

**MEEN 646 – Aerothermodynamics of Turbomachinery**

**Module IV:**  
**Design of Radial Compressor**  
**Part 1: Aero-Thermo Analysis**

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## I. Introduction

This module provides a preliminary design for a single stage radial compressor. Using aerodynamic and thermodynamic analysis, the effect of mass flow rate is noted on the inlet and outlet angles, power and on dimensionless coefficients. Matlab code is used to plot the variation of these parameters. These calculations provide design ground for 3D design of compressor components, which will be addressed in part 2 of this module.

## II. Aero Thermo Design

### 1. Given parameters

Table 1: Design Parameters

$\dot{m}_D$ (Design mass flow rate)	3.5 kg/s
$T_{in}$ (Inlet temperature)	300 K
$P_{01}$ (Inlet total pressure)	1 bar
$\pi_{ref}$ (Reference pressure ratio)	3.0
$\omega$ (Angular velocity)	5000
$(\eta_{is})_{Design}$ (Design efficiency)	0.86
$D_{m2}$ (Inlet mean diameter)	160 mm
$D_3$ (Exit diameter)	240 mm
$B_{h2}$ (Inlet blade height)	100 mm
$B_{h3}$ (Outlet blade height)	40 mm
$\alpha_2$ (Absolute inlet flow angle)	90°
$\beta_3$ (Relative exit angle)	90°

The intention of this analysis is to study the effect of flow rate on performance for a given  $\omega$  for different mass flow rates. Flow rate was varied from 2.5-4.5 kg/s. Efficiency was modelled using the following model.

$$a_0 = -0.3844, a_1 = 3.0222, a_2 = -1.7778$$
$$\eta_{is} = a_0 + a_1 \left( \frac{\dot{m}}{\dot{m}_D} \right) + a_2 \left( \frac{\dot{m}}{\dot{m}_D} \right)^2, \quad \pi = \eta_{is} * \pi_{ref}$$

## 2. Schematic of Radial Compressor

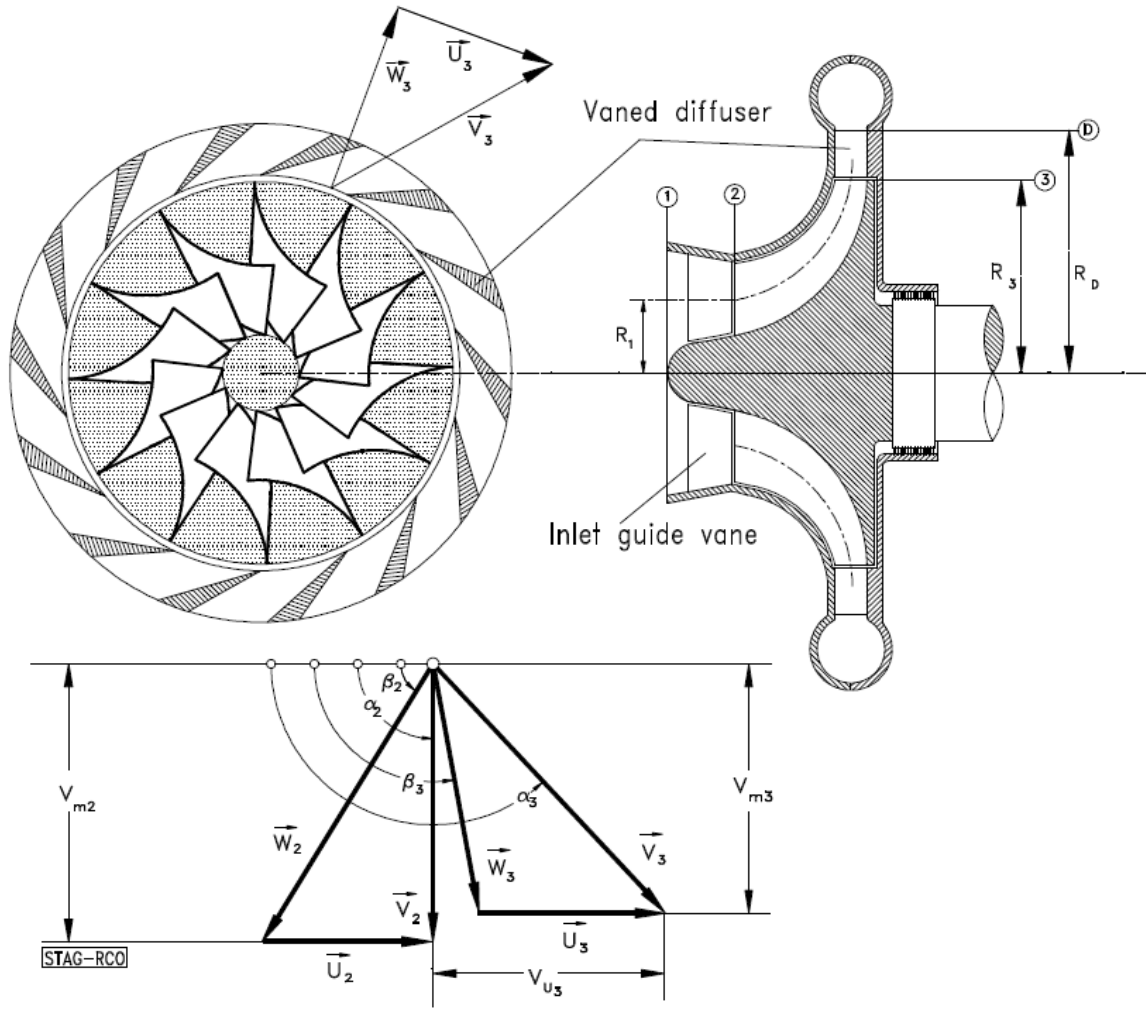


Figure 1: Schematic of Radial Compressor

## 3. Equations

### a. Inlet parameters

$$P_{02} = P_2 + \frac{V_2^2 \rho_2}{2}$$

$$\rho_2 = \frac{P_2}{RT_2}$$

$$V_2 = \frac{\dot{m}}{\rho_2 A_2} = \frac{\dot{m}}{\rho_2 * \pi / 4 * [(D_{m2} + B_{h2})^2 - (D_{m2} - B_{h2})^2]}$$

