

# E9 231: Digital Array Signal Processing

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## 1 Topics

- Spatial Smoothing and the Forward Backward method.
- Direction of Arrival Estimation.

## 2 Class Notes

### 2.1 Spatial Smoothing

- Applicable to arrays with structure for example:
- Rectangular (uniform) array.
- Uniform Linear Array.

$$S_X = \begin{bmatrix} V_S & V_I \end{bmatrix} \begin{bmatrix} * & & \mathbf{0} \\ & * & \\ \mathbf{0} & & * \end{bmatrix} \begin{bmatrix} V_S^H \\ V_I^H \end{bmatrix}$$

where

$$V(\psi) = \begin{bmatrix} V_S & V_I \end{bmatrix}_{N \times (D+1)}$$

Goal: To Remove singularity(improve condition number) in  $S_X$  caused due to correlation between signal and interference. If we have  $N$  sensors, we pick first  $1 : M$  sensors at a time, then we pick next  $2 : M + 1$  sensors and continuing this way we get  $L$  such blocks where  $N = L + M - 1$ . Now we define,

$$V_M(\psi) = \begin{bmatrix} 1 \\ e^{j\psi} \\ \vdots \\ e^{j(M-1)\psi} \end{bmatrix} e^{j(\frac{M-1}{2})\psi}$$
$$V_N(\psi) = \begin{bmatrix} e^{-j(\frac{N-1}{2})\psi} \\ \vdots \\ e^{+j(\frac{N-1}{2})\psi} \end{bmatrix}$$

$V_M^{(l)}(\psi)$  : pick off the  $l^{th}$  length  $M$  block

$$V_M^{(1)}(\psi) = \begin{bmatrix} e^{-j(\frac{N-1}{2})\psi} \\ \vdots \\ e^{-j(\frac{N-1}{2}-(M-1))\psi} \end{bmatrix}$$

$$V_M^{(1)}(\psi) = V_M(\psi)e^{-j(\frac{N-1}{2})\psi}e^{j(\frac{M-1}{2})\psi}$$

$$V_M^{(1)}(\psi) = V_M(\psi)e^{-j(\frac{N-1}{2}-\frac{M-1}{2})\psi}$$

$$V_M^{(l)}(\psi) = V_M(\psi)e^{-j(\frac{N-1}{2}-\frac{M-1}{2}-(l-1))\psi}$$

Recall  $V_S$  is dependent on  $\psi_S$  and  $V_I$  is dependent on  $\psi_I$

$V_M^{(l)}(\psi)$  :  $l$  through  $l + M - 1$  rows of  $V(\psi)$  matrix

$$V_M^{(l)}(\psi) = \begin{bmatrix} V_M^{(l)}(\psi_1) \dots V_M^{(l)}(\psi_{D+1}) \end{bmatrix}$$

where

$$V_M^{(l)}(\psi_{D+1}) = V_M(\psi_{D+1})e^{-j(\frac{N-1}{2}-\frac{M-1}{2}-(l-1))\psi_{D+1}}$$

$$V_M^{(l)}(\psi) = V_M(\psi)D^{(l)}$$

$$D^{(l)} = \text{diag} \begin{bmatrix} e^{-j(\frac{N-1}{2}-\frac{M-1}{2}-(l-1))\psi_1} & e^{-j(\frac{N-1}{2}-\frac{M-1}{2}-(l-1))\psi_2} & \dots & e^{-j(\frac{N-1}{2}-\frac{M-1}{2}-(l-1))\psi_{D+1}} \end{bmatrix}_{(D+1) \times (D+1)}$$

$$V_M(\psi) = \begin{bmatrix} V_M(\psi_1) & V_M(\psi_2) & \dots & V_M(\psi_{D+1}) \end{bmatrix}$$

Remember our model was

$$X = V(\psi)F_S + N$$

$$X^{(l)} = V_M^{(l)}(\psi)F_S + N^{(l)}$$

$$X^{(l)} = V_M(\psi)D^{(l)}F_S + N^{(l)}$$

$$S_X^{(l)} = V_M(\psi)D^{(l)}S_f D^{(l)H}V_M^H(\psi) + \sigma_n^2 I_{M \times M}$$

