

OpenDSS Training Workshop - 2021

PVSystem + InvControl

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EPRI Knoxville, TN

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Instructor



■ Paulo Radatz

Paulo Radatz serves as Engineer/Scientist II at the Electric Power Research Institute (EPRI) in Knoxville, Tennessee, USA. He received both his Masters and Bachelors's degree in electrical engineering, emphasizing energy and automation, from the University of Sao Paulo, Sao Paulo, Brazil. He was awarded a prize for being the best bachelor's student of Polytechnic School of University of Sao Paulo (2015). He has six years of experience with OpenDSS, having taught several OpenDSS trainings in Brazil at conferences, universities, and industry. He is the founder of the largest YouTube channel about OpenDSS in the world.

Agenda



PVSystem Modeling



InvControl – Convergence Method



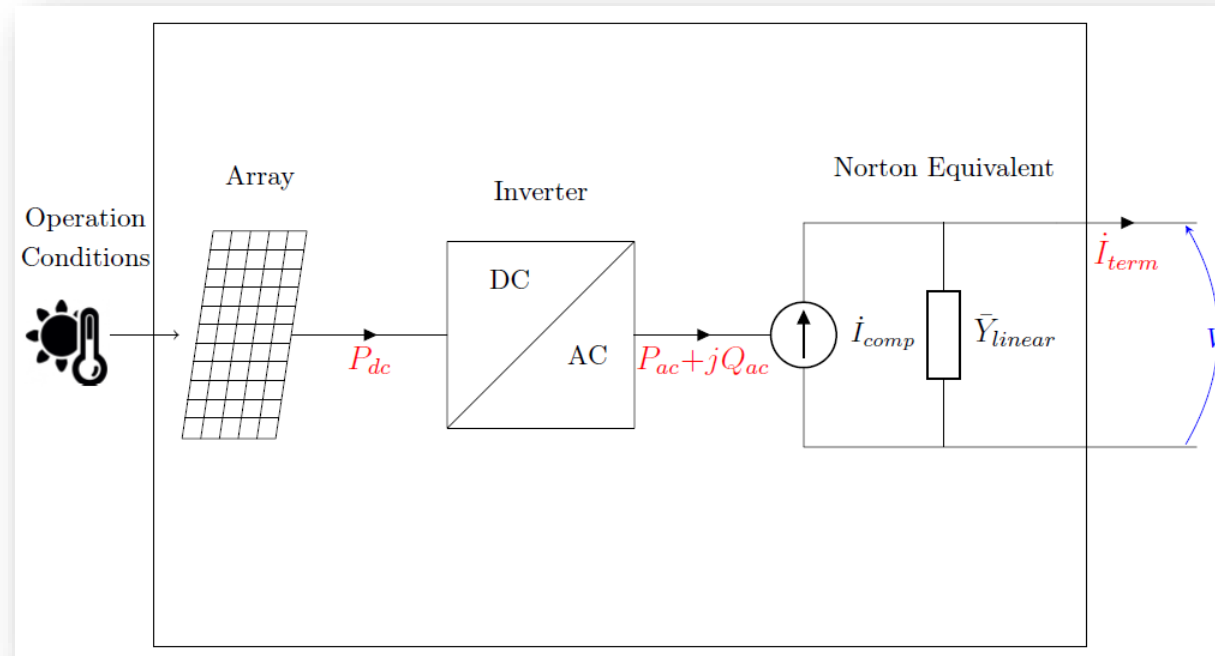
**A Few Examples of Smart Inverter Functions According
IEEE Std 1547-2018**



PVSystem Modeling

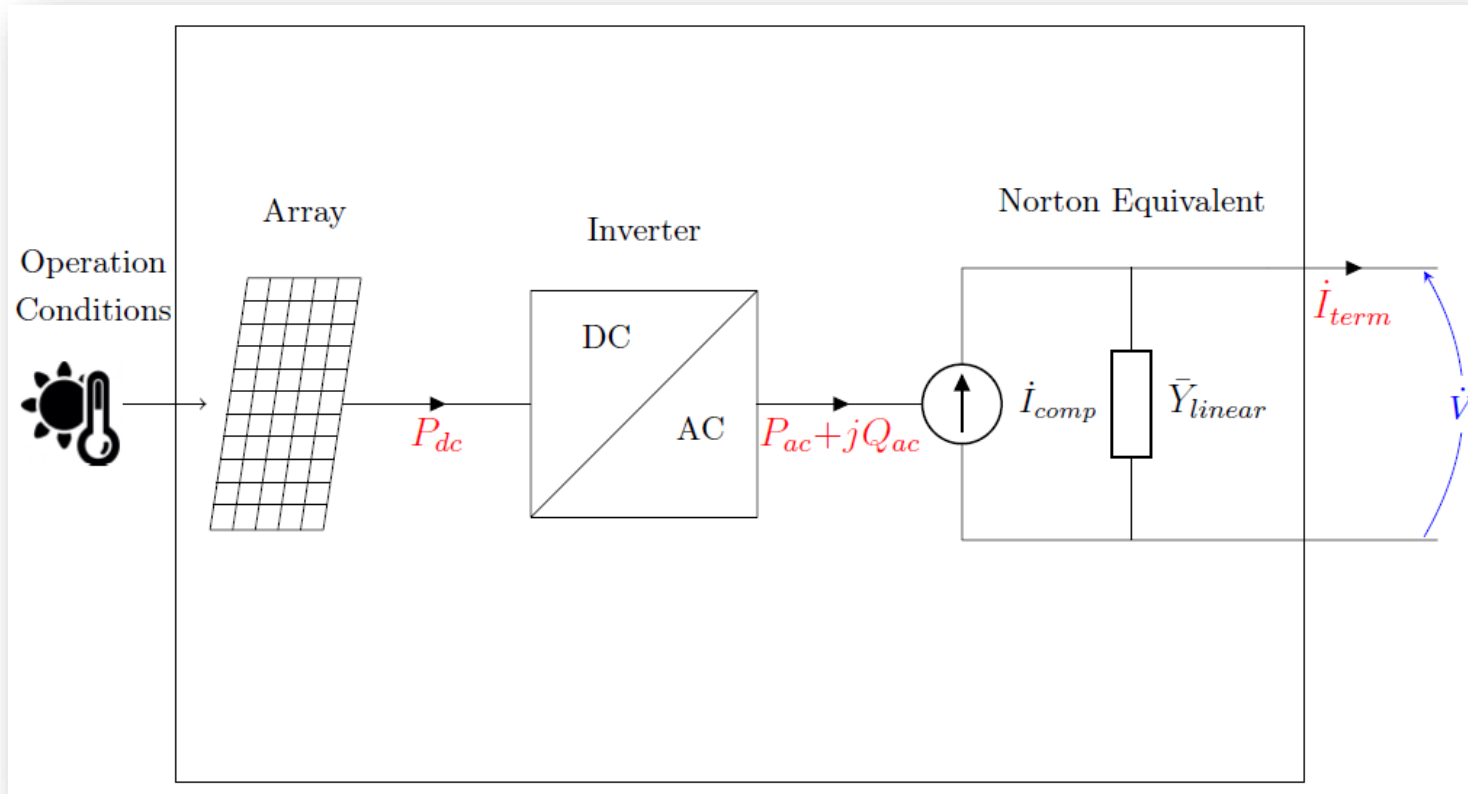
PVSystem Element in OpenDSS

- The PVSystem model combines the photovoltaic (PV) array and the PV inverter into one convenient model to for distribution system impacts studies



Steady State model for QSTS Analysis

PVSystem Element in OpenDSS



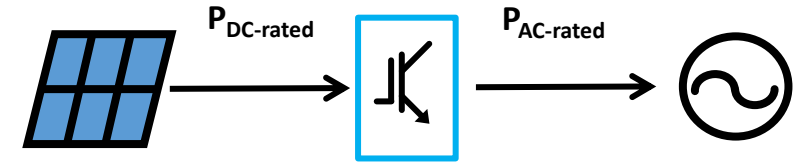
- PVSystem properties
 - PV Array
 - PV Inverter
 - Operating conditions

- Resources:

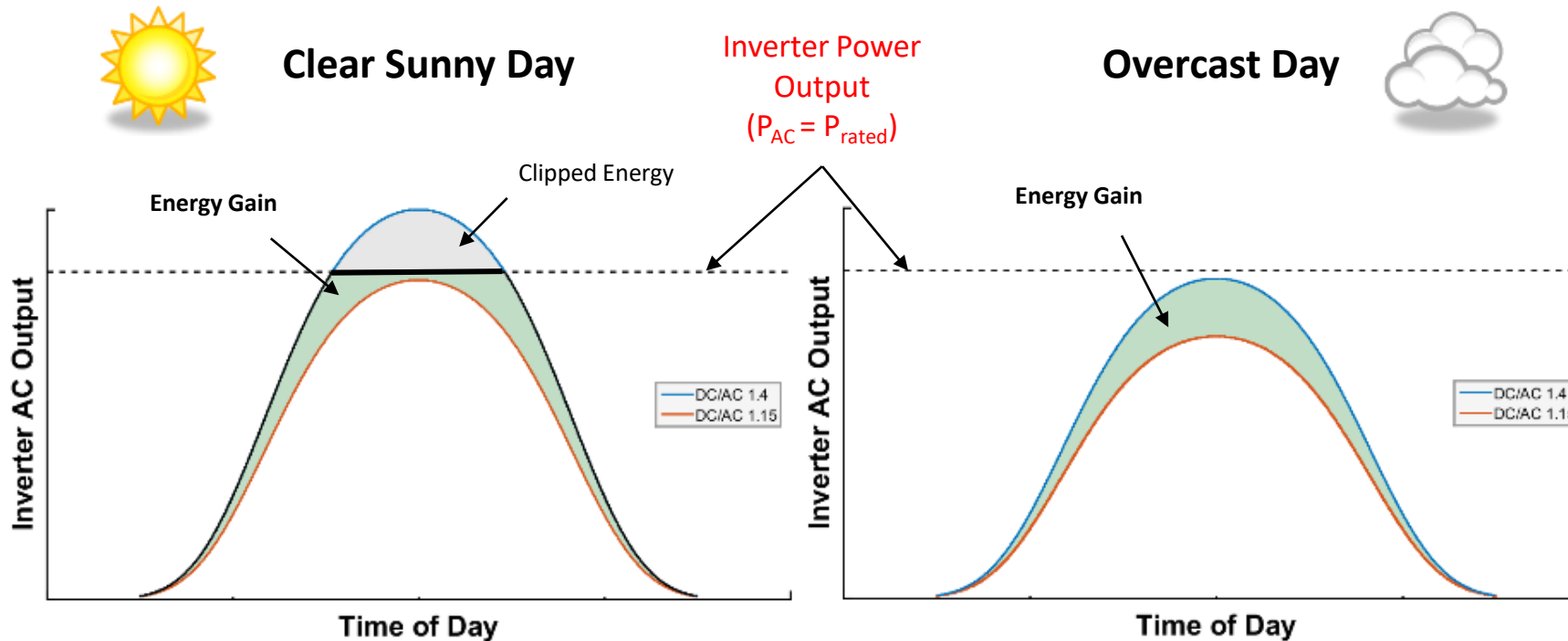
- 2020 OpenDSS training record: <https://www.epri.com/events/C97292AF-0790-4514-B9DF-CCEF80D685E1>
- OpenDSS example folder: C:\Program Files\OpenDSS\Examples\InverterModels\PVSystem
- Pdf document: C:\Program Files\OpenDSS\Examples\InverterModels\PVSystem\PVSystem_InvControl.pdf
- YouTube videos: <https://www.youtube.com/playlist?list=PLhdRxvt3nJ8wTHIm0ohOOSxPr4O61YulY>
- Today's presentation and resource files: https://sourceforge.net/p/electricdss/code/HEAD/tree/trunk/Training/Virtual-2021/Session3/PVSystem_InvControl/

PV system design: DC-to-AC Ratio

- In a PV system with higher DC-to-AC ratio, inverter(s) will generate more active power/energy.
- PV system's AC power output should not exceed the aggregate AC power ratings of the inverters.



$$\frac{P_{DC-rated}}{P_{AC-rated}} = \text{DC-to-AC ratio}$$

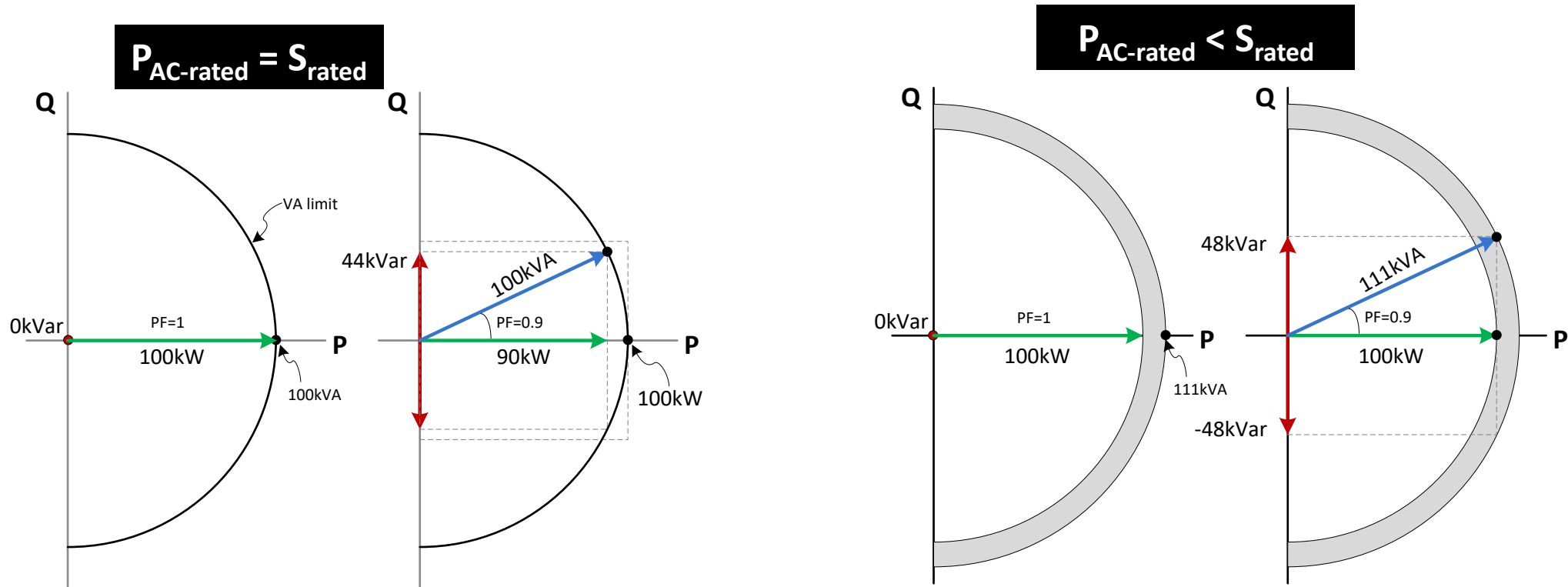


Reference:

Tutorial on Inverter Fundamentals and Grid Support Functions (P174B, Contact: Aminul Huque, mhuque@epri.com)

Inverter design - kVA vs kW Rating

- By design, inverters are volt-ampere (VA) limited device.
- Figures bellow show the transition of inverter operation from rated power at unity power factor to 0.9 power factor for two different inverter designs.

