

Robotic Sensor Systems

Ng Huu Duc

↳ Future Applications:

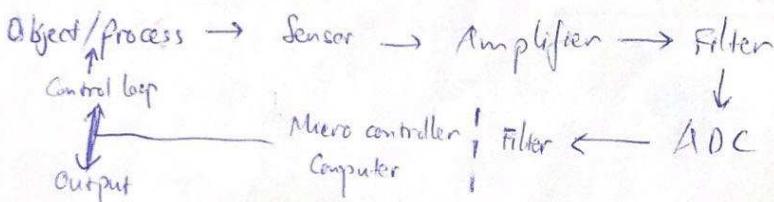
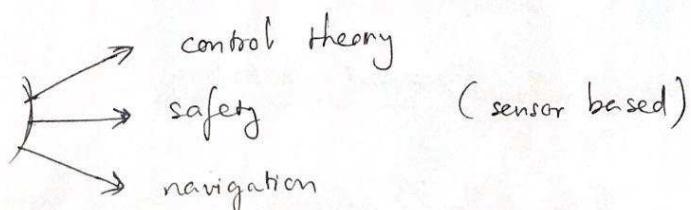
- Industrial Robots: more complex tasks
wider / broader range of manufacturing
- Service Robots: excluding Industrial automation application
- Application: logistics, medical, field, defense

→ Key abilities: CIMMPC

- Configurability
- Interaction ability
- Motion Ability
- Manipulation ability
- Perception ability: suitable choice of sensing modality
- Cognitive ability: reduction of programming & configuration effort

→ Key technologies:

Advances in sensors

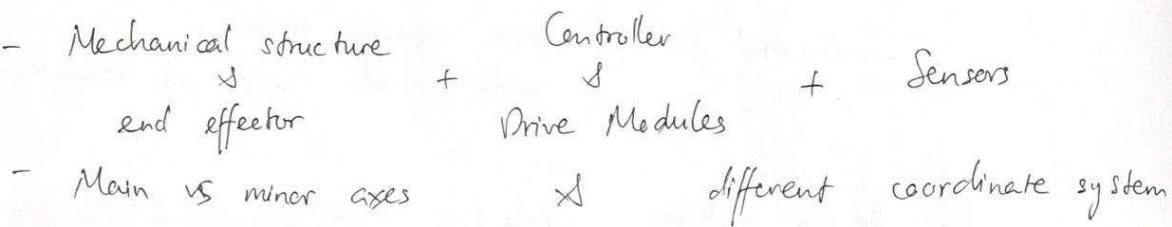


L2, Control & feedback control systems

1) Introduction to industrial robots:

- several driven axes, freely programmable, tools, gripper, sensors..
high-payload, large working area

Components
of robotic
system



2) Internal metrology of industrial robot:

(the scientific study of measurement)

internal
measuring
sensors

+ Control variables:

- Current measurement: current transformers, ammeters
- Velocity measurement: tachogenerators
- Position measurement: encoders

+ Accuracy of industrial robots:

Repeatability

vs

Accuracy

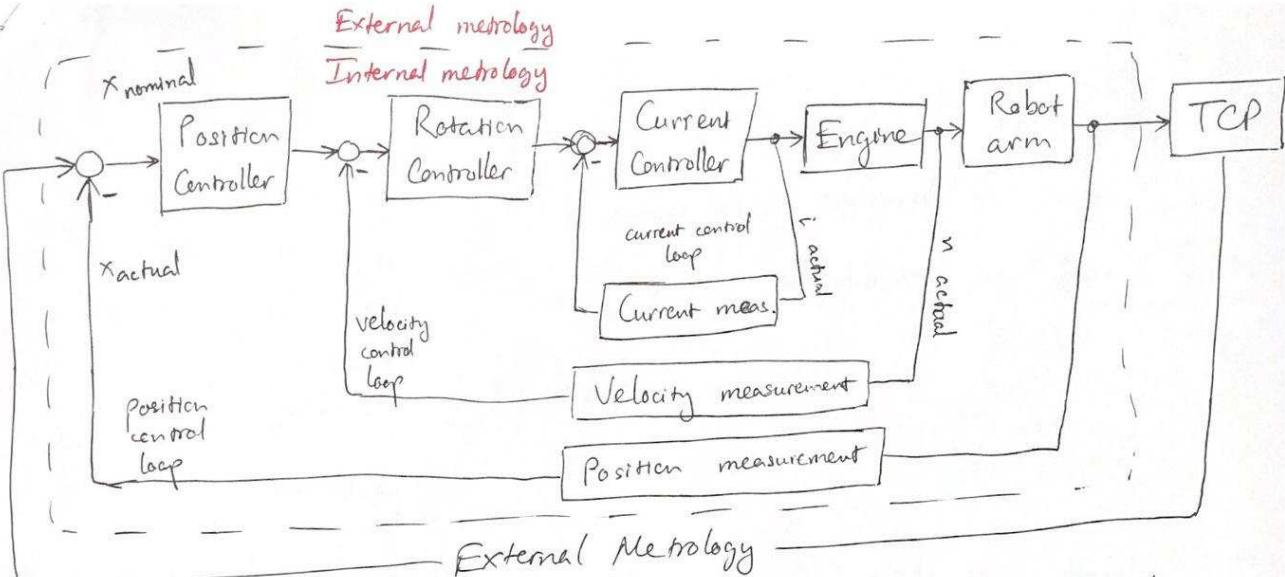
+ Position uncertainty:

+ ISO 9283: standards on how performance should be tested characteristics _____ specified

3, External metrology ..

external measuring sensors

- Poor position accuracy can be compensated with external metrology



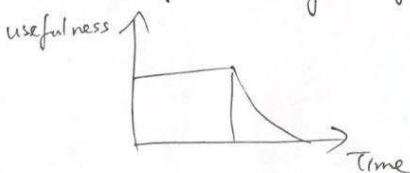
+ In door GPS	Laser Radar	Laser Tracker
Transmitter & receiver 1,5 - 30 m 0,2 mm Range Uncertainty: Example. Assembly on moving main part	Scan arbitrary surfaces 2-30 m 0,1 mm	Dynamic measurements 2-80 m 0,05 mm
+ Open-loop ex: Delta robot, pick & place small, acceptable errors	vs	<u>closed-loop</u>
+ Full Automation separated decoupled no maximum workspace workflow Physical contact necessary Speed	Human-Robot - Collaboration shared coupled yes reduced	

4) Communication between sensors & robots via
industrial ethernet & 5G:

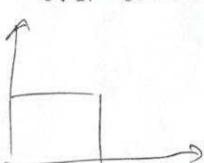
- Real time: for Machine Tools, Industrial Robot Applications.

processing $10\mu s \rightarrow 16ms$ data / results are available within a specified period of time

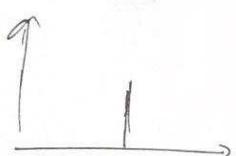
- Usefulness of information over time:



Soft real-time



Hard-real-time



Firm real-time

→ Fieldbus protocol

used for distributed control systems
real-time capabilities

5G

wireless
high data rates
ultra-low latency
security
scalability

real-time

Both: to share & use data

connect more devices, more data
ultra-reliable
ultra low latency → real time

Requirements

Enhance IT structure

Development of new wireless systems

Close the loop in real application

Prove the added value

Universal real-time capable connectivity

Electro magnetic Sensor

L3, Electro magnetic Sensors for robot control:

+ Proprioceptive Sensor	Encoders	Tachometer	Gyroscope
If you can measure \dot{x} → can derive $\ddot{x}, \ddot{\ddot{x}}$	Position / Pose	✓	
	Velocity	✓	✓
	Acceleration	✓	

1, Principles of Electromagnetism: Maxwell's equations

- Gauss' law:

$$\text{electric flux} \quad \Phi_E = \oint \vec{E} \cdot d\vec{A} = \frac{Q_{\text{enc}}}{\epsilon_0}; \quad \epsilon_0 = \text{const} \Leftrightarrow \nabla \cdot \vec{E} = \frac{Q}{\epsilon_0}$$

$$\Leftrightarrow \oint \vec{D} \cdot d\vec{A} = \int \rho dV = Q_{\text{enc}}; \quad \vec{D} = \epsilon \vec{E} \Leftrightarrow \boxed{\nabla \cdot \vec{D} = \rho}$$

- Gauss' law for magnetism:

$$\text{magnetic flux} \quad \Phi_B = \oint \vec{B} \cdot d\vec{A} = 0 \Leftrightarrow \boxed{\nabla \cdot \vec{B} = 0} \Rightarrow \vec{B} \text{ is solenoidal vector fields}$$

divergence
no source
no sink

- Maxwell - Faraday equation

There is no magnetic monopole

$$\boxed{\nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t}}; \quad U = \oint \vec{E} \cdot d\vec{s} = - \iint \frac{\partial \vec{B}}{\partial t} \cdot d\vec{A}$$