$$P_2 = \rho_2 RT_2$$

### b. Outlet parameters

$$P_3 = P_2 \pi$$

$$T_{3s} = T_2 (\pi)^{\frac{k-1}{k}}$$

$$T_3 = T_2 + \frac{T_{3s} - T_2}{\eta_{is}}$$

$$\rho_3 = \frac{P_3}{RT_3}$$

$$W_3 = \frac{\dot{m}}{\rho_3 A_3}$$

c. Velocity calculations

$$V_3 = \sqrt{W_3^2 + U_3^2}$$

$$W_2 = \sqrt{V_2^2 + U_2^2}$$

$$\alpha_3 = 90 + \tan^{-1} \left( \frac{U_3}{W_3} \right)$$

$$\beta_2 = \tan^{-1} \left( \frac{V_2}{U_2} \right)$$

$$\phi = \frac{W_3}{U_3}$$

d. Power calculation

$$Power = \dot{m} * (c_p(T_3 - T_2)) + \frac{V_3^2 - V_2^2}{2}$$

## 4. Results

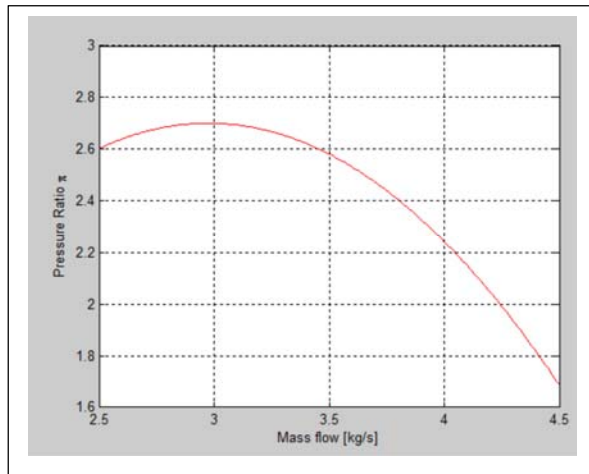


Figure 2: Pressure Ratio vs Mass Flow

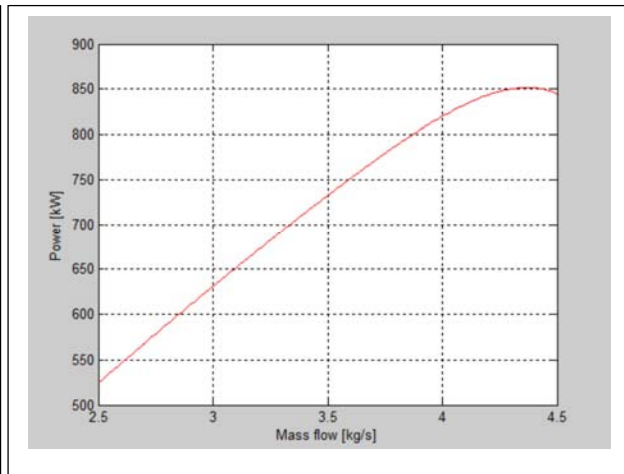


Figure 3: Power vs Mass Flow

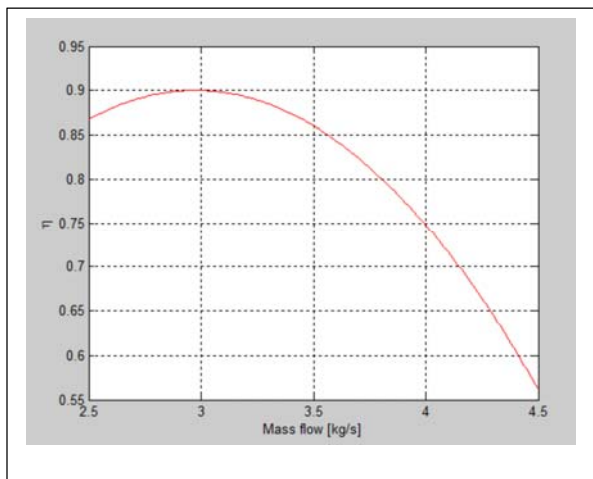


Figure 4: Efficiency vs Mass Flow

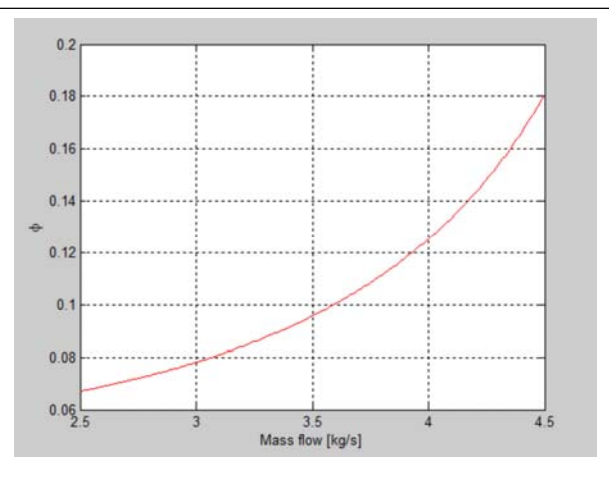


Figure 5: Flow Coefficient vs Mass Flow

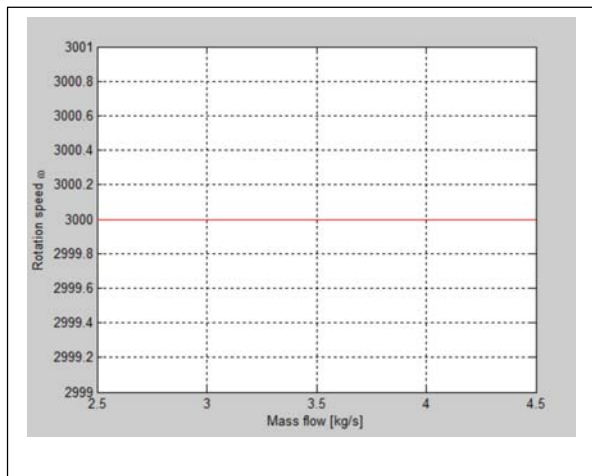


Figure 7: Rotation Speed vs Mass Flow

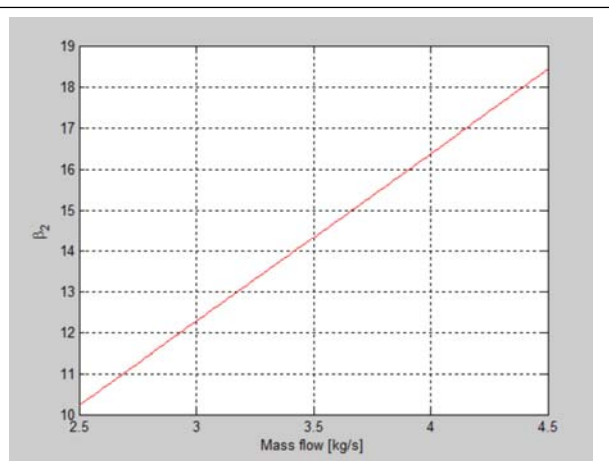


Figure 6: Beta2 vs Mass Flow

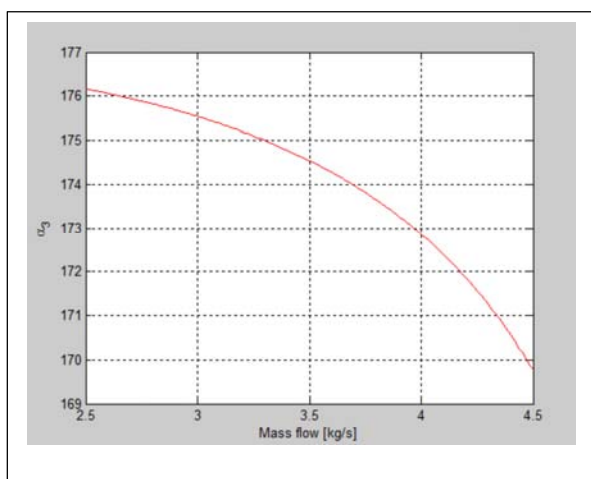