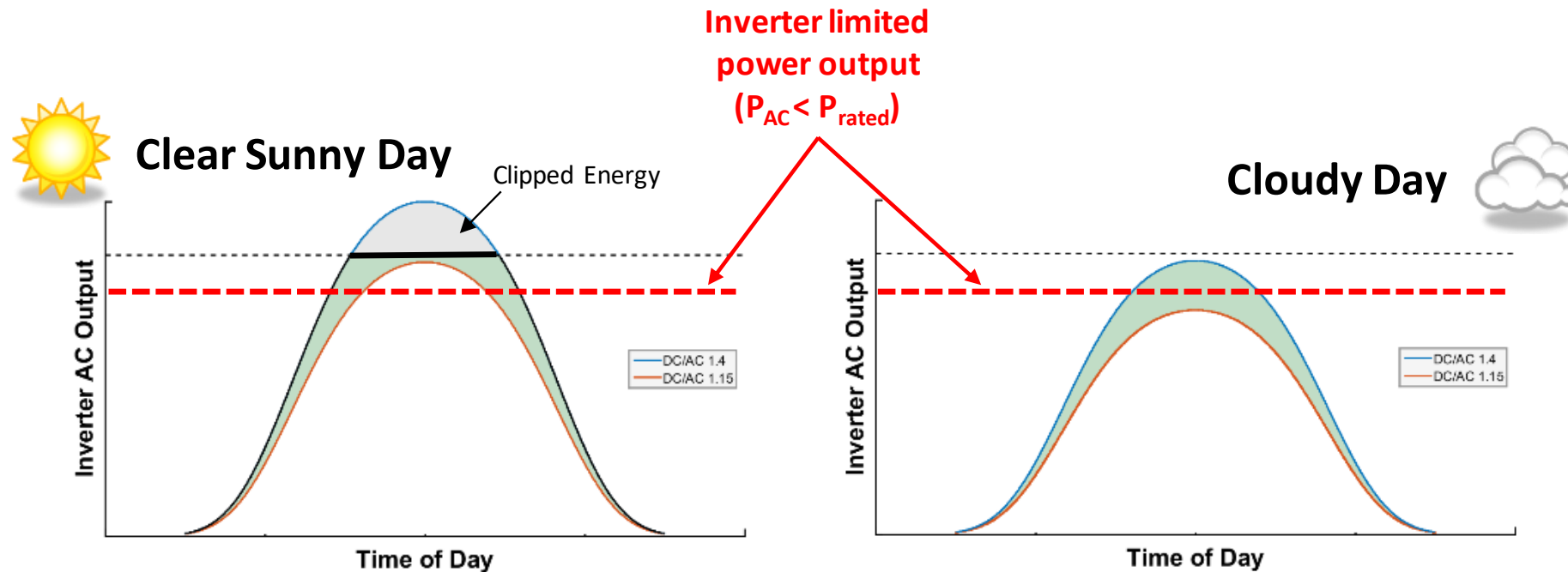


Reference:

Tutorial on Inverter Fundamentals and Grid Support Functions (P174B, Contact: Aminul Huque, mhuque@epri.com)

DC-to-AC Ratio and kVA vs kW Rating

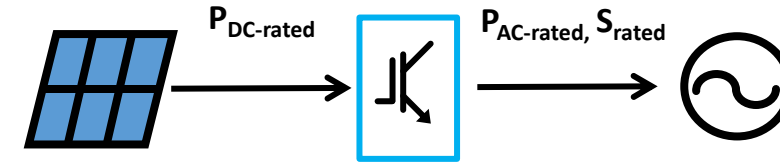
- If the inverter needs to limit its active power output to generate reactive power (in case of kVA=kW ratings) required by the voltage control function, energy loss will be higher for systems with higher DC-to-AC ratio.



Reference:

Tutorial on Inverter Fundamentals and Grid Support Functions (P174B, Contact: Aminul Huque, mhuque@epri.com)

Modeling PVSystem based on DC-to-AC and kVA vs kW



- $P_{DC-rated}$, $P_{AC-rated}$, S_{rated} are the properties that should be modeled
- Current version of PVSystem Model (OpenDSS version 9.3.0.2)
 - There are only two properties: **Pmpp** and **kVA**.
 - When DC-to-AC ratio = 1, **Pmpp** represents both **PDC-rated** and **PAC-rated** (they are the same). And kVA is S_{rated}

When DC-to-AC ratio > 1 , how to model both PDC-rated and PAC-rated?

Modeling PVSystem based on DC-to-AC and kVA vs kW

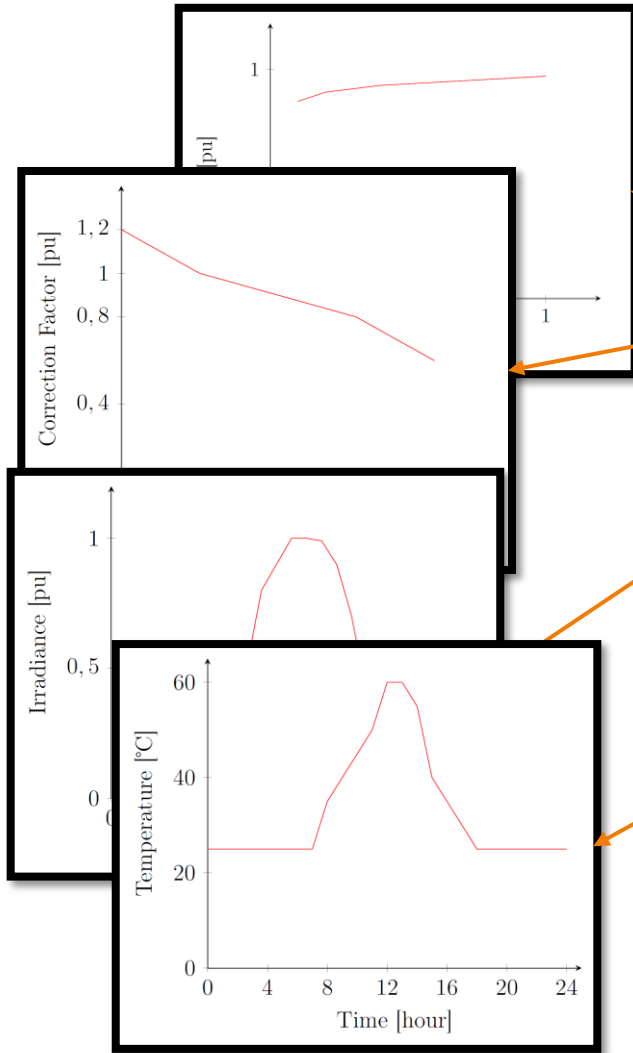
Nameplate information:

- Given
 - Srated, DC-to-AC ratio, and kVA-to-kW ratio
- Then,
 - PAC-rated = Srated / kVA-to-kW ratio
 - PDC-rated = PAC-rated * DC-to-AC ratio = Srated * DC-to-AC ratio / kVA-to-kW ratio

PVSystem modeling:

- $kVA = S_{rated}$
- $P_{mpp} = PDC\text{-}rated$
- $\%P_{mpp} = 100 * PAC\text{-}rated / PDC\text{-}rated = 100 / DC\text{-}to\text{-}AC \text{ ratio}$

Script Example



Clear

New Circuit.TheveninEquivalent bus1=A pu=1.0 basekv=13.8

~ Z0=[10, 10] Z1=[10, 10]

New XYCurve.Eff npts=4 xarray=[.1 .2 .4 1.0] yarray=[0.86 0.9 0.93 0.97]

New XYCurve.FatorPvsT npts=4 xarray=[0 25 75 100] yarray=[1.2 1.0 0.8 0.6]

New Loadshape.Irrad npts=24 interval=1

~ mult=[0 0 0 0 0 0 .1 .2 .3 .5 .8 .9 1.0 1.0 .99 .9 .7 .4 .1 0 0 0 0 0]

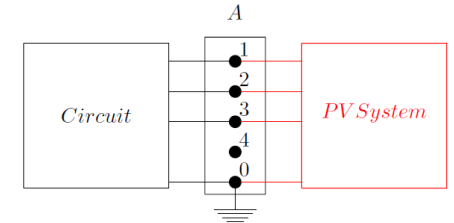
New Tshape.Temp npts=24 interval=1

~ temp=[25 25 25 25 25 25 25 25 35 40 45 50 60 60 55 40 35 30 25 25 25 25 25]

New line.switch bus1=A bus2=B switch=Yes

New PVSystem.PV phases=3 bus1=B kV=13.8 Pmpp=1680 %pmpp=71.428 kVA=1200 pf=0.95

~ conn=wye effcurve=Eff P-TCurve=FatorPvsT irradiance=1 daily=Irrad Tdaily=Temp wattpriority=Yes

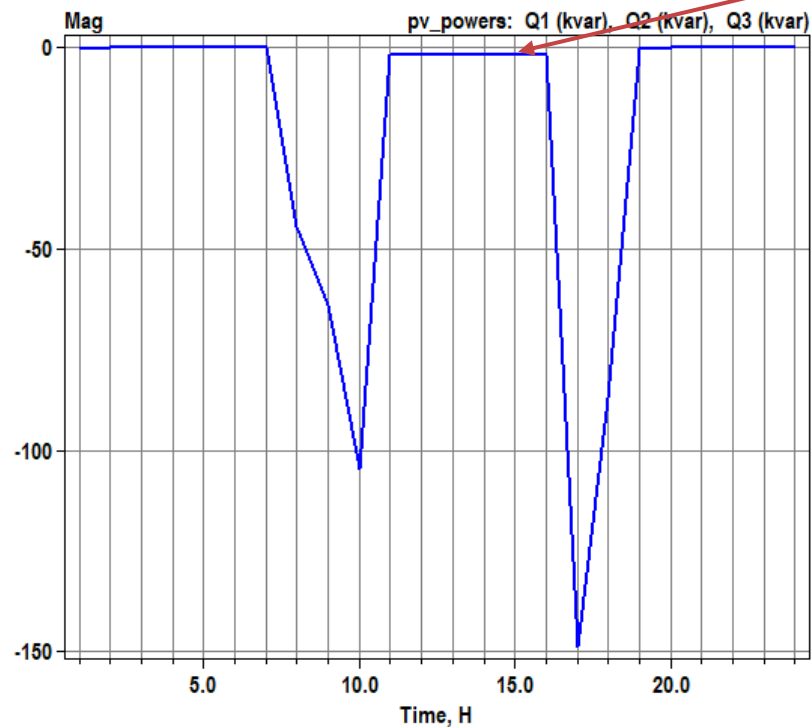
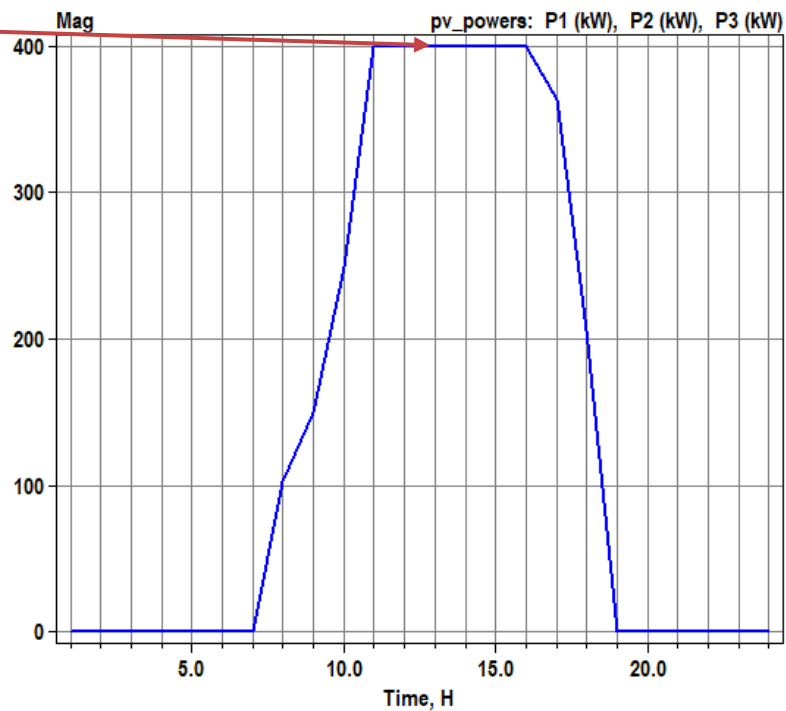


