

Control Engineering

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|---|-----------------------|---|
| L1, Introduction, Linearization | ✓ | Ex1, Linearization ✓ |
| L2, Differential Equation, Linear ODEs Solution | * ✓ | Ex2, Differential Equations
Solve ODEs ✓ |
| L3, Zeros of the characteristic polynomial | ✓ | |
| L4, Unit step, impulse, response, Laplace transformation | ✓ | Ex4, Laplace ✓ |
| L5, Frequency response, Bode diagram (Amplitude & Phase Plot) | * Ex5, Bode Diagram ✓ | |
| L6, Control loop elements | ✓ | ✓ Ex6, Functional Diagram |
| L7, Controller Setting (PID) | * | * Ex7, Control Loop + Bode Diagram |
| L8, Stability of Control Loops | * ✓ Hurwitz, Routh | ✓ Ex8, Stability. Routh, Hurwitz |
| L9, Controller Setting & Stability of control loops. | | Ex9, ____ . Nyquist |
| Nyquist criterion, Gain, phase margins | ★ | Ex10, ____ Nyquist, Bode |
| Controller design in Bode diagram | ★ | Ex11, ____ Controller Design |

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Control Engineering

Lecture 2

Differential Equation

- ODE - Ordinary differential equation 1 variable

$$\downarrow \quad \frac{d^2y}{dt^2} + a_1 \cdot \frac{dy}{dt} + a_0 y = u(t)$$

- PDE - Partial differential equation > 1 variable

$$a \frac{d^2y}{dt^2} + b \frac{d^2y}{dt dx} + c \frac{d^2y}{dx^2} = u(x, t)$$

Nonlinear ODEs:

$$a_2(t) \ddot{y}^2 + a_1(t) \dot{y} y + \frac{a_0(t)}{y} = f(t)$$

Linear ODEs:

$$a_n(t) y^{(n)} + \dots + a_1 y' + a_0 y = f(t)$$

Linear Time Invariant ODEs (LTI systems)

$$a_n y^{(n)} + \dots + a_1 y' + a_0 y = f(t)$$

Solution LTI ODEs: $a_n(t) y^{(n)} + \dots + a_0(t) y = f(t)$

\Rightarrow if $f(t) = 0 \Rightarrow$ ODE homogeneous $\Rightarrow y_h =$ homogeneous solution
 \Rightarrow if $f(t) \neq 0 \Rightarrow$ inhomogeneous $\Rightarrow y_p =$ particular solution
 $y =$ solution

n-th order LTI system $y^{(n)} + a_{n-1} y^{(n-1)} + \dots + a_0 y = 0$

$\lambda_1, \dots, \lambda_n$ are solutions characteristic polynomial:

$$\lambda^n + a_{n-1} \lambda^{n-1} + \dots + a_1 \lambda + a_0 = 0$$

$$\Rightarrow y_h = c_1 e^{\lambda_1 t} + \dots + c_n e^{\lambda_n t}$$

$$z = e^{\alpha+i\beta} = e^\alpha(\cos\beta + i \sin\beta) \\ = e^\alpha \cos\beta + i e^\alpha \sin\beta$$

Define c_1, \dots, c_n from initial conditions

④ if $\lambda_1 = \lambda_2 \Rightarrow$ solution $\begin{cases} y_1 = c_1 e^{\lambda_1 t} \\ y_2 = c_2 + e^{\lambda_1 t} \end{cases}$

$$\lambda_1 = \dots = \lambda_m \Rightarrow$$
 solution $\begin{cases} y_1 = c_1 e^{\lambda_1 t} \\ y_m = c_m t^{(m-1)} e^{\lambda_1 t} \end{cases}$

$$\lambda_1 = \alpha + i\beta, \lambda_2 = \bar{\lambda}_1, \beta \neq 0 \Rightarrow \begin{cases} y_1 = c_1 e^{\alpha t} \cos(\beta t) \\ y_2 = c_2 e^{\alpha t} \sin(\beta t) \end{cases}$$

for LTI : $f(t) = p_m(t) e^{kt}, k \in \mathbb{C}$

with $p_m(t) = p_0 + p_1 t + \dots + p_m t^m$

reuse the $C(\lambda)$

$$= F''(\lambda)$$

$$= F'''(\lambda)$$

$$y_p(t) = \begin{cases} q_m(t) e^{kt} & \text{if } C(k) \neq 0 \\ t q_m(t) e^{kt} & \text{if } C(k) = 0 \quad C'(k) \neq 0 \\ t^2 q_m(t) e^{kt} & \text{if } C(k) = C'(k) = 0 \quad C''(k) \neq 0 \\ q_m(t) & \text{if } C''(k) = 0 \end{cases}$$

