

# Lecture XI: Fluid Simulation

(based on “Fluid Simulation” course notes from SIGGRAPH 2007)

# Example: Fluid Simulation

<https://youtu.be/F5KuP6qEuew>

# Coupled Particle System

- Particles interact with each other depending on their spatial relationship.
  - these relationships are **dynamic**, so geometric and topological changes can take place.
- Each particle  $p_i$  has a potential energy  $E_{Pi}$ .
  - The sum of the pairwise potential energies between the particle  $p_i$  and the other particles.

$$E_{Pi} = \sum_{j \neq i} E_{Pij}$$

# Coupled Particle System

- The force  $f_i$  applied on the particle at position  $p_i$  is

$$f_i = -\nabla_{p_i E_{Pi}} = -\sum_{j \neq i} \nabla_{p_i E_{Pij}}$$

where  $\nabla_{p_i E_{Pi}} = \left( \frac{dE_{Pi}}{dx_i}, \frac{dE_{Pi}}{dy_i}, \frac{dE_{Pi}}{dz_i} \right)$

- Reducing computational costs by **localizing**.
  - potential energies weighted according to distance to particle.

# Smoothed Particle Hydrodynamics (SPH)

- Any quantity  $A$  at any point  $r$  is given by

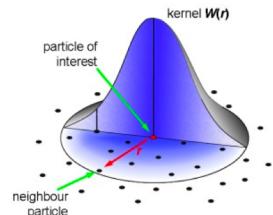
$$A(r) = \sum_j m_j \frac{A_j}{\rho_j} W(|r - r_j|, h)$$

- $W$ : smoothing kernel
- $\rho_j$ : particle density
  - usually Gaussian function or cubic spline.
- $h$ : smoothing length.

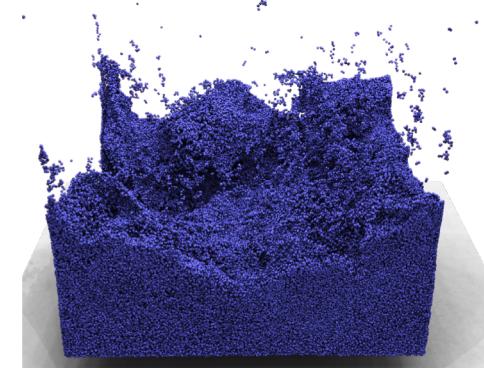
- Example: the density can be calculated as

$$\rho(r) = \sum_j m_j W(|r - r_j|, h)$$

- Applied to pressure and viscosity forces.
- External forces are applied directly to the particles.



[http://www.nuigalway.ie/media/publicsub-sites/engineering/images/bio\\_sphkernel1.jpg](http://www.nuigalway.ie/media/publicsub-sites/engineering/images/bio_sphkernel1.jpg)



[http://rnd-zimmer.de/images/sph\\_particles2.png](http://rnd-zimmer.de/images/sph_particles2.png)

# Smoothed Particle Hydrodynamics

- Derivatives of quantities: by derivatives of  $W$ :

$$\nabla A(r) = \sum_j m_j \frac{A_j}{\rho_j} \nabla W(|r - r_j|, h)$$

- Varying  $h \Leftrightarrow$  tunes the resolution of a simulation locally.
  - Typically use a **large length** in **low particle** density regions and vice versa.
- **Pro:** easy to conserve mass (constant number of particles).
- **Con:** difficult to maintain material **incompressibility**.

# Reminder: Navier-Stokes Equations

- Representing the **conservation of mass** and momentum for an **incompressible** fluid ( $\nabla \cdot \vec{u} = 0$ ):

$$\underbrace{\rho \left( \frac{D\vec{u}}{Dt} + \vec{u} \cdot \nabla \vec{u} \right)}_{\begin{array}{c} \text{Material Derivative} \\ \text{Unsteady acceleration} \end{array}} = \underbrace{\nu \nabla \cdot (\nabla \vec{u})}_{\text{Convective acceleration}} - \underbrace{\nabla p}_{\text{Viscosity}} + \underbrace{\vec{f}}_{\text{Pressure gradient}} + \underbrace{\vec{f}}_{\text{External body forces}}$$

- $p$ : pressure field
- $\nu$ : kinematic viscosity.
- $f$ : body force per density (usually just gravity  $\rho g$ ).

# Reduced form

- No Viscosity:

$$\rho(\vec{u}_t + \vec{u} \cdot \nabla \vec{u}) = -\nabla p + \vec{f}$$

- Incompressibility:

$$\nabla \cdot \vec{u} = 0$$

- Denoted as Euler equations.

- Solid-wall boundary conditions:  $\vec{u} \cdot \hat{n} = 0$

- There is no velocity on the boundary!
- Bouncing creates force\impulse.
- Relate: shooting up and falling own.