Smoothed Subarray: subscript  $SS$  stands for spatial smoothing

$$S_{SS} = \frac{1}{L} \sum_{l=1}^L S_X^{(l)}$$

Claim: The interference in  $S_{SS}$  is more uncorrelated with the desired signal, than in  $S_X$

$$S_{SS} = V_M(\psi) \left( \frac{1}{L} \sum_{l=1}^L D^{(l)} S_f D^{(l)H} \right) V_M^H(\psi) + \sigma_n^2 I_{M \times M}$$

can be shown that

- $S_{SS}$  will be close to diagonal.
- The condition number has improved. The condition number of  $S_{SS}$  is lower than the condition number of  $S_X$

$$\mathbf{S}\mathbf{x} = \begin{bmatrix} \boxed{\mathbf{S}^{(1)}\mathbf{x}} & \boxed{\mathbf{M} \times \mathbf{M}} & & \\ & \boxed{\mathbf{S}^{(2)}\mathbf{x}} & \boxed{\mathbf{M} \times \mathbf{M}} & \\ & & \boxed{\mathbf{S}^{(3)}\mathbf{x}} & \boxed{\mathbf{M} \times \mathbf{M}} \\ & & & \boxed{\mathbf{S}^{(L)}\mathbf{x}} & \boxed{\mathbf{M} \times \mathbf{M}} \end{bmatrix} \mathbf{N} \times \mathbf{N}$$

- If  $L \geq \frac{D}{2}$  guarantees that  $S_{SS}$  will be non-singular.
- $N = L + M - 1$  so for a fixed  $N$  if we decrease  $M$ ,  $L$  will increase correspondingly. We can also say that  $S_{SS}$  is more diagonal. But output  $SNR$  will decrease because of loss of degrees of freedom. Therefore for every  $S_f$  there exists an optimum  $M$  that maximizes output  $SNR$ .

$$V_M(\psi) = \begin{bmatrix} e^{-j(\frac{M-1}{2})\psi} \\ \vdots \\ e^{+j(\frac{M-1}{2})\psi} \end{bmatrix}$$

$$V_M(\psi) = JV_M^*(\psi)$$

$J$  is exchange matrix

$$J = \begin{bmatrix} 0 & \cdots & 0 & 1 \\ 0 & \cdots & 1 & 0 \\ \vdots & \ddots & \vdots & \vdots \\ 1 & \cdots & 0 & 0 \end{bmatrix}$$

$$J^2 = I$$

consider

$$JS_{SS}^*J = JV_M^*(\psi)S_{f,SS}^*V_M^T(\psi)J + \sigma_n^2I$$

Let

$$S_{f,SS} = \frac{1}{L} \sum_{l=1}^L D^{(l)} S_f D^{(l)H}$$

therefore

$$JS_{SS}^*J = V_M(\psi)S_{f,SS}^*V_M^H(\psi) + \sigma_n^2I$$

$S_f$  is supposed to be hermitian symmetric, so we can average them out. Hence, after solving we get,

$$S_{SS,FB} = \frac{1}{2} (S_{SS} + JS_{SS}^*J)$$

$$S_{SS,FB} = V_M \left( \frac{1}{2} (S_{f,SS} + S_{f,SS}^*) \right) V_M^H + \sigma_n^2 I$$

$$S_{f,SS,FB} = \frac{1}{2} (S_{f,SS} + S_{f,SS}^*)$$

Uncorrelated sources: for a ULA  $S_X$  is toeplitz, then it has a structure which looks like

$$S_X = \begin{bmatrix} 1 & r & r^2 & \dots & r^{N-1} \\ r^{-1} & 1 & r & \dots & r^{N-2} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ r^{-(N-1)} & r^{-(N-2)} & r^{-(N-3)} & \dots & 1 \end{bmatrix}$$

Here we can use ideas from min redundant array to pick subsets of elements with unique separation between elements. If signal were decorrelated, we would have got a toeplitz structure. However, here we can consider a toeplitz approximation. Important thing about toeplitz matrix is that its inversion is computationally very fast.

computations:  $M^3 \rightarrow M^2$

Can also do a weighted averaging of submatrices.