Figure 9: Alpha3 vs Mass Flow

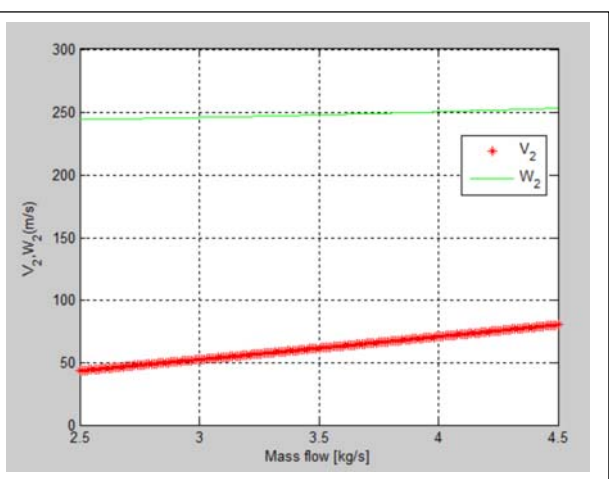


Figure 8: Inlet Velocity vs Mass Flow

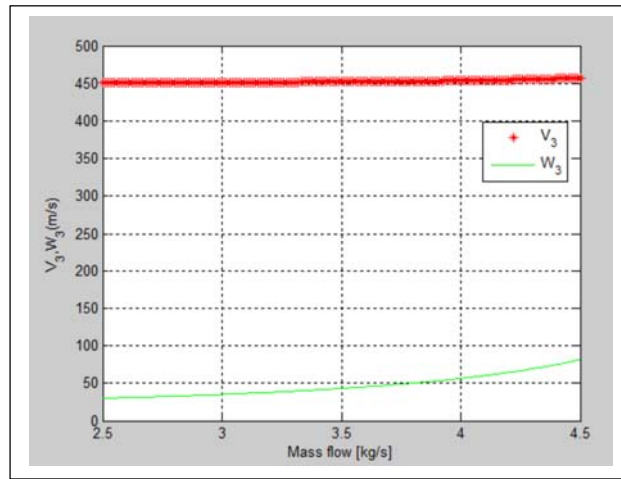


Figure 10: Outlet Velocity vs Mass Flow

## 5. Table of Design Parameters

Table 2: Complete Design Parameters

Mass flow rate	$\dot{m}_D$	3.5	kg/s
Inlet temperature	$T_2$	300	K
Inlet pressure	$P_2$	97,867	Pa
Outlet temperature	$T_3$	408	K
Outlet pressure	$P_3$	252,500	Pa
Pressure ratio	$\pi$	2.58	
Angular velocity	$\omega$	3,000	Rad/s
Design efficiency	$(\eta_{is})_{Design}$	0.86	
Inlet mean diameter	$D_{m2}$	160	mm
Exit diameter	$D_3$	300	mm
Inlet blade height	$B_{h2}$	100	mm
Outlet blade height	$B_{h3}$	40	mm
Absolute inlet flow angle	$\alpha_2$	90	deg
Relative inlet flow angle	$\beta_2$	14.3	deg
Absolute exit angle	$\alpha_3$	174.5	deg
Relative exit angle	$\beta_3$	90	deg
Flow coefficient	$\phi$	0.0957	
Absolute inlet velocity	$V_2$	61.26	m/s
Relative inlet velocity	$W_2$	247.7	m/s
Absolute outlet velocity	$V_3$	452.1	m/s
Relative outlet velocity	$W_3$	43.05	m/s
Power	P	732	kW