# Splitting

- Consider PDE:

$$\frac{dq}{dt} = a(q) + b(q)$$

- Solution mechanism: one after the other:

$$q'(t) = q(t) + \Delta t a(q)$$
$$q'(t + \Delta t) = q'(t) + \Delta t b(q')$$

- First-order accurate
- **Good for:** when solving separately is much easier.

$$\rho \left( \frac{D\vec{u}}{Dt} \right) = -\nabla p + \vec{f}$$

# Discrete inviscid NS Equations

- Three split steps in each iteration:
- Advection:  $\frac{D\vec{u}}{Dt} = 0$ .
- Body forces:  $u_t = \vec{f}$ .
- Pressure and incompressibility:

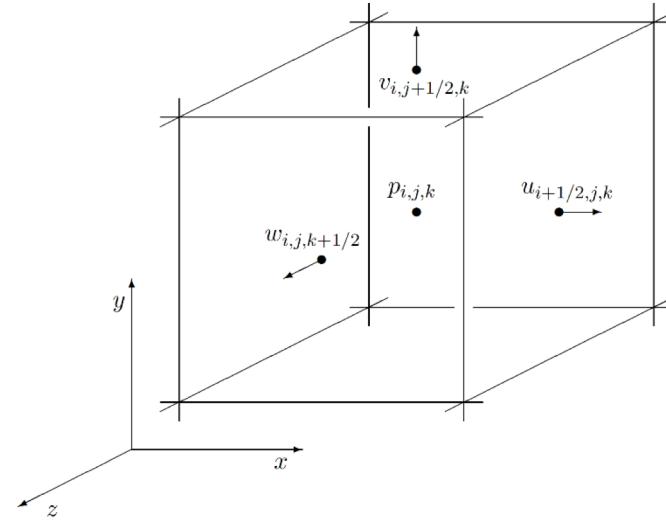
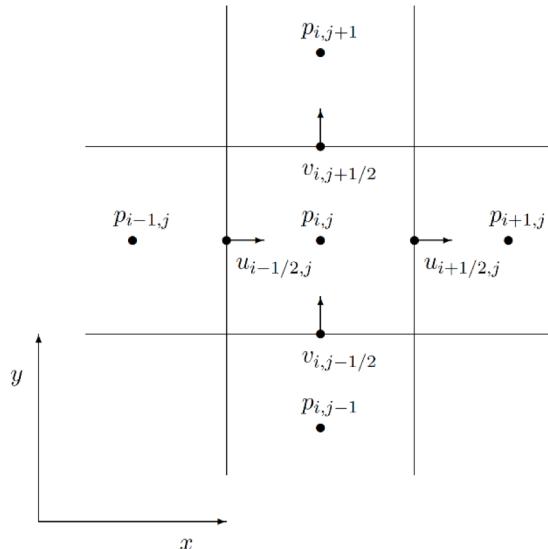
$$\begin{aligned}\rho u_t + \nabla p &= 0 \text{ so that} \\ \nabla \cdot \vec{u} &= 0\end{aligned}$$

# Discrete inviscid NS Equations

- For each time step:
- $U(t)$ : all discrete values of  $\vec{u}$ .  $F$  for  $\vec{f}$ .
  - $U^A = \text{advect}(U(t), \Delta t, U(t))$  (Advection)
  - $U^B = U^A + \Delta t F$  (Body forces)
  - $U(t + \Delta t) = \text{project}(U^B, \Delta t)$  (Pressure and incompressibility)

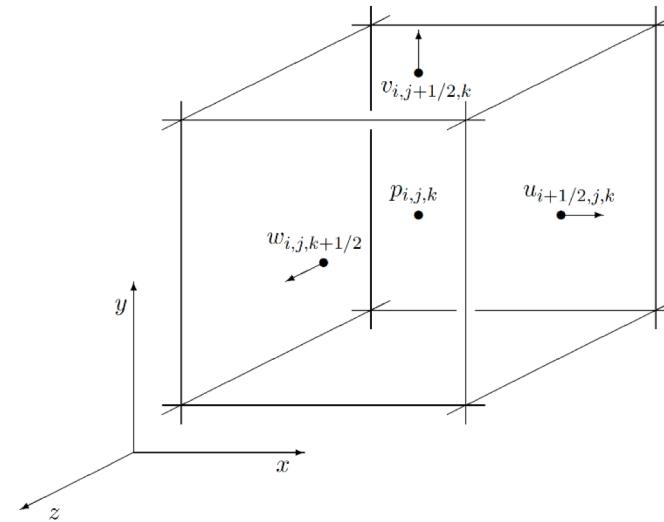
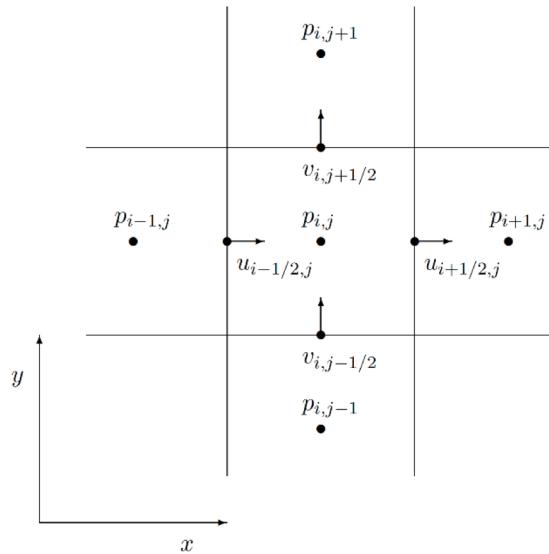
# MAC Grid