Particular Solution for ODEs: y_p

$f(t)$	\rightarrow	y_p
$\alpha e^{\beta t}$		$Ae^{\beta t}$
$a \cos(\beta t) + b \sin(\beta t)$		$A \cos(\beta t) + B \sin(\beta t)$
n^{th} order polynomial		$A_n t^n + A_{n-1} t^{n-1} + \dots + A_1 t + A_0$

Linearization:

$$\frac{\partial F}{\partial x_i} x_i + \dots = \dots$$

Control Engineering

- $F(\omega) = \int_{-\infty}^{\infty} f(t) e^{j\omega t} dt$

Partial Fraction Decomposition

- $i(t) = \int_{-\infty}^t \delta(\tau) d\tau \Rightarrow i(t) = \delta(t) \Rightarrow h(t) = \int_{-\infty}^t g(\tau) d\tau \Rightarrow g(t) = \frac{d h(t)}{dt}$

$$y(t) = \sum_{i=1}^n u(t_i) g(t-t_i) \Delta t \\ = \int_0^t u(\tau) g(t-\tau) d\tau$$

$$y(t) = \int_{-\infty}^{+\infty} u(\infty) g(t-\infty) d\infty = \int_{-\infty}^{+\infty} g(\infty) u(t-\infty) d\infty \\ \Rightarrow y(t) = g(t) * u(t) = u(t) * g(t)$$

convolution operator

- $F(s) = \int_{-\infty}^{\infty} f(t) e^{-st} dt = \mathcal{L}\{f(t)\}, s = \sigma + j\omega, \sigma > \alpha > 0$

$$f(t) = \begin{cases} \frac{1}{2\pi j} \int_{\alpha-j\infty}^{\alpha+j\infty} F(s) e^{st} ds & t \geq 0 \\ 0 & t < 0 \end{cases} = \mathcal{L}^{-1}\{F(s)\}$$

$$\mathcal{L}\{\dot{f}(t)\} = -f(-0) + s \cdot \mathcal{L}\{f(t)\}$$

- $x = x_0 e^{j\varphi} \in \mathbb{C} \quad |x| = \sqrt{\operatorname{Re}^2(x) + \operatorname{Im}^2(x)} = x_0$

$$= x_0 (\cos \varphi + j \sin \varphi) \quad \varphi = \arctan \frac{\operatorname{Im}(x)}{\operatorname{Re}(x)}$$

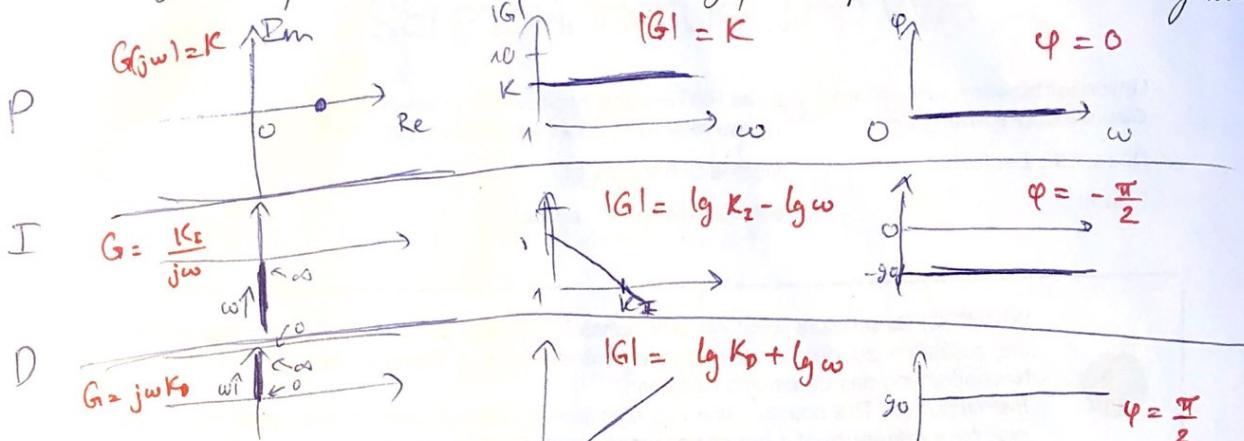
$$= x_0 \cos \varphi + j x_0 \sin \varphi$$

$$= \operatorname{Re}(x) + j \operatorname{Im}(x) \Rightarrow e^{\alpha+j\beta} = e^\alpha \cdot \cos \beta + j e^\alpha \sin \beta$$