Varying magnetic fields \vec{B} induce electric fields \vec{E}

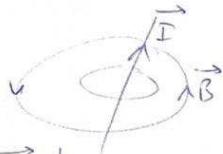
- Ampère's circuital law

$$\boxed{\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}}; \quad \oint \vec{H} \cdot d\vec{s} = \iint \vec{J} \cdot d\vec{A} + \iint \frac{\partial \vec{D}}{\partial t} \cdot d\vec{A}$$

$$\vec{H} = \frac{\vec{B}}{\mu_0}, \quad \mu_0 = \text{const}$$

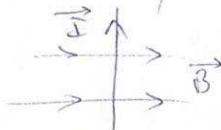
$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{end}} + \mu_0 \epsilon_0 \frac{d\Phi_E}{dt}$$

+) Magnetic field:



$$B = \frac{\mu_0 I}{2\pi R}; \quad \mu_0 = 4\pi \cdot 10^{-7}$$

- Magnetic force for current



$$\vec{F} = \vec{I} \times \vec{B} \cdot l$$

- [for moving charge]

$$\vec{F} = q \cdot \vec{v} \times \vec{B}$$

Lorentz force

+) Hall effect:

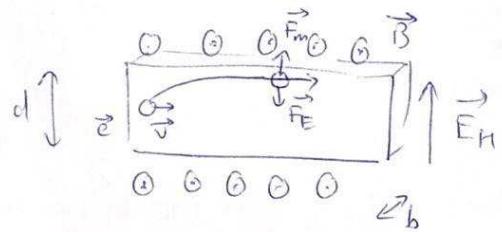
$$\vec{F}_m = \vec{F}_E$$

$$\Leftrightarrow q \vec{v} \times \vec{B} = q \vec{E}_H = q \frac{\vec{U}_H}{d}$$

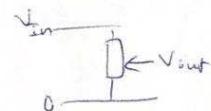
$$\Leftrightarrow \vec{U}_H = \vec{v}_0 \cdot \vec{B} \cdot d \quad \text{Hall emf}$$

$$= \frac{\vec{I}}{n \cdot Q} \frac{\vec{B} \cdot d}{b} \quad (\text{cause current density } \vec{J}_0 = \frac{I}{n \cdot Q} \frac{\vec{I}}{b \cdot d})$$

$$= R_H \cdot \frac{\vec{I} \cdot \vec{B}}{b} \quad (R_H : \text{Hall constant})$$



2) Positioning sensors:



+) Potentiometer: works according to Ohm's law

[Turning Potentiometer] [Sliding Potentiometer] when joint rotate, the gear turns the potentiometer--

+) Induction-based Sensors:

- Resolver ..

- Inductive Transducer

- Transverse Armature Transducer: based on Maxwell bridge

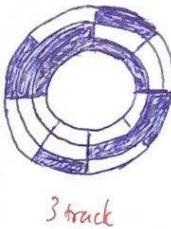
- Differential Transducer

- Inductosyn

+/- Rotary Encoders:

- Absolutely Encoder

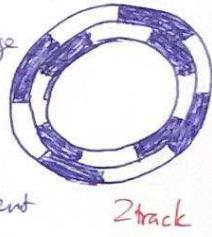
maintain info when power is removed
 pos info available immediately
 relationship encoder value & physical pos.
 set at assembly



3 track

vs Incremental Encoder

immediately report pos change
 doesn't keep track
 have to go back to fixed point to init measurement



2 track

- Magnetic Encoder

Components:
 Disk, conditioning circuit
 Hall sensor
 magnetoresistive

vs Optical Encoder

Code disk, LED, Scanner

- Number of track \Rightarrow resolution:

$$n \text{ track} \Rightarrow \text{resolution: } \frac{2\pi}{2^n}$$

	Advantages	Disadvantages
Potentiometer	Simple low cost	Limited range Accuracy limited Wear out (due to contact)
Resolver	Non-contact	Analog Requires decoding circuit Expensive
Inductive Transducer	Non-contact High accuracy	Limited range Analog
Magnetic Encoder ✓	Non-contact Robust	Decoding required usually lower reso
Optical Encoder	Non-Contact	Gray decoding required Complex wiring

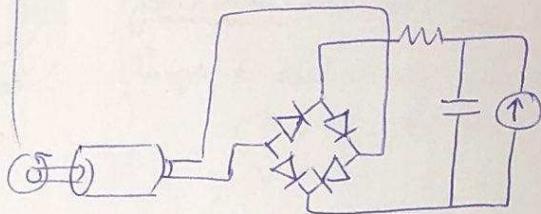
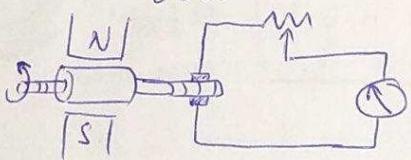
3) Speed Sensors:

Maxwell - Faraday equations

$$\frac{\partial \vec{B}}{\partial t} \rightarrow \frac{\partial \vec{E}}{\partial t}$$

/tā'kōmētər/ Tachometer based on DC machine | Tachometer using AC generator

$$V = \frac{\vec{B} P_n z}{60a} = K \cdot n$$



4) Acceleration Sensors:

+ Mechanical Gyroscopes (conservation of angular momentum)

$$C_y = -I\Omega w_z$$

Torques lead to displacement

$$C_z = I\Omega w_y$$

+ Micro Electro-Mechanical System Gyroscope (MEMS)

$$\vec{a}_{\text{Coriolis}} = 2(\vec{v} \times \vec{\omega})$$

Change in capacitance \Rightarrow proportional to Coriolis force

Capacitive & Piezoelectric Sensors

/pli'zaɪ/

Q1,

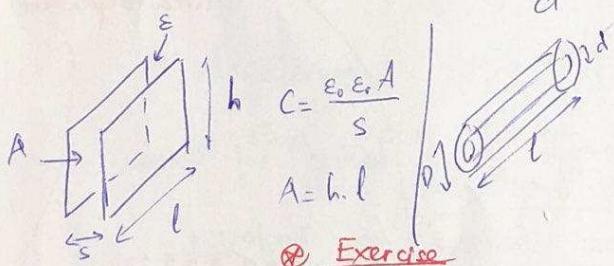
→ Motivation for Robotics: capacitive collision avoidance

1) Electro technical Basis of Capacitance

- $U_{AB} = \int_A^B \vec{E} \cdot d\vec{s}$; $U_{AB} \sim Q$
- 1st Maxwell's equation: $\frac{Q}{\epsilon_0} = \oint \vec{E} \cdot d\vec{A} = \Phi_E$; If $E = \text{const over Area } A$: $\frac{Q}{\epsilon_0} = E \cdot A = \Phi_E$
- $Q = C \cdot U$

2) Capacitive Sensors:

$$\rightarrow C = \epsilon_r \epsilon_0 \frac{a, b}{d}$$



C : capacitance

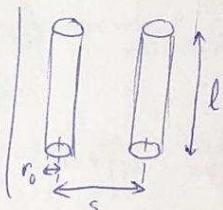
ϵ_0 : absolute dielectric constant of vacuum

ϵ_r : relative dielectric constant

a, b : electrode length, width .. $ab = A$

d : distance between electrodes

$$C = \frac{2\pi \epsilon_0 \epsilon_r l}{\ln \frac{D}{d}}$$

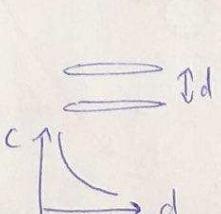


$$C = \frac{\pi \epsilon_0 \epsilon_r l}{\ln \frac{s}{r_0}}$$

$s \gg r_0$

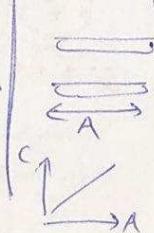
→ Capacitive Transducers:

- Distance Sensors



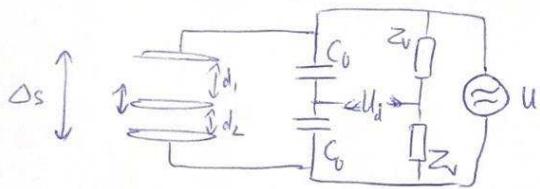
- non-contact
- wear-free

- Surface Transducers



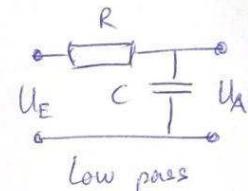
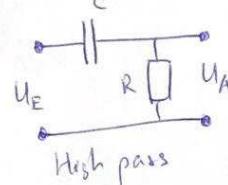
- Determination of object displacements

- Simple Differential Arrangement



Ex: Capacitive Pressure Sensor

- High pass / Low pass filter



→ Accelerometer: change $\vec{a} \Rightarrow \vec{F} \rightarrow$ change position of electrode

Ex: Airbag Deployment.

Capacitive Touch Screen

Capacitive Gyroscope

Accelerometer-based Control

② Pros & Cons:

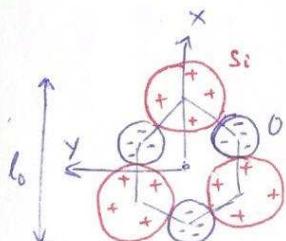
(+) Non-contact - wear-free
Simple, low power consumption
Penetrates insulating materials
Low temperature dependence
Extreme temp. range
Resolution sub nm

(-) Required AC voltage
Disturbance of measuring power
Impairment by insulating walls
dust & moisture

3) Electrotechnical Basics of Piezo Effect:

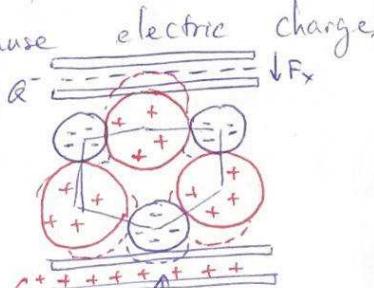
→ Motivation for robotics

→ Piezo effect: deformations of crystal



- Here quartz (SiO_2)
- An asymmetrical charge dist.

