Distance relays, function 21, use voltage and current measurements to estimate distance to the fault. OpenDSS incorporates a simplified version of this function that was developed to compare the general performance of distance-based schemes to other candidates, on distribution systems with a high penetration of solar photovoltaic generation<sup>1</sup>. It lacks important features for protection system design, and should not be used for that purpose.

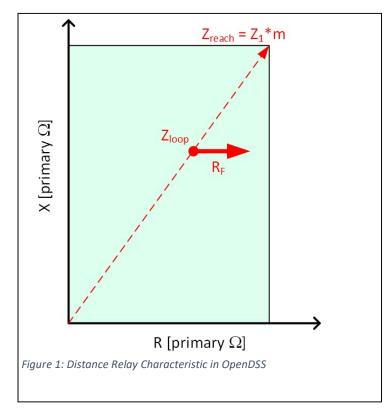


Figure 1 shows the rectangular tripping region of the OpenDSS distance relay on the RX diagram. The shape is not adjustable, and the implementation does not account for polarization or loading effects. Especially for ground faults, the fault resistance,  $R_F$ , may become high enough to shift the apparent impedance outside of the tripping region.

The basic input parameters are the "line" sequence impedances,  $Z_1$  and  $Z_0$ , with a reach multiplier, m. From phasor measurements  $V_{\phi}$  and  $I_{\phi}$ , the relay constructions loop impedances,  $Z_{loop}$  [1]:

$$k_{0} = (Z_{0} - Z_{1})/3Z_{1}$$

$$I_{R} = I_{A} + I_{B} + I_{C}$$

$$Z_{Loop-AG} = V_{A}/(I_{A} + k_{0}I_{R})$$

$$Z_{Loop-AB} = (V_{A} - V_{B})/(I_{A} - I_{B})$$

There are usually six loop impedances, three for the ground loops and three for the phase-to-phase loops. See [1] for more background, including effects not implemented here.

The distance relay function works with other relay parameters, including reclose. The new ones are:

- Type should be input as "distance"
- **Z1MAG** and **Z1ANG**, the positive-sequence <u>primary</u> impedance in ohms and degrees.
- **ZOMAG** and **ZOANG**, the zero-sequence <u>primary</u> impedance in ohms and degrees. The effect of this impedance is incorporated into  $k_0$ .
- **Mphase** is the reach in per-unit of Z1MAG ∠ Z1ANG, used in Figure 1 for the three phase-to-phase loops.
- **Mground** is the reach in per-unit of Z1MAG  $\angle$  Z1ANG, used in Figure 1 for the three phase-to-ground loops. By using  $k_0$ , the ground reach can be expressed on the same base as phase reach.

A test case is shown in Figure 2, where the line impedances per mile come from example 4.1 of [2]. The input file is *DistanceRelayTest.dss* on SourceForge [3]. The line impedances per mile define  $Z_1$  and  $Z_0$ , so

<sup>&</sup>lt;sup>1</sup> This material is based upon work supported by the U.S. Department of Energy's Office of Energy Efficiency and Renewable Energy (EERE) under Solar Energy Technologies Office (SETO) Agreement Number 34233.

that *Mphase* and *Mground* become the desired reach in miles of line, rather than per-unit of the total impedance. The test case simulates 7 faults in a span of 1.2 seconds, run at time step of 0.01 seconds. Figure 3 shows the total source current,  $I_{plotted}$  in Figure 2, through the sequence of fault initiation, fault clearing and reclosing. The event log is provided in Table 1.