- Marker-and-Cell
- Different values are stored in different locations
- Advantages:
  - Stability
  - Staggered instead of collocated.



# MAC Grid

- In our case:
  - **Velocities**: on mid-edges
    - Each dimension  $\vec{u} = (u, v, w)$  on each type of mid-edge!
  - **Pressures**: in mid cells.
  - **Interpolation**: by bilinear\trilinear functions.

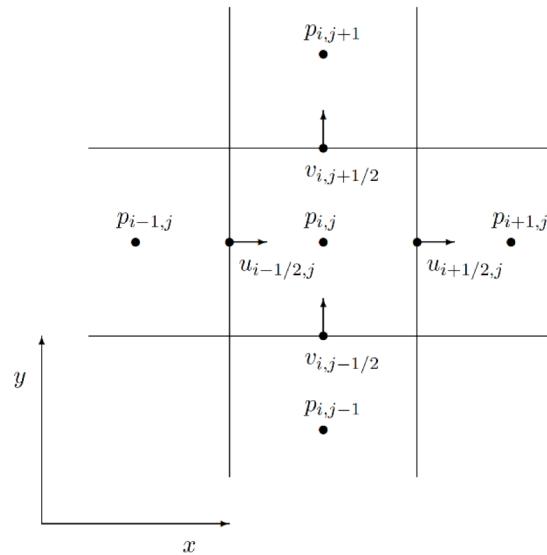


# Derivatives

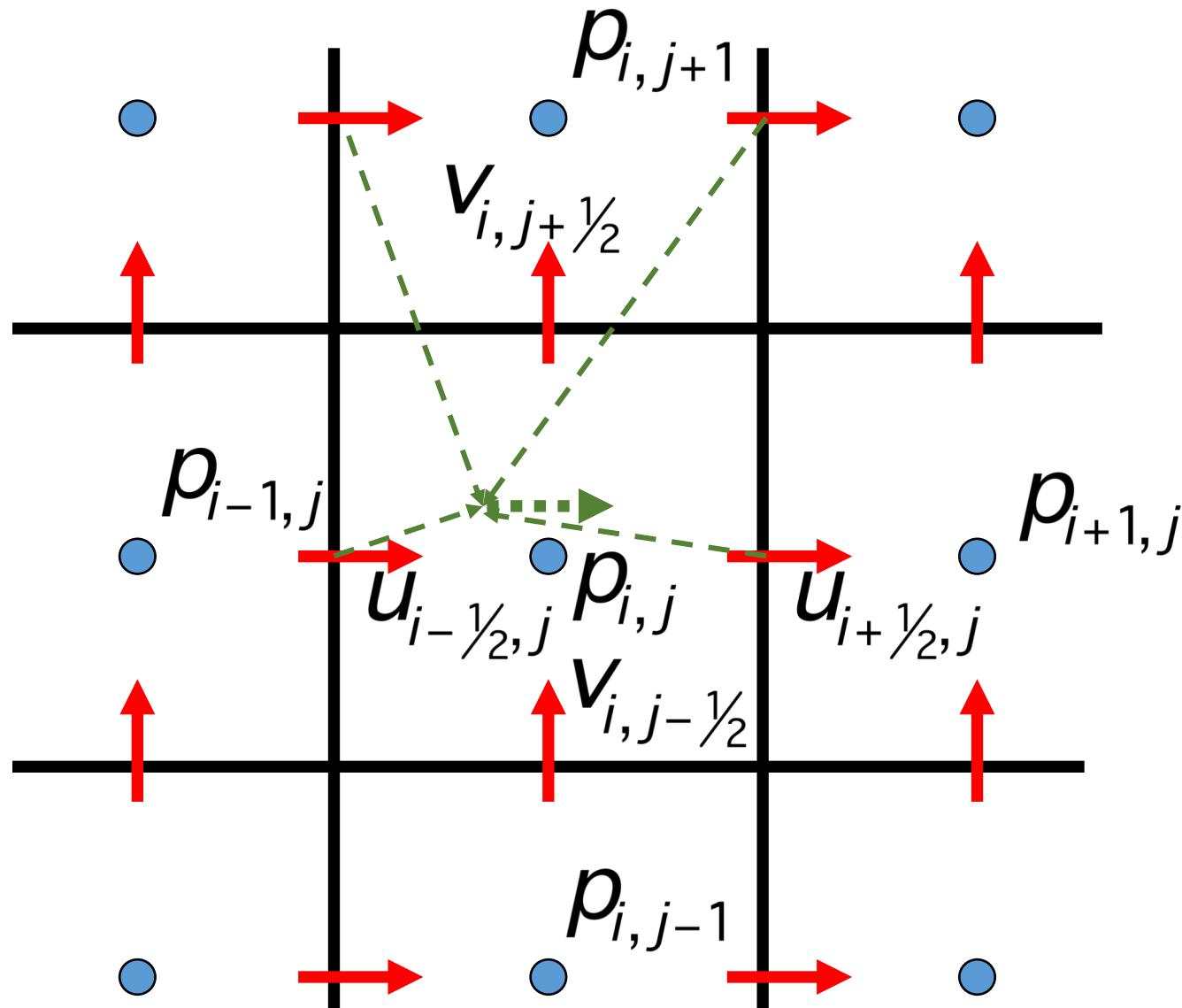
- Central differences:

$$\frac{\partial u}{\partial x} \approx \frac{u_{i+1/2} - u_{i-1/2}}{\Delta x}$$

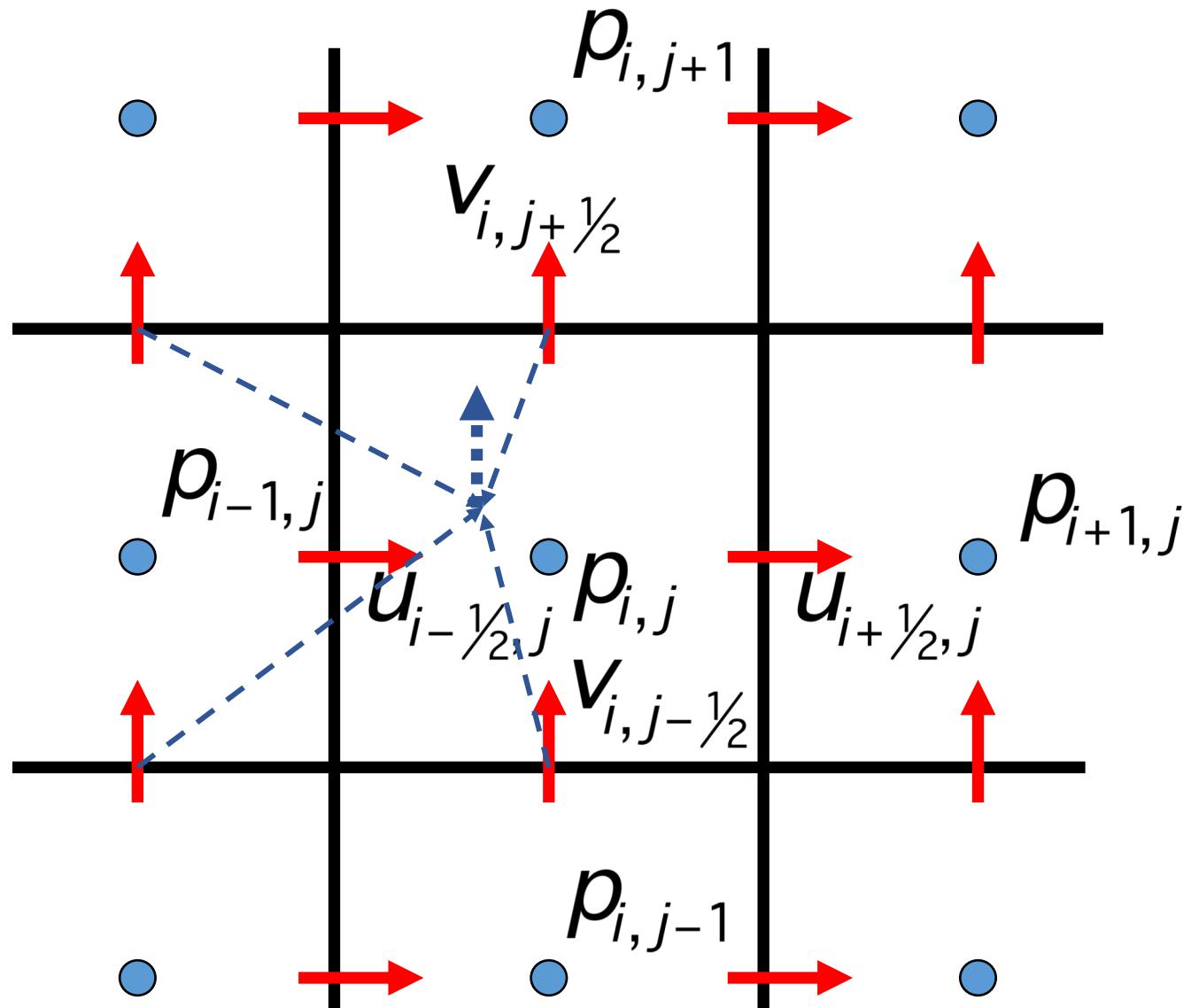
- Derivatives of mid-edges live on grid centers.
- And vice versa.