### III. Solidworks design

#### 1. Compressor

##### a. Compressor casing

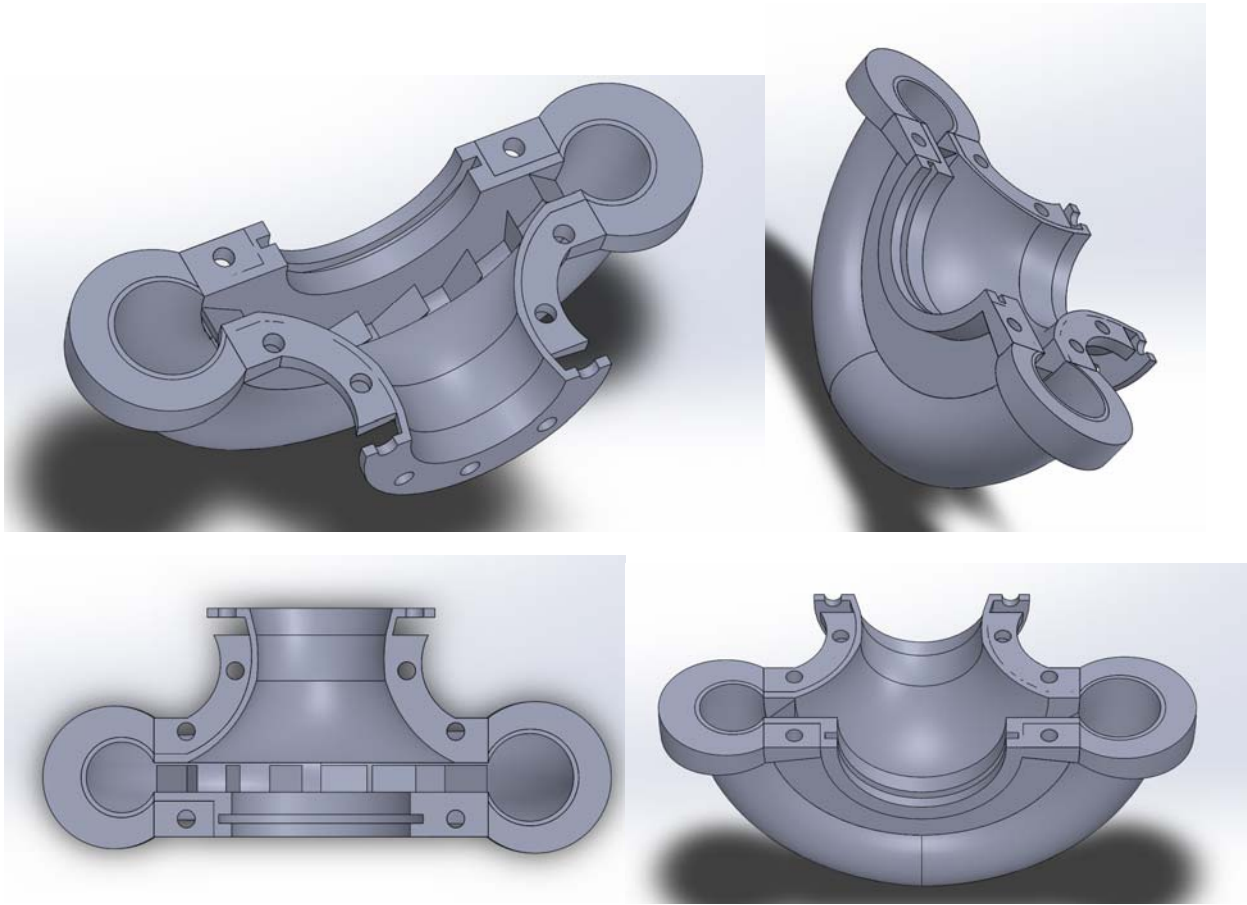


Figure 11: Bottom casing



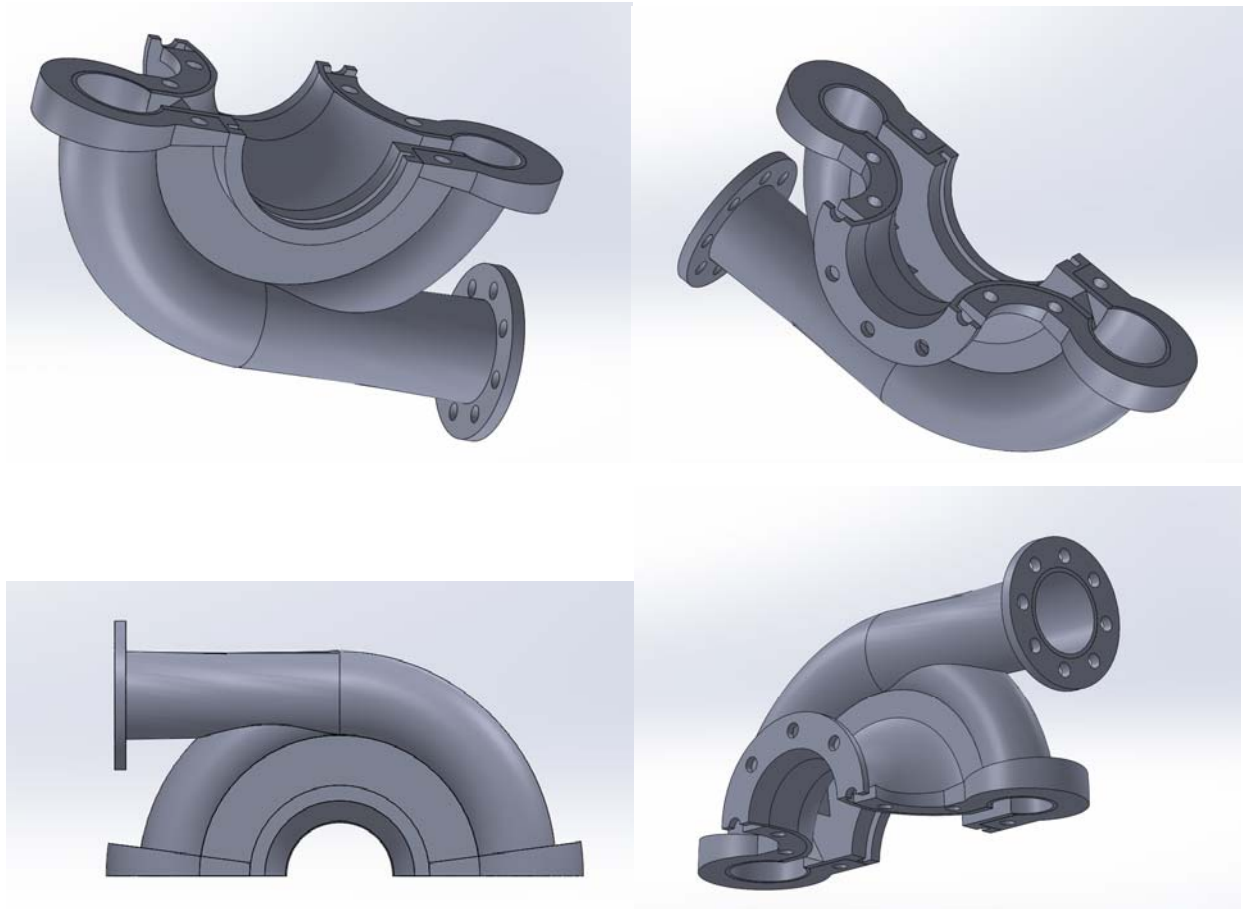


Figure 12: Top casing

b. Impeller design

