(r, \vartheta) \\ &\Rightarrow g(r) = 0 \end{aligned}$$

$$\text{So } P = P(r)$$

$$r^2 \frac{du^2}{dr^2} + r \frac{du}{dr} - u = 0 \quad (\text{Candy Euler ODE})$$

$$u \propto r^\alpha$$

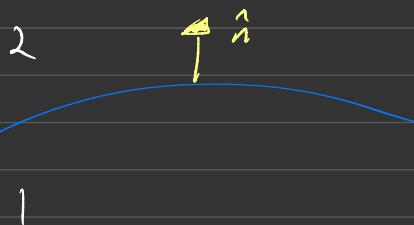
$$\alpha(\alpha-1)r^{\alpha-2} + \alpha r^{\alpha-1} - r^{\alpha-2} = (\alpha^2 - 1)r^{\alpha-2} = 0$$

$$r, \frac{1}{r} \Rightarrow u(r) = Ar + B\frac{1}{r}$$

$$\frac{dP}{dr} = -\frac{G\rho_0 A}{r^2} + \frac{\rho_0}{r} (Ar + B\frac{1}{r})^2$$

$$= -\frac{G\rho_0 A}{r^2} + \rho_0 A^2 r + \frac{2\rho_0 AB}{r} + \frac{\rho_0 B^2}{r^3}$$

$$P(r) = P_0 + \frac{G\rho_0 A}{r} + \frac{1}{2}\rho_0 A^2 r^2 + 2\rho_0 ABr + \frac{-\rho_0 B^2}{2r^2}$$

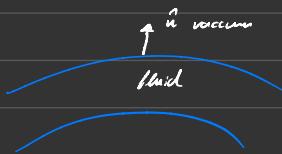


$$\sigma_1 \cdot \hat{n} - \sigma_2 \cdot \hat{n} = \gamma \nabla \cdot \hat{e}_z \hat{n}$$

at boundary

Assume  $\gamma = 0$ , i.e. no surface tension

$$\sigma_1 \cdot \hat{n} = \sigma_2 \cdot \hat{n} = 0$$



$$\hat{n} = \hat{e}_r = \cos\theta \hat{e}_x + \sin\theta \hat{e}_y$$

$$\Rightarrow (\sigma_1 \cdot \hat{n})_x = (\sigma_1 \cdot \hat{e}_x) \cos\theta + (\sigma_1 \cdot \hat{e}_y) \sin\theta$$

$$= \sigma_{xx} \cos\theta + \sigma_{xy} \sin\theta$$

$$(\sigma_1 \cdot \hat{n})_y = \sigma_{yx} \cos\theta + \sigma_{yy} \sin\theta$$

$$\Rightarrow \sigma_{xx} = \sigma_{yy} = \sigma_{zz} = 0$$

$$\sigma_{ij} = -\rho f_{ij} + \gamma \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