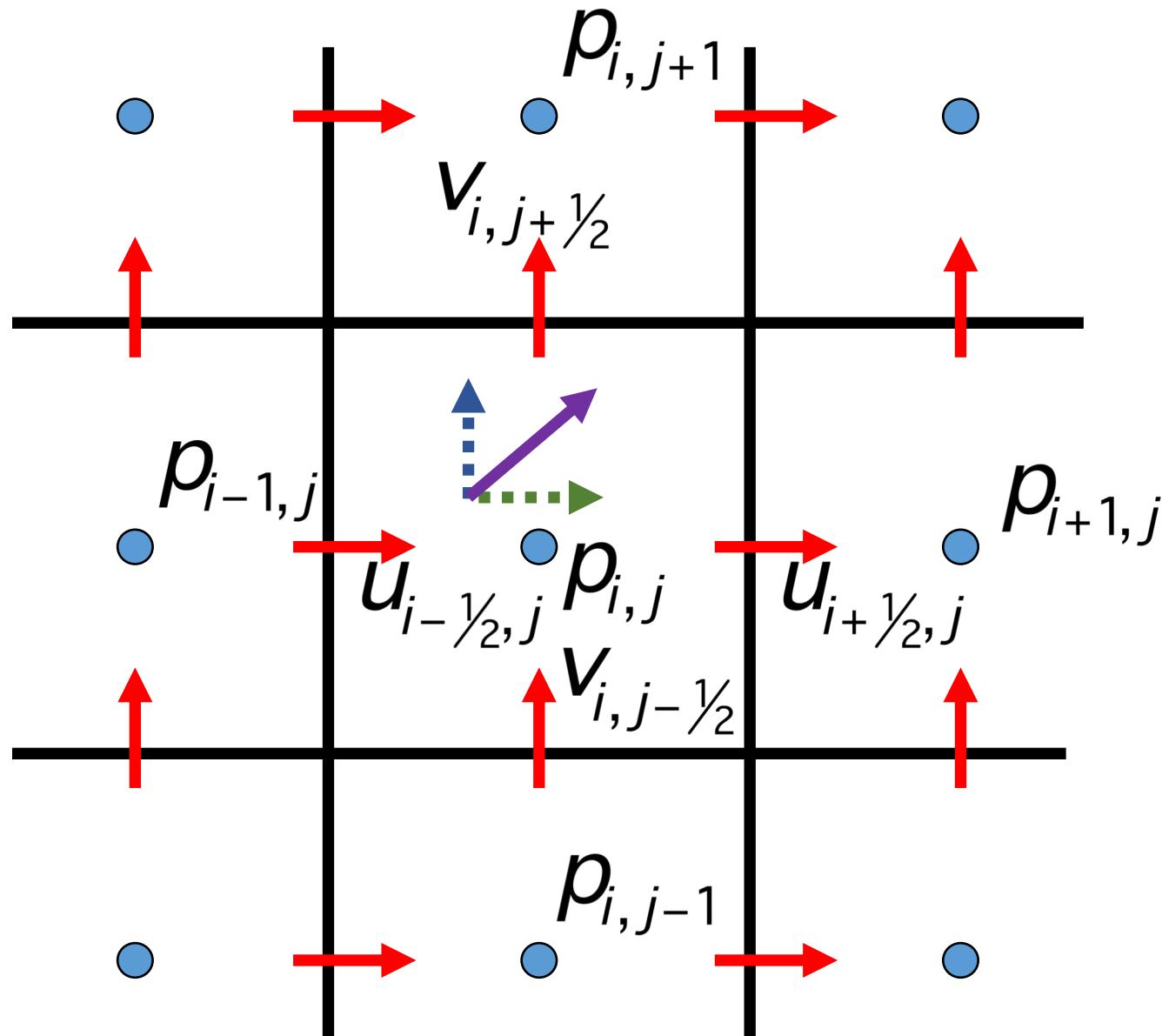
# Interpolation



# Interpolation



# Interpolation



# Advection

- Continuous equation:

$$\frac{Dq}{Dt} = q_t + \vec{u} \cdot \nabla q = 0$$

- Naïve discretization:

$$\frac{q_i(t + \Delta t) - q_i(t)}{\Delta t} + (u_i, v_i, w_i) \frac{q_{i+1}(t) - q_{i-1}(t)}{2\Delta x}$$

- Conditionally **unstable**!

- Will blow up for every  $\Delta t$ .