Example 1: dc-ac-1_4--kw-kva-1-Ppriority.dss

```
New PVSystem.PV phases=3 bus1=B kV=13.8 Pmpp=1680 %Pmpp=71.428 kVA=1200
```

```
~ conn=weff effcurve=Eff P-TCurve=FatorPvsT irradiance=1 daily=Irrad Tdaily=Temp wattpriority=Yes
```

kW maximum
1200kW



P priority
kVA-to-kW = 1.0

- DC-to-AC = 1.4
- kVA-to-kW = 1.0
- Inverter: P priority
- Inverter: Volt-Var

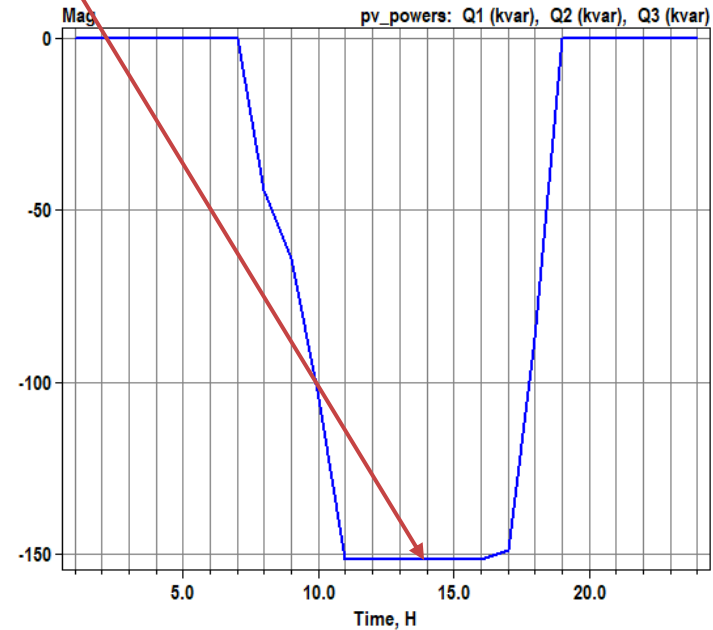
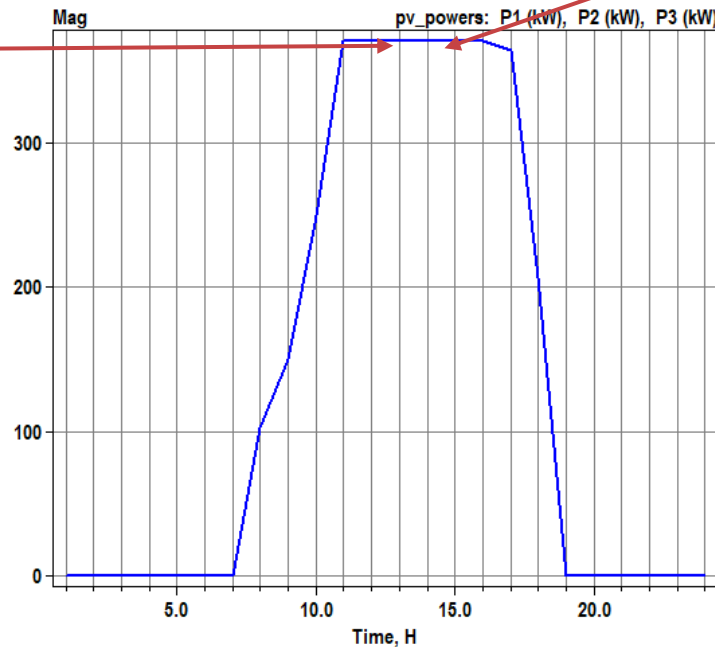
- $kVA=1200$
- $P_{mpp} = kVA / kVA\text{-to-kW} * DC\text{-to-AC} = 1680$
- $\%P_{mpp} = kVA / kVA\text{-to-kW} / P_{mpp} * 100 = 71.428$

Example 2: dc-ac-1_4--kw-kva-1-Qpriority.dss

```
New PVSystem.PV phases=3 bus1=B kV=13.8 Pmpp=1680 %Pmpp=71.428 kVA=1200  
~ conn=weffcurve=Eff P-TCurve=FatorPvsT irradiance=1 daily=Irrad Tdaily=Temp wattpriority=no
```

kVA maximum 1200kVA
kW not max

Q priority



- DC-to-AC = 1.4
- kVA-to-kW = 1.0
- Inverter: Q priority
- Inverter: Volt-Var

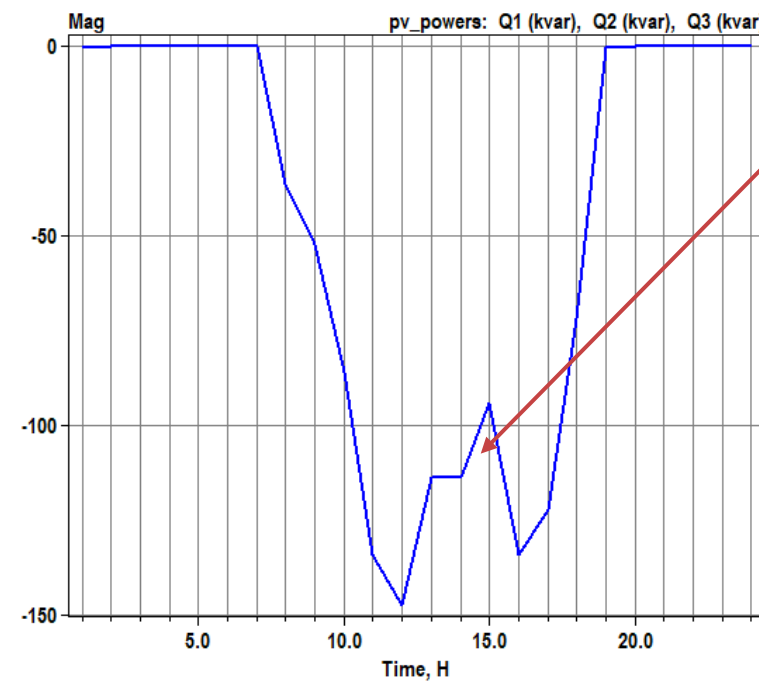
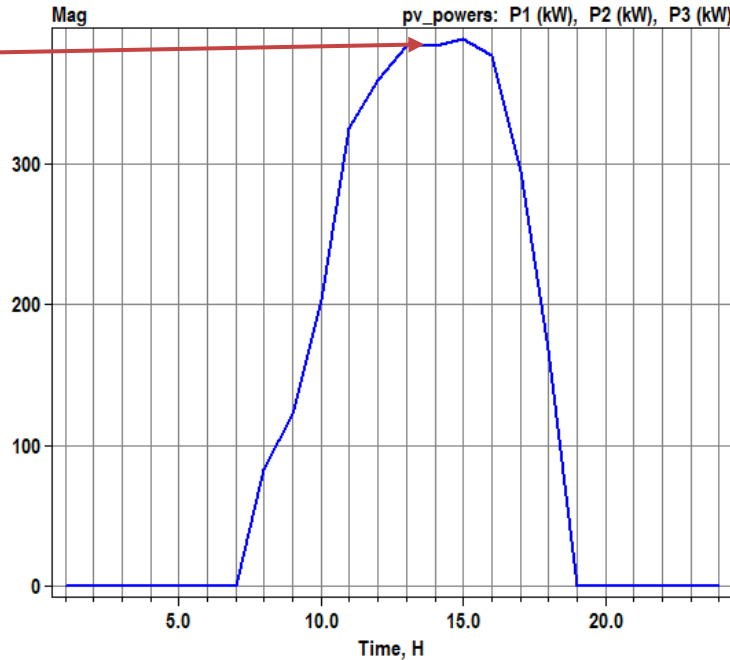
- $kVA=1200$
- $P_{mpp} = kVA / kVA\text{-to-kW} * DC\text{-to-AC} = 1680$
- $\%P_{mpp} = kVA / kVA\text{-to-kW} / P_{mpp} * 100 = 71.428$

Example 3 - dc-ac-1_15--kw-kva-1-Ppriority.dss

```
New PVSystem.PV phases=3 bus1=B kV=13.8 Pmpp=1380 %Pmpp=86.956 kVA=1200
```

```
~ conn=weye effcurve=Eff P-TCurve=FatorPvsT irradiance=1 daily=Irrad Tdaily=Temp wattpriority=Yes
```

Not limited
kW < 1200



P priority

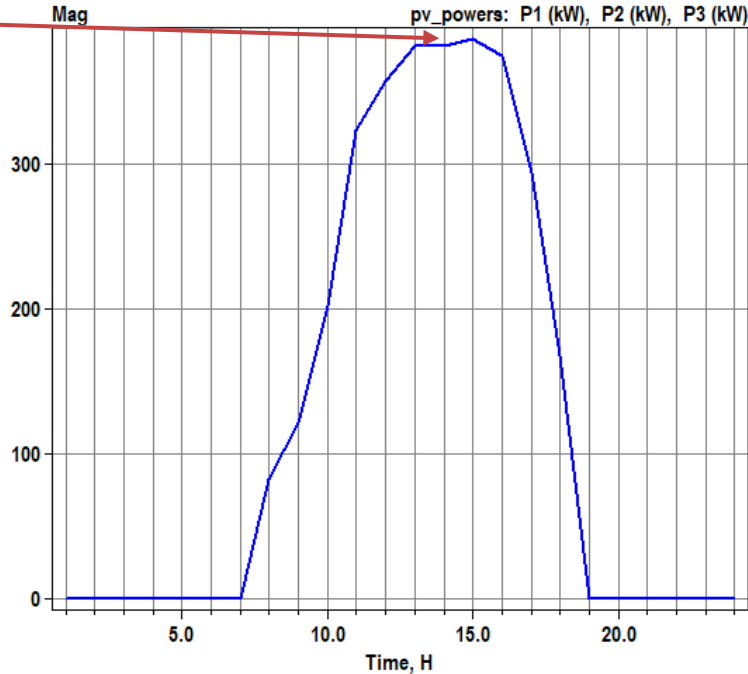
- DC-to-AC = 1.15
- kVA-to-kW = 1.0
- Inverter: P priority
- Inverter: Volt-Var

- $kVA=1200$
- $P_{mpp} = kVA / kVA\text{-to-kW} * DC\text{-to-AC} = 1380$
- $\%P_{mpp} = kVA / kVA\text{-to-kW} / P_{mpp} * 100 = 86.956$

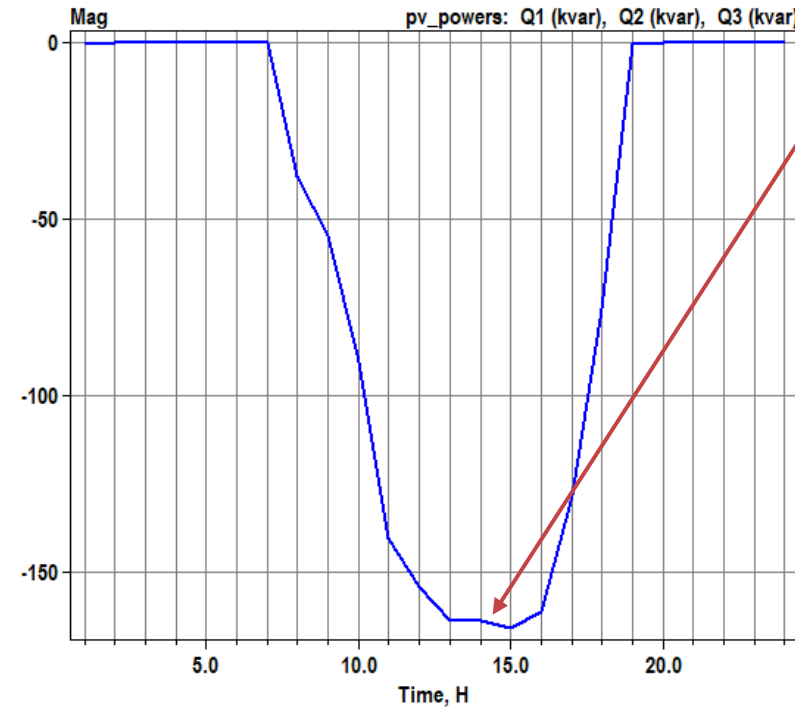
Example 4 - dc-ac-1_15--kw-kva-1_1.dss

```
New PVSystem.PV phases=3 bus1=B kV=13.8 Pmpp=1380 %Pmpp=86.956 kVA=1320  
~ conn=weffcurve=Eff P-TCurve=FatorPvsT irradiance=1 daily=Irrad Tdaily=Temp
```

Not limited



Not limited



- DC-to-AC = 1.15
- kVA-to-kW = 1.1
- Inverter: Volt-Var
- $kVA=1320$
- $P_{mpp} = kVA / kVA\text{-to-kW} * DC\text{-to-AC} = 1380$
- $\%P_{mpp} = kVA / kVA\text{-to-kW} / P_{mpp} * 100 = 86.956$

Using PVSystem when having kW measurements (System operating with unity power factor)

PVSystem modeling:

- $P_{mpp} = P_{AC-rated}$
- $\%P_{mpp} = 100$
- Irradiance=1
- Unitary PV system Curves
- kVA should be greater or equal to P_{mpp}
- $Irradiance[t] = kW_measurements[t] / P_{mpp}$

<https://www.epri.com/research/products/000000003002020102>

Example (kwMeasurements.dss)

