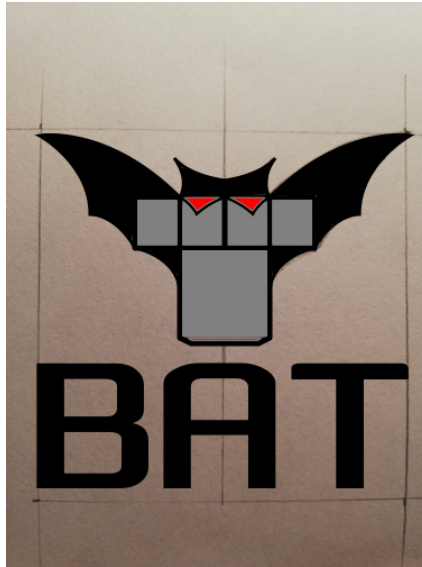


# BAT - Bolt Analysis Tool



## User Manual

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Issue: 0.1  
Date: January 9, 2021

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# Symbols and Abbreviations

## Symbols

$\alpha_A$	tightening factor
$\alpha_b$	coeff. of lin. thermal expansion of the bolt
$\alpha_c$	coeff. of lin. thermal expansion of the clamped part (plate)
$\delta_b$	elastic compliance of the bolt
$\delta_c$	elastic compliance of the clamped part (plate)
$\lambda$	under-head bearing angle of bolt
$\mu_{th}$	coeff. of friction in bolt thread
$\mu_{uh}$	coeff. of friction under bolt head
$\nu$	bolt utilization factor
$\varphi$	helix angle / slope of bolt thread
$\Phi$	load factor of concentric joint (also: force ratio or relative compliance factor)
$\Phi_n$	load factor for concentric clamping and concentric force load introduction via the clamped parts
$\rho$	friction angle in bolt thread
$\sigma_n$	normal stress in the bolt
$\sigma_v$	von-Mises stress in the bolt
$\tau$	shear stress in the bolt
$A_1$	nominal cross section of threaded bolt
$A_3$	minimal thread cross section
$A_p$	pitch cross section of threaded bolt
$A_s$	stress cross section of threaded bolt
$d$	nominal threaded bolt diameter
$d_2$	pitch diameter of threaded bolt
$d_3$	minimal diameter of threaded bolt
$d_h$	minimal contact diameter under bolt head
$d_s$	stress diameter of threaded bolt
$F_A$	external, axial bolt load
$F_M$	preload after tightening / assembly preload
$F_{PA}$	additional axial plate load
$F_Q$	external, shear bolt load

$F_{SA}$	additional axial bolt load
$F_V$	service preload incl. embedding and thermal influence
$f_Z$	plastic deformation due to embeddding
$F_Z$	preload loss due to embedding
$l_K$	joint clamped length
$M_p$	prevailing torque of bolt locking device
$n$	load introduction factor
$p$	pitch of bolt thread

### **Abbreviations**

BAT	Bolt Analysis Tool
TBJ	through-bolt joint
TTJ	tapped thread joint

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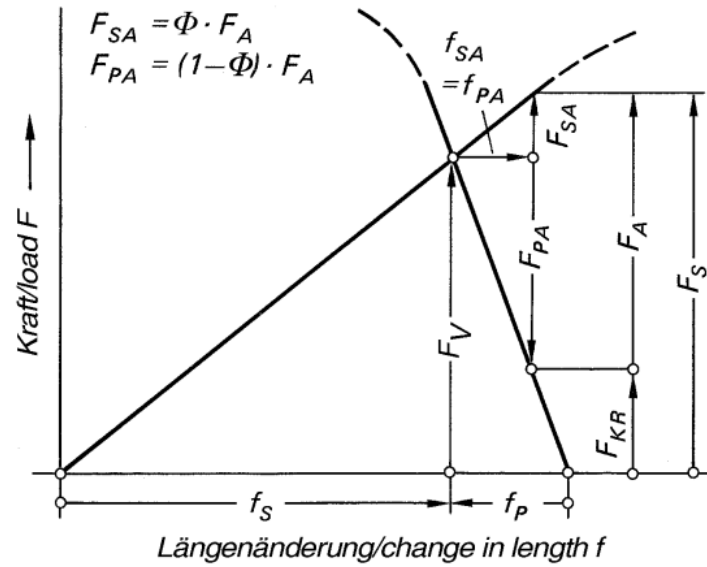
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# 1 Introduction

This document will include the BAT (Bolt Analysis Tool) User Manual [1] [2] [3].

$$p(\Theta|\mathbf{y}) = \frac{p(\mathbf{y}|\Theta) p(\Theta)}{p(\mathbf{y})}, \quad (1.1)$$



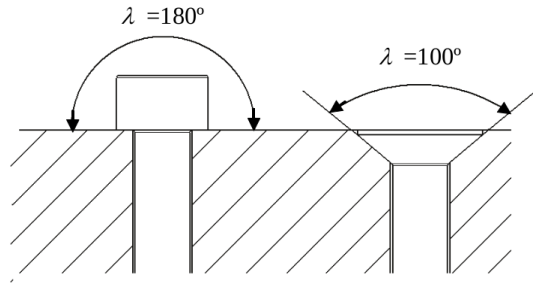
**Figure 1.1:** Joint diagram for the working state of a concentrically loaded bolted joint with  $n = 1$  [3]

## 2 Bolt and Thread Geometry

$D_{Km}$  is the *effective diameter of under head/nut friction torque* and is defined by

$$D_{Km} = \frac{D_{hole} + d_h}{2} \quad (2.1)$$

where  $D_{hole}$  is the *through-hole diameter* in the clamped parts and  $d_h$  is the *minimum bearing surface outer diameter* of the bolt head or nut.