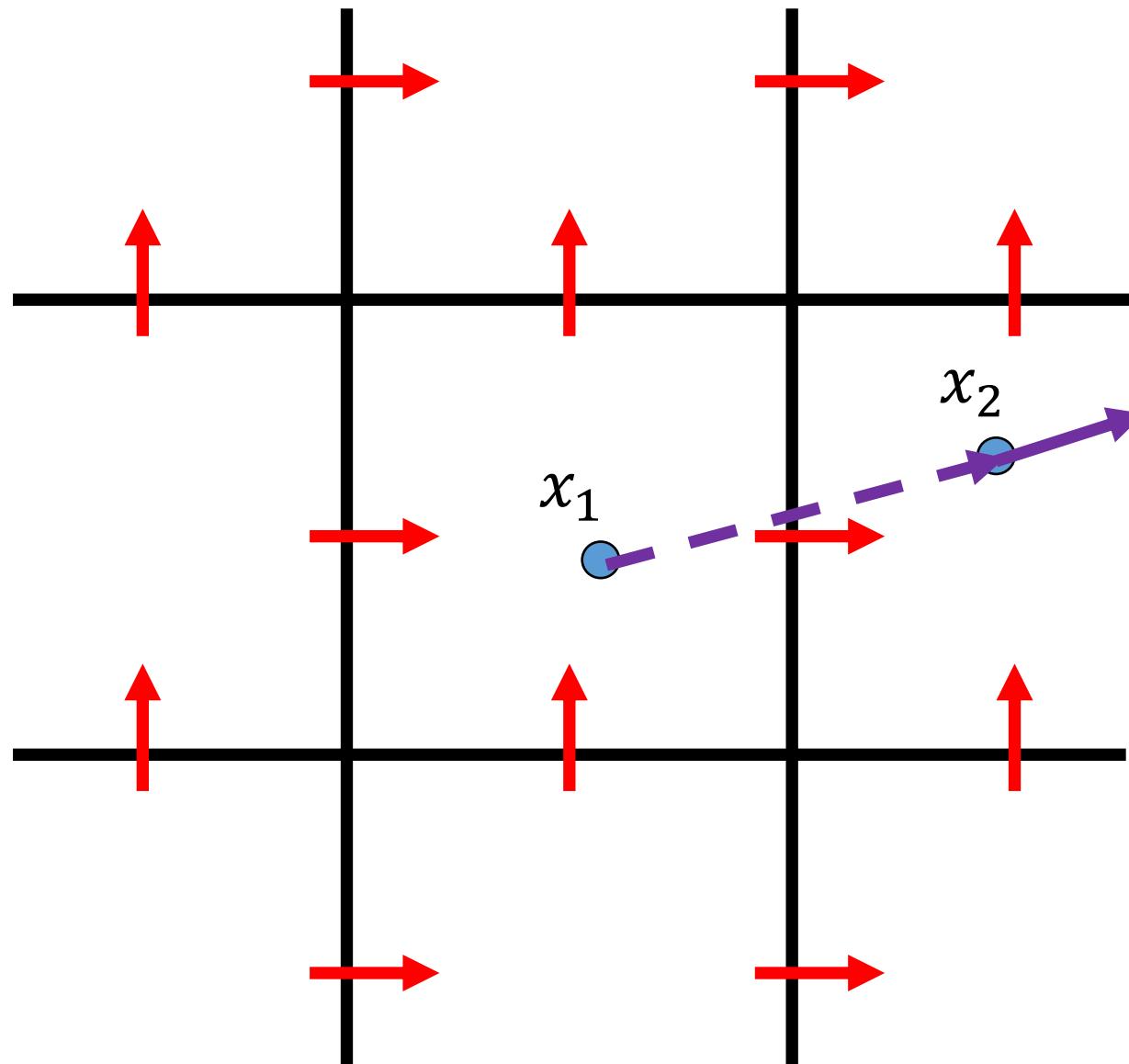
# Semi-Lagrangian

- Recall that  $\frac{Dq}{Dt} = 0$  is trivial for Lagrangian particles.
- **Insight:** if we have  $q(t)$  at some grid point  $x_2$  with velocity  $\vec{u}$  it was **advected** from another point  $x_1$  in the grid:

$$\vec{u} = \frac{x_2 - x_1}{\Delta t}$$

- Value  $q(t)$  at  $x_2$  = value  $q(t - \Delta t)$  in  $x_1$ .
- Getting  $q(t - \Delta t)$  in  $x_1$  from bi\trilinear interpolation.