⇒ cause electric charges

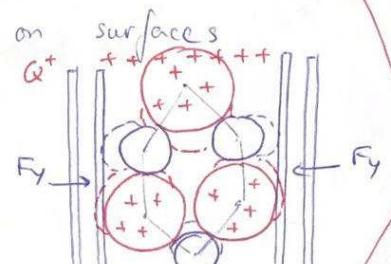


Longitudinal Piezo effect.

- Area independent

$$Q_x = d_{11} \cdot F_x$$

lattice of certain ion crystals

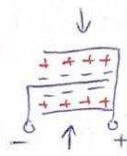


Transversal Piezo effect

$$Q_y = d_{12} \cdot \frac{F_y}{l_x}$$

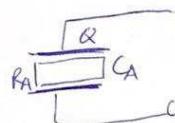
+ Basic Principles

- Increase charge



$$Q_A = n \cdot Q \quad (\text{parallel connection})$$

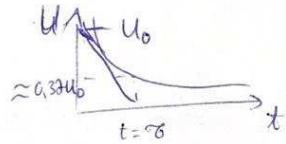
- Capacitive properties
Discharge will drop U



$$Q = d \cdot F = C_A \cdot U_A$$

$\Rightarrow U_A = \frac{d \cdot F}{C_A}$ with
 } d: piezo coeff.
 } F: mecha. force
 } CA: inherent capacitance

- Discharge func: $U(t) = U_0 e^{-t/\tau}$
 $\tau = R \cdot C$



⊗ Exercise

- Double element

$$C = 2C_0$$

$$R = R_0 / 2$$

$$d = 2d$$

$$\tau = \tau_0$$

$$U = U_0$$

4) Piezoelectric sensors

+ Force & Torque Measurement

- Pairs of piezo plates \Rightarrow longitudinal piezo effect $\Rightarrow F_z$
- Multi component force transducers \Rightarrow shear effect $\Rightarrow F_y, F_x$
- For torque, arrange sensor to capture tangential in circuit & electrically switched



+ Pressure Measurement

- Accelerations can falsify pressure measurement

\Rightarrow Thus, use seismic mass in the
the acceleration-compensated pressure transducers

- Spring mass oscillator

- An indirect measurement \Rightarrow from measuring deflection r of the mass m
 of acceleration

} spring force F_c

→ Reciprocal Piezo Effect: typical range: 10 - 200 μm

Apply electric field \Rightarrow a piezo electric element \Rightarrow generate mechanical stresses

Ex: \Rightarrow Piezo electric drive

Ex: Piezo electric actuator as Injector for Diesel Engine

Electro magnetic Sensors for Robot Vision

L5) 1) Electromagnetic sensors for robot vision:

- Exteroceptive sensor: info from environment
- Wave-particle duality:

2) Photo sensors

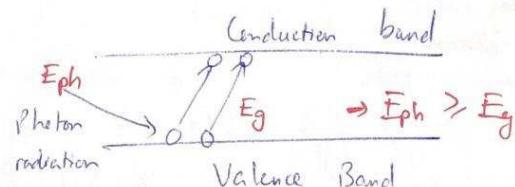
- Black body produce a special type of light, continuous light
 - there is connection between light intensity, temperature and wavelength
 - absorb all incoming radiations
- Planck's law: energy spectrum of a black body with temp. T

$$E_\lambda = \frac{C_1}{\lambda^5} \cdot \frac{1}{e^{\frac{C_2}{\lambda T}} - 1}$$

- External photo electric effect
- Planck energy \rightarrow $E_\lambda = h \cdot f$ \rightarrow $h \cdot \frac{c}{\lambda}$
 Planck const freq

$$E_{kin} = E_{ph} - w_A = h \cdot f - w_A$$

- Inner photo electric effect



- Inner photo electric effect:

Photon diode
 Image sensor
 CMOS

UV to near IR
 Fast response time
 small build size

- External photo electric effect

Photo multiplier
 Photo tube

UV to near IR
 High sensitivity
 large receiving surfaces

3, Electromagnetic Waves:

④ Derivation of the wave equation:

time dependent, non-homogeneous wave eqns.

$$\vec{\nabla} \times \vec{E} = -\dot{\vec{B}}$$

$$\vec{\nabla} \times \vec{H} = \vec{j} + \dot{\vec{D}}$$

$$\Rightarrow \Delta \vec{E} - \frac{1}{c^2} \frac{\partial^2 \vec{E}}{\partial t^2} = \mu_0 (\vec{j} + \dot{\vec{P}})$$

$$c = \frac{C_0}{n}, n = \sqrt{\epsilon}$$

time-dependent, homogeneous wave eqn.

$$\vec{j} = \vec{0}, \vec{P} = (\epsilon - 1) \epsilon_0 \vec{E}$$

$$\Rightarrow \Delta \vec{E} = \frac{1}{c^2} \frac{\partial^2 \vec{E}}{\partial t^2}$$

$$\Rightarrow \text{Solution: } \vec{E}(x, t) = \vec{E}_0 \cos(\vec{k} \cdot \vec{x} - \omega t) \quad \text{wave no. vector } \vec{k}, |k| = \frac{2\pi}{\lambda}$$

$$E = \frac{E_0}{r} \cos(kr - \omega t)$$

⑤ Optical Doppler effect

moving source
fix observer

$$f_o = f_s \frac{1 - \frac{v}{c}}{1 + \frac{v}{c}}$$

f_o - freq of the observed

f_s - freq when send



$$f_o = f_s \left(1 - \frac{v}{c}\right)$$

GPS (Global Positioning System)

- civil L1 - signal wave 1575,42 MHz

- Triangulation with several satellites

+ iGPS: transmitter rotates with unique freq ~~40-50 Hz~~, ~~fixed~~
fixed receiver

→ Application: large volume positioning

→ LiDAR (Light Detection and Ranging)

- Time-of-flight measurement principle $d = \frac{c \cdot t}{2}$

- Phase shift measurement principle : $d = \frac{\lambda_{\text{mod}} \cdot \phi}{4\pi}$
 (complex sensor design required)

- Application: Robot navigation (SLAM)
 Autonomous driving
 Geodesy

$$\phi = \tan^{-1} \left(\frac{s_0 - s_2}{s_1 - s_3} \right)$$

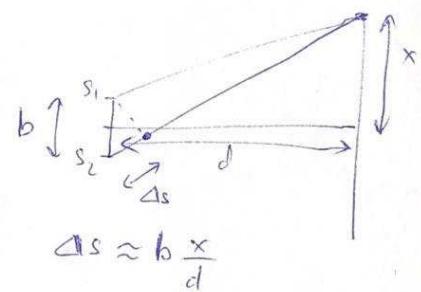
+ Wave properties: Interference

- Intensity $I = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos \delta$; $\delta = \varphi_2 - \varphi_1$

- Prequisites - constant phase
 - appropriate polarization (not perpendicular)

- Young - experiment:

$$\begin{aligned} \text{min intensity: } \Delta s &= \left(n + \frac{1}{2}\right) \lambda \quad n \in \mathbb{N} \\ \text{max } \Delta s &= n \lambda \end{aligned}$$



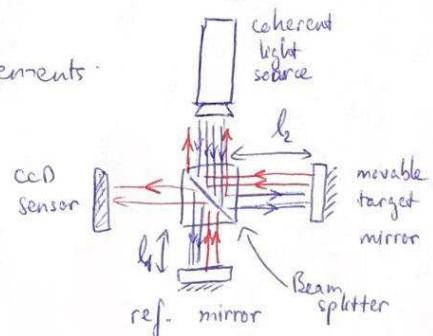
+ Interferometry for distance measurements:

- Michelson Interferometry $\Delta s = 2(l_1 - l_2)$

- At CCD sensor:

$$I = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos \delta, \quad \delta = \left(\frac{2\pi}{\lambda}\right) \cdot 2(l_2 - l_1)$$

$$I_1 = I_2 = \frac{I_0}{4}$$



+ Laser Tracker - range 30-70m
 - uncertainty 10 μm/m

highly accurate 6D position tracking

+ Laser Radar - freq. of signal modulated in range 100 GHz

3D scanning of parts environments - reflected signal is phase shift modulation of ref. signal

texture mapping

4) Electromagnetic waves for communication:

- Antenna: open oscillating circuit
- Electromagnetic (EM) waves enable wireless data transmission / communication

Thermoelectric & Ultrasonic Sensors

L6)

1) Thermoelectric Sensors

+ Heat transfer & Temperature Measurement:

for liquid, gas - Convection (Heat flux density) $j_q = \alpha \Delta T$

for solid - Conduction $j_q = -\lambda \nabla T$

- Heat radiation $P = A \sigma T^4$

+ General overview of instruments:

Mechanical Contact Thermometers	Electronic contact Thermometers	Radiation Thermometers
-200 - 630 °C	- 220 - 1500 °C	-100 - 3500 °C
<ul style="list-style-type: none"> - Liquid in glass thermometer - Bi metallic thermometers 	<ul style="list-style-type: none"> - Resistance thermo. - Metal resistance thermo. - Semi conductor resist. thermo. - Thermocouples 	<ul style="list-style-type: none"> - Radiation pyrometer - Thermography (infrared camera)

we will go into these
I by 1

+ Laws of Thermodynamics

+ Temperature scales : T_K, T_C, T_F
Kelvin, Celsius, Fahrenheit

$$T_C = T_K - 273,15$$

$$T_F = T_C \cdot 1,8 + 32$$

+ Liquid in glass Thermometers:

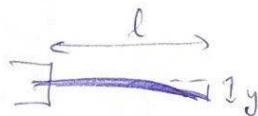
$$\Delta V = V_0 \cdot \beta \cdot \Delta T, S = \frac{dh}{dT} = \frac{V_0 \beta}{\pi r^2}$$

mercury range (-35, 300)
lower temp. \Rightarrow pentane
alcohol.

