


Control Engineering

- L1, Introduction, Linearization ✓
- L2, Differential Equation, Linear ODEs Solution ★ ✓
- L3, Zeros of the characteristic polynomial ✓
- L4, Unit step, impulse, response, Laplace transformation ✓
- L5, Frequency response, Bode diagram (Amplitude & Phase Plot) ★ Ex5, Bode Diagram ✓
- L6, Control loop elements ✓
- L7, Controller Setting (PID) ★
- L8, Stability of Control loops ★ ✓ Hurwitz, Routh
- L9, Controller Setting & Stability of control loops.
- Nyquist criterion, ✓ Gain, phase margins ★
- L10, Controller design in Bode diagram ★
- Ex1, Linearization ✓
- Ex2, Differential Equations
Solve ODEs ✓
- Ex4, Laplace ✓
- Ex6, Functional Diagram
- ★ Ex7, Control loop + Bode Diagram
- ✓ Ex8, Stability. Routh, Hurwitz
- ✓ Ex9, — . Nyquist
- Ex10, — Nyquist, Bode
- Ex11, — Controller Design


Nguyen Duc

Control Engineering

Lecture 2

Differential Equation

- ODE - Ordinary differential equation (1 variable)

$$\frac{d^2 y}{dt^2} + a_1 \frac{dy}{dt} + a_0 y = u(t)$$

- PDE - Partial differential equation > 1 variable

$$a \frac{d^2 y}{dt^2} + b \frac{d^2 y}{dt dx} + c \frac{d^2 y}{dx^2} = u(x, t)$$

Nonlinear ODEs:

$$a_2(t) \ddot{y}^2 + a_1(t) \dot{y} y + \frac{a_0(t)}{y} = f(t)$$

Linear ODEs:

$$a_n(t) y^{(n)} + \dots + a_1(t) \dot{y} + a_0(t) y = f(t)$$

Linear Time Invariant ODEs (LTI Systems)

$$a_n y^{(n)} + \dots + a_1 \dot{y} + a_0 y = f(t)$$

Solution Linear ODEs

$$a_n(t) y^{(n)} + \dots + a_0(t) y = f(t)$$

if $f(t) = 0 \Rightarrow$ ODE homogeneous $\Rightarrow y_h =$ homogeneous solution

if $f(t) \neq 0 \Rightarrow$ inhomogeneous $\Rightarrow y_p =$ particular solution

$y =$ solution

n-th order LTI system $y^{(n)} + a_{n-1} y^{(n-1)} + \dots + a_0 y = 0$

$\lambda_1 \dots \lambda_n$ are solutions characteristic polynomial:

$$\lambda^n + a_{n-1} \lambda^{n-1} + \dots + a_1 \lambda + a_0 = 0$$

$$\Rightarrow y_h = c_1 e^{\lambda_1 t} + \dots + c_n e^{\lambda_n t}$$

$$z = e^{\alpha + i\beta} = e^{\alpha}(\cos\beta + i\sin\beta) \\ = e^{\alpha}\cos\beta + i e^{\alpha}\sin\beta$$

Define c_1, \dots, c_2 from initial conditions

⊗ if $\lambda_1 = \lambda_2 \Rightarrow$ solution $\begin{cases} y_1 = c_1 e^{\lambda_1 t} \\ y_2 = c_2 t e^{\lambda_1 t} \end{cases}$

$\lambda_1 = \dots = \lambda_m \Rightarrow$ solution $\begin{cases} y_1 = c_1 e^{\lambda_1 t} \\ \vdots \\ y_m = c_m t^{(m-1)} e^{\lambda_1 t} \end{cases}$

$\lambda_1 = \alpha + i\beta, \lambda_2 = \bar{\lambda}_1, \beta \neq 0 \Rightarrow \begin{cases} y_1 = c_1 e^{\alpha t} \cos(\beta t) \\ y_2 = c_2 e^{\alpha t} \sin(\beta t) \end{cases}$

for LTI: $f(t) = p_m(t) e^{kt}, k \in \mathbb{C}$

with $p_m(t) = p_0 + p_1 t + \dots + p_m t^m$

$y_p(t) = \begin{cases} q_m(t) e^{kt} & \text{if } C(k) \neq 0 \\ t q_m(t) e^{kt} & C(k) = 0, C'(k) \neq 0 \\ t^2 q_m(t) e^{kt} & C(k) = C'(k) = 0, C''(k) \neq 0 \\ q_m(t) = q_0 + \dots + q_m t^m \end{cases}$

reuse the $C(\lambda)$

$\Rightarrow C(\lambda) = \lambda^m$

Particular Solution for ODEs: y_p

$f(t)$	\rightarrow	y_p
$\propto e^{\beta t}$		$A e^{\beta t}$
$a \cos(\beta t) + b \sin(\beta t)$		$A \cos(\beta t) + B \sin(\beta t)$
n^{th} order polynomial		$A_n t^n + A_{n-1} t^{n-1} + \dots + A_1 t + A_0$