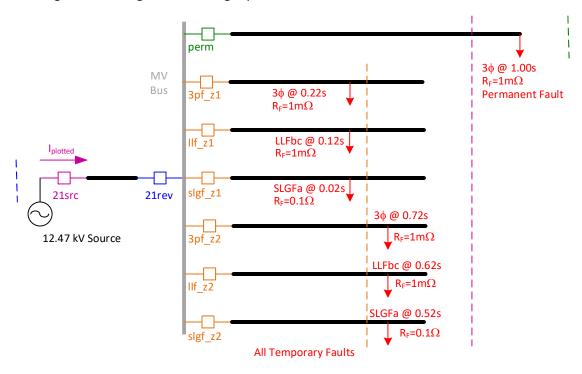


Figure 2: Test System for Distance Relays

## Some notes of interpretation:

- The six individual feeder relays in **orange** are set to reach 1.4 miles. They detect, clear and reclose the three temporary faults that are 1.2 miles away, but not the three temporary faults that are 1.6 miles away. These relays have a tripping delay of 0.02 seconds.
- The source relay in magenta reaches 2.5 miles, but has a longer delay of 0.03 seconds. This relay trips the three faults not detected by the feeder relays. As shown in Figure 3, that set of three faults has lower currents than the first set. The gap between the two sets of faults allows the source relay time to reset, otherwise, it could lock out during the second set of three faults. The reset time for the source relay is 0.2 seconds.
  - The source relay doesn't trip for any of the first three faults, because its delay is longer than any of the feeder relays.
  - The source relay doesn't trip for the permanent fault because it's out of reach.
- The seventh feeder relay in **green** reaches 3.5 miles. It's the only one to detect the permanent three-phase fault at the end of the line, and trips four times to lockout between 1.0 and 1.2 seconds.
- The receiving end line relay in **blue** reaches 3.0 miles (not shown to scale) in the reverse direction from the faults. It detects none of them. The delay is 0.01 seconds, so if the directional determination failed, or the *MonitoredTerminal* changes from 2 to 1, it would trip.

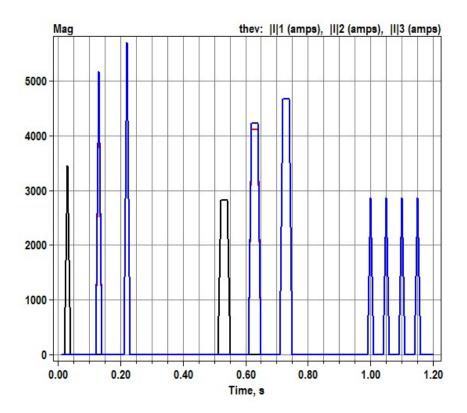


Figure 3: Source current magnitudes during test sequence

## Incremental Distance

A time-domain or incremental version of distance protection, sometimes referred to as TD21, was originally developed decades ago as an option for ultra-high-voltage (UHV) transmission lines. In one available implementation [4, 5], the incremental voltage and current signals are derived from one-cycle memory waveforms. Many settings are the same as for conventional function 21. Other than speed, the TD21 function may be helpful with inverter-based sources that don't generate much fault current. A time-domain model of this relay has been implemented to work with COMTRADE files, obtained from either transient simulation or field measurement. A fast-phasor version of TD21 [6] is available for OpenDSS [7]. It requires  $\Delta t$  no more than one cycle, and preferably 1 millisecond.

## References

- 1. Schweitzer and Kasztenny, "Distance protection: Why have we started with a circle, does it matter, and what else is out there?", 2018. <a href="https://doi.org/10.1109/CPRE.2018.8349791">https://doi.org/10.1109/CPRE.2018.8349791</a>
- 2. W. H. Kersting, Distribution System Modeling and Analysis, 3<sup>rd</sup> Ed., CRC Press, 2016.
- 3. [online] https://sourceforge.net/p/electricdss/code/HEAD/tree/trunk/Test/DistanceRelayTest.DSS
- 4. Schweitzer et. al., "Speed of Line Protection Can We Break Free of Phasor Limitations?", 2015. https://doi.org/10.1109/CPRE.2015.7102184
- Schweitzer et. al., "Performance of Time-Domain Line Protection Elements on Real-World Faults", 2016. <a href="https://doi.org/10.1109/CPRE.2016.7914904">https://doi.org/10.1109/CPRE.2016.7914904</a>
- 6. Dzienis et. al. "Analysis of High-Speed-Distance Protection", 2011. https://doi.org/10.1109/APAP.2011.6180585
- 7. [online] https://sourceforge.net/p/electricdss/code/HEAD/tree/trunk/Test/TD21RelayTest.DSS