+ Bi metallic Thermometers [-50, 400°C]

$$y = \alpha \cdot \frac{l^2}{d} \Delta T$$

deflection coeff. /
 thickness



+ Resistance Thermometers. $R \uparrow$ as $T \uparrow$

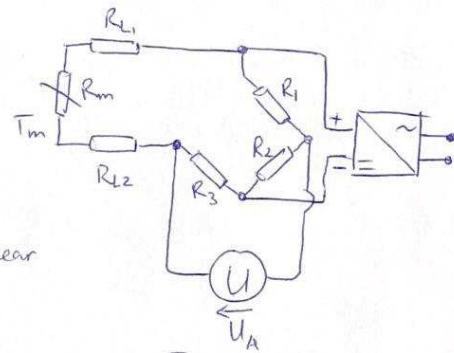
Platinum [-200, 850°C] (Pt)

{ NTC Thermistor (Negative temp coeff) . Silicon, zinc oxide }
PTC Thermistor (Positive _____) : Selenium } semi conductor resistance thermometer

With Wheatstone's Bridge

$$U_A \sim R_m + R_{L1} + R_{L2} - R_s$$

With Pt, resistance curve almost linear



+ Thermo couple:

Seebeck effect

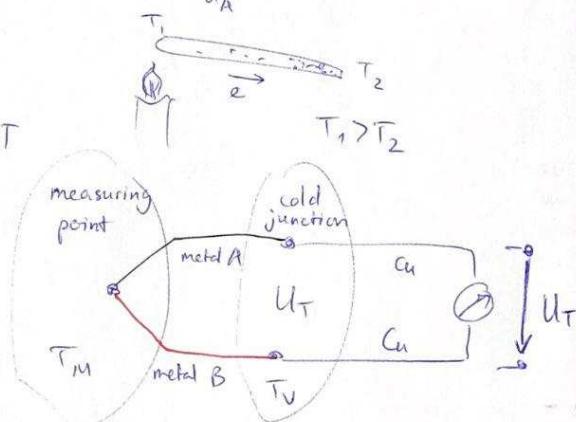
$$U_{\text{Seebeck}} = \alpha \cdot \Delta T$$

$$U_T = K_{A/\text{Pt}} \cdot (T_M - T_V) + K_{B/\text{Pt}} \cdot (T_V - T_M)$$

$$U_T = K_{AB} \cdot (T_M - T_V)$$

- Preferred thermo couples:

iron - constantan
nickel - chromium - nickel
platinum - rhodium - platinum



+ Radiation thermometers : infrared detection

Pyrometer | 1 spot

Thermography | an image

Mechanical Thermometer	Contact Thermometer	Electronic Thermometer	Contact Thermometer	Radiation Thermometer
Sensors				
Liquid in glass Thermometer	Bimetallic Thermometer	Resistance Thermometers	Thermocouple	Pyrometer
Temperature Range	$[-35, 300^\circ\text{C}]$	$[-50, 400^\circ\text{C}]$	$[-200, 850^\circ\text{C}]$	$[-100, 3000^\circ\text{C}]$
Pros	No additional equipment required Small uncertainty	Robust (shock vibration)	Versatile applicability High penetration rate Cheap Accurate Relatively accurate Small delay	Wider range Moving object
Cons	No remote measurement possible Limited accuracy Time delay to respond / contact	Passive sensor (Need power source)	Need cold junction compensation Active sensor	Very accurate Complex
Scope	Industrial temperature monitoring High temp monitoring Industry	Construction measurement	Precision measurement	Monitoring cables & pipeline

+)Quartz Thermometer:

- Resonance freq of quartz crystal depends on temp.
- Resolution: $10^{-3} \sim 10^{-6}$ K
- Complex

+)DTS (Distributed Temperature Sensing)

~~Pulse echo method~~

vs

through-transmission method

+)Fibre Bragg Grating

(+) one side accessibility

(-) pass through 2 times

must align sender & receiver
access from both sides

can't determine depth of defect

+)A-scan

\rightarrow {B-scan
C-scan

+)Noise Thermometer

2)Ultra sonic Sensors: waves as movement of matter

- Piezo electric effect

- Use AC current \Rightarrow deform a Piezo element

\rightarrow Measuring thickness...

- Velocity depends on temp., direction of wave, physical state, static pressure,...

+)Acoustic Impedance Z

$$Z = c \times \rho, \quad \rho: \text{density}$$

$$R = \frac{Z_2 - Z_1}{Z_2 + Z_1} \quad (\text{sound pressure reflection coeff.})$$

$$R^2 = Q = \frac{l_r}{l_o} \quad (\text{sound power reflection coeff.})$$

$$T = \frac{2Z_2}{Z_2 + Z_1} \quad (\text{transmission coeff.}) = 1 - Q$$

$$+)
$$S_{\text{vacuum}} = 0 \Rightarrow R_{\text{vacuum}} = 1 \Rightarrow \text{total reflection}$$$$

Machine Vision

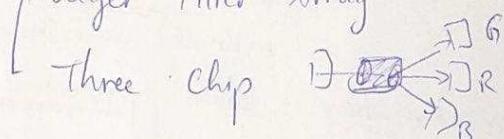
L7

1) Image Acquisition:

+ Sensor: photo bucket

- The pixel and data transfer architecture [CCD CMOS]

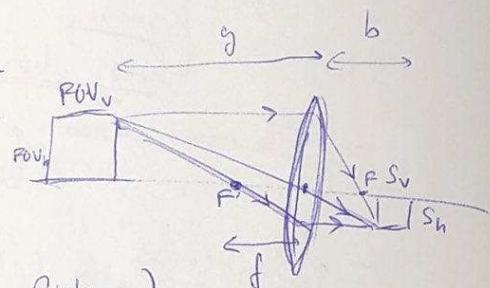
- Filter color with: [Color Filter Array]



- Image Resolution

FOV (Field of view)

$$\text{Image pixel size} = \frac{\text{FOV}}{\text{Pixel count}}$$



+ Optics: PMAG (Primary magnification)

- For desired FOV and WD (Working Distance)

$$M = \frac{S_h}{\text{FOV}_h} = \frac{b}{g}$$

M: magnification

$$\frac{1}{f} = \frac{1}{g} + \frac{1}{b}; f = \frac{g \cdot S_h}{\text{FOV}_h + S_h}$$

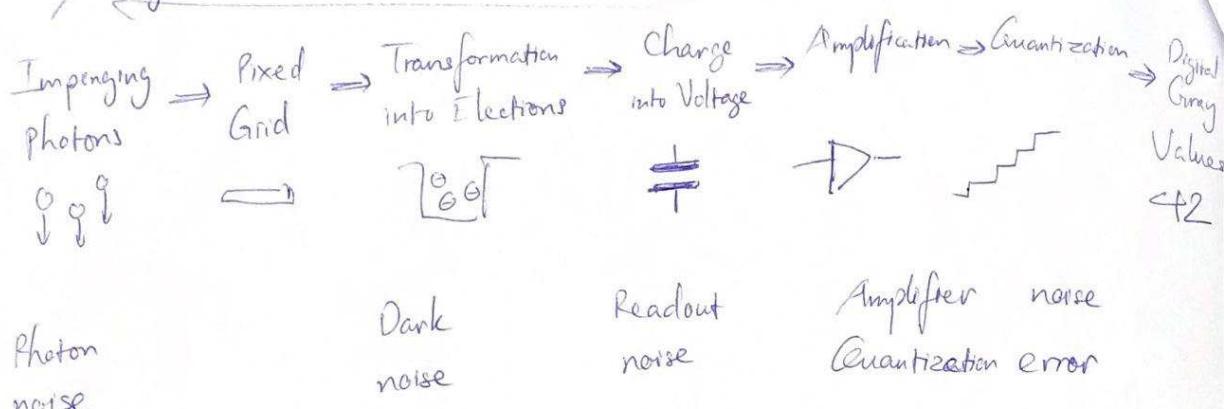
f: focal length

+ Lighting: cameras → algorithm can not compensate bad illumination
designed for imaging, not human-viewing

Techniques: Direct / Diffuse bright field illumination
Direct / ~~dark~~ field illumination