- $G(j\omega) = \frac{Z(j\omega)}{N(j\omega)} \Rightarrow \begin{cases} |G| = \frac{|Z|}{|N|} \text{ amplitude} \\ \varphi_G = \varphi_Z - \varphi_N \text{ phase} \end{cases}$

$$G = G_1 G_2 \Rightarrow \lg |G| = \lg |G_1| + \lg |G_2|; \quad \varphi = \varphi_1 + \varphi_2$$

Frequency response and their Nyquist plots & Bode diagram

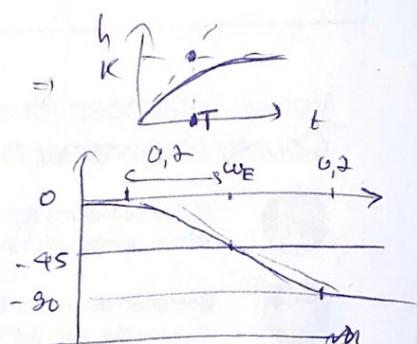
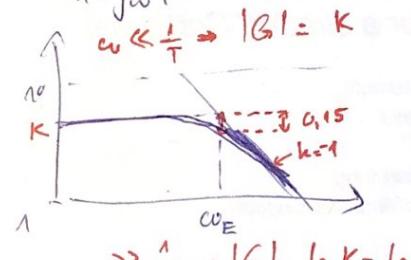
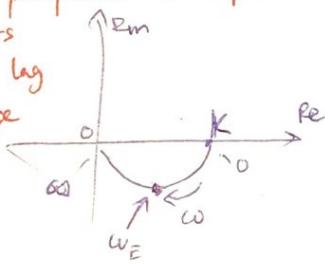


First order lag

$$T_L y + y = K u \Rightarrow G(j\omega) = \frac{K}{1 + j\omega T_L} \Rightarrow \omega_E = \frac{1}{T_L}$$

output is proportional to input

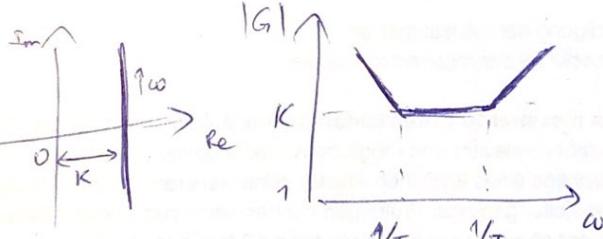
but reacts with a lag of response



PID element

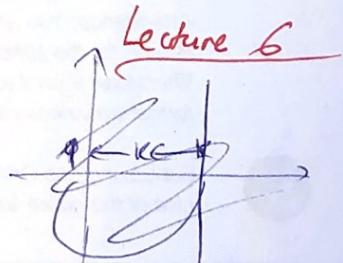
$$G = K_R \left(1 + \frac{1}{T_n s} + T_V s \right)$$

$$T_V \ll T_n$$



PT₂ 2nd order lag

$$G = \frac{K \omega_0^2}{s^2 + 2D\omega_0 s + \omega_0^2}$$



$$\text{poles: } s_{1,2} = -\omega_0 (D \pm \sqrt{D^2 - 1}) \Rightarrow D > 1 \Rightarrow s_{1,2} \in \mathbb{R}$$