$$\sigma_{xx}$$

$$\left. \begin{array}{l} \\ \\ \end{array} \right\} \rho = 0$$

$$\beta = 0$$

|

|

|

|

$$u_x = - \left( A_y + \frac{B_y}{x^2 + y^2} \right)$$

$$u_y = A_x + \frac{B_x}{x^2 + y^2}$$

$$\vec{u} = \text{Aréd}$$

$$\rho = \rho_0 + \frac{G \gamma \rho}{r} + \frac{1}{2} \rho_0 A^2 r^2$$

$$\rho_0 + \frac{G \gamma \rho}{r} + \frac{1}{2} \rho_0 A^2 r^2 = 0$$

$$\rho_0 + \frac{G \gamma \rho}{r} + \frac{1}{2} \rho_0 A^2 r^2 = 0$$

$$A = \sqrt{\frac{2 G \gamma}{ab(a+b)}}$$

$$\rho_0 = \frac{-(a^2 + ab + b^2)}{ab(a+b)} G \gamma \rho$$

$$|\vec{u}(a)| = 24 \text{ km} \cdot \text{s}^{-1}$$

$$|\vec{u}(b)| = 16 \text{ km} \cdot \text{s}^{-1}$$

$$|\vec{u}(a)|^2 a = 3.86 \cdot 10^7 \text{ km}^3 \cdot \text{s}^{-2}$$

$$|\vec{u}(b)|^2 b = 3.58 \cdot 10^7 \text{ km}^3 \cdot \text{s}^{-2}$$

$$G\gamma = 3.79 \cdot 10^7 \text{ km}^3 \text{s}^{-2}$$

$$\frac{G\gamma}{n^2} = \frac{mn^2}{n}$$

$$\Rightarrow n = \sqrt{\frac{G\gamma}{m}}$$

$$n^2 r = G\gamma$$

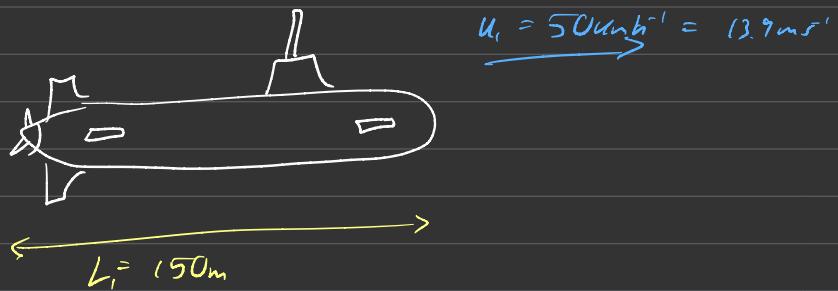
$$\vec{n} = \sqrt{\frac{G\gamma}{r}} \hat{e}_d$$

$$\rho(r) \quad (\vec{\nabla} \cdot \vec{n} \neq 0)$$
$$\vec{\nabla} \cdot (\rho \vec{n}) = 0$$

Only solution of

$$\gamma = \rho = 0 \quad \text{and} \quad \rho = 0$$

## Reynolds number for



$$\rho_i = 1000 \text{ kg m}^{-3}$$

$$\eta_1 = 10^{-3} \text{ Pa s}$$

$$Re = \frac{\rho_i U_i L_i}{\eta_1} = 2.08 \cdot 10^9$$

$$\frac{\delta}{3m}$$

$$\frac{\rho_i U_i L_i}{\eta_2} = Re$$

$$\eta_2$$

$$\rho_i + NTP = \rho_i \approx 1.2 \text{ kg m}^{-3}$$

$$\eta_2 = 1.8 \cdot 10^{-5} \text{ Pa s}$$

$$U_2 = \frac{g_2 Re}{\rho_2 L_2} = 1 \times 10^4 \text{ m} \cdot \text{s}^{-1}$$

$$PV = Nk_B T$$

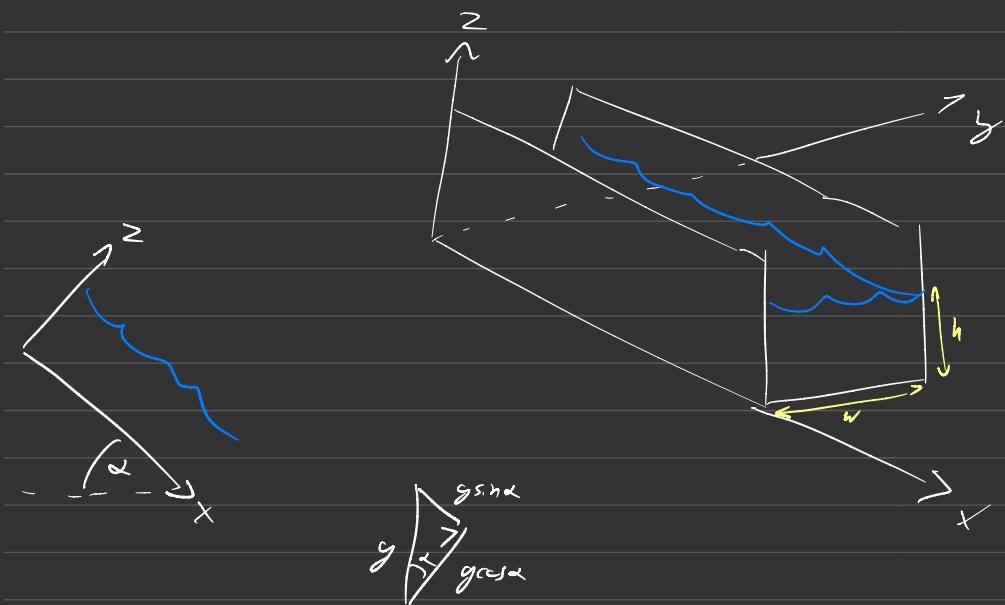
$$\rho = \frac{k_B T}{m} \rho_0$$

$$\rho = \frac{m \rho}{k_B T}$$

## Agreement revisited

Don't assume "very wide"

So we need to include width in our analysis



Assumptions

'steady'