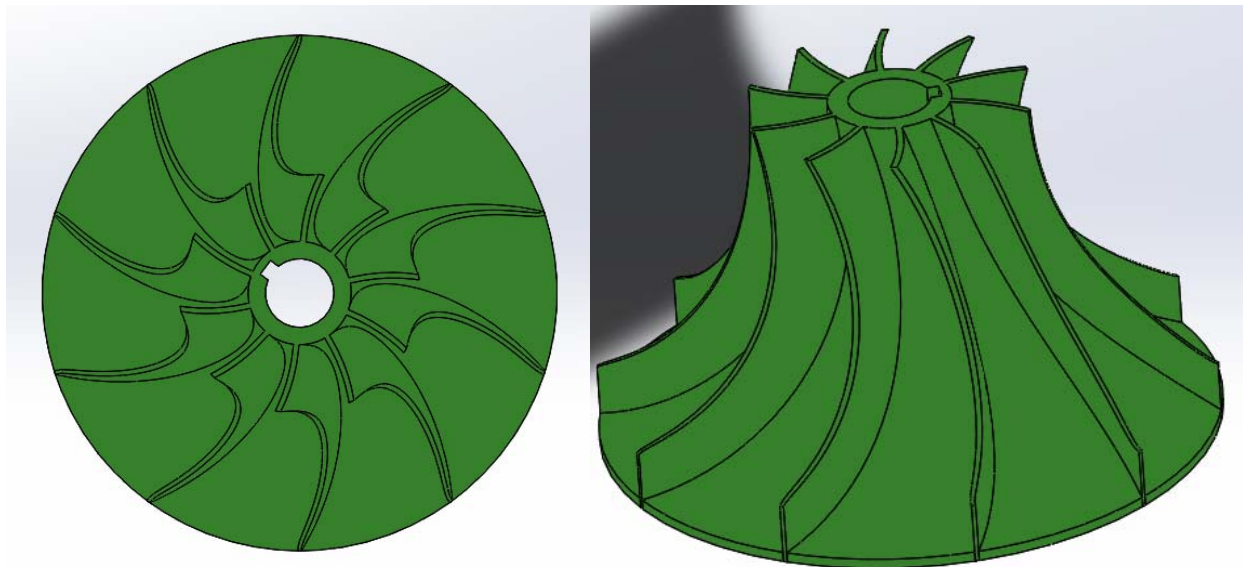


Figure 13: Impeller

c. Bearing housing arrangement

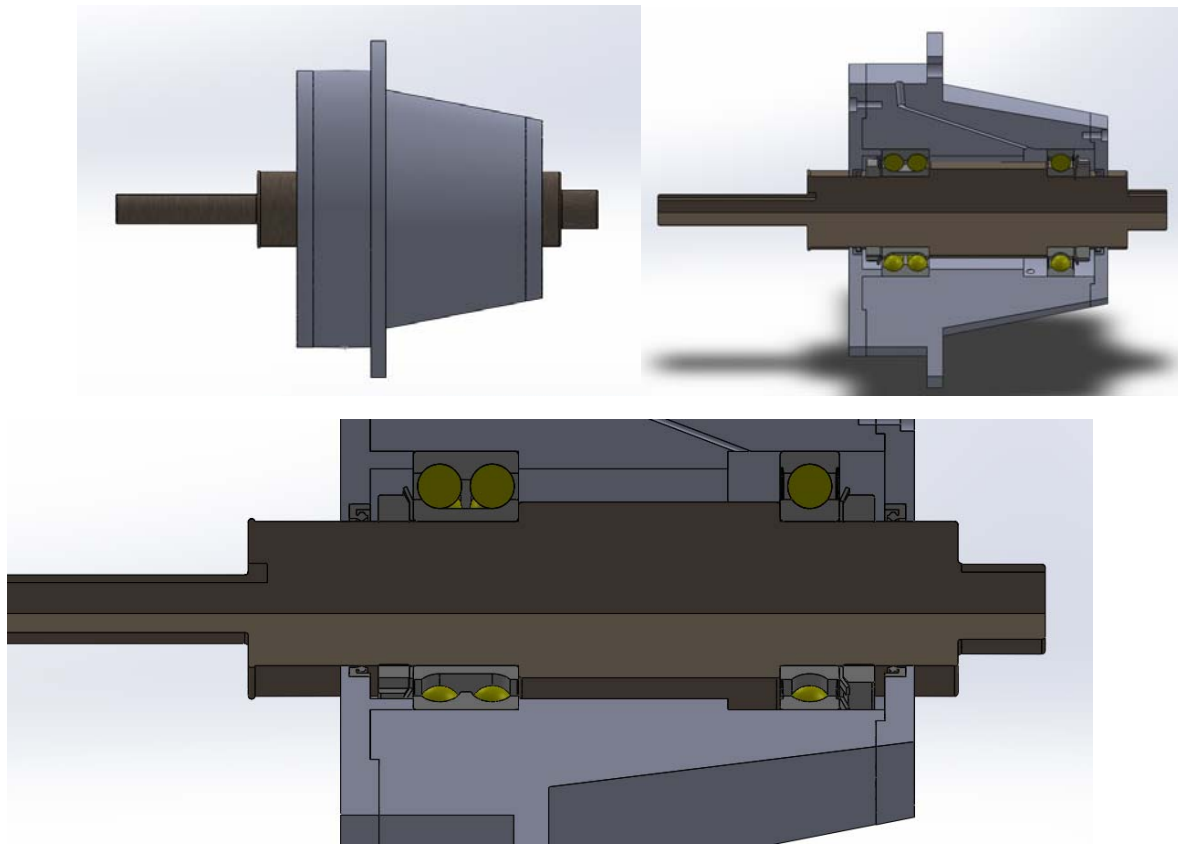
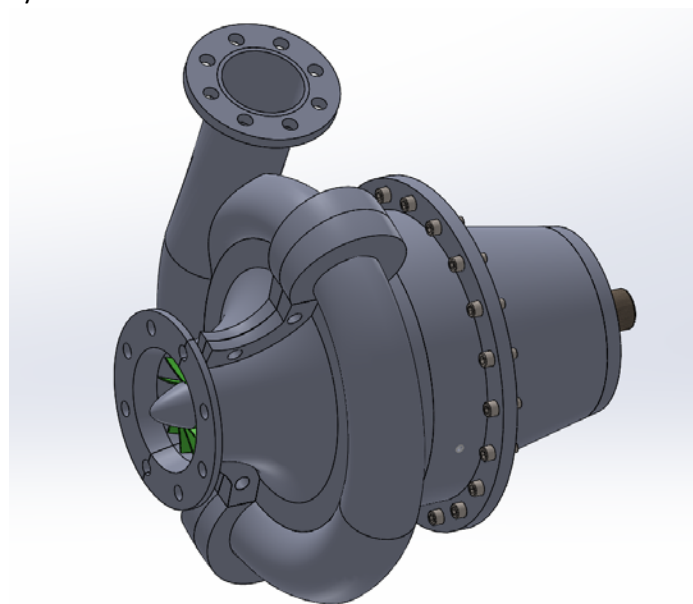
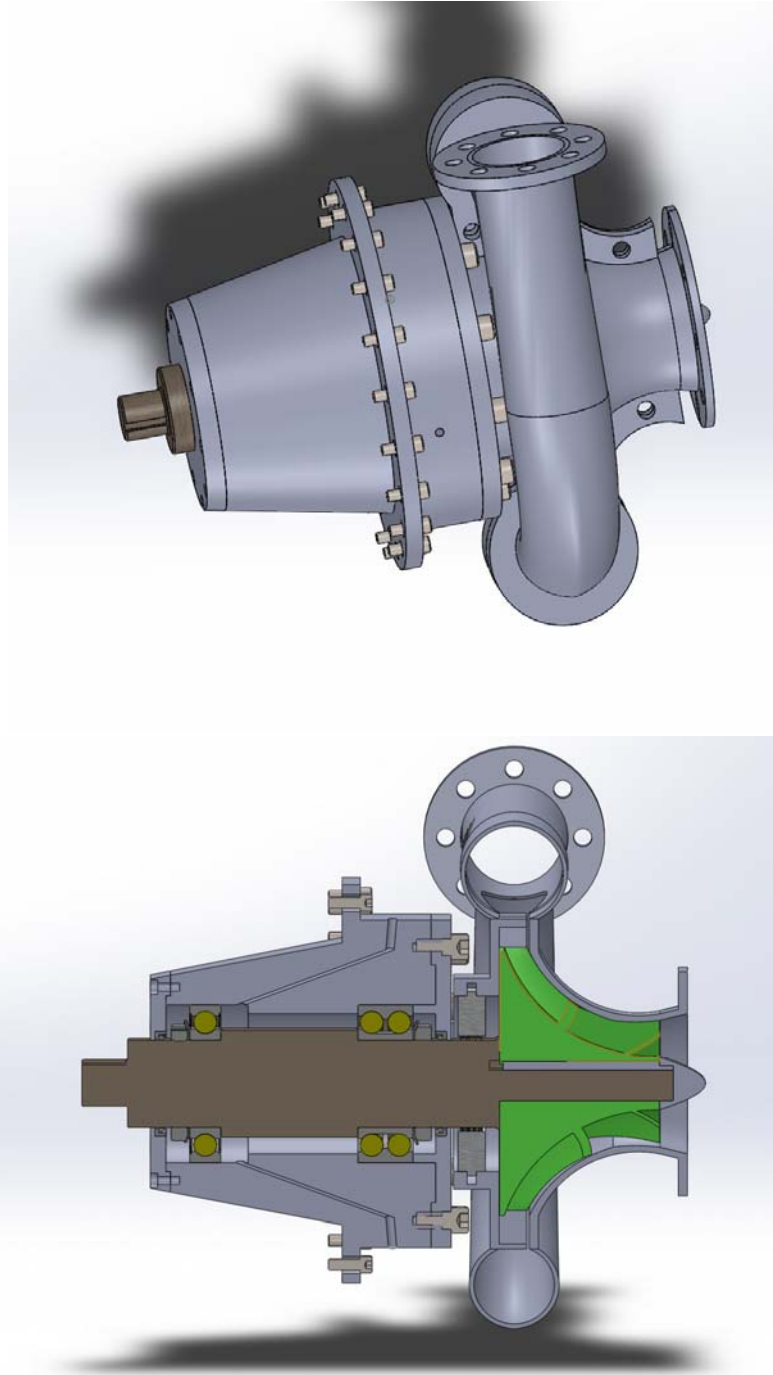