# Semi-Lagrangian



# Extrapolation

- Position  $x_1$  might be outside of the fluid
- We need to extrapolate the flow field to be defined everywhere.
- Grid boundaries: “no-stick” condition:  $\vec{u} \cdot \hat{n} = 0$ 
  - More simply in our case: just  $\vec{u} = 0$  outside.
- In grid, outside of fluid: more complicated...
  - Basic idea: closest-neighbor interpolation.

$$\rho u_t + \nabla p = 0 \text{ s.t. } \nabla \cdot \vec{u} = 0$$

# Incompressibility

- Let us take the divergence on  $\rho u_t + \nabla p = 0$ :

$$\nabla \cdot \rho \frac{\partial u}{\partial t} + \nabla \cdot \nabla p = 0 \rightarrow$$

$$\rho \frac{\partial}{\partial t} (\nabla \cdot u) + \nabla \cdot \nabla p = 0$$

- That's because " $\frac{\partial}{\partial t}$ " and " $\nabla \cdot$ " work on independent variables and therefore commute.

# Incompressibility

- We need to solve for  $\nabla \cdot \vec{u} = 0$ 
  - Pressure is solved for to make this happen.
- Idea: discretize  $\rho \frac{\partial}{\partial t} (\nabla \cdot u) + \nabla \cdot \nabla p = 0$  as

$$\nabla \cdot \nabla p = -\rho \frac{(\nabla \cdot u)(t + \Delta t) - (\nabla \cdot u)(t)}{\Delta t}$$

- As we want  $(\nabla \cdot u)(t + \Delta t) = 0$  we solve for:

$$\Delta p = \rho \frac{(\nabla \cdot u)(t)}{\Delta t}$$

# The Discrete Divergence

- Lives in faces (like pressure)

$$\nabla \cdot \vec{u} \approx \frac{u_{i+1/2} - u_{i-1/2}}{\Delta x} + \frac{v_{j+1/2} - v_{j-1/2}}{\Delta x} + \dots$$

- Laplacian of pressure is similar:

$$\Delta p \approx \frac{p_{i,j} - p_{i-1,j}}{\Delta x} + \frac{p_{i,j} - p_{i+1,j}}{2\Delta x} + \dots$$

- Need to solve for pressure and consequently velocity.
  - Details are a bit nasty (Section 4.3 of notes)

$$\rho u_t + \nabla p = 0 \text{ s.t. } \nabla \cdot \vec{u} = 0$$

# Velocity from pressure

- The discretization of

$$u_t = -\frac{1}{\rho} \nabla p$$

- Becomes  $u(t + \Delta t) = u(t) - \frac{\Delta t}{\rho} (p_{i+1} - p_{i-1})$ 
  - And similarly for every dimension.
- The advantage of MAC: gradient of pressures lives on mid-edges, like velocities!

# Fluid Surface Conditions

- “Ghost” pressure for solid walls:

$$p_{i+1} = p_i + \frac{\rho \Delta x}{\Delta t} u_{i+1/2}$$

- Just inverting the pressure equation.
- For free boundary (water surface):  $p_i = 0$ .