Incompressible

Unidirectional

Constant dam and body force  $\vec{u} = u\hat{x}$

$$\vec{\nabla} \cdot \vec{u} = 0 = \frac{\partial u}{\partial x} \Rightarrow \vec{u} = u \hat{e}_x = u(y, z) \hat{e}_x$$

$$\frac{D\vec{u}}{Dt} = \frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \vec{\nabla}) \vec{u}$$

$$= \frac{\partial u}{\partial t} \hat{e}_x + u \frac{\partial u}{\partial x} \hat{e}_x$$

$$= \vec{0}$$

$$\vec{0} = \rho \vec{f} - \vec{\nabla} P + \gamma \vec{\nabla}^2 \vec{u}$$

$$= \rho g \sin \alpha \hat{e}_x - \rho g \cos \alpha \hat{e}_z$$

$$- \frac{\partial P}{\partial x} \hat{e}_x - \frac{\partial P}{\partial y} \hat{e}_y - \frac{\partial P}{\partial z} \hat{e}_z$$

$$+ \gamma \left( \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) \hat{e}_x$$

$$x: 0 = \rho g \sin \alpha - \frac{\partial P}{\partial x} + \gamma \left( \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right)$$

$$y: 0 = - \frac{\partial P}{\partial y}$$

$$z: -\rho g \cos \alpha - \frac{\partial P}{\partial z} = 0$$

## Boundary conditions

$$u(0, z) = 0$$

$$u(w, z) = 0$$

$$u(y, 0) = 0$$

$\sigma \cdot \hat{n}$  conditions at  $A_{r,r} - H_2O$  boundary

$$\sigma_{A_{r,r}} = \begin{bmatrix} -P_{A_{r,r}} & 0 & 0 \\ 0 & -P_{A_{r,r}} & 0 \\ 0 & 0 & -P_{A_{r,r}} \end{bmatrix}$$

$$\sigma_{H_2O} = \begin{bmatrix} -P & 2\frac{\partial u}{\partial y} & 2\frac{\partial u}{\partial z} \\ 2\frac{\partial u}{\partial y} & -P & 0 \\ 2\frac{\partial u}{\partial z} & 0 & -P \end{bmatrix}$$

$$\frac{\partial u_r}{\partial x_r} = u_y = u_z = 0 \quad \nabla \left( \frac{\partial u_r}{\partial y} + \frac{\partial u_r}{\partial z} \right)$$
$$\frac{\partial u_r}{\partial x} = 0$$

$$\sigma_{A_{r,r}} \cdot \hat{e}_z = \begin{bmatrix} 0 \\ 0 \\ -P_{A_{r,r}} \end{bmatrix}, \quad \sigma_{H_2O} \cdot \hat{e}_z = \begin{bmatrix} 2\frac{\partial u}{\partial z} \\ 0 \\ -P \end{bmatrix}$$

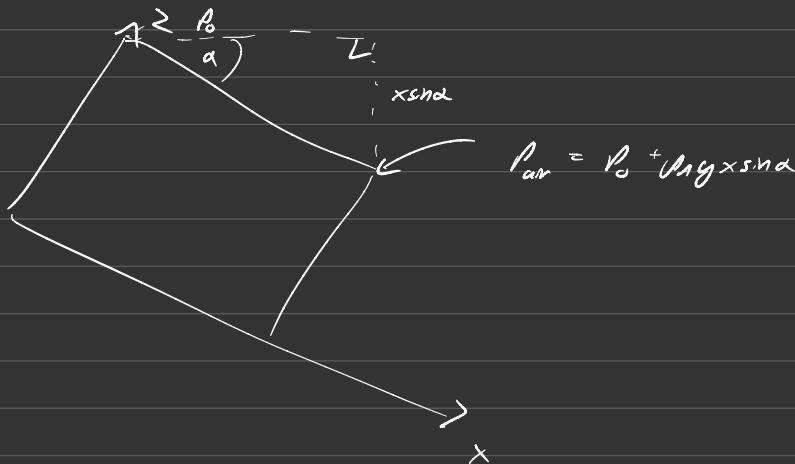
Then all BC's are

$$\left\{ \begin{array}{l} u(0, z) = 0 \\ u(w, z) = 0 \\ u(y, 0) = 0 \\ \frac{\partial u}{\partial z}(y, h) = 0 \end{array} \right.$$

$$\rho_{ar} = \rho \text{ at } z = h$$

Then

$$\left\{ \begin{array}{l} x: 0 = \rho \cos \alpha - \frac{\partial \rho}{\partial x} + \gamma \left( \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right) \\ y: 0 = - \frac{\partial \rho}{\partial y} \\ z: - \rho g \cos \alpha - \frac{\partial \rho}{\partial z} = 0 \\ \Rightarrow \rho = f(x) - \rho g z \cos \alpha \end{array} \right.$$