Figure 14: Bearing housing arrangement

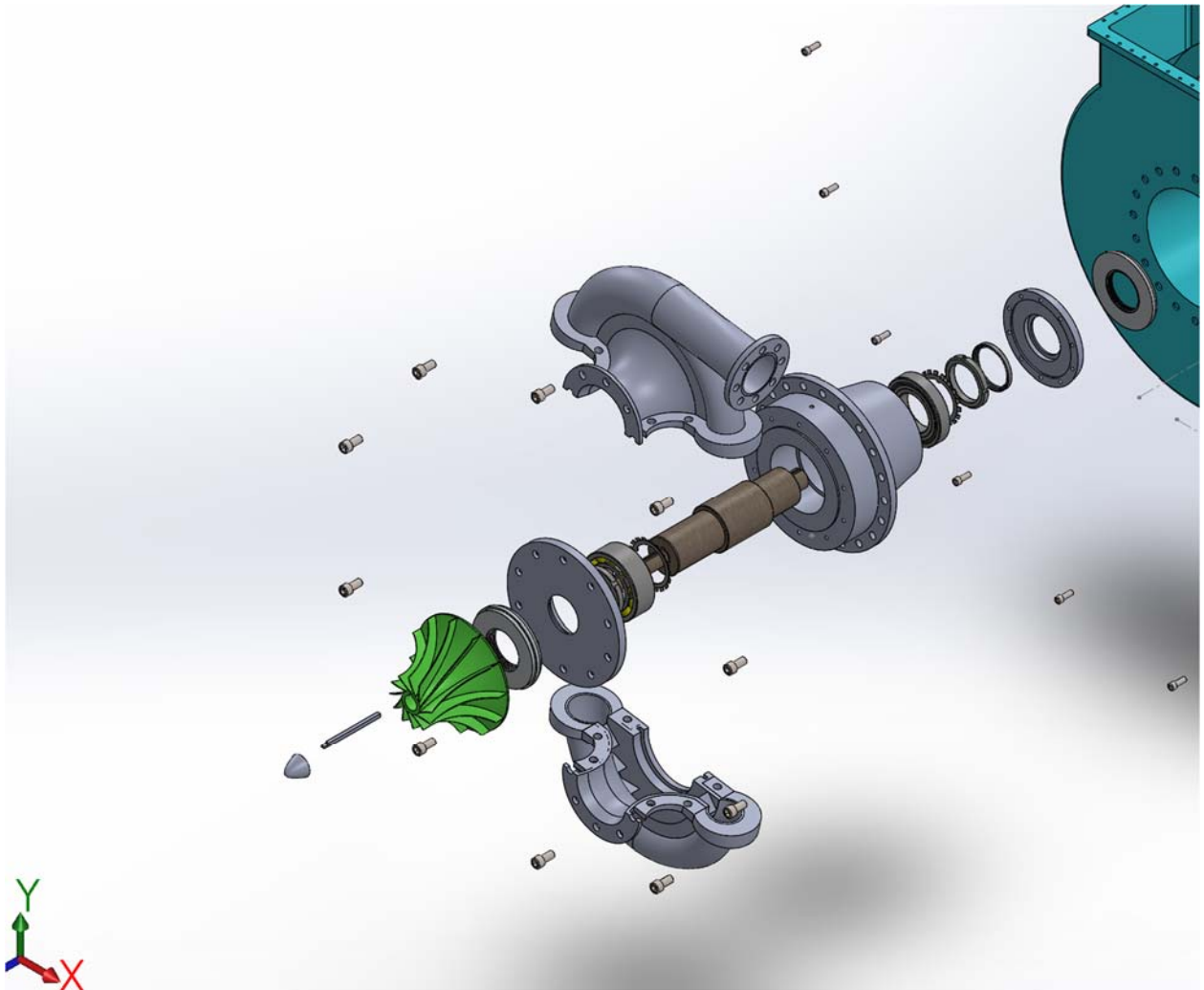
d. Full assembly





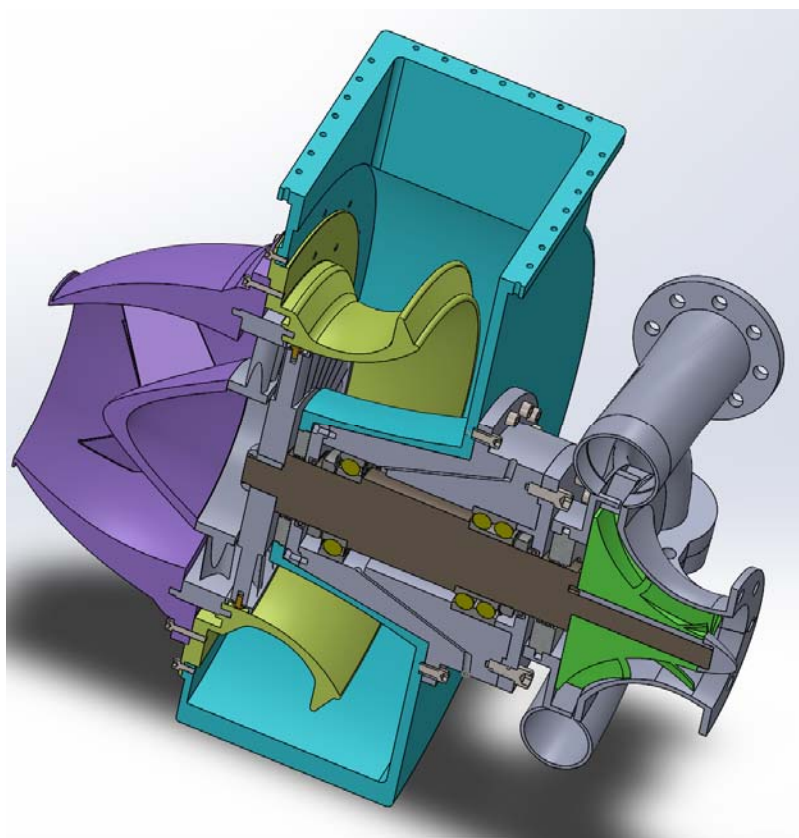