**Figure 2.1:** Definition of under head bearing angle [2]

## 3 Method B: ECSS-E-HB-32-23A

This chapter provides a quick overview and summary of the equations used in **BAT**. A detailed description can be found in the complete ECSS-E-HB-32-23A ESA handbook [2]. Some used variables in the following equations have been changed compared to [2] by the author to increase clarity and consistency.

### 3.1 Preload and Torques

The torque present at the thread interface  $M_{th}$  is dependent of the *axial bolt preload*  $F_V$  and is given by

$$M_{th} = F_V \tan(\varphi + \rho) \frac{d_2}{2} \quad (3.1)$$

and the *under-head torque*  $M_{uh}$  due to friction between bolt head or nut and the adjacent clamped part (or shim) is defined by

$$M_{uh} = F_V \frac{\mu_{uh} D_{Km}}{2} \frac{1}{\sin \lambda/2} \quad (3.2)$$

where  $\lambda$  is the *under head bearing angle* seen in Figure 2.1. It is assumed that the friction force for  $M_{uh}$  is acting at mean bearing radius of the bolt head  $D_{Km}$  (2.1).  $\varphi$  is the helix angle of the thread and  $\rho$  is given by the relation

$$\tan \rho = \frac{\mu_{th}}{\cos \theta/2} \quad (3.3)$$

where  $\theta$  is the half angle of the thread grooves (for Unified or Metric threads  $\theta = 60^\circ$ ).

The *total installation torque*  $T_A$  (without torque device scatter) applied to bolt head or nut during tightening to produce the axial bolt preload  $F_V$  is

$$T_A = M_{th} + M_{uh} + M_p \quad (3.4)$$



where  $M_p$  is the *prevailing torque* of the locking device. With the approximation  $\tan \varphi \tan \rho \ll 1$  the expression  $\tan(\varphi + \rho)$  can be written as  $\tan(\varphi + \rho) \approx \tan \varphi + \tan \rho$ . Now equation (3.4) can be rewritten to

$$T_A = F_V \underbrace{\left[ \frac{d_2}{2} \left( \tan \varphi + \frac{\mu_{th}}{\cos \theta/2} \right) + \frac{\mu_{uh} D_{Km}}{2 \sin \lambda/2} \right]}_K + M_p \quad (3.5)$$

where  $K$  is the *joint coefficient*.

For calculation of the minimum and maximum axial bolt preload, BAT implements the *experimental coefficient method* [2] with an explicit torque scatter torque of the tightening device  $T_{scatter}$ . Therefore the minimum and maximum total installation torques are defined

$$T_A^{min} = T_A - T_{scatter}, \quad T_A^{max} = T_A + T_{scatter}. \quad (3.6)$$

To calculate the minimum and maximum *axial bolt preload after tightening*  $F_M^{min/max}$ , (3.5) and (3.6) are combined

$$F_M^{min} = \frac{T_A^{min} - M_p^{max}}{K^{max}}, \quad F_M^{max} = \frac{T_A^{max} - M_p^{min}}{K^{min}}. \quad (3.7)$$

If also the thermal influence and embedding is considered, this leads to the minimum and maximum *axial bolt preload at service*  $F_V^{min/max}$

$$F_V^{min} = \frac{T_A^{min} - M_p^{max}}{K^{max}} + \Delta F_{Vth} - F_Z \quad (3.8a)$$

$$F_V^{min} = F_M^{min} + \Delta F_{Vth} - F_Z \quad (3.8b)$$

$$= \frac{T_A^{min} - M_p^{max}}{\frac{d_2}{2} \left( \tan \varphi + \frac{\mu_{th}^{max}}{\cos \theta/2} \right) + \frac{\mu_{uh}^{max} D_{Km}}{2 \sin \lambda/2}} + \Delta F_{Vth} - F_Z \quad (3.8c)$$

$$F_V^{max} = \frac{T_A^{max} - M_p^{min}}{K^{min}} + \Delta F_{Vth} \quad (3.9a)$$

$$F_V^{max} = F_M^{max} + \Delta F_{Vth} \quad (3.9b)$$

$$= \frac{T_A^{max} - M_p^{min}}{\frac{d_2}{2} \left( \tan \varphi + \frac{\mu_{th}^{min}}{\cos \theta/2} \right) + \frac{\mu_{uh}^{min} D_{Km}}{2 \sin \lambda/2}} + \Delta F_{Vth} \quad (3.9c)$$

where  $\Delta F_{Vth}$  is thermal preload change and  $F_Z$  is the preload loss due to embedding.

## 4 References

- [1] Guidelines for threaded fasteners. ESA Guideline ESA PSS-03-208 Issue 1, Structures and Mechanism Division ESTEC, December 1989.
- [2] Space engineering - threaded fasteners handbook. ECSS Handbook ECSS-E-HB-32-23A, ECSS European Cooperation for Space Standardization, 16 April 2010.
- [3] Systematic calculation of highly stressed bolted joints - joints with one cylindrical bolt. VDI Guideline VDI2230 Part 1, VDI - Verein Deutscher Ingenieure, November 2015.