\Rightarrow depends on clamping ratio

$$D = 1 \Rightarrow s_1 = s_2 \in \mathbb{R} \quad (s_1 = s_2 = -\omega_0)$$

$$D < 1$$

Lecture 6

PT_n element can be splitted into PT₁ & PT₂ elements

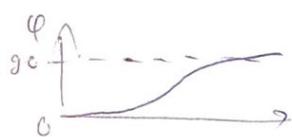
Minimal Phase system

\Rightarrow no poles

or zeros

with positive real part

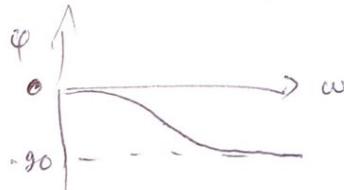
$$G(s) = K(1+Ts)$$



\Rightarrow have the minimal possible phase shift

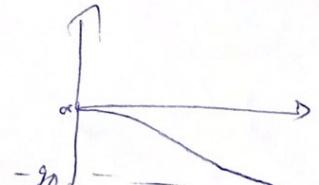
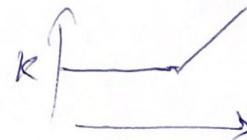
\Rightarrow the phase response (ϕ graph) can be derived from amplitude response ($|G|$ graph)

$$G(s) = \frac{K}{1+Ts}$$

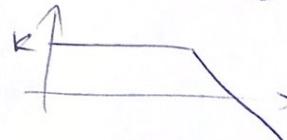


Non minimal phase system

$$G(s) = K(1-Ts)$$



$$G(s) = \frac{K}{1-Ts}$$



$$G = \frac{G_1}{1 + G_1 G_2}$$

Lecture 8: Stability

- overshoot, response time, max deviation
transient tolerance band, settling time, steady state deviation

- Hurwitz / Routh : $a_i > 0 \quad i = 0, \dots, n$ (1st condition)

Hurwitz:

a_3	$\frac{a_1}{a_3} - \frac{0}{a_1}$
a_4	$\frac{a_2}{a_4} - \frac{a_0}{a_2}$
a_5	$\frac{a_3}{a_5} - \frac{a_1}{a_3}$

 $= H$

$$\boxed{H_i > 0}$$

Hurwitz determinants > 0

Routh

a_n	a_{n-2}	$a_{n-4} \dots$
a_{n-1}	a_{n-3}	$a_{n-5} \dots$

$$\frac{a_{n-2} - a_{n-3}}{a_{n-1}} \frac{a_n}{a_{n-1}} \dots$$

$$\boxed{R_n > 0} \quad (1\text{st column}) \quad \times$$

Routh test values > 0

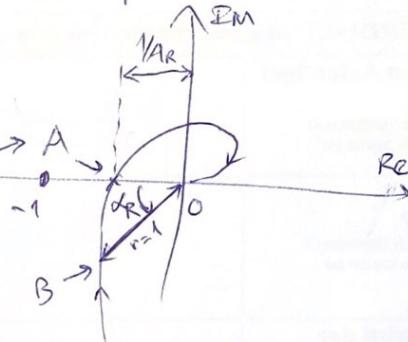
number of sign changes

\Rightarrow no of roots of characteristics polynomial with positive real part.

gain margin A_R

phase margin $\omega_d \alpha_R$

Nyquist plot

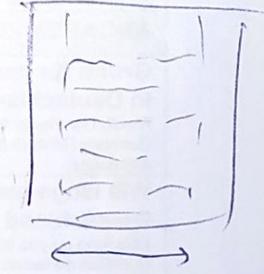


\Rightarrow Gain margin: point A

$$A_R = \frac{1}{|G(j\omega_\pi)|} \quad \text{with } \omega_\pi = -(2n+1)\pi$$

when the graph intersects "neg Real axis"

$A_R > 1 \Rightarrow$ stability



margin: is where u are safe, secured
paper margin like SUM

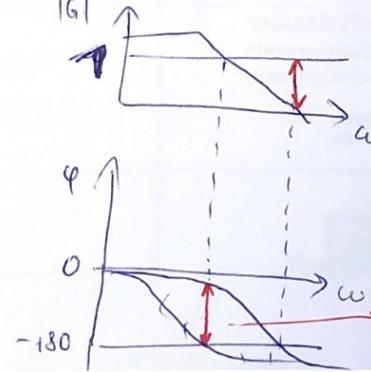
gain margin: { distance to 0 at $\varphi = -\infty$