Linearization:

$$\frac{\partial F}{\partial x_i} x_i + \dots = \dots$$

Control Engineering

$$- F(\omega) = \int_{-\infty}^{\infty} f(t) e^{j\omega t} dt$$

Partial Fraction Decomposition

$$- 1(t) = \int_{-\infty}^t \delta(\tau) d\tau \Rightarrow i(t) = \delta(t) \Rightarrow h(t) = \int_{-\infty}^t g(\tau) d\tau \Rightarrow g(t) = \frac{d h(t)}{dt}$$

$$y(t) = \sum_{i=1}^n u(t_i) g(t-t_i) \Delta t$$

$$= \int_0^t u(\tau) g(t-\tau) d\tau$$

$$y(t) = \int_{-\infty}^{+\infty} u(\tau) g(t-\tau) d\tau = \int_{-\infty}^{+\infty} g(\tau) u(t-\tau) d\tau$$

$$\Rightarrow y(t) = g(t) * u(t) = u(t) * g(t)$$

convolution operator

$$- F(s) = \int_{-\infty}^{\infty} f(t) e^{-st} dt = \mathcal{L}\{f(t)\}, \quad s = \sigma + j\omega, \quad \sigma > \alpha > 0$$

$$F(s) \longleftrightarrow f(t)$$

$$f(t) = \begin{cases} \frac{1}{2\pi j} \int_{\alpha-j\infty}^{\alpha+j\infty} F(s) e^{st} ds & t \geq 0 \\ 0 & t < 0 \end{cases} = \mathcal{L}^{-1}\{F(s)\}$$

$$\mathcal{L}\{\dot{f}(t)\} = -f(-0) + s \cdot \mathcal{L}\{f(t)\}$$

$$- x = x_0 \cdot e^{j\varphi} \in \mathbb{C}$$

$$|x| = \sqrt{\operatorname{Re}^2(x) + \operatorname{Im}^2(x)} = x_0$$

$$= x_0 (\cos\varphi + j\sin\varphi)$$

$$\varphi = \arctan \frac{\operatorname{Im}(x)}{\operatorname{Re}(x)}$$

$$= x_0 \cos\varphi + j x_0 \sin\varphi$$

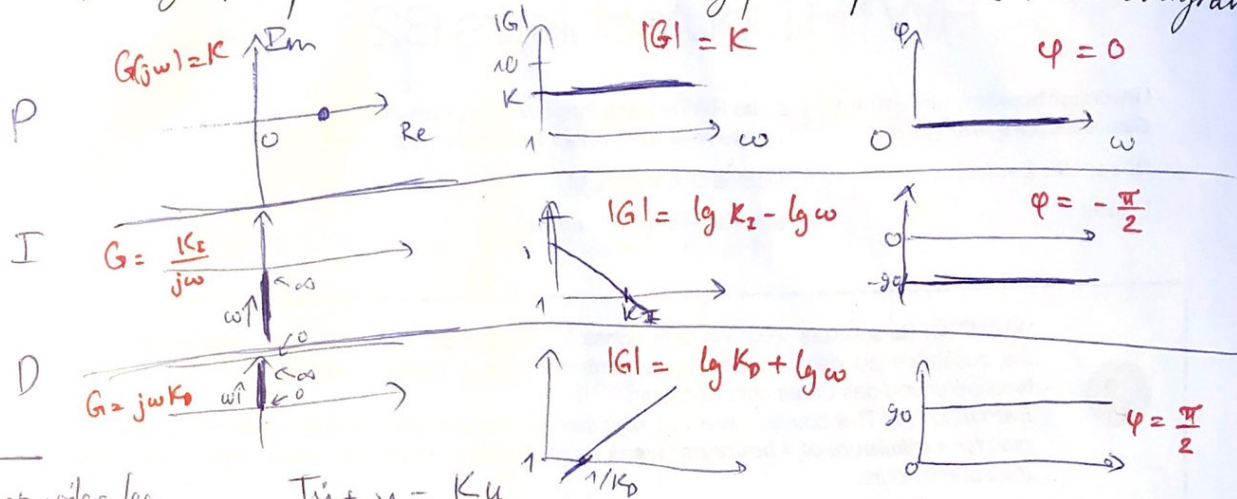
$$= \operatorname{Re}(x) + j \operatorname{Im}(x)$$