**Fast forward to chapter (9)**

## 2.2 Frequency wave number spectrum/DOA estimation

Quadratic algorithms:

- The  $\psi$  is varied and a quadratic function of  $V(\psi)$  is computed. Then we find the  $D + 1$  peaks of the above and call them.

$$\hat{\psi}_1, \hat{\psi}_2, \dots, \hat{\psi}_{D+1}$$

- Assume  $D$  is known

$$X[k] = V(\psi_s)F_s[k] + N[k]$$

where  $k = 1, \dots, K$

$P(\psi)$  = spatial power spectrum

This is obtained by scanning  $\psi$ , forming a beam and measuring the power at output of array.

### Approach 1: Beam scan algorithm

$$\hat{P}_B(\psi) = \frac{1}{K} \sum_{k=1}^K |V^H(\psi)X[k]|^2 \quad -\pi \leq \psi \leq \pi$$

subscript  $B$  stands for Bartlett Beamformer

$$\hat{P}_B(\psi) = \frac{1}{K} \sum_{k=1}^K V^H(\psi)X[k]X^H[k]V(\psi)$$

$$\hat{P}_B(\psi) = V^H(\psi)C_X V(\psi)$$

where

$$C_X = \frac{1}{K} \sum_{k=1}^K X[k]X^H[k]$$

Ideally  $C_X$  should be equal to  $S_X$

- Select  $D$  or  $D + 1$  peaks of  $\hat{P}_B(\psi)$  as  $\hat{\psi}_1 \dots \hat{\psi}_D$
- Drawback: Resolution cannot exceed  $\frac{2}{N}$  for a ULA.
- In case of a ULA, the Bartlett Beamformer reduces to an FFT operation as

$$V(\psi) = C \begin{bmatrix} 1 \\ e^{j\psi} \\ \vdots \\ e^{j(N-1)\psi} \end{bmatrix}$$

$$V^H(\psi)X[k] = C \sum_{l=0}^{N-1} X_K[l] e^{jl\psi}$$

This is FFT of

$$[X_k(0) \dots X_k(N-1)]$$

It is also known as the Bartlett method of power spectrum estimation in time series analysis.

### Approach 2: Apply weighting or the Welch Method

Here we apply window to  $X[k]$  to get

$$\begin{bmatrix} W(0)X_k(0) \\ \vdots \\ W(N-1)X_k(N-1) \end{bmatrix}$$

which further can be written as

$$W_{N \times N} \begin{bmatrix} X_k(0) \\ \vdots \\ X_k(N-1) \end{bmatrix}$$

where,

$$W_{N \times N} = \text{diag}[W(0), \dots, W(N-1)]$$

$$\hat{P}_{BW}(\psi) = \frac{1}{K} \sum_{k=1}^K |V^H(\psi)W X[k]|^2$$

$$\hat{P}_{BW}(\psi) = V^H(\psi)C_{X,W}V(\psi)$$

where

$$C_{X,W} = W C_X W^H$$

- We have applied a window (for ex: Kaiser) to data before taking the FT
- Affect the main lobe to side lobe ratios.
- Reject weak interferers in the sidelobe region
- Beam (main lobe) broadens which implies loss in resolution.

### Another option

We can improve the performance by FB averaging

- Conjugate Symmetric arrays:

$$V(\psi) = JV^*(\psi)$$

$$\hat{P}_{B,FB}(\psi) = \frac{1}{2K} \sum_{k=1}^K |V^H(\psi)(X[k] + JX^*[k])|^2 \quad -\pi \leq \psi \leq \pi$$

$$\hat{P}_{B,FB}(\psi) = V^H(\psi)C_{X,FB}V(\psi)$$

where

$$C_{X,FB} = \frac{1}{2}(C_X + JC_X^*J)$$