- (a) Direct / Diffuse back light
- Diffuse light
- Structured illumination
- On-axis illumination
- Collimated illumination

+> Physical Model & Noise Sources:



+> Interference and Mitigation measures:

CHEVB

- > Vibration:
 - { reduce exposure time
 - utilize clamping system
 - multiple inspection with image averaging
- > Contamination:
 - utilize { protective housing
 - air curtains, cleaning with compressed air
- > Heat:
 - increase working distance / use endoscopy
 - { cooling
 - heat-absorbing filter disks
- > Electromagnetism:
 - { shielding, fiber glass cable
 - use suitable signal conditioning
- > Brightness:
 - { flash controllers
 - mitigate ambient light
 - triggering of lighting through camera

2) Image Processing:

+> Machine Vision Software:

+ General Machine Vision Algorithms:

- Geometric manipulation: shift shifting, rotating, sampling . .
- Content statistics: image histogram, thresholding . .
- Image enhancement : reduce noise , better contrast
- Connectivity : extraction & analyse of 2D shapes
- Edge detection:
- Correlation: model vs template
- Geometric search: locates features within an image
- OCR / OCV : optical character recognition / verification
- Convolution & Spatial Filter
- Canny Edge detector
- Hough transform

3) Integration & Application:

+ Classic Image Processing

Pros

- + Rule-based feature extraction
- + Explicit relationship between input data and features

Cons

- Expert / domain knowledge necessary
- Mathematical formulation not always possible or very elaborate
- A priori knowledge of features to be extracted necessary

Machine Learning

- + Implicit feature extraction
- + Unsupervised learning of data distribution
- + Few process knowledge needed for modelling
- + Simple integration of further process data

- Extracted features typically not interpretable
- Data annotation (time consuming costly)

Data Acquisition & Sensor Fusion

L8)

Sensors within a Data Acquisition System and Signal Processing

→ Definition:

$\begin{cases} \text{Stimulus} \\ \text{Transducer: one type energy} \rightarrow \text{another} \\ \text{Sensor:} \end{cases}$
 electrical signal

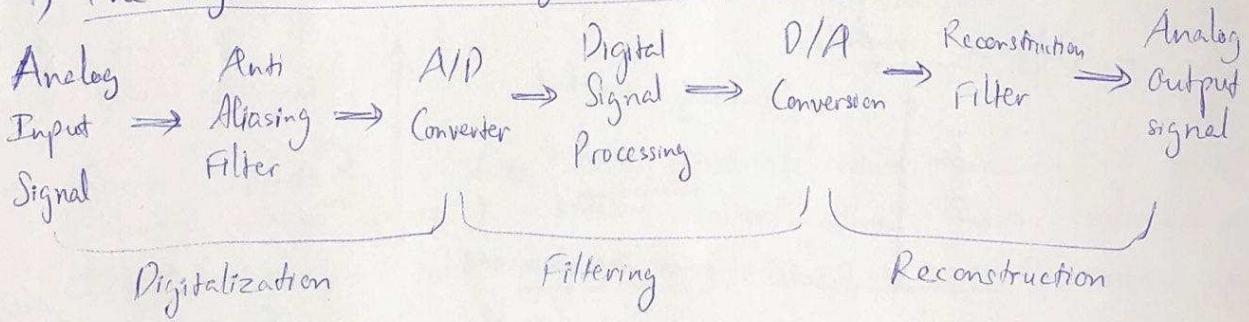
- Sensor includes transducer(s)

→ Classification:

$\begin{cases} \text{sensors} \\ \text{direct vs hybrid (one or more transducer)} \end{cases}$

$\begin{cases} \text{contact (directly positioned on or inside object) vs noncontact} \\ \text{active (require energy supply) vs passive} \end{cases}$

→ The signal chain in digital signal processing



→ Sampling: time-continuous → discrete signal

Quantization: continuous-value signal → series of discrete-value signals

Encoding: discrete value and time signal → another digital (binary digital)

→ Ideal Sampling

narrow Dirac impulse

vs

Realistic Sampling

mean signal value over sampling duration

- Shannon - Nyquist sampling theorem:
Sampling freq must \geq 2x max freq.
- Anti - aliasing : analog low-pass filter



+ Quantization:

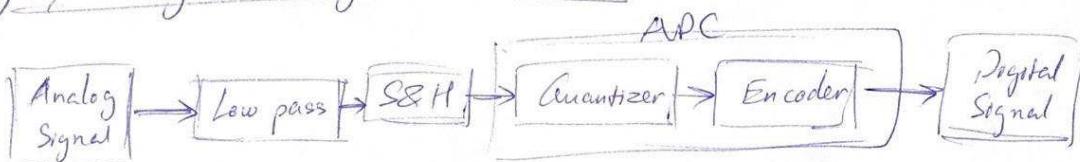
- equivalent to a rounding operation
- rounding is a irreversible process
- subject to quantization error/noise

Signal-to-noise ratio (SNR) $SNR_{dB} = 20 \cdot \log_{10}(2^n)$

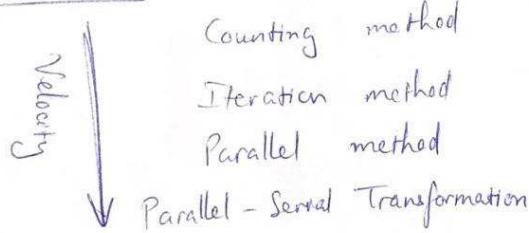
+ Binary encoding:

- # decision thresholds $L = 2^B - 1$
- robust in transmission

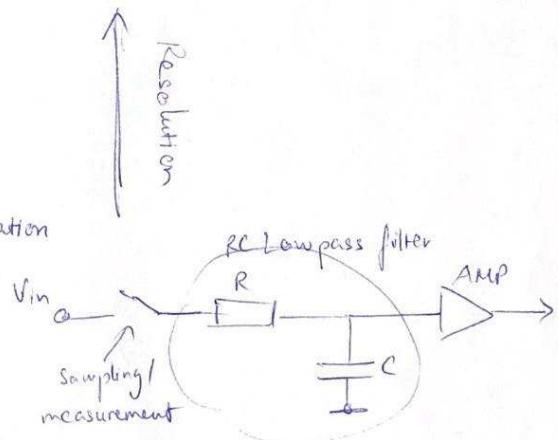
2) Analog-to-digital Converters



+ Different methods:



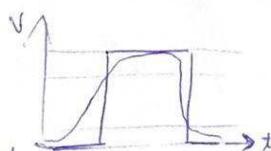
+ Sample and Hold:



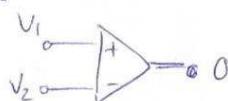
+ Schmitt trigger

remove noise

well-defined level of signal



- Analog Comparator



1 if $V_1 > V_2$
else 0

when input is between
2 levels \rightarrow retain its value
(hysteresis)

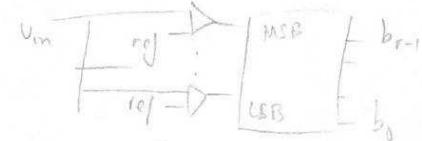
- V/F converter (Voltage-to-freq converter)

$$f_{\text{out}} \propto V_{\text{in}} : f_{\text{out}} = \frac{V_{\text{in}}}{R_{\text{in}}} \cdot \frac{1}{t_{\text{os}}}$$

- PWM converter :

$$\text{pulse duration } t_{\text{PWM}} \propto V_{\text{in}} : D = \frac{t_{\text{PWM}}}{T_0} = k \cdot V_{\text{in}}$$

- Flash converter



- SAC converter (Successive-approximation converter)

3) Encoding & digital-to-analog converters

Input signal

↓
Source encoding → Channel encoding → Line encoding

Disturbance

Source decoding ← Channel decoding ← Line decoding ←

↓
Transmitted signal

- Source encoding : = data compression (reduce amount of data)
(discretize, quantize, compress...) ⇒ allow faster transmission
- Channel encoding : add redundant data, protect against transmission errors
- Line encoding : how data is transferred to binary signal

4) Line encoding

- encoded signals are analog transmitted via TTL (Transistor-to-Logic)
0 vs 1 is less susceptible to interference as continuous analog signals
each environment will influence the signal in different ways
→ thus we have different coding scheme

Binary line code

RZ (Return to Zero) code

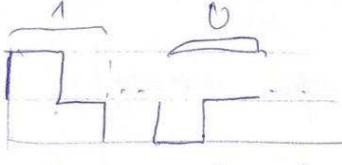
NRZ (Non Return to Zero) code

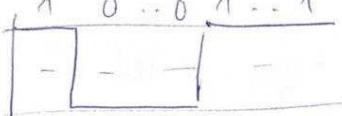
Block code

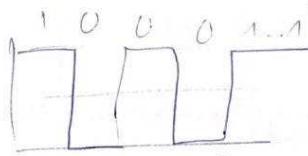
Manchester coding

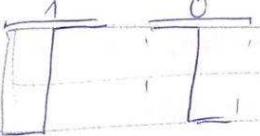
4B5B

Mobifid Monitored Sun 93 (MMS93) ↗

- RZ
 

need 3 states
return to neutral state between pulse
self synchronizing
half data rate
- NRZ
 

no neutral state
needs synchronization
capacitive problem
full data rate
- Differential NRZ
 

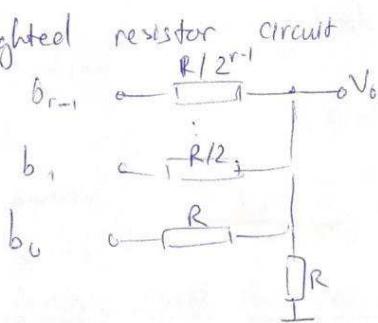
0: level change vs 1: no level change
full data rate
no prob. for long sequences of 0s
- Manchester code
 

no neutral state
self synchronization
no capacitive prob
half data rate

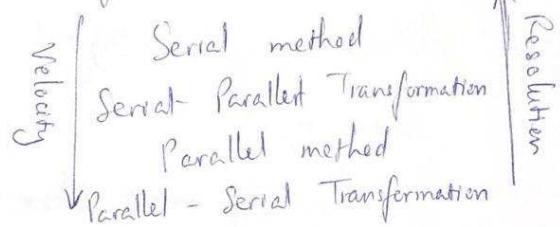
+)DAC

- PWM

- Binary weighted



$$V_o = V_{ref} \cdot \sum_{i=1}^r \frac{1}{2^i} b_{r-i}$$



4) Sensor fusion techniques:

+)Definition: combining sensory data → better than each individual sensor.