$$\Rightarrow e^{\alpha+j\beta} = e^{\alpha} \cdot \cos\beta + j e^{\alpha} \cdot \sin\beta$$

$$- G(j\omega) = \frac{Z(j\omega)}{N(j\omega)} \Rightarrow \begin{cases} |G| = \frac{|Z|}{|N|} & \text{amplitude} \\ \varphi_G = \varphi_Z - \varphi_N & \text{phase} \end{cases}$$

$$G = G_1 G_2 \Rightarrow \lg |G| = \lg |G_1| + \lg |G_2|; \quad \varphi = \varphi_1 + \varphi_2$$

Frequency response and their Nyquist plots & Bode diagram



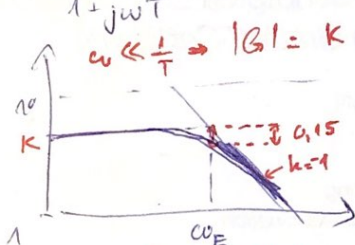
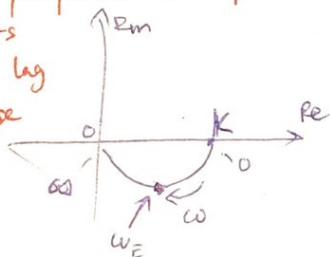
First order lag

$$T_I y + y = K u$$

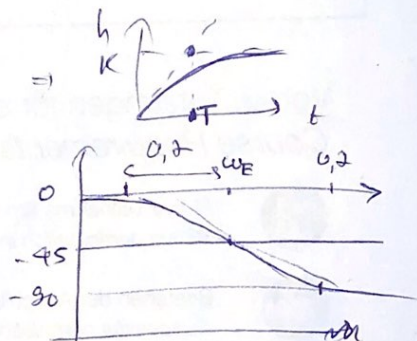
PT₁ element

$$\Rightarrow G(j\omega) = \frac{K}{1+j\omega T} \Rightarrow \omega_E = \frac{1}{T}$$

output is proportional to input but reacts with a lag of response



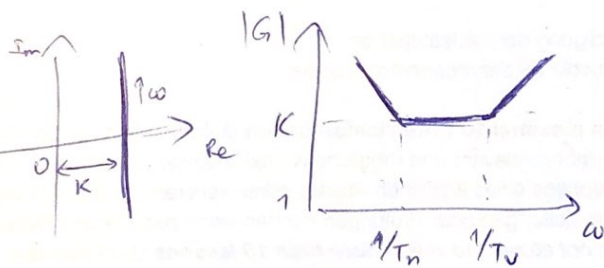
$$\omega \gg \frac{1}{T} \Rightarrow |G| = \lg K - \lg \omega T$$



PID element

$$G = K_P \left(1 + \frac{1}{T_I s} + T_D s \right)$$

$$T_D \ll T_I$$



PT₂ 2nd order lag

$$G = \frac{K \omega_0^2}{s^2 + 2D\omega_0 s + \omega_0^2}$$

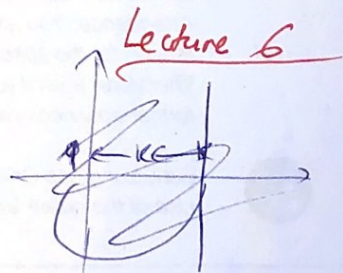
poles: $s_{1,2} = -\omega_0 (D \pm \sqrt{D^2 - 1})$