## Table 1: Event Log for Distance Relay Test Case

```
Hour=0, Sec=0.03, ControlIter=1, Element=Fault.slqf z1, Action=**APPLIED**
Hour=0, Sec=0.04, ControlIter=1, Element=Relay.slqf z1, Action=OPENED ON 21 0.781 PU DIST G1
Hour=0, Sec=0.04, ControlIter=2, Element=Fault.slqf z1, Action=**CLEARED**
Hour=0, Sec=0.06, ControlIter=1, Element=Relay.slqf z1, Action=CLOSED
Hour=0, Sec=0.13, ControlIter=1, Element=Fault.llf z1, Action=**APPLIED**
Hour=0, Sec=0.14, ControlIter=1, Element=Relay.llf z1, Action=OPENED ON 21 0.735 PU DIST G2 G3 P23
Hour=0, Sec=0.14, ControlIter=2, Element=Fault.llf z1, Action=**CLEARED**
Hour=0, Sec=0.16, ControlIter=1, Element=Relay.llf z1, Action=CLOSED
Hour=0, Sec=0.22, ControlIter=1, Element=Fault.3pf z1, Action=**APPLIED**
Hour=0, Sec=0.23, ControlIter=1, Element=Relay.3pf z1, Action=OPENED ON 21 0.736 PU DIST G1 G2 G3 P12 P13 P23
Hour=0, Sec=0.23, ControlIter=2, Element=Fault.3pf z1, Action=**CLEARED**
Hour=0, Sec=0.25, ControlIter=1, Element=Relay.3pf z1, Action=CLOSED
Hour=0, Sec=0.26, ControlIter=1, Element=Relay.slgf z1, Action=RESET
Hour=0, Sec=0.36, ControlIter=1, Element=Relay.llf z1, Action=RESET
Hour=0, Sec=0.45, ControlIter=1, Element=Relay.3pf z1, Action=RESET
Hour=0, Sec=0.52, ControlIter=1, Element=Fault.slgf z2, Action=**APPLIED**
Hour=0, Sec=0.55, ControlIter=1, Element=Relay.21src, Action=OPENED ON 21 0.507 PU DIST G1
Hour=0, Sec=0.55, ControlIter=2, Element=Fault.slgf z2, Action=**CLEARED**
Hour=0, Sec=0.57, ControlIter=1, Element=Relay.21src, Action=CLOSED
Hour=0, Sec=0.62, ControlIter=1, Element=Fault.llf z2, Action=**APPLIED**
Hour=0, Sec=0.65, ControlIter=1, Element=Relay.21src, Action=OPENED ON 21 0.490 PU DIST G2 G3 P23
Hour=0, Sec=0.65, ControlIter=2, Element=Fault.llf z2, Action=**CLEARED**
Hour=0, Sec=0.67, ControlIter=1, Element=Relay.21src, Action=CLOSED
Hour=0, Sec=0.72, ControlIter=1, Element=Fault.3pf z2, Action=**APPLIED**
Hour=0, Sec=0.75, ControlIter=1, Element=Relay.21src, Action=OPENED ON 21 0.490 PU DIST G1 G2 G3 P12 P13 P23
Hour=0, Sec=0.75, ControlIter=2, Element=Fault.3pf z2, Action=**CLEARED**
Hour=0, Sec=0.77, ControlIter=1, Element=Relay.21src, Action=CLOSED
Hour=0, Sec=0.95, ControlIter=1, Element=Relay.21src, Action=RESET
                ControlIter=1, Element=Fault.perm, Action=**APPLIED**
Hour=0, Sec=1.01, ControlIter=1, Element=Relay.perm, Action=OPENED ON 21 0.735 PU DIST G1 G2 G3 P12 P13 P23
Hour=0, Sec=1.05, ControlIter=1, Element=Relay.perm, Action=CLOSED
Hour=0, Sec=1.06, ControlIter=1, Element=Relay.perm, Action=OPENED ON 21 0.735 PU DIST G1 G2 G3 P12 P13 P23
Hour=0, Sec=1.1, ControlIter=1, Element=Relay.perm, Action=CLOSED
Hour=0, Sec=1.11, ControlIter=1, Element=Relay.perm, Action=OPENED ON 21 0.735 PU DIST G1 G2 G3 P12 P13 P23
Hour=0, Sec=1.15, ControlIter=1, Element=Relay.perm, Action=CLOSED
Hour=0, Sec=1.16, ControlIter=1, Element=Relay.perm, Action=OPENED ON 21 0.735 PU DIST G1 G2 G3 P12 P13 P23 & LOCKED OUT
```