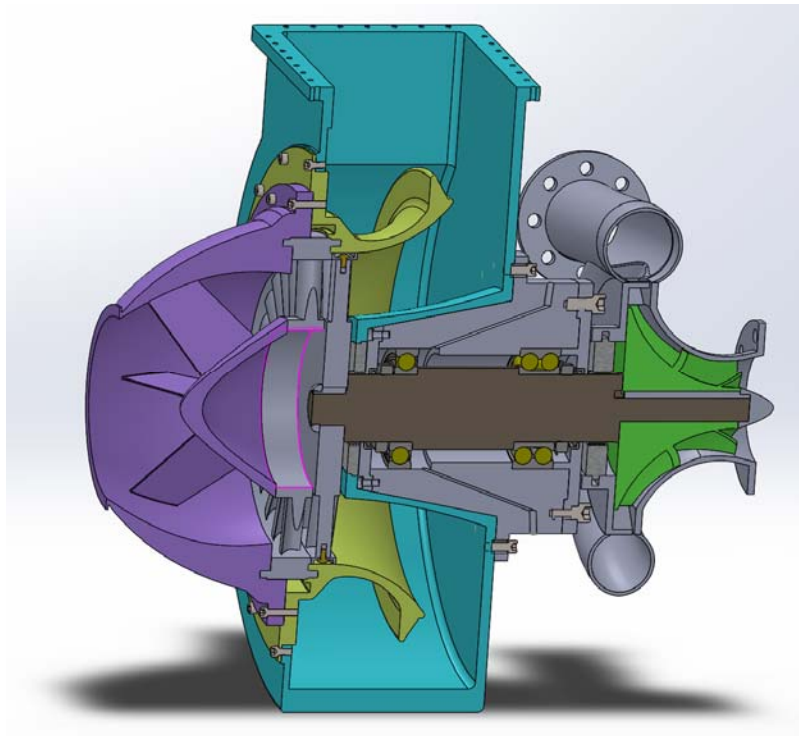
*Figure 15: Compressor full assembly*

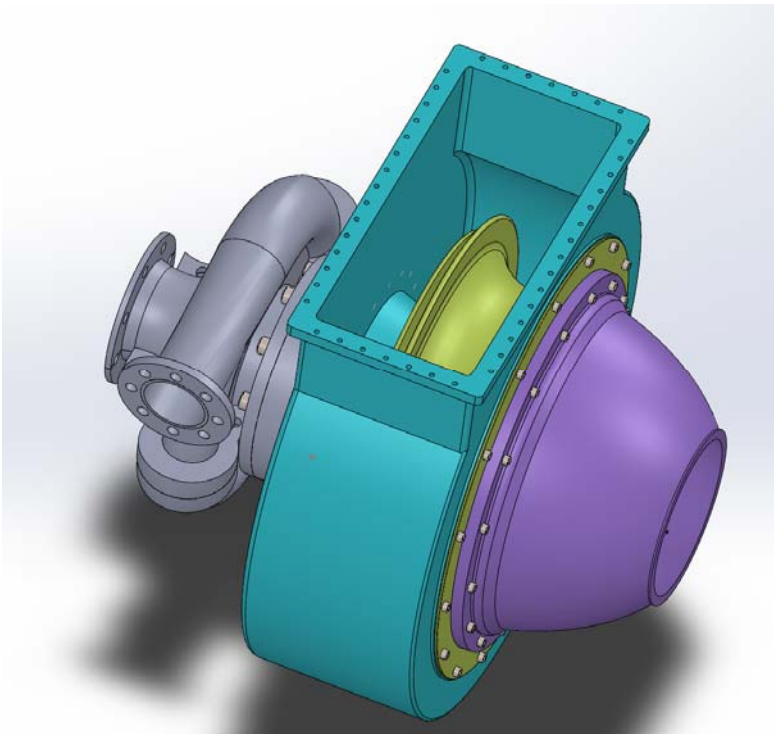
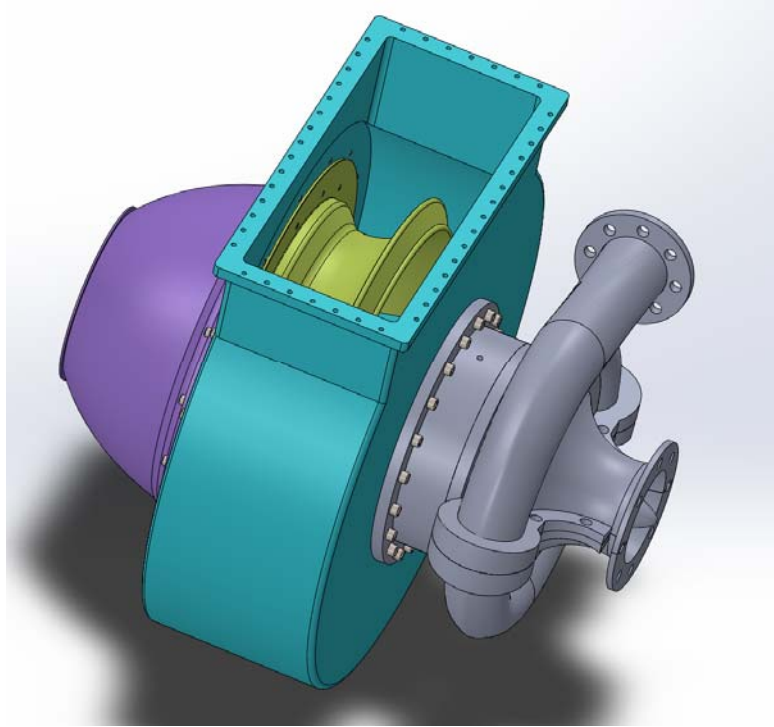
e. Explored view