\Rightarrow Depends on damping ratio

$$D > 1 \Rightarrow s_{1,2} \in \mathbb{R}$$

$$D = 1 \Rightarrow s_1 = s_2 \in \mathbb{R} \quad (s_1 = s_2 = -\omega_0)$$

$$D < 1$$



PT_n element can be splitted into PT_1 & PT_2 elements

Minimal phase system \Rightarrow no poles

$$G(s) = K(1 + Ts)$$

or zeros

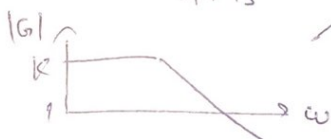
with positive real part

\Rightarrow have the minimal possible phase shift

\Rightarrow the phase response (φ graph) can be derived from amplitude response ($|G|$ graph)

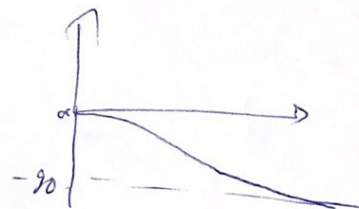
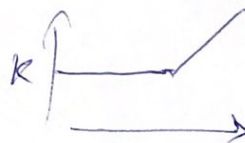


$$G(s) = \frac{K}{1 + Ts}$$

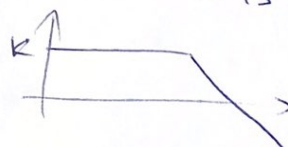


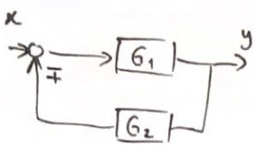
Non minimal phase system

$$G(s) = K(1 - Ts)$$



$$G(s) = \frac{K}{1 - Ts}$$





$$G = \frac{G_1}{1 \pm G_1 G_2}$$

Lecture 8: Stability

- overshoot, response time, max deviation
- transient tolerance band, settling time, steady state deviation

— Hurwitz / Routh : $a_{ii} > 0 \quad i = 0, \dots, n$ (1st condition)

Hurwitz:
$$\begin{vmatrix} a_3 & a_1 & 0 \\ a_4 & a_2 & a_0 \\ a_5 & a_3 & a_1 \end{vmatrix} = H$$

Routh
$$\begin{array}{c|cc} a_n & a_{n-2} & a_{n-4} \dots \\ a_{n-1} & a_{n-3} & a_{n-5} \dots \\ \hline a_{n-2} - a_{n-3} \frac{a_n}{a_{n-1}} & \dots & \end{array}$$

$$H_i > 0$$

Hurwitz determinants > 0

$$R_n > 0 \quad (\text{1st column}) \quad \times$$

Routh test lines > 0

number of sign changes

\Rightarrow no of roots of characteristics polynomial with positive real part.

Nyquist plot

gain margin A_R

phase margin α_R

\Rightarrow Gain margin: point A

$$A_R = \frac{1}{G_0(j\omega_\pi)} \quad \text{with } \omega_\pi = -(2n+1)\pi$$

when the graph intersect "neg Real axis"

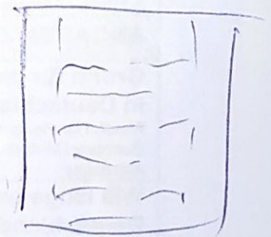
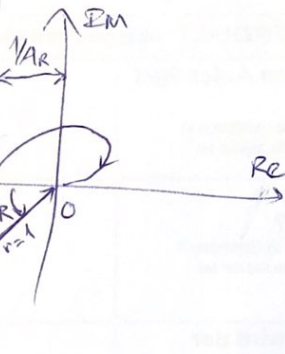
$$A_R > 1 \Rightarrow \text{stability}$$

\Rightarrow Phase margin: point B

$$\alpha_R = \varphi_0(\omega_d) - \varphi_0(\omega_\pi)$$

$$\omega_d : |G_0(j\omega_d)| = 1$$

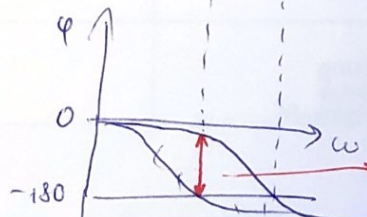
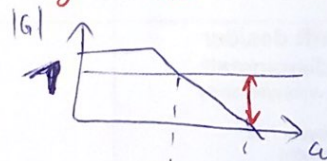
$$\alpha_R > 0 \Rightarrow \text{stability}$$



paper margin
like SUM

margin: is where
u are safe, secured

gain margin: $\left\{ \begin{array}{l} \text{distance to } 0 \\ \text{at } \varphi = -\pi \end{array} \right.$



phase margin: $\left\{ \begin{array}{l} \text{distance to } -\pi \\ \text{at } |G|=1 \end{array} \right.$
 $|G|=1 \Rightarrow \log |G| = 0$