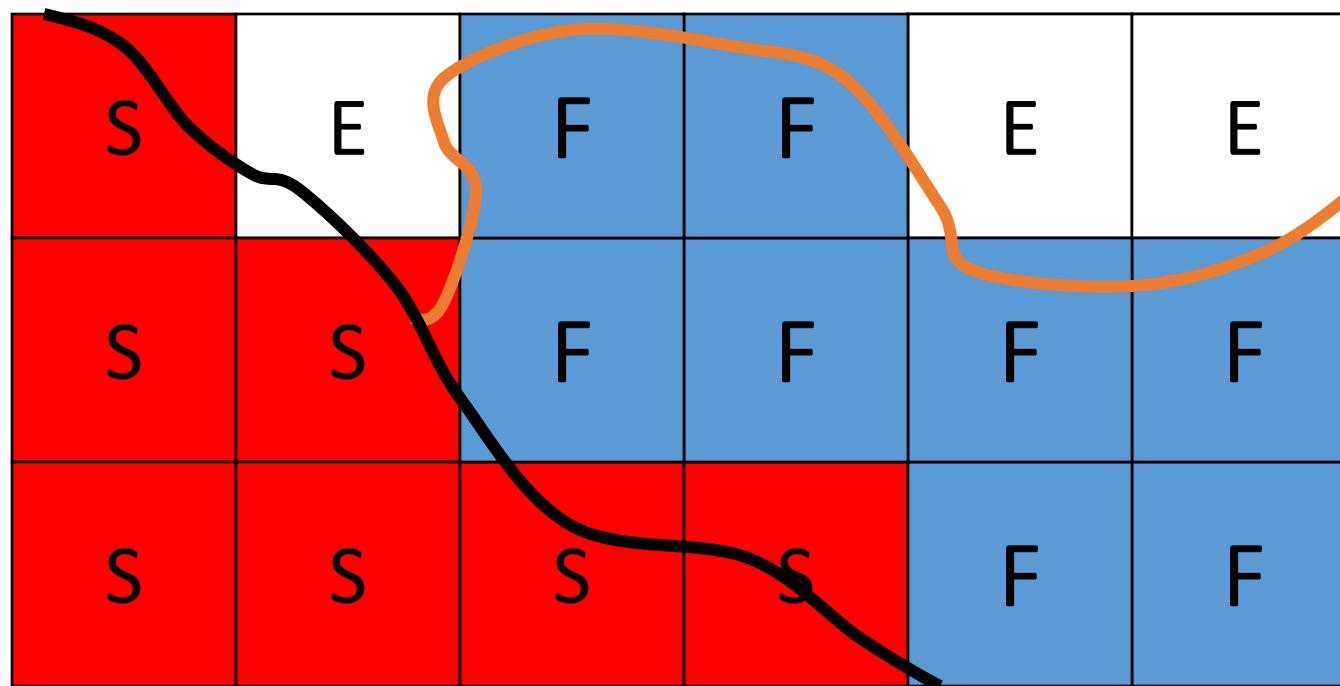


# Linear Equations

- End up with a sparse set of linear equations to solve for pressure
  - Matrix is symmetric positive (semi-)definite
- In 3D on large grids, direct methods unsatisfactory
- Instead use Preconditioned Conjugate Gradient, with Incomplete Cholesky preconditioner

# Discrete Boundaries

- Grid cells are either solid, fluid, or empty.



# Voxelization is Suboptimal

- “8-bit water”
  - Waves less than a grid cell high aren’t “seen” by the fluid solver – thus they don’t behave right
  - Strangely textured surface
- Solid wall artifacts:
  - If boundary not grid-aligned, noticeable geometric error.
  - Slopes are turned into stairs.

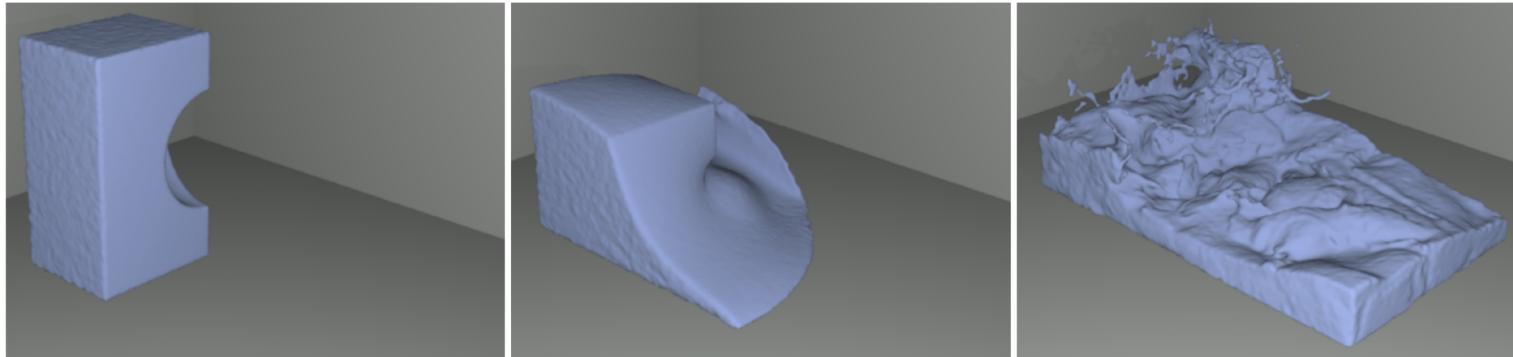
# Marker Particles

- Simplest approach is to use marker particles
- Sample fluid volume with particles  $\{x_p\}$
- At each time step, mark grid cells containing any marker particles as **Fluid**, rest as **Empty** or **Solid**
- Advect particles with velocity:

$$\frac{Dx_p}{Dt} = 0$$

# Rendering Marker Particles

- Need to wrap a surface around the particles
  - e.g. blobbies, or Zhu & Bridson '05
- Problem: rendered surface has bumpy detail that the fluid solver doesn't have access to
  - The simulation can't animate that detail properly if it can't "see" it.
- Result: looks fine for splashy, noisy surfaces, but fails on smooth, glassy surfaces.



# Level Sets

- Model a function  $\phi(x)$  on the grid so that the fluid boundaries are at  $\phi(x) = 0$
- In particular, best behaved type of implicit surface function is signed distance:

$$\phi(x) = \begin{cases} dist(x, surface) & x \text{ outside} \\ -dist(x, surface) & x \text{ inside} \end{cases}$$

- e.g. the book [Osher&Fedkiw'02]

# Surface Capturing

- Evolving  $\phi(x)$  on the grid by advection as well.
- The surface ( $\phi(x) = 0$ ) moves at the velocity of the fluid
- Topological changes automatically inferred.

$$\frac{D\phi}{Dt} = 0$$



# Reinitializing

- Advecting  $\phi(x)$  this way doesn't preserve signed distance property
  - Eventually gets badly distorted
  - Causes problems particularly for extrapolation, also for accuracy in general
- Reinitialize: recompute distance to surface every once in a while.
  - Ideally shouldn't change surface at all, just values in the volume