+)Motivation: sensor deprivation, limited spatial / temporal coverage
imprecision, uncertainty

Complementary fusion
not directly depend on other
→ resolve incompleteness
robot skin & overhead camera

Competitive fusion
independent, same property
→ fault tolerance, robustness
indoor GPS & odometry

Cooperative fusion
Be independent sensors
→ info that not available from 1
Stereo-camera

Signal Preprocessing

Filtration & noise removal

Lg/

1) Motivation

- Main / raw signal is mixed with unwanted interfering signal → filtering
- How can noise be described & ideally attenuated → noise removal
- Extract relevant characteristics of signal for the task → signal feature extraction

2) Signal Filtering

+ Purpose : - separate useful / relevant signal } improve signal quality
 - attenuate unwanted part }

+ Types

- Passive filters without power supply
 just passive elements such as capacitors, coils, resistors, crystals
- Analog filters time continuous
 components: [passive active]

vs

vs

vs

Active Filters

require external power supply
 also active elements
 (amplifiers / transistors)

Digital filters

time discrete

logic components / processors
 (adder, multiplier, time lags)

④ Analog filters

+ Passive filters

high quality requires high effort

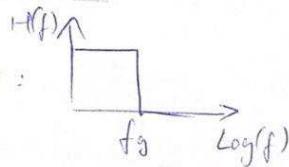


Active filters

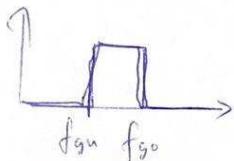
high quality factor
amplification

≠ Ideal filters:

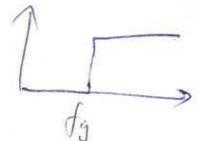
- Low pass:
(speaker)



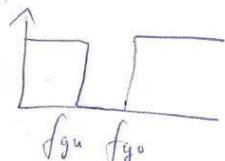
- Bandpass:
(Microphone)



- High pass:
(pedometer)
sudden events

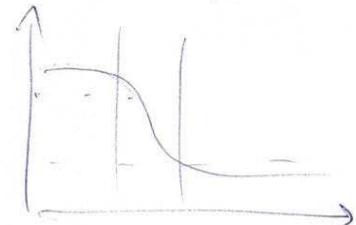


- Bandstop:
(net hum)

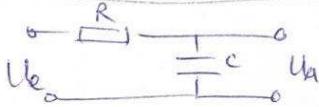


+ Real filters:

- pass band
- filter attenuation band
- transition band
- phase angle φ_f



Passive 1st order low pass filter



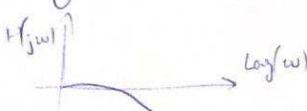
$$H(j\omega) = \frac{1}{1 + j\omega RC} = \frac{1}{1 + (\omega RC)^2} - j \frac{\omega RC}{1 + (\omega RC)^2}$$

$$A = |H| = \frac{1}{\sqrt{1 + \omega^2 R^2 C^2}}$$

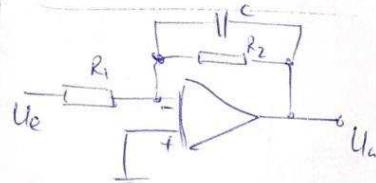
$$\omega_g = \frac{1}{RC}$$

$$\varphi_p = -\arctan(\omega RC)$$

$$\omega = \omega_0 \xrightarrow{\text{---}} \omega = 0$$

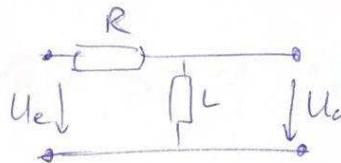


Active low-pass filter

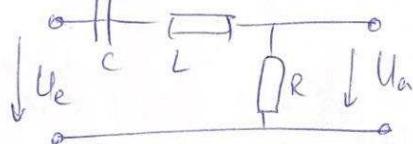


$$H(j\omega) = -\frac{R_2}{R_1} \cdot \frac{1}{1 + j\omega R_2 C} = -\frac{R_2}{R_1} \cdot \frac{1}{1 + (\omega R_2 C)^2} + j \frac{R_2}{R_1} \cdot \frac{\omega R_2 C}{1 + (\omega R_2 C)^2}$$

→ High pass



→ → Band pass



$$H(\omega) = \frac{j\omega RC}{1 + j\omega RC - \omega^2 LC}$$

⊗ Digital filters

input 10011000 . . .
output 0110011 . . .

- Higher reproducibility, precision, flexibility, robustness to word size disturbances

→ IIR (Infinite Impulse Response Filter)

- Feedback might cause instabilities

$$y(n) = \sum_{k=0}^M b_k \cdot x(n-k) + \sum_{l=1}^N a_l y(n-l)$$

→ FIR (Finite Impulse Response) Filter

- Never unstable

$$y(n) = \sum_{k=0}^M b_k \cdot x(n-k)$$

3) Noise

- Signal
+
Intrinsic noise

⇒

Sensor

+

Electronics noise

- Stationary noise
fixed probability distribution

vs Non-stationary noise
time-varying distribution

+) Some distribution :

- Normal / Gauss
- Uniform
- Maxwell
- Poisson

+) - Mean : $E(X) = \mu = \sum x_i p_i = \int x \cdot p(x) dx$

- Variance : $\text{Var}(X) = \sigma_x^2 = E(X^2) - (E(X))^2$
 $= \sum (x_i - E(X))^2 p(x_i)$
 $= \int (x - E(X))^2 p(x) dx$

- Standard deviation : $\sigma_x = \sqrt{\text{Var}(X)}$

- Properties : $\text{Var}(ax + b) = a^2 \text{Var}(x)$

$\text{Var}(x+y) = \text{Var}(x) + \text{Var}(y) - 2 \cdot \text{Cov}(x, y)$

$\text{Cov}(x, y) = E(xy) - E(x) \cdot E(y)$

(= 0 if x, y not correlated)

② +) Correlation integral : whether 2 signals are correlated

$$\rho(\tau) = K \int s(t) m(t+\tau) dt$$

→ $s(t)$ signal func

$m(t)$ reference signal

$$K = \begin{cases} 1 & \text{non-periodic signals} \\ \frac{1}{2T} & \text{random integrals} \\ \lim_{t \rightarrow \infty} 1/2T & \end{cases}$$

- Auto correlation $m(t) = s(t)$

- (usual integral) $m(t) = 1$

7) Description & Detection of Noise

- Power spectral density $S(\omega)$

$$S(\omega) = \langle F_x(\omega)^2 \rangle = \langle F_x(\omega) F_x^*(\omega) \rangle$$

- Power spectrum

$$S_{xx}(\omega) = \frac{1}{2\pi} \int_{-\infty}^{\infty} r_{xx}(t) \cdot e^{-i\omega t} dt, \quad r_{xx}(t) = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} f(\tau) f(\tau+t) d\tau$$

- White noise $\frac{d S_{xx}(\omega)}{d\omega} = \text{const}$

Colored noise $\frac{d S_{xx}(\omega)}{d\omega} \neq \text{const}$, if

$$\begin{aligned} &\propto \frac{1}{f} \Rightarrow \text{"pink noise"} \\ &\propto \frac{1}{f^2} \Rightarrow \text{"red noise"} \end{aligned}$$

