$$G(s) = \frac{1}{s^2 + b_1 s + mgL}$$

$$E(s) = gd - g = gd \left[1 - \frac{g}{gd}\right]$$

$$= gd \left[\frac{s^2 + \frac{b+kd}{5} + \frac{mgL+kp}{5} - \frac{kp}{5}}{s^2 + \frac{b+kd}{5} + \frac{mgL+kp}{5}}\right]$$

$$= gd \left[\frac{s^2 + \frac{b+kd}{5} + \frac{mgL}{5}}{s^2 + \frac{b+kd}{5} + \frac{mgL}{5}}\right]$$

$$e_{ss} = \lim_{s \to 0} s E(s) = \lim_{s \to 0} s \left[ \frac{s^2 + b + kd}{s^2 + b + kd} s + \frac{mgL}{s} \right] g^{d}(s)$$

For 
$$k+1=1$$
, ess =  $\frac{mgL}{mgL+kp}$  = finite constant
$$k=0 \implies \text{system is Type 0 with PD control}$$

For integral control, replace kp with kps+kx;

$$\frac{1}{50} \left( \frac{kps+k_E}{s} \right)$$

$$5^2 + \frac{b+kd}{t}s + \frac{mgL}{t} + \frac{1}{t} \left( \frac{kps+k_T}{s} \right)$$

$$\frac{g}{gq} = \frac{\frac{1}{J}(k_p s + k_r)}{s^3 + \frac{b + k_d}{J}s^2 + \frac{mgL + k_p}{J}s + \frac{k_r}{J}}$$

$$E(s) = \varnothing^{d}(s) \left[1 - \frac{s}{s^{3}}\right] = \frac{s\left[s^{2} + \frac{b + kds}{J} + \frac{mgL}{J}\right]}{s^{3} + \frac{b + kds}{J} + \frac{mgL}{J}} \varnothing^{d}(s)$$

(cont.)

By FVT, 
$$e_{ss} = \lim_{s \to 0} s E(s)$$

$$= \lim_{s \to 0} s \frac{s \left[s^2 + \frac{b+kd}{s} + \frac{wgL}{J}\right]}{s^3 + \frac{b+kd}{J}s^2 + \frac{kg}{J} + \frac{kg}{J}} \cdot p^d(s)$$
Let  $p^d(s) = \int_{sk+l}$ 

For k+1=2, ess = mat = finite constant

With PID control, system is type 1 with respect to reference inputs

PID: For a step, ess = 0

PID: For a ramp, ess = mgh

$$\tau = kpe - kds \phi = (kp + kds)e$$

$$\frac{E}{W} = \frac{-6}{1 + (k_{dS} + k_{p})G}$$

$$\frac{E}{W} = \frac{-1/f}{5^2 + \frac{b+kd}{J}s + \frac{mgL+kp}{J}}$$

For W= constant > W(s) = Wo )

$$e_{ss} = \lim_{s \to 0} s\left(\frac{E}{W}\right) \frac{w_0}{s}$$

$$\left[e_{ss} = -\frac{1}{mgL + kp}\right]$$

(cont.)

TANIAL.

W.10 (b) cont.

For PID control, 
$$\frac{E}{W} = \frac{-G}{1 + (kds + kp + \frac{kz}{s})G}$$

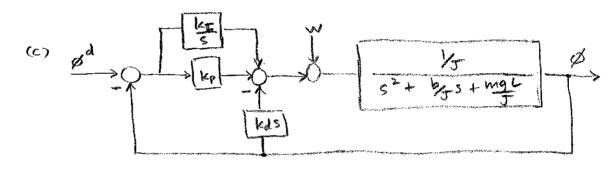
$$= \frac{-Gs}{s + (kds^2 + kps + kz)G}$$

$$= \frac{-\frac{1}{2}s}{s^3 + \frac{1}{2}s^2 + \frac{mgLs}{s} + (kds^2 + kps + kz) \cdot \frac{1}{s}}$$

$$= \frac{-\frac{1}{2}s}{s^3 + \frac{1}{2}s^2 + \frac{mgL + kps + kz}{s} + \frac{kz}{s}}$$

For a constant disturbance,

$$e_{ss} = \lim_{s \to 0} s E(s) = \lim_{s \to 0} s(\frac{E}{W}) \frac{V_0}{s}$$



From part (a), 
$$\frac{d}{dd} = \frac{\frac{1}{f}(kps+kr)}{\frac{1}{f}(kps+kr)}$$

CLCE: 
$$s^3 + \frac{b+kd}{J}s^2 + \frac{mgL+kp}{J} = 0$$

Evan's  $\left[ 1 + k \pm \frac{\sqrt{J}}{s \left[ s^2 + \frac{b+kd}{J}s + \frac{mgL+kp}{J} \right]} \right] = 0$ 

See Matlab results for root locus vs.  $k_{\rm I}$ .

System transient response is not degraded by fairly large values of  $k_{\rm I}$ .  $k_{\rm I}=30$  works well.

CACTOR

## 10/23/12 8:45 AM /Users/timmcl.../uuv\_rl\_vs\_ki.m 1 of 1

```
% simulation of UUV with lead control
J = 45;
m = 200;
g = 9.81;

L = 0.03;
b = 5;
kp = 95;
k\bar{d} = 112;
ki = 30;
tfinal = 40;
% H is the TF taken from Evan's form for ki
numH = 1/J;
denH = [1 (b+kd)/J (m*g*L+kp)/J 0];
H = tf(numH, denH);
figure(1);
rlocus(H); hold on;
rlocus(H,ki,'b^'); hold off;
title('UUV roll control, root locus vs. ki');
axis([-15 5 -10 10]);
nCL = [kp/J ki/J];
dCL = [1 (b+kd)/J (m*g*L+kp)/J ki/J];
sysCL = tf(nCL,dCL);
figure(2);
[yCL,t,xCL] = step(sysCL,tfinal);
plot(t,yCL); grid;
title('UUV Roll Response, PID Control');
xlabel('time (sec)');
ylabel('roll angle (rad)');
```