Lecture 9, Stability: Nyquist criterion

Pre conditions

[single control loop
linear system (including delay)
graphical representation of $G_o(j\omega)$
(Bode, Nyquist)] \Rightarrow Properties of [open loop
Nyquist plot] \Rightarrow stability of closed loop

$$n = m + p$$

$$G_z(s) = \frac{G_o(s)}{1 + G_o(s)}$$

m : no. of revolutions of Nyquist plot of $G_o(j\omega)$ around -1
clock wise

p : number of poles of $G_o(s)$ in right half plane

n : number of poles of $G_z(s)$ in right half plane

Notes Draw finished Nyquist plots from $\omega: -\infty \rightarrow +\infty$, closed the loop
in a way, the arrow turn right $\uparrow \rightarrow$ go right

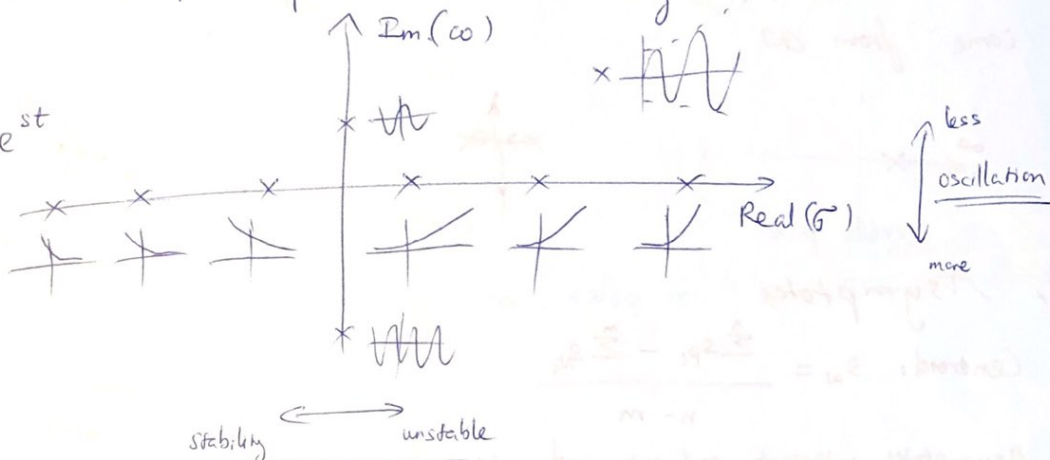
- Simple Nyquist version?

Root locus

why? Because poles positions \Rightarrow stability

S-Plane

wave form: $= e^{st}$



Rules

$$1 + K \cdot G(s) = 0$$

$$1 + K \cdot \frac{Q(s)}{P(s)} = 0$$

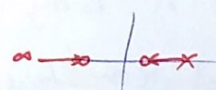
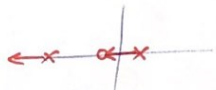
1, There are n lines (loci) $n = \max(\text{degree of } P \& Q)$

2, As $k: 0 \rightarrow \infty$, the roots move from poles to zeros of $G(s)$

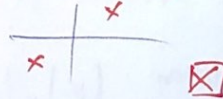
$$\text{rank}(P(s)) = \text{rank}(G(s))$$

$$\text{rank}(P) > \text{rank}(Q)$$

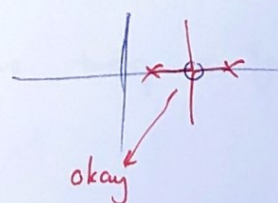
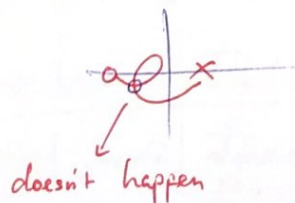
$$\text{rank}(P) < \text{rank}(Q)$$



3, when roots are complex they occur in conjugate pairs



4, Never loci crosses over its path

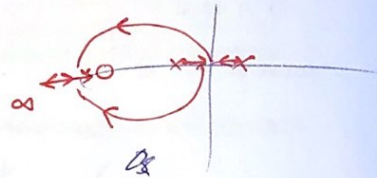
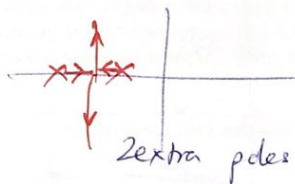
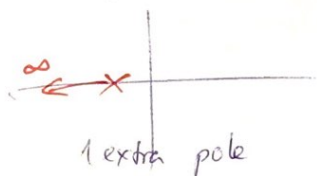