\Rightarrow Phase margin: point B

$$\alpha_R = \varphi_o(\omega_d) - \varphi_o(\omega_\pi)$$

$$\omega_d : |G_o(j\omega_d)| = 1$$

$\alpha_R > 0 \Rightarrow$ stability



phase margin { distance to -180 at $|G| = 0$ $\log |G| = 0$

Lecture 5, Stability : Nyquist criterion

Pre conditions

single control loop
 linear system (including delay) \Rightarrow Properties of $\begin{cases} \text{open loop} \\ \text{Nyquist plot} \end{cases}$ \Rightarrow stability
 graphical representation of $G_o(j\omega)$
 (Bode, Nyquist)

$$n = m + p \quad G_z(s) = \frac{G_s(s)}{1 + G_o(s)}$$

m : no. of revolutions of Nyquist plot of $G_o(j\omega)$ around -1

p : number of poles of $G_o(s)$ in right half plane clock wise

n : number of poles of $G_z(s)$ in right half plane

Note: Draw finished Nyquist plots from $\omega: -\infty \rightarrow +\infty$, closed the loop
 In a way, the arrow turns right $\uparrow \rightarrow$ go right

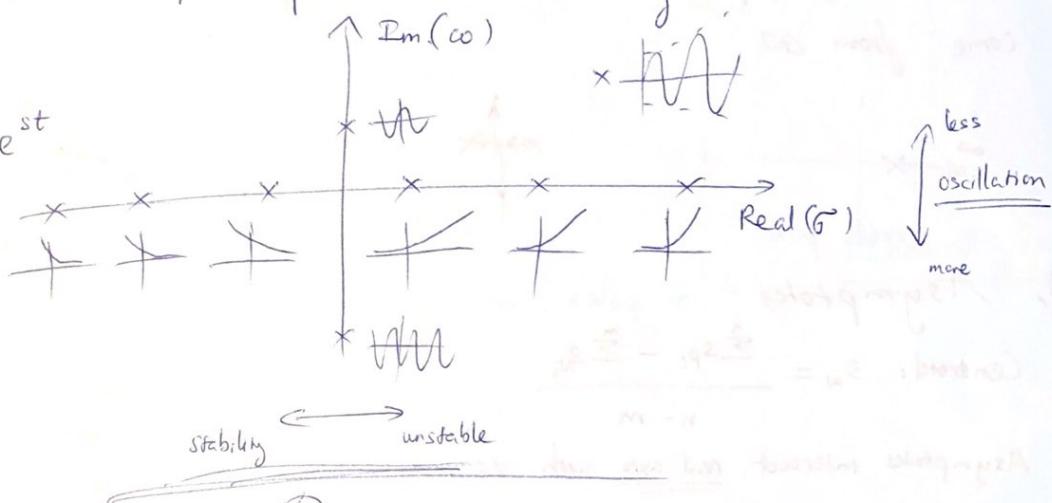
- Simple Nyquist version ?

Root Locus

why? Because poles positions \Rightarrow stability

S-Plane

wave form: $= e^{st}$



Rules

$$1 + K \cdot G(s) = 0$$

$$1 + K \cdot \frac{Q(s)}{P(s)} = 0$$

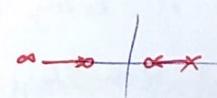
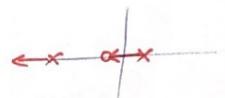
1) There are n lines (loci) $n = \max$ (degree of P & Q)

2) As $K: 0 \rightarrow \infty$, the roots move from poles to zeros of $G(s)$

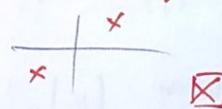
$$\text{rank}(P(s)) = \text{rank}(G(s))$$

$$\text{rank}(P) > \text{rank}(Q)$$

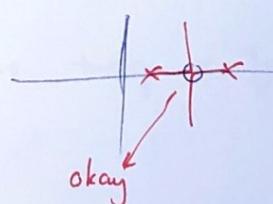
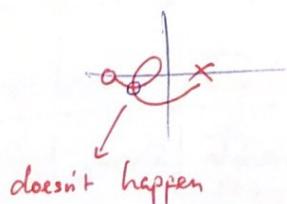
$$\text{rank}(P) < \text{rank}(Q)$$



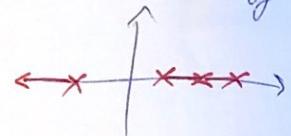
3) when roots are complex they occur in conjugate pairs



4) Never loci crosses over its path

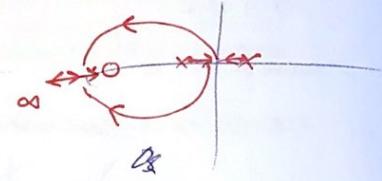
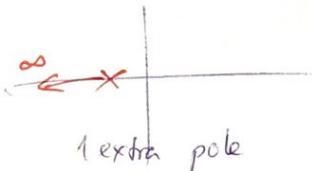