Clear

New Circuit.TheveninEquivalent bus1=A pu=1.0 basekv=13.8

~ Z0=[10, 10] Z1=[10, 10]

New XYCurve.Eff npts=4 xarray=[.1 .2 .4 1.0] yarray=[1 1 1 1]

New XYCurve.FatorPvsT npts=4 xarray=[0 25 75 100] yarray=[1 1 1 1]

New Loadshape.Irrad npts=24 interval=1

~ mult=[0 0 0 0 0 0 .1 .2 .3 .5 .8 .85 0.93 0.93 .92 .9 .7 .4 .1 0 0 0 0 0]

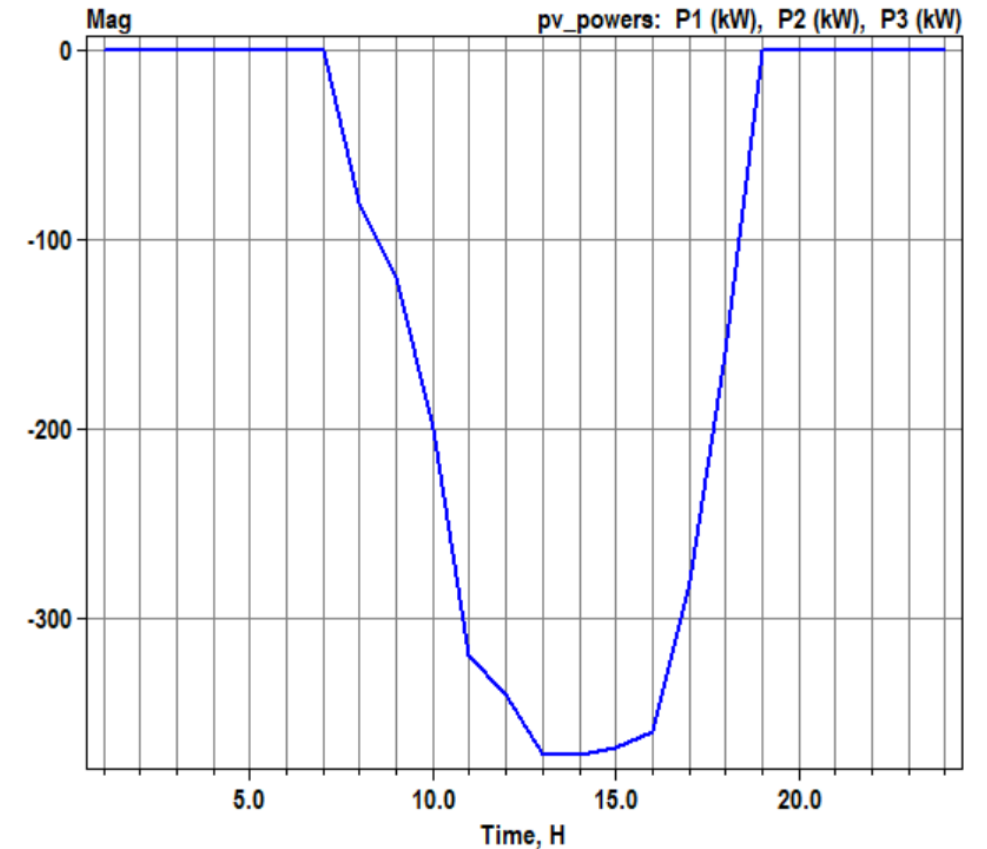
New Tshape.Temp npts=24 interval=1

~ temp=[25 25]

New PVSystem.PV phases=3 bus1=A kV=13.8 Pmpp=1200 %pmpp=100 kVA=1200

~ conn=wye effcurve=Eff P-TCurve=FatorPvsT irradiance=1 daily=Irrad Tdaily=Temp

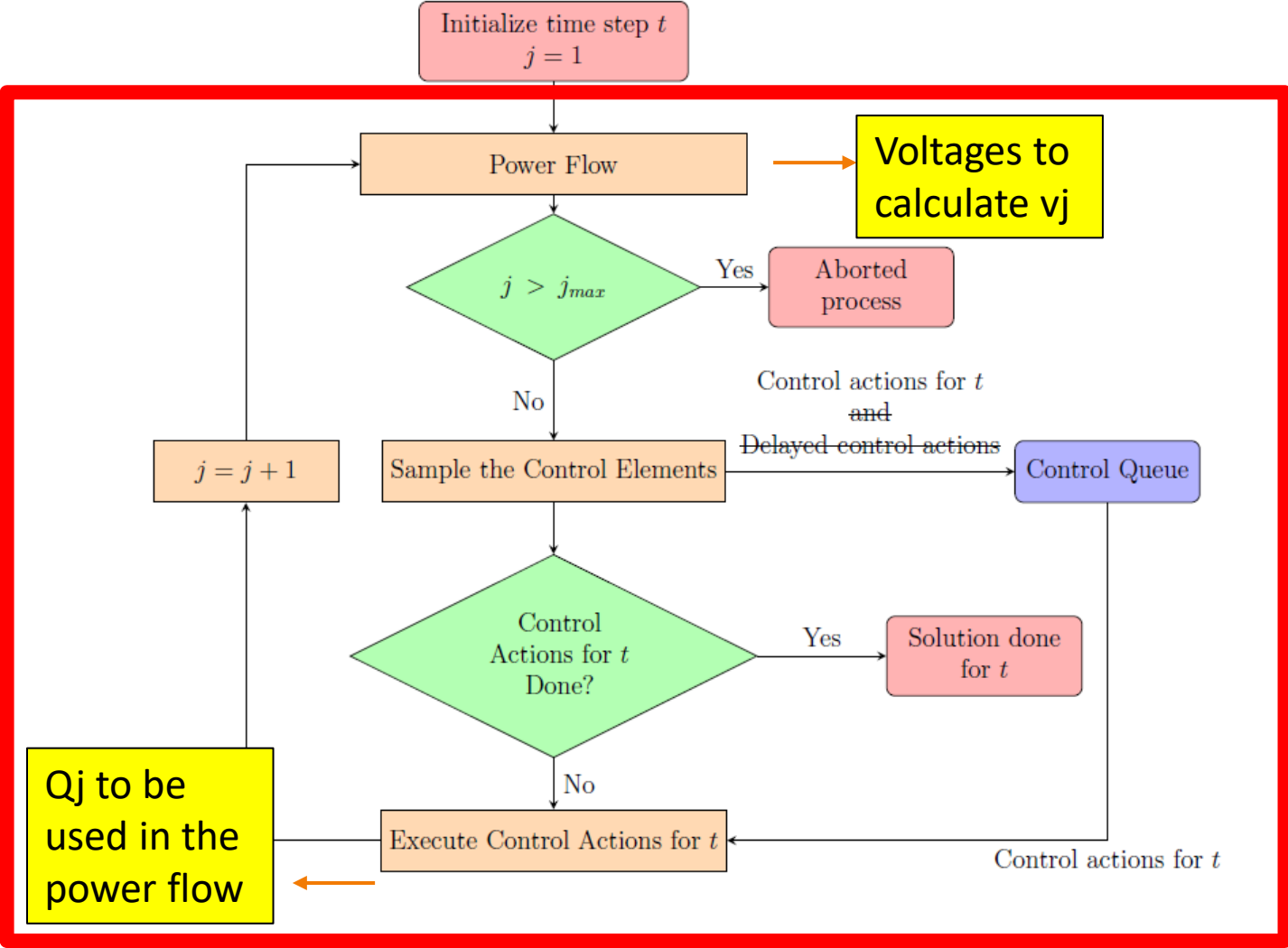
Pac[t] = kW measurements = irrad x Pmpp





InvControl – Convergence Method

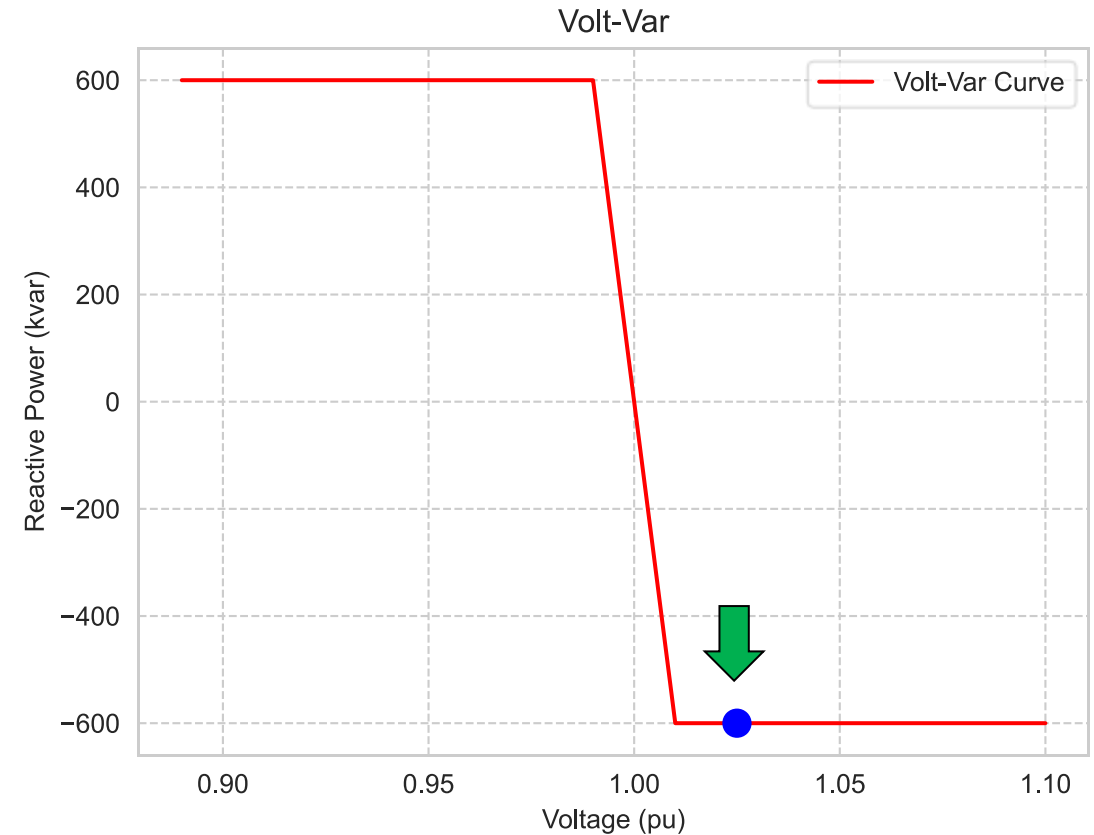
OpenDSS QSTS Simulation Process



The reason to have the convergence method




Control Iteration (i)	Voltage v_i	Desired Reactive power Q_i
1	1.025	-600
2	0.967	600
3	1.030	-600
4	0.967	600
5	1.030	-600