5, The portion of real axis to the left of an odd number of open loop poles & zeros are path of the loci
($K > 0$, for $K < 0 \Rightarrow$ even number of poles, zeros)



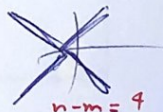
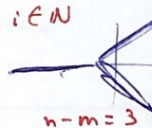
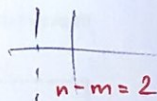
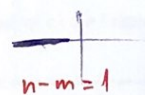
6, Loci leave / enter real axis at 90°

7, Not enough poles / zeros to make a pair \Rightarrow extra lines go to or come from ∞



8, Asymptotes: n poles, m zeros $\Rightarrow n-m$ asymptotes / Asymptotes
Centroid: $s_w = \frac{\sum s_{p_i} - \sum s_{z_i}}{n-m}$

Asymptotes intersect real axis with α_i : $\alpha_i = \begin{cases} \frac{2i-1}{n-m} \pi, & K > 0 \\ \frac{2i}{n-m} \pi, & K < 0 \end{cases}$
 $i = 1, \dots, (n-m)$



9, If there are at least 2 lines $\rightarrow \infty$, the sum of all roots is CONSTANT

⊗ Break away point: ...

⊗ Angle of departure (poles): $\varphi_{p_1} = \sum_{i=1}^m \varphi_{N_i} - \sum_{i=2}^n \varphi_{p_i} - \begin{cases} \pi + q2\pi, & K > 0 \\ 0 + q2\pi, & K < 0 \end{cases} \quad q \in \mathbb{Z}$

⊗ Angle of entry (zeros): $\varphi_{N_1} = \sum_{i=1}^n \varphi_{p_i} - \sum_{i=2}^m \varphi_{N_i} +$

⊗ Phase condition: A point on s plane, satisfy \rightarrow lies on root locus

$$\sum_{i=1}^m \varphi_{N_i} - \sum_{i=1}^n \varphi_{p_i} = \varphi_0(s) = \begin{cases} \pi + q2\pi & K > 0 \\ 0 + q2\pi & K < 0 \end{cases}$$

⊗ Magnitude condition: $|K| \cdot |G_0(s)| = 1$

Point satisfies both conditions \Rightarrow pole location of $G_w(s)$, $G_z(s)$ with K

⊗ Gain of a point on root locus

$$|K| = \frac{\prod_{i=1}^n |s - s_{p_i}|}{\prod_{i=1}^m |s - s_{N_i}|}$$

⊗

State Space

$$G(s) = \frac{b_0 + b_1 s + \dots + b_{n-1} s^{n-1}}{a_0 + a_1 s + \dots + a_n s^n} \quad (a_n = 1)$$

$$\Rightarrow \dot{x} = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & 1 \\ -a_0 & -a_1 & -a_2 & \dots & -a_{n-1} \end{bmatrix} x + \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} u$$

Canonical form

$$y = [b_0 \ b_1 \ \dots \ b_{n-1}] x$$

Set $G(s) = \frac{y}{u} = \frac{y}{x} \cdot \frac{x}{u}$

\swarrow Numerator \searrow Denominator

$$\begin{cases} \dot{x} = Ax + Bu \\ y = Cx + Du \end{cases}$$

A: system matrix

B: input

C: output

D: in-output

only A is a part of closed loop (also called Frobenius matrix)

\Rightarrow Stability, damping... depend only on A

Stability:

characteristic polynomial: $\det(sI - A)$

eigenvalues with negative real parts

If $u = -Kx$

$$\Rightarrow \dot{x} = (A - BK)x$$

$$= A_k x$$

$$\Rightarrow \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & 1 \\ -a_0 - k_1 & -a_1 - k_2 & -a_2 - k_3 & \dots & -a_{n-1} - k_n \end{bmatrix}$$

Change $K \Rightarrow$ change $A_k \Rightarrow$ change poles positions
(even number of poles)