$$f(x) - \rho_A g h \cos \alpha = P_0 + \rho_A g x \sin \alpha$$

$$f(x) = P_0 + \rho_A g x \sin \alpha + \rho_A g h \cos \alpha$$

$$\rho = P_0 + \rho_A g x \sin \alpha + \rho_A g (h - z) \cos \alpha$$

$$\frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} = - \frac{(\rho_0 - \rho_A) g s \sin \alpha}{\eta}$$

$$\text{Assume } u = u_H + u_p$$

$$\frac{\partial^2 u_H}{\partial y^2} + \frac{\partial^2 u_H}{\partial z^2} = 0$$

$$\frac{\partial^2 u_p}{\partial y^2} + \frac{\partial^2 u_p}{\partial z^2} = - \frac{(\rho_0 - \rho_A) g s \sin \alpha}{\eta}$$

$$u_p = c_1 y^2 + \cancel{c_2} \overset{\circ}{y} z + \cancel{c_3} \overset{\circ}{z}^2 + c_4 y + \cancel{c_5} \overset{\circ}{z} + \cancel{c_6}$$

$$\frac{\partial^2 u_p}{\partial y^2} = 2c_1$$

$$\frac{\partial^2 u_p}{\partial z^2} = 2c_3$$

$$\frac{\partial^2 u_p}{\partial y^2} + \frac{\partial^2 u_p}{\partial z^2} = 2(c_1 + c_3) = -\frac{(p_0 - p_1) g \sin \alpha}{2}$$

$$u_p(0, z) = c_1 z^2 + c_3 z + c_6 = 0$$

$$\Rightarrow c_3 = c_5 = c_6 = 0$$

$$u_p(w, z) = c_1 w^2 + c_2 w z + c_4 w = 0$$

$$c_2 = 0, \quad c_1 w + c_4 = 0$$

$$c_1 = -\frac{(p_0 - p_1) g \sin \alpha}{2w}$$

$$c_4 = \frac{(p_0 - p_1) g \sin \alpha}{2w}$$

then

$$u_p = \frac{(p_0 - p_1) g \sin \alpha}{2w} (wy - yz)$$

$$\frac{\partial^2 u_H}{\partial y^2} + \frac{\partial^2 u_H}{\partial z^2} = 0$$

$$u_H(y, z) = Y(y) Z(z)$$

$$Y'' Z + Y Z'' = 0$$

$$\frac{Y''}{Y} + \frac{Z''}{Z} = 0$$

$$\Rightarrow \frac{Y''}{Y} = -\lambda, \quad \frac{Z''}{Z} = \lambda$$

$$\Rightarrow Y''(y) + \lambda Y(y) = 0 \quad \left. \begin{array}{l} \\ \end{array} \right\}$$
$$Z''(z) - \lambda Z(z) = 0 \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$\lambda > 0 : Y(y) = A \cos(\sqrt{\lambda} y) + B \sin(\sqrt{\lambda} y)$$

$$\lambda = 0 : A + B y \quad X$$

$$\lambda < 0 : Y(y) = A \cosh(\sqrt{-\lambda} y) + B \sinh(\sqrt{-\lambda} y) \quad X$$

$$Y(0) = Y(\infty) = 0$$

so  $\lambda > 0$  a sood with

$$Y(0) = A = 0 \quad , \quad Y(w) = B \sin(\sqrt{\lambda} y) = 0$$

$$\sqrt{\lambda} = \frac{n\pi}{w} \quad , \quad n \in \mathbb{Z}$$

Then

$$Z^n - \left(\frac{n\pi}{w}\right)^2 Z = 0$$

$$\Rightarrow Z(z) = \sinh\left(\frac{n\pi z}{w}\right), \cosh\left(\frac{n\pi z}{w}\right)$$

$$u_H(y, z) = \sum_{n=0}^{\infty} \sin\left(\frac{n\pi y}{w}\right) \left[ c_n \sinh\left(\frac{n\pi z}{w}\right) + b_n \cosh\left(\frac{n\pi z}{w}\right) \right]$$

$$u(y, z) = u_H + u_p$$

$$u(y, 0) = \frac{(u - u_p) \sin \omega (wy - yz)}{2y}$$

$$+ \sum_{n=1}^{\infty} b_n \sin\left(\frac{n\pi y}{w}\right) = 0$$

$$\sum_{n=1}^{\infty} l_n \sin\left(\frac{n\pi y}{w}\right) = \frac{(\rho - \rho_1)}{2y} g w \sin x (y^2 - wy)$$