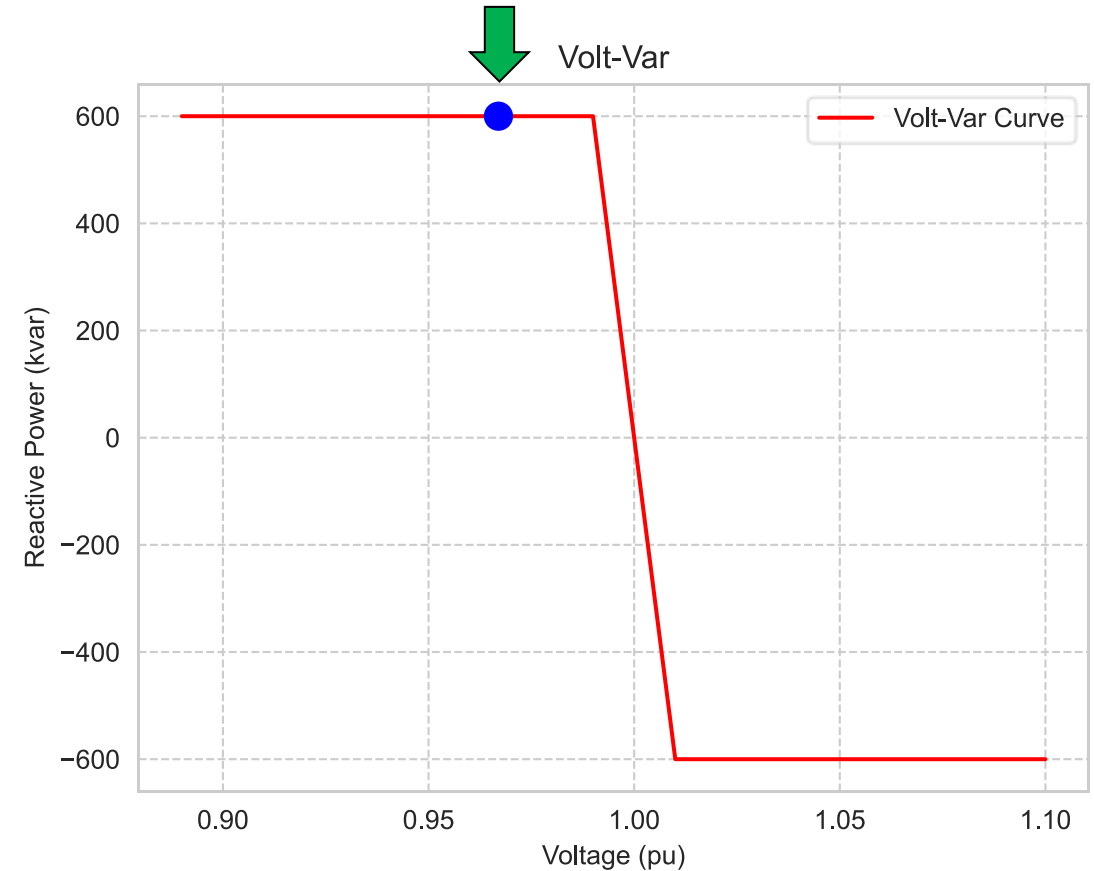


NoConvergence.dss


The reason to have the convergence method



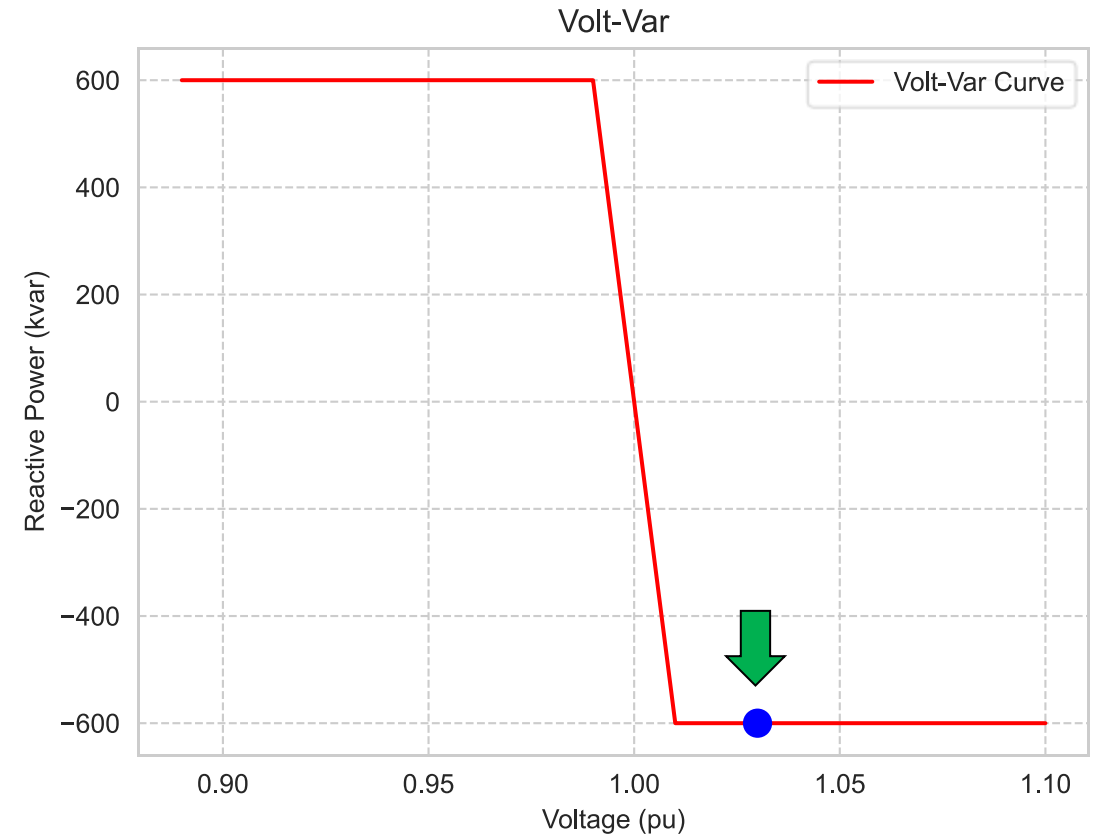
Control Iteration (i)	Voltage v_i	Desired Reactive power Q_i
1	1.025	-600
2	0.967	600
3	1.030	-600
4	0.967	600
5	1.030	-600




The reason to have the convergence method



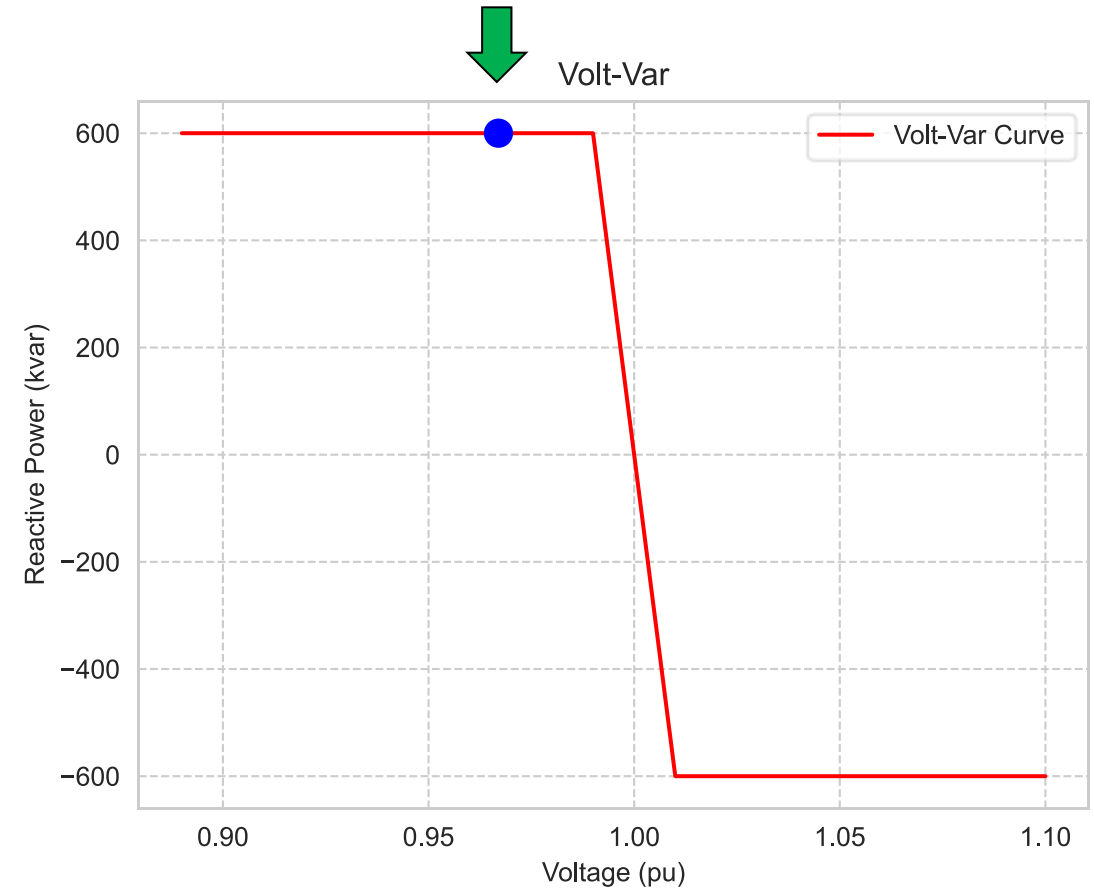
Control Iteration (i)	Voltage v_i	Desired Reactive power Q_i
1	1.025	-600
2	0.967	600
3	1.030	-600
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5	1.030	-600




The reason to have the convergence method



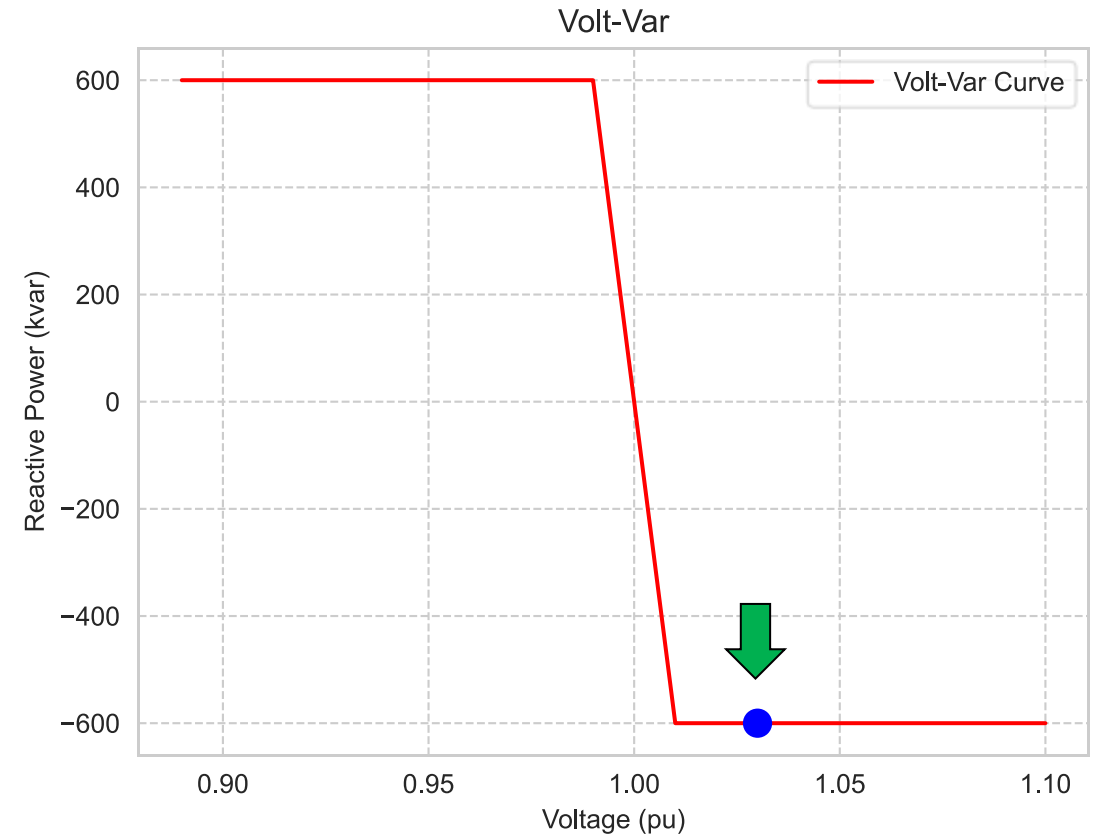
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
The reason to have the convergence method



Control Iteration (i)	Voltage v_i	Desired Reactive power Q_i
1	1.025	-600
2	0.967	600
3	1.030	-600
4	0.967	600
5	1.030	-600



How the convergence process works



Control Iteration (i)	Voltage v_i	Reactive power Q_i	Desired Reactive power
1	1.0253	-120.8	-600
2	1.019	-216.64	-600
3	1.014	-293.31	-600
4	1.0099	-353.47	-594
5	1.0059	-353.65	-354