8) Signal extraction techniques

- strategies depend on noise type
- some are unavoidable

Bandpass require a priori knowledge

Lock-in amplification use reference signal

→ Sensor fusion : Kalman- Filter

- Prediction stage: $\hat{x}_k^- = F \hat{x}_{k-1}^+ + B u_{k-1}$

$$P_k^- = F P_{k-1}^+ F^T + Q$$

- Correction stage $\tilde{z}_k = y_k - H \hat{x}_k^-$
 $K_k = P_k^- H^T (R + H P_k^- H^T)^{-1}$

$$\hat{x}_k^+ = \hat{x}_k^- + K_k \tilde{z}_k$$

$$P_k^+ = (I - K_k H) P_k^-$$

→ RMS (Root Mean Square) to calculate power

$$RMS = \sqrt{\frac{1}{t_2 - t_1} \int_{t_1}^{t_2} f^2(t) dt}$$

$$\Rightarrow SNR \text{ (Signal to Noise Ratio)} = \frac{P_{\text{signal}}}{P_{\text{noise}}} = \frac{RMS_{\text{signal}}^2}{RMS_{\text{noise}}^2}$$

$$= 20 \log_{10} \frac{RMS_{\text{signal}}}{RMS_{\text{noise}}}$$

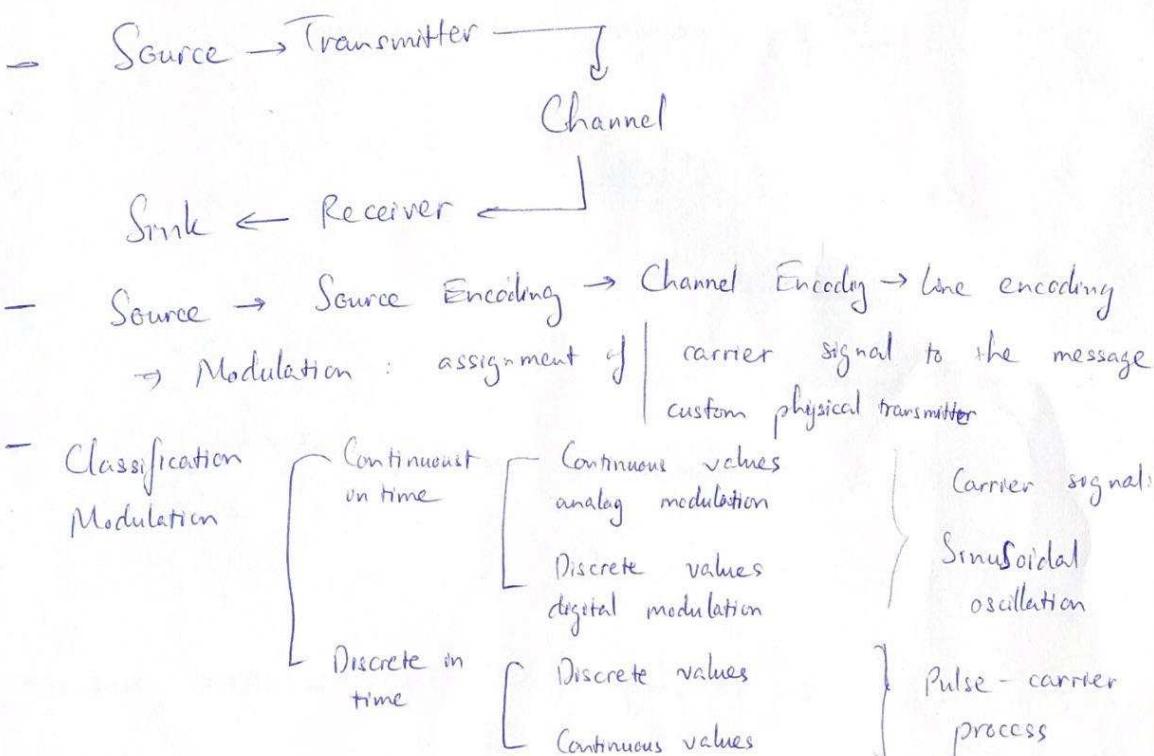
Communication & Signal Transmission

40)

1) Challenges in data transmission:

- Different forms (text, speech, pics..)
- Large distances, limited time
- Certain bandwidth

2) Information Systems & Data Transmission principles



3) Amplitude Modulation (AM)

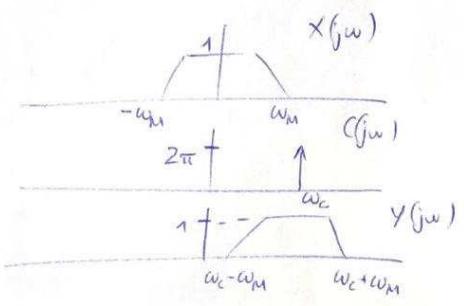
- AM using complex exponential carrier

$$c(t) = e^{j(\omega_c t + \theta_c)}$$

$$\text{If } \theta_c = 0 \Rightarrow y(t) = x(t) \cdot e^{j\omega_c t}$$

$$Y(j\omega) = X(j\omega - j\omega_c)$$

$$C(j\omega) = 2\pi \delta(\omega - \omega_c)$$



- Sinusoidal carrier: $c(t) = \cos(\omega_c t + \theta_c)$
 - If $\theta_c = 0 \Rightarrow C(j\omega) = \pi [\delta(\omega - \omega_c) + \delta(\omega + \omega_c)]$
 - $Y(j\omega) = \frac{1}{2} [X(j\omega - j\omega_c) + X(j\omega + j\omega_c)]$
- Synchronous Demodulation of AM signals: $w(t) = y(t) \cdot \cos(\omega_c t)$
 $= \frac{1}{2} x(t) + \frac{1}{2} x(t) \cos(2\omega_c t)$
 \Rightarrow low pass filter for $\frac{1}{2} x(t)$

- Asynchronous demodulation of AM: envelope detector
- Multiplexing
- Single-side band AM: $H(j\omega) = \begin{cases} -j & \omega > 0 \\ +j & \omega < 0 \\ 0 & \omega = 0 \end{cases}$
- + Frequency Modulation (FM)
 - Require larger band width
 - Not linear
 - More effort required to be analyzed

3) Transmission Media

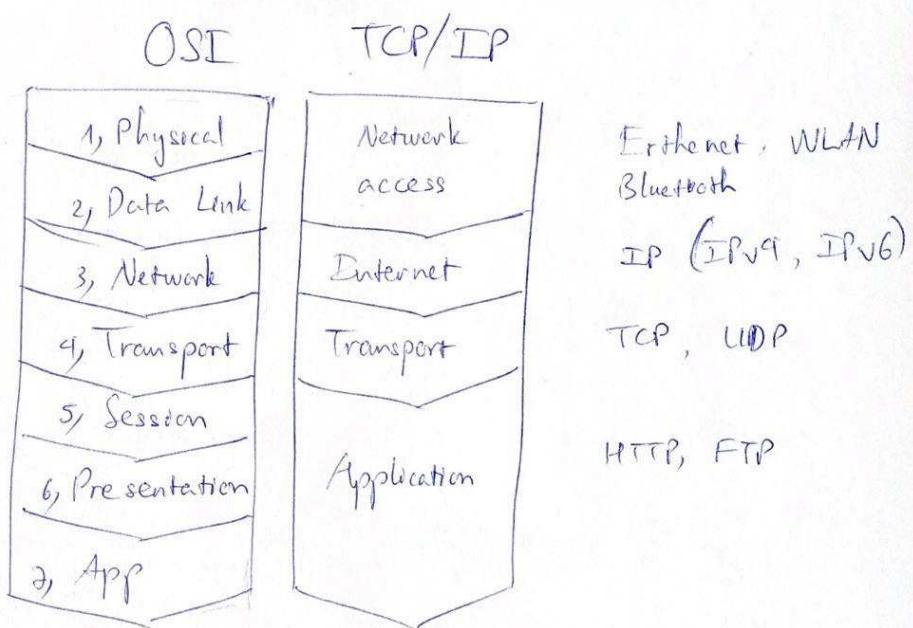
- Cablebased Transmission
- Wireless: Antenna
- Mobile communications standards
- 5G

4) Network topologies & data transmission protocols

⊕ Topologies: - P2P

- Bus
- Field buses

⊗ Protocols



5) Robot communication with ROS

- Publisher node — subscriber node
- ROS messages

\Rightarrow AM using complex exponential carrier

$$c(t) = e^{j(\omega_c t + \theta_c)}$$

$$y(t) = x(t) \cdot c(t)$$

$$- \text{ If } \theta_c = 0 \Rightarrow y(t) = x(t) \cdot e^{j\omega_c t} \Rightarrow x(t) = y(t) e^{-j\omega_c t}$$

$$- C(j\omega) = 2\pi \delta(\omega - \omega_c)$$

$$Y(j\omega) = X(j(\omega - \omega_c))$$

\Rightarrow AM using sinusoidal carrier signal.

