

A Generalized Non-Equilibrium Bounce-Back Condition for Multi-Component DdQn Lattice Boltzmann Models with Wetting Applications.

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(Dated: February 5, 2026)

Abstract will come here...

I. INTRODUCTION

Introduction will come here...

II. KNUDSEN EXPANSION

In diffusive scaling, we get the following for a Knudsen expansion,

$$\begin{aligned} f_i^{(0)} &= f_i^{\text{eq},(0)} = w_i \rho^{(0)}, \\ f_i^{(1)} &= f_i^{\text{eq},(1)} = w_i \rho^{(1)} + w_i \rho^{(0)} \frac{\mathbf{u}^{(1)} \cdot \mathbf{c}_i}{c_s^2}, \\ f_i^{(2)} &= f_i^{\text{eq},(2)} - \frac{\tau}{Sh} \left(c_{i\alpha} \partial_\alpha f_i^{\text{eq},(1)} \right). \end{aligned} \quad (1)$$

This gives the non-equilibrium part up to second order in Knudsen number,

$$\begin{aligned} f_i^{\text{neq}} &= -\frac{\tau}{Sh} \left(\partial_\alpha \left(w_i c_{i\alpha} \rho^{(1)} \right) + \frac{\rho^{(0)}}{c_s^2} \partial_\alpha \left(w_i c_{i\alpha} c_{i\beta} u_\beta \right) \right) \\ &\quad + \mathcal{O}(Kn^3). \end{aligned} \quad (2)$$

We now want to plug this into the equation for the NEBB boundary condition,

$$\begin{aligned} f_i^{\text{neq}} &= f_q^{\text{neq}} - \sum_\alpha w_i c_{i\alpha} N_\alpha, \\ N_\alpha &= \frac{1}{\sum_i^{\text{in}} w_i c_{i\alpha}^2} \sum_i^{\text{par}} f_i c_{i\alpha} \equiv C_\alpha \sum_i^{\text{par}} f_i c_{i\alpha}. \end{aligned} \quad (3)$$

$$\underline{\underline{M}} = \begin{pmatrix} -12B_{00}^i + 9B_{11} + 9B_{22} & -18B_{01} & -18B_{02} \\ -18B_{01} & 9B_{00} - 27B_{11} & -54B_{12} \\ -18B_{02} & -54B_{12} & 9B_{00} - 27B_{22} \end{pmatrix} \quad (9)$$

$$\underline{\underline{M}} = \begin{pmatrix} -27B_{00} + 9B_{11} & -18B_{01} & -54B_{02} \\ -18B_{01} & 9B_{00} - 12B_{11} + 9B_{22} & -18B_{12} \\ -54B_{02} & -18B_{12} & 9B_{11} - 27B_{22} \end{pmatrix} \quad (10)$$

$$\underline{\underline{M}} = \begin{pmatrix} -27B_{00} + 9B_{22} & -54B_{01} & -18B_{02} \\ -54B_{01} & -27B_{11} + 9B_{22} & -18B_{12} \\ -18B_{02} & -18B_{12} & 9B_{00} + 9B_{11} - 12B_{22} \end{pmatrix} \quad (11)$$

We now want to add stress corrections,

$$f_i^{\text{neq}} = f_q^{\text{neq}} - \sum_\alpha w_i c_{i\alpha} N_\alpha - \sum_\mu \sum_\nu w_i c_{i\mu} c_{i\nu} M_{\mu\nu} \quad (4)$$

The corrections can be found using the expected Navier-Stokes second moment,

$$\Pi_{\alpha\beta}^{\text{NS}} = -\tau c_s^2 \rho (\partial_\alpha u_\beta + \partial_\beta u_\alpha) \quad (5)$$

The velocity gradients can be estimated using finite differences. We now want to ensure the following,

$$\sum_i c_{i\alpha} c_{i\beta} f_i = \Pi_{\alpha\beta}^{\text{NS}}. \quad (6)$$

This gives the following tensor equation,

$$\sum_\mu \sum_\nu Q_{\alpha\beta\mu\nu} M_{\mu\nu} = B_{\alpha\beta} \quad (7)$$

With the following definitions,

$$\begin{aligned} Q_{\alpha\beta\mu\nu} &\equiv -\sum_i^{\text{in}} w_i c_{i\alpha} c_{i\beta} c_{i\mu} c_{i\nu}, \\ B_{\alpha\beta} &\equiv \Pi_{\alpha\beta}^{\text{NS}} - A_{\alpha\beta}, \\ A_{\alpha\beta} &\equiv 2 \sum_i^{\text{out}} c_{i\alpha} c_{i\beta} f_i + \sum_i^{\text{par}} c_{i\alpha} c_{i\beta} f_i \\ &\quad + \sum_i^{\text{in}} c_{i\alpha} c_{i\beta} \left(2w_i \rho \frac{\mathbf{u} \cdot \mathbf{c}_i}{c_s^2} - \sum_\gamma w_i c_{i\gamma} N_\gamma \right). \end{aligned} \quad (8)$$

For a boundary in the yz , xz and xy -planes, Eq. (7) can be solved if we use the D3Q27 stencil,

$$(9)$$

$$(10)$$

$$(11)$$