$$l_n = \frac{2}{w} \int_0^w \frac{(\rho - \rho_1)}{2y} g w \sin x (y^2 - wy) \sin\left(\frac{n\pi y}{w}\right) dy$$

$$= -2 \frac{(\rho - \rho_1) g w^2 \sin x}{y^5 n^3} \left( \frac{1 - \cos(n\pi)}{n^3} \right)$$

$$\cos(n\pi) = (-1)^n$$

$$= \begin{cases} 0 & \text{if } n \text{ is even} \\ -4 \frac{(\rho - \rho_1) g w^2 \sin x}{y^5 n^3} \end{cases}$$

$$\left. \frac{\partial u}{\partial z} \right|_{z=0} = \sum_{n=1}^{\infty} \frac{n\pi}{w} \sin\left(\frac{n\pi y}{w}\right) \left[ a_n \cosh\left(\frac{n\pi z}{w}\right) + b_n \sinh\left(\frac{n\pi z}{w}\right) \right] \Big|_{z=0} = 0$$

$$\Rightarrow a_n \cosh\left(\frac{n\pi b}{w}\right) + b_n \sinh\left(\frac{n\pi b}{w}\right) = 0$$

$$a_n = -\frac{\sinh\left(\frac{n\pi h}{w}\right)}{\cosh\left(\frac{n\pi h}{w}\right)} b_n$$

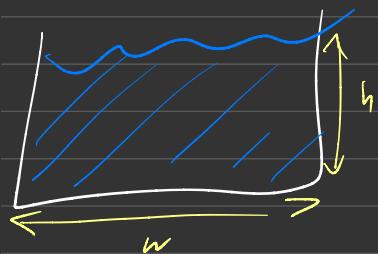
$$a_n \sinh\left(\frac{n\pi z}{w}\right) + b_n \cosh\left(\frac{n\pi z}{w}\right)$$

$$= b_n \left( \frac{\cosh\left(\frac{n\pi}{w}(h-z)\right)}{\cosh\left(\frac{n\pi h}{w}\right)} \right)$$

$$\Rightarrow u(y, z) = \frac{(\rho_0 - \rho_1) g \sin^2}{2y} [w y - y^2$$

$$- \frac{8w^2}{n^3} \sum_{\text{odd}} \frac{\sin\left(\frac{n\pi y}{w}\right) \cosh\left(\frac{n\pi h-z}{w}\right)}{n^3 \cos\left(\frac{n\pi h}{w}\right)}$$

$$dQ = \vec{u} \cdot d\vec{s}$$



$$Q = \int_{\text{cross sec}} u dy dz$$

$$= \int_0^h \left( \int_0^h u(y, z) dz \right) dy$$

$$Q = \frac{(\rho_0 - \rho_1) g s m_2}{2 \gamma} \left[ \frac{\omega^3 h}{6} - \frac{8\omega}{\pi^3} \sum_{n=odd}^{\infty} \frac{1}{n^3 \cos\left(\frac{n\pi h}{\omega}\right)} \dots \right]$$

$$\begin{aligned} & \left( \int_0^h \sin\left(\frac{n\pi y}{\omega}\right) dy \right) \left( \int_0^h \cosh\left(\frac{n\pi(h-z)}{\omega}\right) dz \right) \\ &= \left[ \frac{-\omega}{n\pi} (\cos(n\pi) - 1) \right] \left[ \frac{\omega}{n\pi} \sinh\left(\frac{n\pi h}{\omega}\right) \right] \end{aligned}$$

$$Q = \frac{(\rho_0 - \rho_1) g \omega^3 h s m_2}{12 \gamma} \left[ 1 - \frac{96\omega}{\pi^5 h} \sum_{n=odd} \frac{\tanh\left(\frac{n\pi h}{\omega}\right)}{n^5} \right]$$

$$\omega = 1.2 \text{ m}$$

$$h = 1.8 \text{ m}$$

$$\tan \alpha = \frac{1 \text{ cm}}{182.4 \text{ m}}$$

$$u\left(\frac{\omega}{2}, h\right) = 96.8 \text{ ms}^{-1}$$

$$Q = 110 \text{ m}^3 \text{s}^{-1}$$

in reality:  $40000 \text{ m}^3/\text{day}$

$$\rightarrow 0.4 \text{ m}^3 \cdot \text{s}^{-1}$$