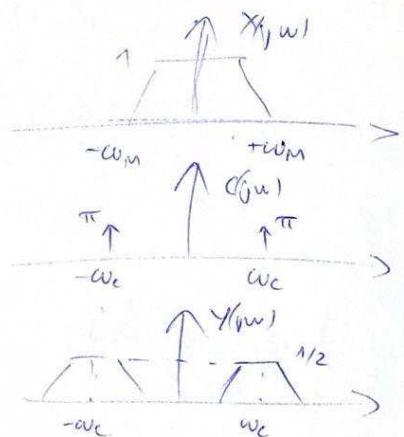
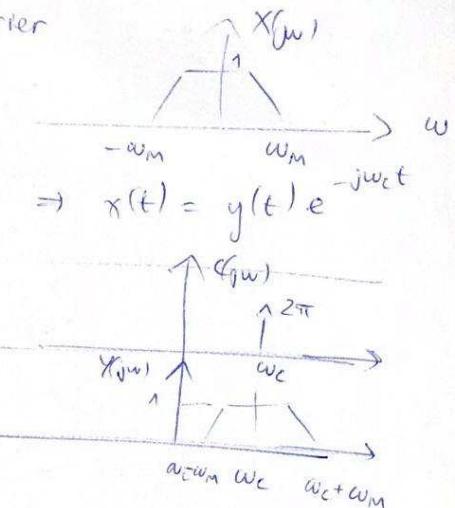
$$c(t) = \cos(\omega_c t + \theta_c)$$

$$- \text{ If } \theta_c = 0 \Rightarrow y(t) = x(t) \cdot \cos(\omega_c t)$$

$$- C(j\omega) = \pi [\delta(\omega - \omega_c) + \delta(\omega + \omega_c)]$$

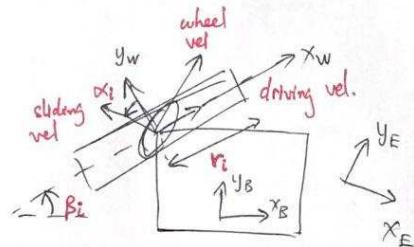
$$Y(j\omega) = \frac{1}{2} [X(j(\omega - \omega_c)) + X(j(\omega + \omega_c))]$$

$\omega_c > \omega_m$, else leads to overlap



RSS Formulas

$$3) u_i = \frac{1}{r_i} [1 + \tan \alpha_i] \begin{bmatrix} c\beta_i & s\beta_i \\ -s\beta_i & c\beta_i \end{bmatrix} \begin{bmatrix} -p_{y,i} & 1 & 0 \\ p_{x,i} & 0 & 1 \end{bmatrix} \begin{bmatrix} \omega_z \\ v_x \\ v_y \end{bmatrix} = H_i \downarrow$$



$$1 \rightarrow 2: {}^1T_2 \text{ (2 in coord. 1)} \quad {}^B T_w \quad {}^w T_{v_B} \quad {}^z v_B$$

$$3) \text{ Gauss law } \Phi_E = \oint \vec{E} d\vec{A} = \frac{Q_{\text{enc}}}{\epsilon_0}; \quad \vec{D} = \epsilon \vec{E}, \quad \vec{\nabla} \cdot \vec{E} = \frac{Q}{\epsilon_0}, \quad \vec{\nabla} \cdot \vec{D} = \rho$$

$$\Phi_B = \oint \vec{B} d\vec{A} = 0; \quad \vec{H} = \frac{\vec{B}}{\mu_0}, \quad \vec{\nabla} \cdot \vec{B} = 0 \text{ (div)}$$

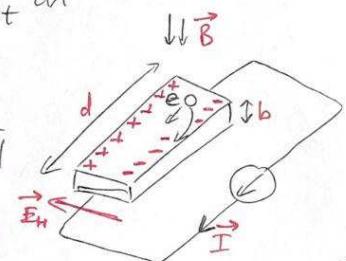
$$\text{MF} \quad \vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \text{ (curl)}, \quad \oint \vec{E} ds = - \iint \frac{\partial \vec{B}}{\partial t} dA$$

$$\text{Ampere circuit law} \quad \vec{\nabla} \times \vec{H} = \vec{j} + \frac{\partial \vec{D}}{\partial t}, \quad \oint \vec{H} ds = \iint j dA + \iint \frac{\partial D}{\partial t} dA$$

$$\text{Lorentz force} \quad \vec{F} = q \vec{v} \times \vec{B} = \vec{I} \vec{B} l$$

$$\text{Hall effect:} \quad q \vec{E}_H = q \vec{v} \times \vec{B} = q \frac{\vec{U}_H}{d}, \quad \vec{V}_0 = \frac{1}{nq} \cdot \frac{\vec{I}}{b \cdot d}$$

$$U_H = \vec{J}_0 \cdot \vec{B} d = \frac{\vec{I}}{nq} \cdot \frac{\vec{B}}{b} = R_H \cdot \frac{\vec{I} \cdot \vec{B}}{b}$$



$$4) C = \frac{\epsilon_0 \epsilon_r A}{d} \quad \text{shape A}; \quad \frac{2\pi \epsilon_0 \epsilon_r l}{ln \frac{D}{d}} \quad ; \quad \frac{\pi \epsilon_0 \epsilon_r l}{ln \frac{s}{r_0}} \quad s \gg r_0$$

$$Q = d \cdot F = Q_A \cdot U_A \Rightarrow U_A = \frac{d \cdot F}{C_A} \quad (\text{d - piezo coeff.})$$

$$C = R \cdot C \Rightarrow U(t) = U_0 \cdot e^{-t/\tau}$$

$$Q_x = d_{11} \cdot F_x, \quad Q_y = d_{12} \frac{l_y}{l_x} F_y, \quad d_{12} = -d_{21}$$

longitudinal transversal

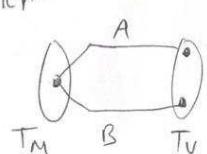
$$5) c_0 = f \cdot \lambda, \quad c_0 = 3 \cdot 10^8 \text{ m/s} \approx 1,07 \cdot 10^8 \text{ km/h} \quad E_\lambda = h \cdot f = h \cdot \frac{c}{\lambda}, \quad h \text{ Planck const.}$$

$$f_{\text{obs}} = \frac{f_{\text{send}}}{1 - \frac{v}{c}} \text{ (seur} \leftrightarrow), \quad f_{\text{obs}} = f_{\text{send}} \left(1 - \frac{v}{c}\right) \text{ (obs} \leftrightarrow)$$

$$I = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos \delta, \quad \delta = \varphi_2 - \varphi_1$$

$$6) \Delta V = V_0 \cdot \beta \cdot \Delta T, \quad S = \frac{dh}{dT} = \frac{V_0 \beta}{\pi r^2} \quad ; \quad y = \alpha \frac{l^2}{d} \Delta T$$

$$U_T = K_A / \rho_f (T_M - T_V) + K_B / \rho_f (T_V - T_M) = K_{AB} (T_M - T_V)$$

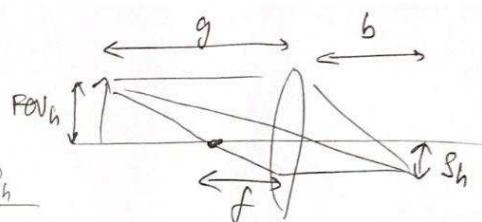


$$Z = \frac{C_p}{C_f}, \quad R = \frac{Z_2 - Z_1}{Z_2 + Z_1} \Rightarrow R^2 = \rho = \frac{l}{l_V}$$

$$T = \frac{1}{1 - R^2}$$

$$\Rightarrow M = \frac{S_h}{FOV_h} = \frac{b}{g}$$

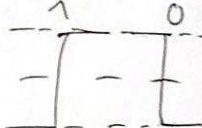
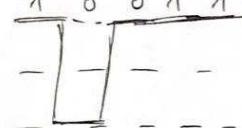
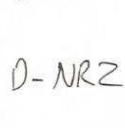
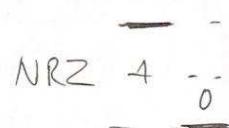
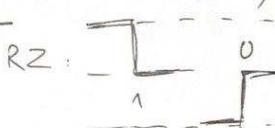
$$\frac{1}{f} = \frac{1}{b} + \frac{1}{g} \Rightarrow f = \frac{g \cdot S_h}{FOV_h + S_h}$$



$$r = x \cdot \cos\theta + y \cdot \sin\theta$$

$$g(x, y) = \sum_{s=-a}^a \sum_{t=-b}^b w(s, t) \cdot f(x+s, y+t)$$

$$8) L = 2^B - 1 ; SNR_{dB} = 20 \cdot \log_2(2^n), n: \# \text{Nb. bits}$$



$$V_o = V_{ref} \sum_{i=1}^r \frac{1}{2^i} b_{r-i}$$

$$9) w_c \Leftrightarrow A = \frac{1}{\sqrt{2}}$$

$$\text{FIR: } y(n) = \sum_{k=0}^M b_k x(n-k)$$

$$r_{xx}(\infty) = K \int s(t) \cdot s(t+\infty) dt .$$

$$r_{xx}(\infty) = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T s(t) s(t+\infty) dt \quad \text{auto correlation}$$

$$p(\infty) = K \int s(t) m(t+\infty) dt$$

cross-corr.

$$K = \begin{cases} 1 & \text{non-perfective} \\ \frac{1}{2T} & \text{random} \\ \lim_{T \rightarrow \infty} \frac{1}{2T} & \end{cases}$$

$$10) c(t) = e^{j(w_c t + \theta_c)}$$

$$y(t) = x(t) \cdot c(t)$$

$$C(j\omega) = 2\pi \cdot \delta(\omega - \omega_c)$$

$$Y(j\omega) = X(j\omega - j\omega_c)$$

$$c(t) = \cos(\omega_c t + \theta_c)$$

$$y(t) = x(t) \cdot \cos(\omega_c t)$$

$$C(j\omega) = \pi [\delta(\omega - \omega_c) + \delta(\omega + \omega_c)]$$

$$Y(j\omega) = \frac{1}{2} [X(j\omega - j\omega_c) + X(j\omega + j\omega_c)]$$

Ng Flue Dac