◆ Desired Reactive Power

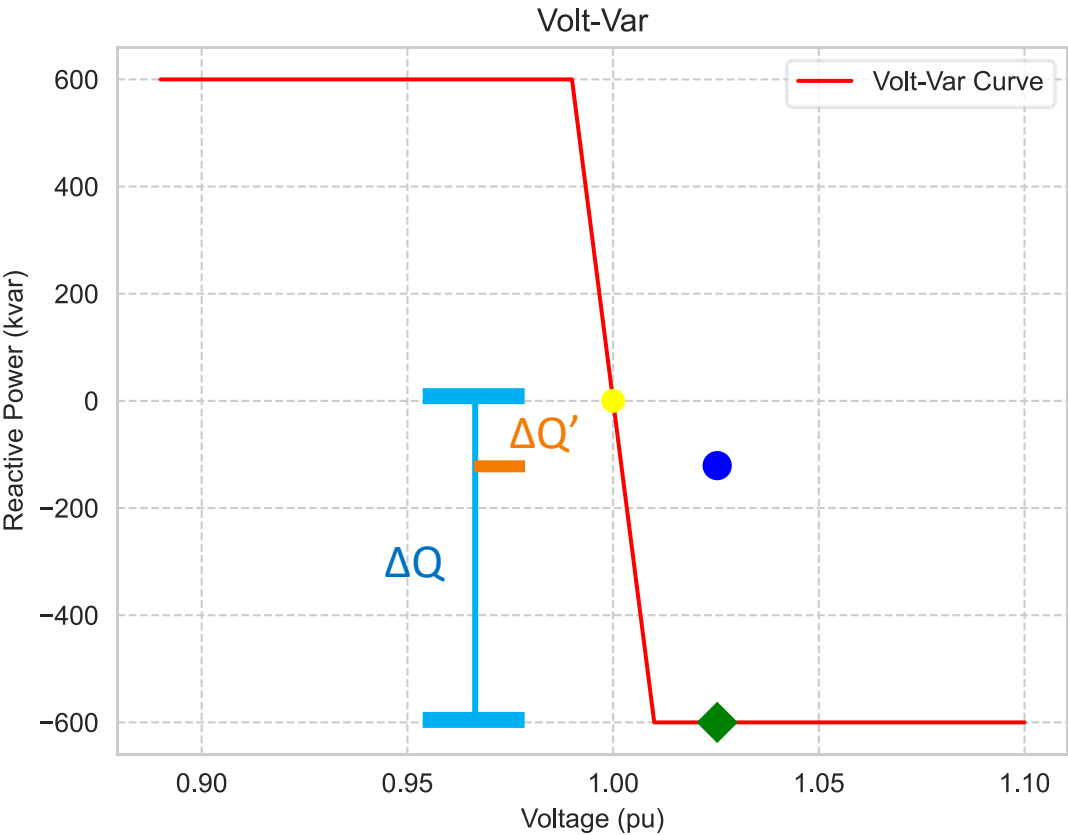
● Reactive Power Q_i

● Reactive Power Q_{i-1}

$\Delta Q = \text{Desired Reactive Power} - \text{Reactive Power } Q_{i-1}$


$\Delta Q' = \text{deltaq_factor} * \Delta Q$

deltaq_factor = 0.2






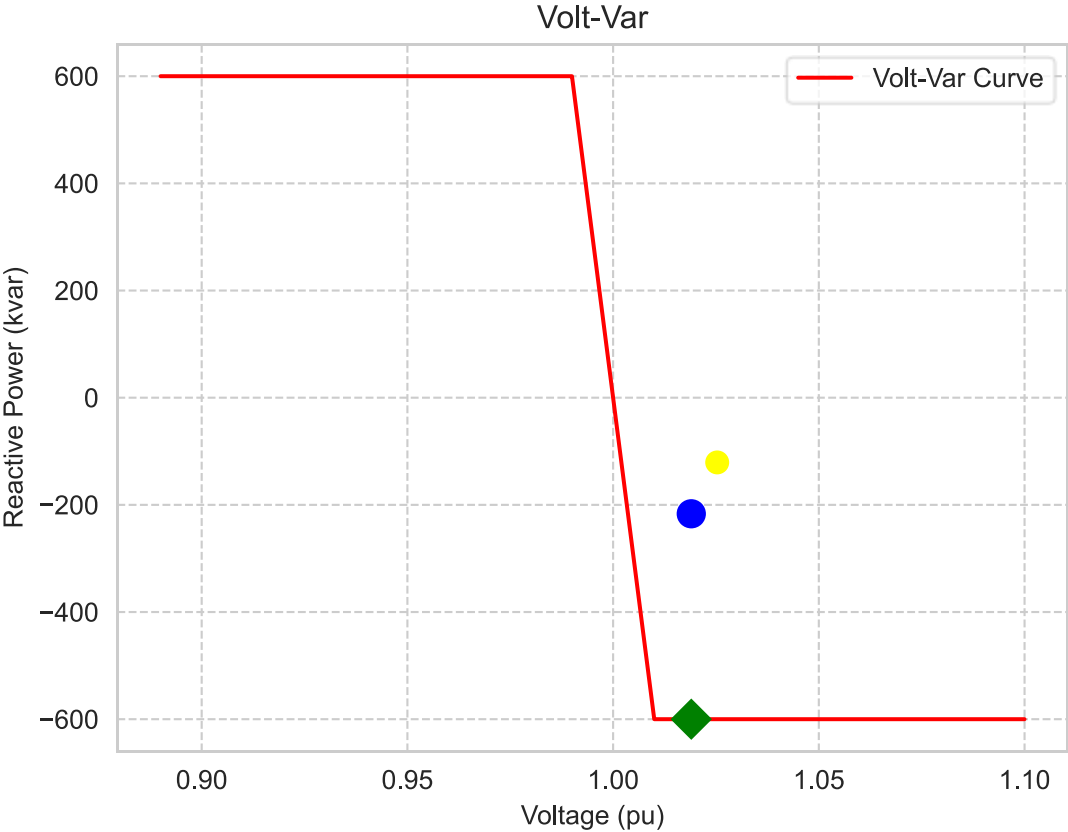
Convergence.dss

How the convergence process works



Control Iteration (i)	Voltage v_i	Reactive power Q_i	Desired Reactive power
1	1.0253	-120.8	-600
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3	1.014	-293.31	-600
4	1.0099	-353.47	-594
5	1.0059	-353.65	-354

-  Desired Reactive Power
-  Reactive Power Q_i
-  Reactive Power Q_{i-1}

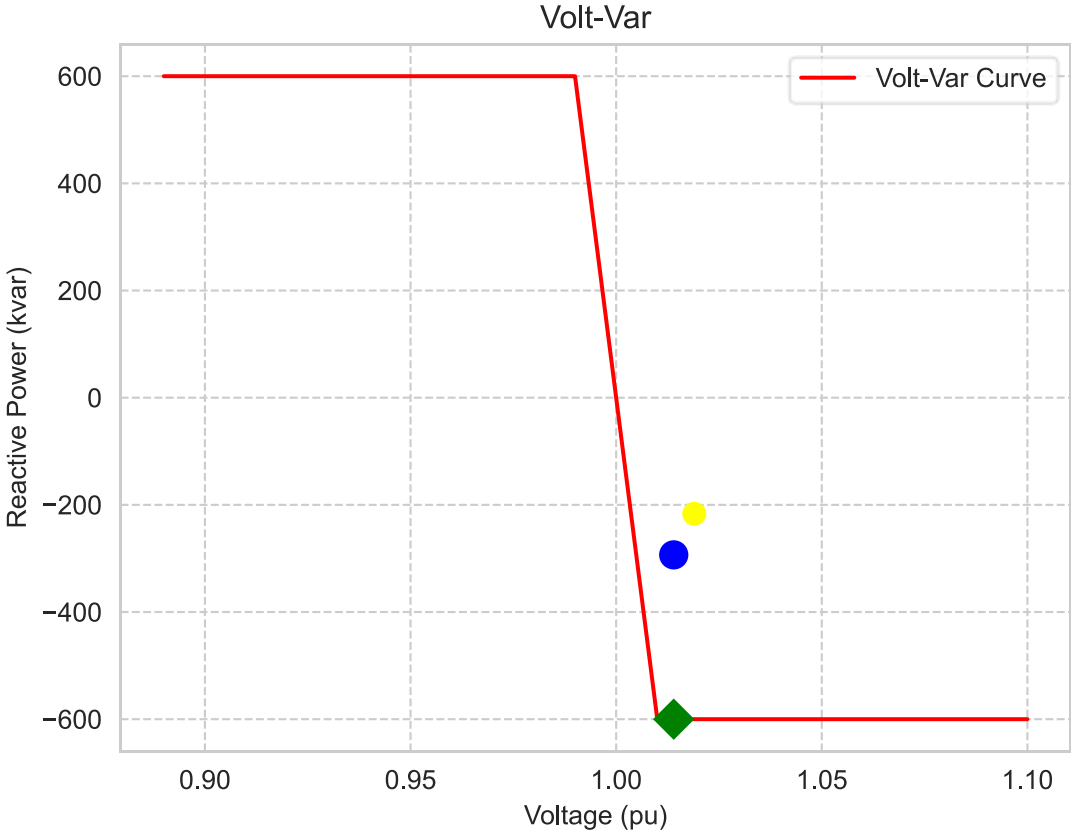


How the convergence process works

➡

Control Iteration (i)	Voltage v_i	Reactive power Q_i	Desired Reactive power
1	1.0253	-120.8	-600
2	1.019	-216.64	-600
3	1.014	-293.31	-600
4	1.0099	-353.47	-594
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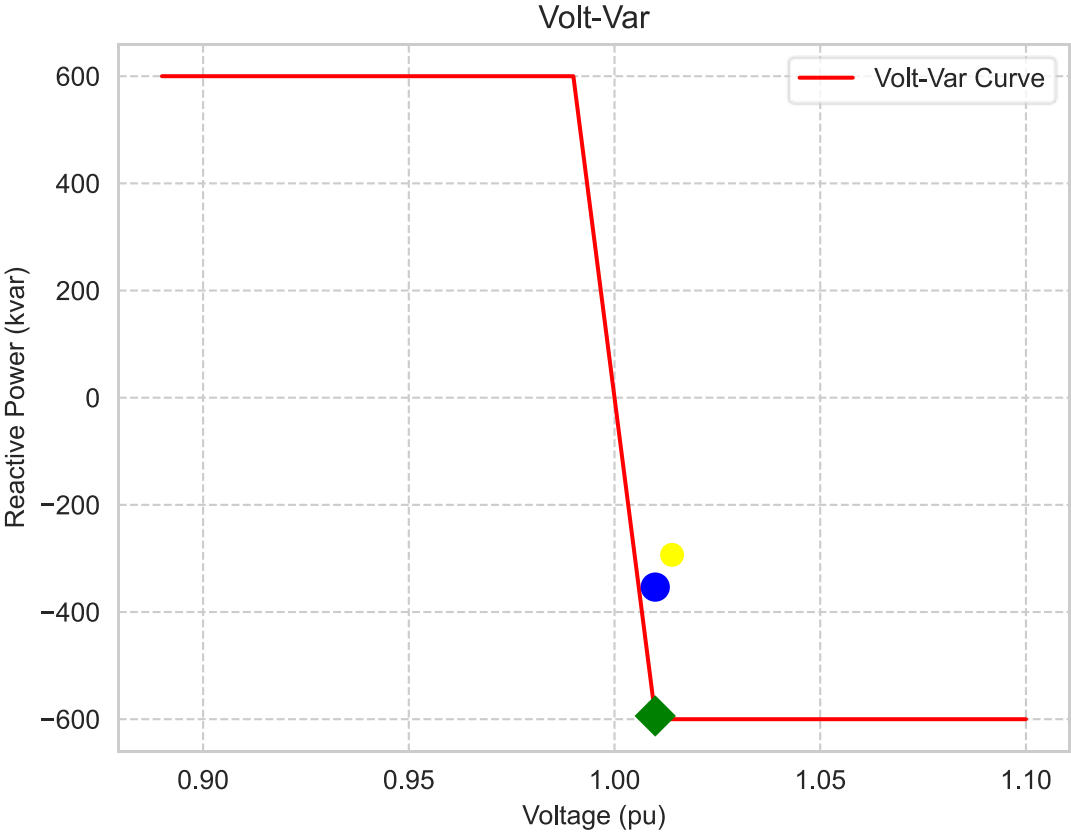
- ◆ Desired Reactive Power
- Reactive Power Q_i
- Reactive Power Q_{i-1}



How the convergence process works

Control Iteration (i)	Voltage v_i	Reactive power Q_i	Desired Reactive power
1	1.0253	-120.8	-600
2	1.019	-216.64	-600
3	1.014	-293.31	-600
4	1.0099	-353.47	-594
5	1.0059	-353.65	-354

- ◆ Desired Reactive Power
- Reactive Power Q_i
- Reactive Power Q_{i-1}



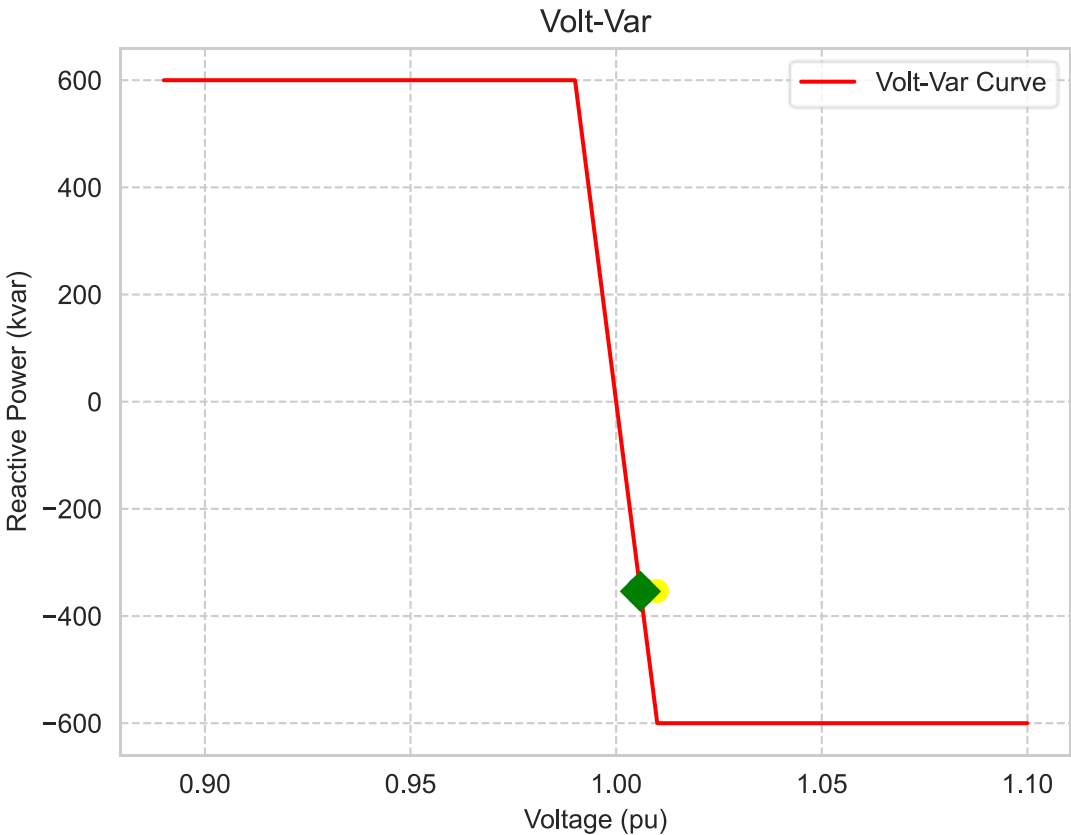
How the convergence process works

Control Iteration (i)	Voltage v_i	Reactive power Q_i	Desired Reactive power
1	1.0253	-120.8	-600
2	1.019	-216.64	-600
3	1.014	-293.31	-600
4	1.0099	-353.47	-594
5	1.0059	-353.65	-354

- ◆ Desired Reactive Power
- Reactive Power Q_i
- Reactive Power Q_{i-1}

It converges when:

- $|v_i - v_{i-1}| < VoltageChangeTolerance$
- $|Q_i - \text{Desired } Q_i| < VarChangeTolerance$



<https://publicdownload.epri.com/PublicAttachmentDownload.svc/AttachmentId=74500>