5) The portion of real axis to the left of an odd number of open loop poles & zeros are path of the loci
 $(K>0, \text{ for } K<0 \Rightarrow \text{even number of poles, zeros})$



6) Loci leave / enter real axis at 90°

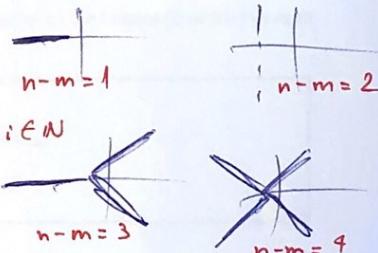
7) Not enough poles / zeros to make a pair \Rightarrow extra lines go to or come from ∞



8) Asymptotes: n poles, m zeros $\Rightarrow n-m$ asymptotes / a sym p tht

$$\text{Centroid: } s_w = \frac{\sum_{i=1}^n s_{p_i} - \sum_{i=1}^m s_{N_i}}{n-m}$$

Asymptotes intersect real axis with α_i : $\alpha_i = \begin{cases} \frac{2i-1}{n-m}\pi, & K>0 \\ \frac{2i}{n-m}\pi, & K<0 \\ i=1, \dots, n-m \end{cases}$



9) If there are at least 2 lines $\rightarrow \infty$, the sum of all roots is CONSTANT

- ⊗ Break away point: ...
- ⊗ Angle of departure (poles): $\varphi_{P_1} = \sum_{i=1}^m \varphi_{N_i} - \sum_{i=2}^n \varphi_{P_i} - \begin{cases} \pi + q2\pi, & K>0 \\ 0 + q2\pi, & K<0 \end{cases} q \in \mathbb{Z}$
- ⊗ Angle of entry (zeros): $\varphi_{N_n} = \sum_{i=1}^n \varphi_{P_i} - \sum_{i=1}^{n-1} \varphi_{N_i} + \dots$
- ⊗ Phase condition: A point on S plane, satisfy \rightarrow lies on root locus
- ⊗ $\sum_{i=1}^m \varphi_{N_i} - \sum_{i=1}^n \varphi_{P_i} = \varphi_0(s) = \begin{cases} \pi + q2\pi & K>0 \\ 0 + q2\pi & K<0 \end{cases}$
- ⊗ Magnitude condition: $|K| \cdot |G_0(s)| = 1$
- Point satisfies both conditions \Rightarrow pole location of $G_w(s), G_z(s)$ with K
- ⊗ Gain of a point on root locus $|K| = \frac{\prod_{i=1}^n |s - s_{p_i}|}{\prod_{i=1}^m |s - s_{N_i}|}$

State Space

$$G(s) = \frac{b_0 + b_1 s + \dots + b_{n-1} s^{n-1}}{a_0 + a_1 s + \dots + a_n s^n} \quad (a_n = 1)$$

$$\Rightarrow \dot{x} = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \ddots & 1 \\ -a_0 & -a_1 & -a_2 & \dots & -a_{n-1} \end{bmatrix} x + \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} u$$

Canonical form

$$y = [b_0 \ b_1 \ \dots \ b_{n-1}] x$$

Set $G(s) = \frac{Y}{U} = \frac{Y}{X} \cdot \frac{X}{U}$

↙ ↘
Numerator Denominator

$$\begin{cases} \dot{x} = Ax + Bu \\ y = Cx + Du \end{cases}$$

A: system matrix only A is a part of closed loop (also called Frobenius matrix)
 B: input —————
 C: output —————
 D: in-output —————

\Rightarrow Stability, damping... depend only on A

Stability:

characteristic polynomial: $\det(sI - A)$

eigenvalues with negative real parts

$$\text{If } u = -Kx$$

$$\Rightarrow \dot{x} = (A - BK)x$$

$$= A_k x \Rightarrow \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \cdots & 1 \\ -a_0 - k_1 & -a_1 - k_2 & -a_2 - k_3 & \cdots & -a_{n-1} - k_n \end{bmatrix}$$