CE exam prep

1, Linearization

$$x = X - X_0$$

$$Y = f(X) \Rightarrow y = f'(X_0) \cdot x$$

Linearize each element

$$Y = f(X, u) \Rightarrow y = \left. \frac{\partial f}{\partial X} \right|_{X_0, u_0} \cdot x + \left. \frac{\partial f}{\partial u} \right|_{X_0, u_0} \cdot u$$

$$\star \frac{dY}{dt} + f(Y) = g(X) \Rightarrow \underline{y} + f'(X_0) y = g'(X_0) x$$

2 Solve ODEs

$$a_n(t) y^{(n)} + \dots + a_0(t) y = f(t)$$

→ Homogeneous solution:

characteristic polynomial:

$$C(\lambda) = \lambda^n + a_{n-1} \lambda^{n-1} + \dots + a_1 \lambda + a_0 = 0$$

$$\Rightarrow \lambda_0: \lambda_1, \dots, \lambda_n$$

$$\Rightarrow y_h = c_1 e^{\lambda_1 t} + \dots + c_n e^{\lambda_n t}$$

$$\text{if: } \lambda_1 = \lambda_2 \Rightarrow \begin{cases} y_1 = c_1 e^{\lambda_1 t} \\ y_2 = c_2 t e^{\lambda_2 t} \end{cases}$$

$$\text{if: } \lambda_1 = \bar{\lambda}_2 \Rightarrow \begin{cases} y_1 = c_1 e^{\alpha t} \cos \beta t \\ y_2 = c_2 e^{\alpha t} \sin \beta t \end{cases}$$

$$\rightarrow \text{Particular solution: } y_p = p(t) y_h(t); \quad p(t) = \int \frac{1}{y_h(t)} f(t) dt + c_p$$

$$\rightarrow y_G = y_h + y_p$$

3, Laplace

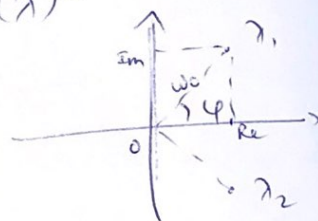
Damping Ratio from 2nd Characteristic polynomial

$$C(\lambda) \Rightarrow \lambda_{1,2} \Rightarrow$$

$$\omega_0 = \sqrt{\operatorname{Re}(\lambda)^2 + \operatorname{Im}(\lambda)^2}$$

$$\eta = \frac{|\operatorname{Re}(\lambda)|}{\omega_0}$$

$$= \cos(\varphi)$$



4, Root Locus

1) Phase condition: A point on S-plane satisfy

$$\sum_{i=1}^m \varphi_{N_i} - \sum_{i=1}^n \varphi_{P_i} = \varphi_0(s) = \begin{cases} \pi + q2\pi & K > 0 \\ 0 + q2\pi & K < 0 \end{cases}$$

2) lies on root locus

3) Magnitude condition $|K| \cdot |G_0'(s)| = 1$

(?)

Satisfies both \Rightarrow pole location

5, Routh, Hurwitz

Only for closed loop func(?)

6, State Space: Canonical form

7, Linear Sampling: $y = \int u dt$

$$\Rightarrow y_k - y_{k-1} = \int_{t_{k-1}}^{t_k} u dt$$

8, Bode diagram

+ Correction table: for PT_1 , PT_2
from $\omega_E = \omega_0$ (intersection point of 2 asymptotes)

$$PT_2: D < 1$$

$$(\lg |G| - \lg |\text{Asymptote}|) \times (1 \text{ unit length})$$

$$\frac{\lg(\text{Value}) - \lg(\text{left})}{\lg(\text{Right}) - \lg(\text{Left})} = \frac{A}{S} \rightarrow \text{usually unit length } (\lg 1 - \lg 0,1 = 1)$$

$$+ \varphi = \varphi_N - \varphi_D$$

$$\varphi_D = \arctan \frac{\text{Im}}{\text{Re}}$$

Note: it's $\frac{1}{T}$ not T

9, Functional Diagram: use the unit step response graph to represent the block
sign "-" on the right

10, Gain margin A_R from $\omega_{\pi} \text{ where } -(2n+1)\pi = \varphi_{\pi}$
Phase margin α_R from $|G_0(j\omega_s)| = 1$

11) Time discrete difference equation:

Example: $u = -2y - 5\dot{y}$

$$\Rightarrow u_k = -2y_k - \frac{5}{T}(y_k - y_{k-1})$$

$$\dot{y} \Rightarrow \frac{1}{T}(y_k - y_{k-1})$$

12) Nyquist Criterion:

close the loop going right


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