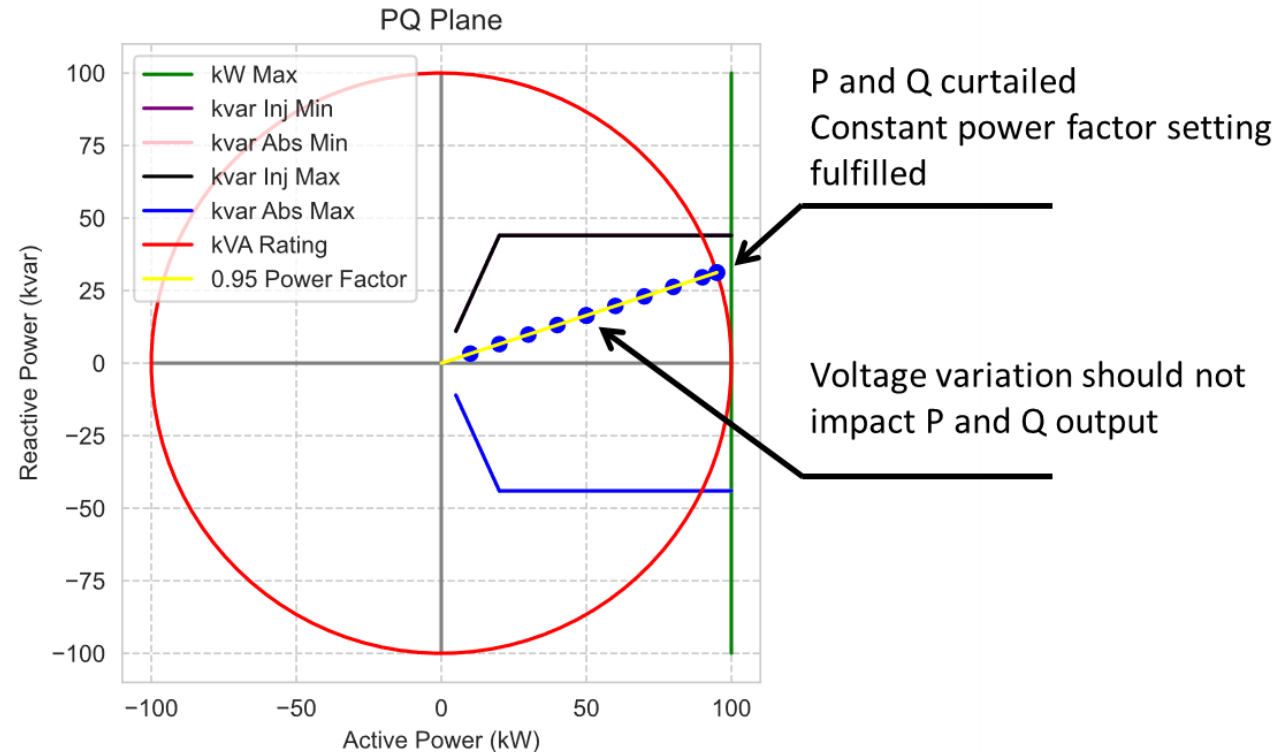


A Few Examples of Smart Inverter Functions According IEEE Std 1547-2018

Example # 1 Constant Power Factor

```
New PVSystem.PV phases=3 bus1=A Pmpp=100 kV=13.8 kVA=100 %Pmpp=100 pf=0.95 irradiance=P_pu  
~ kvarMax=44 kvarMaxAbs=44 pfpriority=Yes
```

P_pu = [0.1, 0.2, 0.3, 0.4, 0.5, 0.6, 0.7, 0.8, 0.9, 1.0]

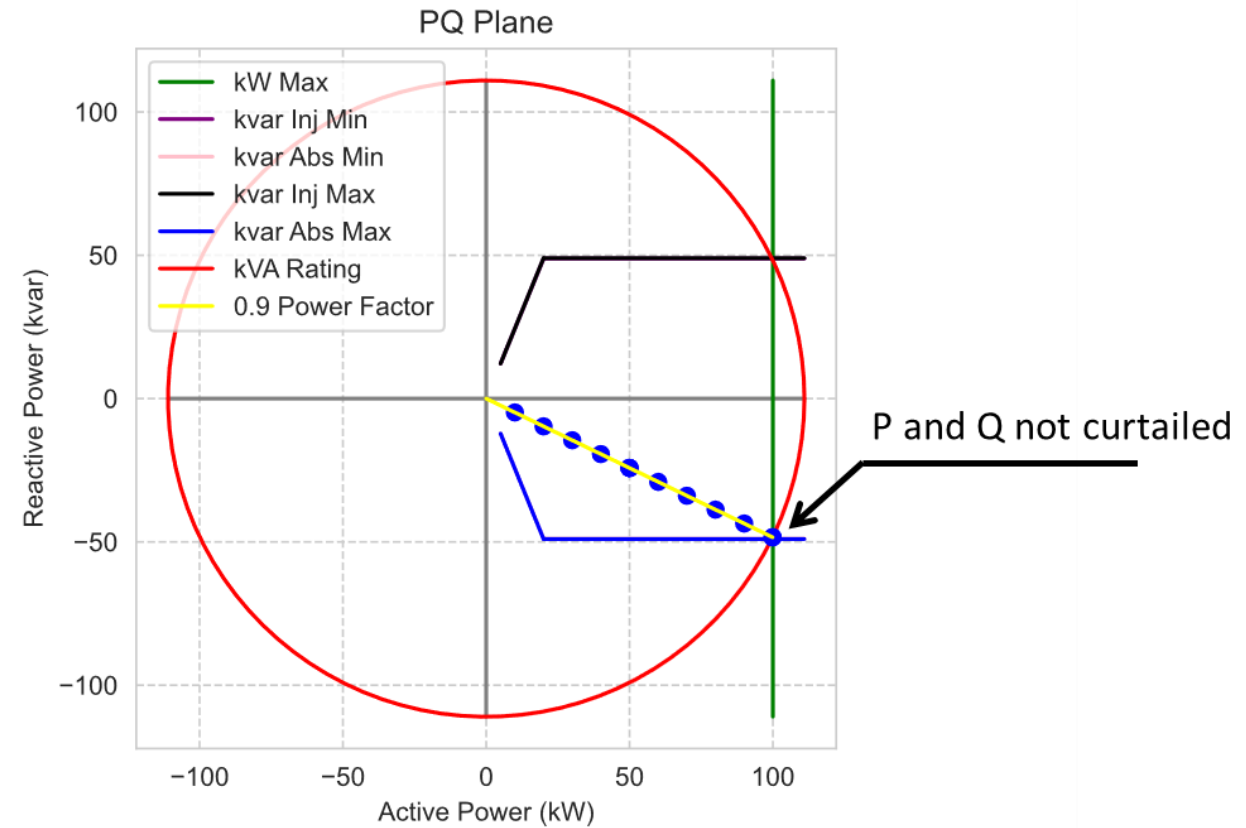


Example1.py

Example # 2 Constant Power Factor

New PVSystem.PV phases=3 bus1=A Pmpp=100 kV=13.8 kVA=112 %Pmpp=100 pf=-0.9 irradiance=P_pu
~ kvarMax=44 kvarMaxAbs=44 pfpriority=Yes

P_pu = [0.1, 0.2, 0.3, 0.4, 0.5, 0.6, 0.7, 0.8, 0.9, 1.0]

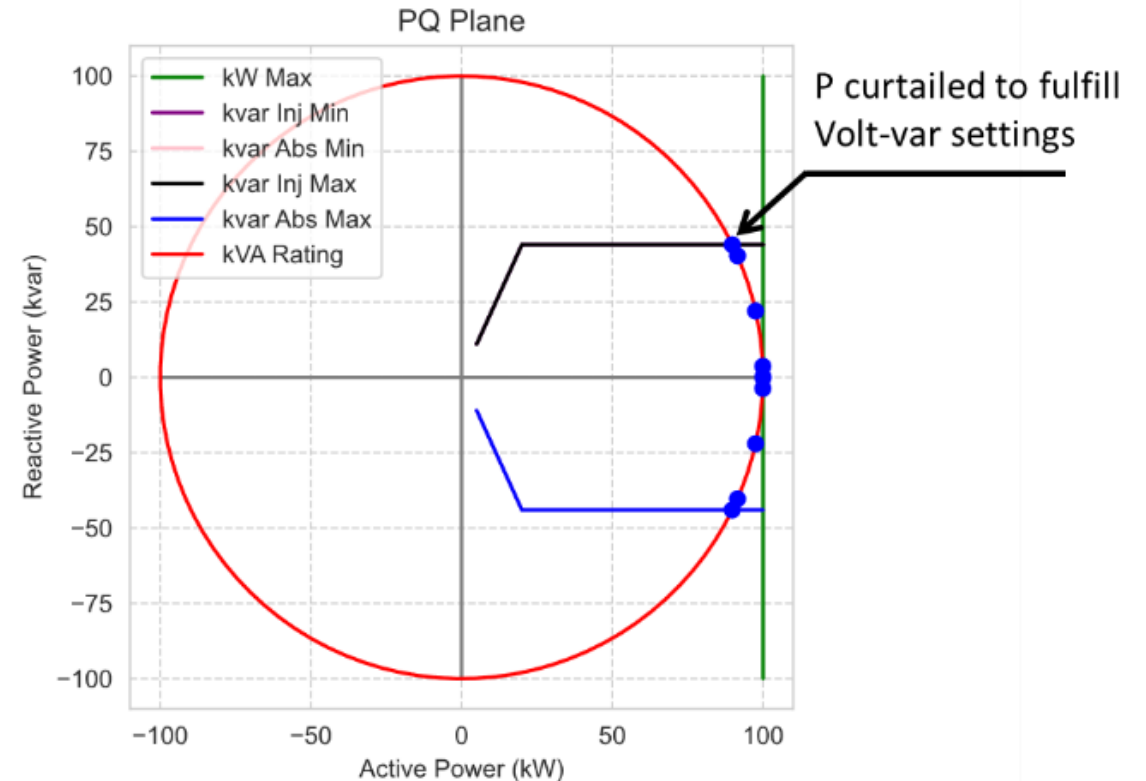
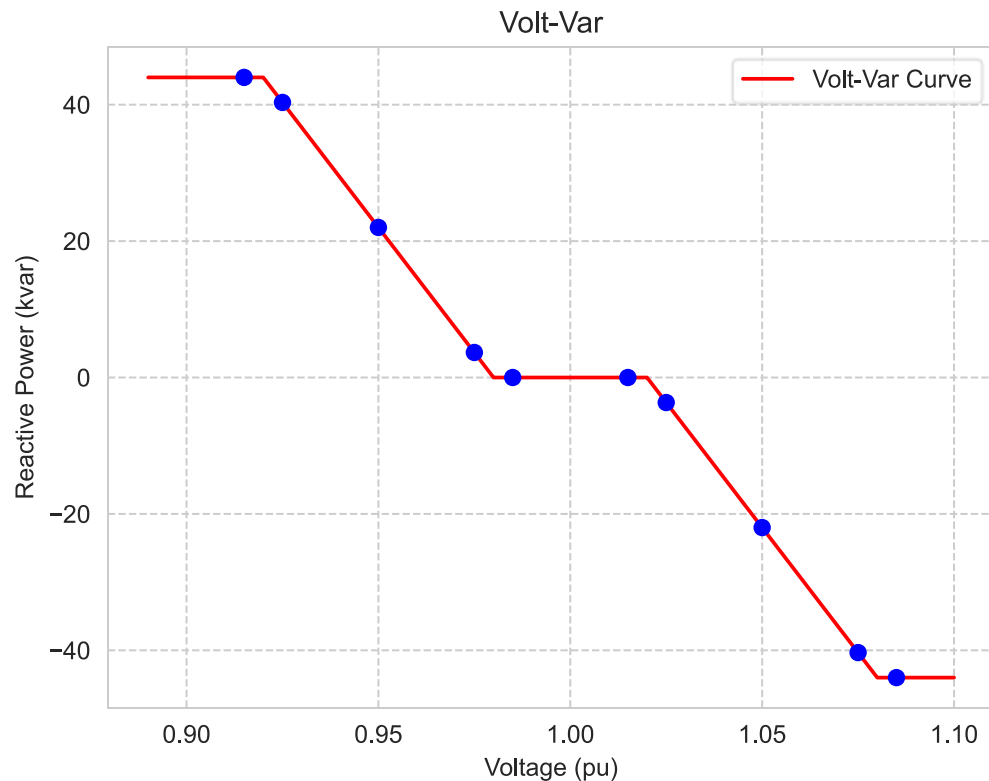


Example2.py

Example # 3 Volt-Var (Example3.py)

```
New PVSystem.PV phases=3 bus1=A Pmpp=100 kV=13.8 kVA=100 %Pmpp=100 irradiance=1 kvarMax=44 kvarMaxAbs=44 wattpriority=No
New XYcurve.generic npts=5 yarray=[1 1 0 -1 -1] xarray=[0.5 0.92 1.0 1.08 1.5]
New InvControl.VoltVar mode=VOLTVAR voltage_curvex_ref=rated vvc_curve1=generic RefReactivePower=VARMAX
```