Change $K \Rightarrow$ change $A_k \Rightarrow$ change poles positions
(even number of poles)

$$\frac{x}{n} \cdot \frac{x}{n} = \frac{\Delta}{n} = (z)0 - z^2$$

denominator denominator

CE exam prep

1) Linearization

$$x = X - X_0$$

$$Y = f(X) \Rightarrow y = f'(X_0)x$$

Linearize each element

$$Y = f(X, u) \Rightarrow y = \frac{\partial f}{\partial X} \Big|_{X_0, u_0} \cdot x + \frac{\partial f}{\partial u} \Big|_{X_0, u_0} \cdot u$$

$$\star \underline{dY} + f(Y) = g(X) \Rightarrow \underline{y} + f(Y_0)y = g(X_0)x$$

2) Solve ODEs

$$a_n(t) y^{(n)} + \dots + a_0(t) y = f(t)$$

\Rightarrow Homogeneous solution:

Characteristic polynomial:

$$C(\lambda) = \lambda^n + a_{n-1}\lambda^{n-1} + \dots + a_1\lambda + a_0 = 0$$

$$\Rightarrow \text{Nz: } \lambda_1, \dots, \lambda_n$$

$$\Rightarrow y_h = c_1 e^{\lambda_1 t} + \dots + c_n e^{\lambda_n t}$$

$$\text{if: } \lambda_1 = \lambda_2 \Rightarrow \begin{cases} y_1 = c_1 e^{\lambda_1 t} \\ y_2 = c_2 + t e^{\lambda_1 t} \end{cases} \quad \dots = \lambda_m$$

$$\text{if: } \lambda_1 = \bar{\lambda}_2 \Rightarrow \begin{cases} y_1 = c_1 e^{\lambda_1 t} \\ y_2 = c_2 e^{\lambda_1 t} \sin pt \end{cases} \quad \bar{\lambda}_1 = \alpha + i\beta$$

$$\Rightarrow \text{Particular solution: } y_p = p(t) y_H(t) ; \quad p(t) = \int \frac{1}{y_H(t)} f(t) dt + c_p$$

$$\Rightarrow y_G = y_h + y_p$$

3, Laplace

Damping Ratio from 2nd characteristic polynomial

$$C(\lambda) \Rightarrow \lambda_{1,2} \Rightarrow \omega_0 = \sqrt{\operatorname{Re}(\lambda)^2 + \operatorname{Im}(\lambda)^2}$$

$$\zeta = \frac{|\operatorname{Re}(\lambda)|}{\omega_0}$$

$$= \cos(\varphi)$$

4, Root Locus

↳ Phase condition: A point on S-plane satisfy

$$\sum_{i=1}^m \arg z_i - \sum_{i=1}^n \arg p_i = \arg G_0(s) = \begin{cases} \pi + q2\pi & K > 0 \\ 0 + q2\pi & K < 0 \end{cases}$$

↳ lies on root locus

↳ Magnitude condition $|K| \cdot |G_0(s)| = 1$ (8)

satisfies both \Rightarrow pole location

5, Routh, Hurwitz?

Only for closed loop func (9)

6, State Space: Canonical form

7, Linear Sampling: $y = \int u dt$

$$\Rightarrow y_k - y_{k-1} = \int_{t_{k-1}}^{t_k} u dt$$

8) Bode diagram

+ Correction table: for PT_1 , PT_2
from $\omega_E = \omega_0$ (intersection point of 2 asymptotes)

$$PT_2: D < 1$$

$$(\lg |G| - \lg |\text{Asymptote}|) * (\text{1 unit length})$$

$$\frac{\log(\text{Value}) - \log(\text{left})}{\log(\text{Right}) - \log(\text{left})} = \frac{A}{S} \rightarrow \text{usually unit length } (\lg 1 - \lg 0,1 = 1)$$

+ $\varphi = \varphi_n - \varphi_0$

$$\varphi_0 = \arctan \frac{\text{Im}}{\text{Re}}$$

Note: it's $\frac{1}{T}$ not T

9) Functional Diagram: use the unit step response graph
to represent the block

sign "-" on the right

10) Gain margin A_R from $\omega_{\infty} - (2n+1)\pi = \varphi_{\infty}$

Phase margin φ_R from $|G_b(j\omega_s)| = 1$

11) Time discrete difference equation:

Example: $u = -2y - 5\dot{y}$

$$\Rightarrow u_k = -2y_k - \frac{5}{T}(y_u - y_{u-1})$$

$$\dot{y} \Rightarrow \frac{1}{T}(y_k - y_{k-1})$$

12) Nyquist Criterion:

close the loop going right


Nyquist criterion