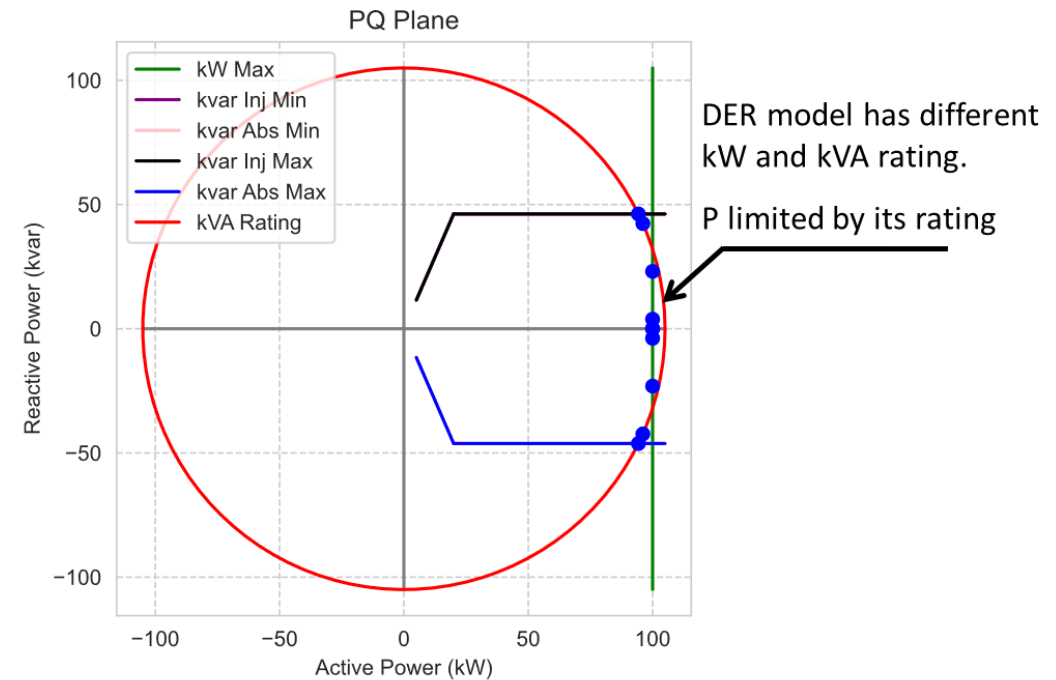
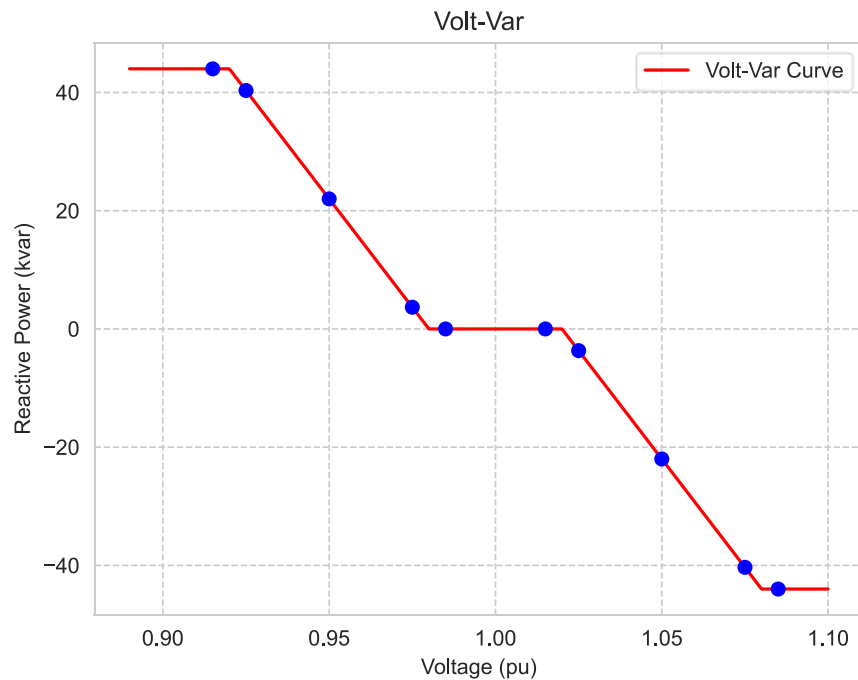
$v_{pu} = [0.915, 0.925, 0.95, 0.975, 0.985, 1.015, 1.025, 1.05, 1.075, 1.085]$



Example # 4 Volt-Var (Example4.py)

```
New PVSystem.PV phases=3 bus1=A Pmpp=100 kV=13.8 kVA=105 %Pmpp=100 irradiance=1 kvarMax=44 kvarMaxAbs=44 wattpriority=No
New XYcurve.generic npts=5 yarray=[1 1 0 -1 -1] xarray=[0.5 0.92 1.0 1.08 1.5]
New InvControl.VoltVar mode=VOLTVAR voltage_curvex_ref=rated vvc_curve1=generic RefReactivePower=VARMAX
```

$v_pu = [0.915, 0.925, 0.95, 0.975, 0.985, 1.015, 1.025, 1.05, 1.075, 1.085]$

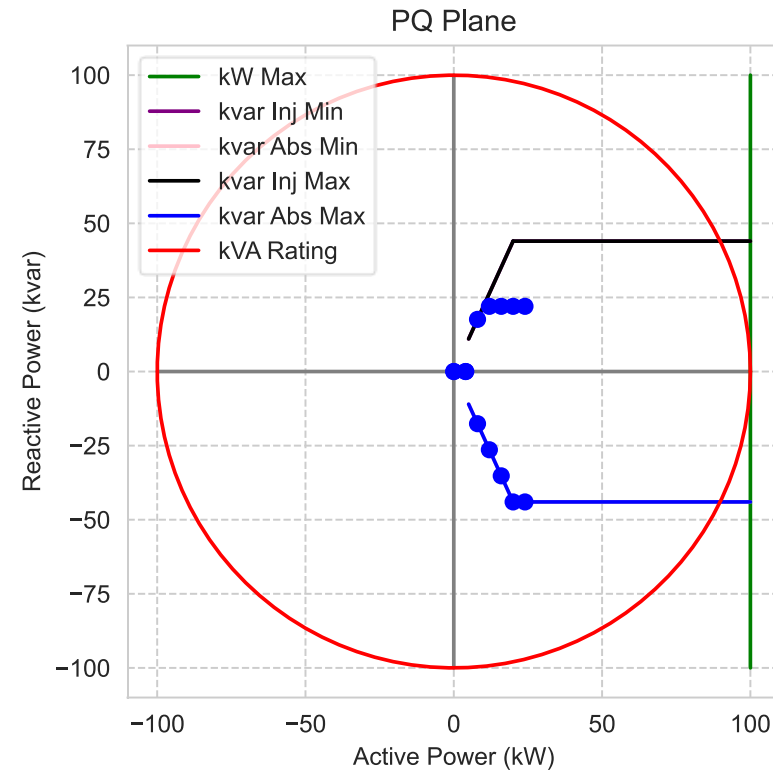
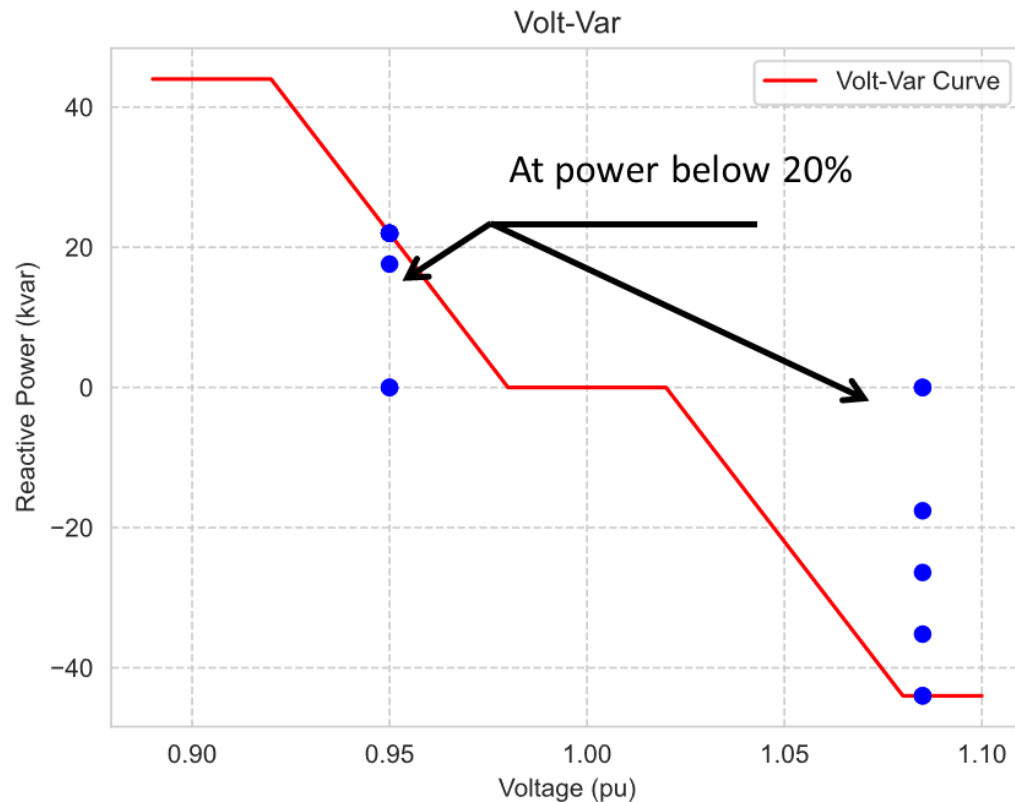


Example # 5 Volt-Var (Example5.py)

```
New PVSystem.PV phases=3 bus1=A Pmpp=100 kV=13.8 kVA=100 %Pmpp=100 irradiance=1 kvarMax=44 kvarMaxAbs=44 wattpriority=No  
~ %PminNoVars=5 %PminkvarMax=20
```

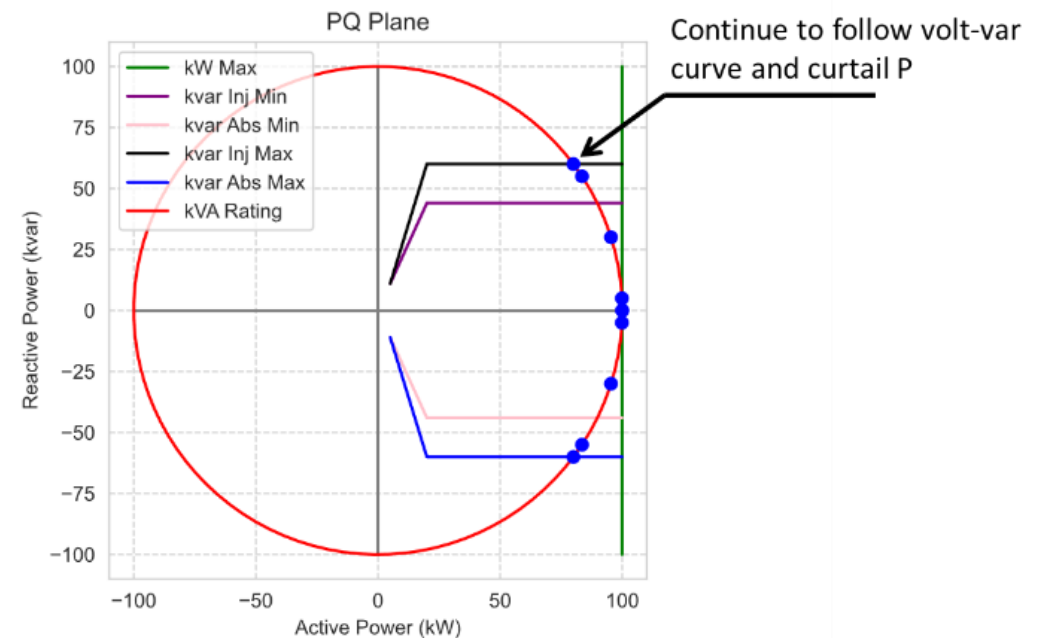
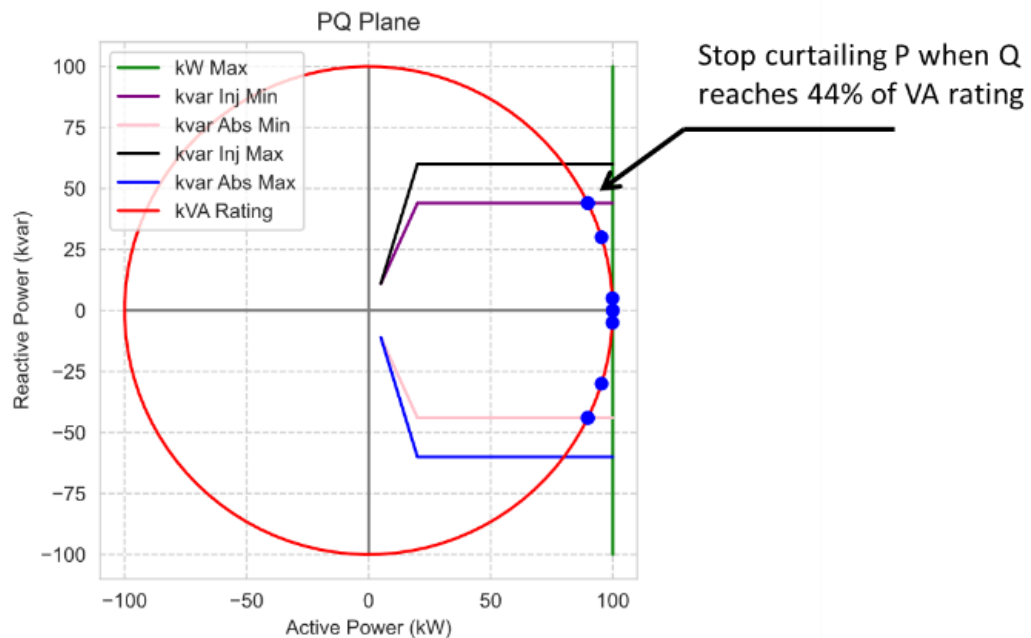
```
New XYcurve.generic npts=5 yarray=[1 1 0 -1 -1] xarray=[0.5 0.92 1.0 1.08 1.5]
```

```
New InvControl.VoltVar mode=VOLTVAR voltage_curvex_ref=rated vvc_curve1=generic RefReactivePower=VARMAX
```



Model Limitations

- OpenDSS can't use positive sequence component voltage value for the applicable voltage as required in IEEE Std 1547-2018 Clause 4.6.3.
- OpenDSS can't model inverters with capabilities greater than reactive power minimum requirements specified in IEEE Std 1547-2018.



A blue-tinted photograph of four people, two men and two women, standing in a row. They are all wearing white lab coats with the EPRI logo on the left chest. The man on the far left has curly hair and glasses. The man next to him has short dark hair and glasses. The woman next to him is wearing a white hard hat and has short dark hair. The man on the far right has short brown hair, a beard, and glasses. They are all smiling and looking towards the camera. The background is a solid blue color.

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