*Figure 16: Compressor exploded view*

## 2. Complete Turbocharger





*Figure 17: Complete Turbocharger full assembly*



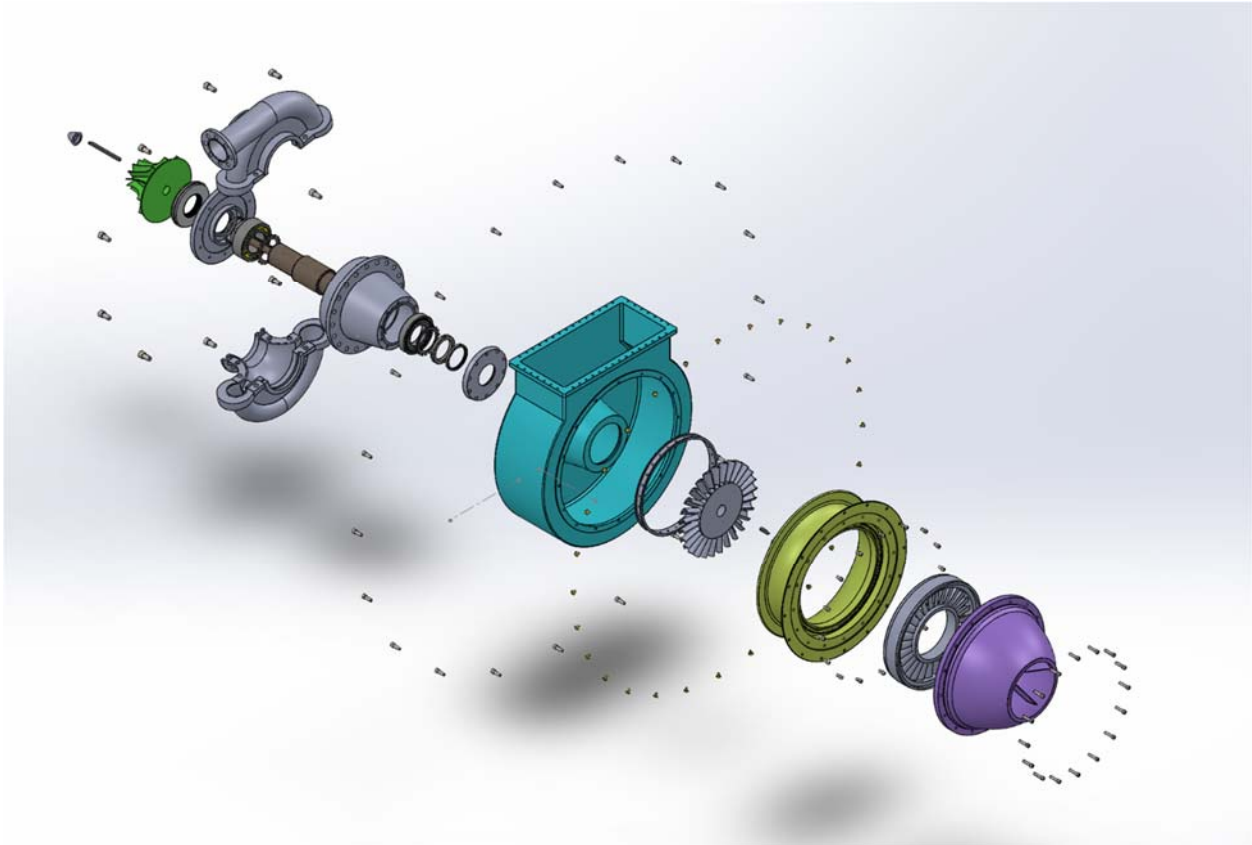


Figure 18: Turbocharger exploded view

## References

[1] Schobeiri, Meinhard T., *Turbomachinery Flow Physics and Dynamic Performance – Chapter 5*, 2<sup>nd</sup> Ed. Springer 2012. Print & Online

%%% MEEN 646 Module 4 %%%

```

clear all
clc
mdot_d=3.5;
T2=300;
p02=10^5;
pi_ref=3.0;
om=3000; %rad/s
eta_d=0.86;
Dm2=0.16;
Rm2=0.08;
D3=0.3;
R3=0.15;
hb2=0.1;
hb3=0.04;
alp2=pi/2;
bet3=pi/2;
mdot=[2.5:0.01:4.5];
R=287;
k=1.3975; %subjected to change
cp=1009; %subjected to change

a0=-0.3844; a1=3.0222; a2=-1.7778;

U2=om*(Dm2/2); U3=om*(D3/2);
IR2=Dm2/2-hb2/2; OR2=Dm2/2+hb2/2;
A2=pi*(OR2^2-IR2^2);
A3=pi*D3*hb3;

for i=1:length(mdot)
    %Efficiency parameters (given)
    eta(i)=a0+a1*(mdot(i)/mdot_d)+a2*(mdot(i)/mdot_d)^2;
    p_ratio(i)=eta(i)*pi_ref;
    %Inlet parameters
    syms a %a=V2
    a=solve(p02==mdot(i)*R*T2/(A2*a)+mdot(i)*a/(2*A2),a);
    b(i,1:2)=double(vpa(a));
    V2(i)=double(vpa(min(a)));
    rho2(i)=mdot(i)/(A2*V2(i));
    P2(i)=rho2(i)*R*T2;
    %Outlet parameters
    P3(i)=P2(i)*p_ratio(i);
    T3s=T2*(p_ratio(i)^((k-1)/k));
    T3(i)=T2+(T3s-T2)/eta(i);
    rho3(i)=P3(i)/(R*T3(i));
    W3(i)=mdot(i)/(rho3(i)*A3);
    %Velocity calculations
    bet2(i)=atan(V2(i)/U2);
    bet2_deg(i)=bet2(i)*180/pi; %in degree
    W2(i)=sqrt(V2(i)^2+U2^2);
    %check(i)=acos(U3/V3(i));
    V3(i)=sqrt(W3(i)^2+U3^2);
    alp3(i)=pi/2+atan(U3/W3(i));
    alp3_deg(i)=alp3(i)*180/pi; %in degree
    %Additional calculations
    phi(i)=W3(i)/U3;
    ome(i)=om;
    %Power(i)=(abs(mdot(i)*cp*(T3(i)-T2)))/10^3;
    Power(i)=mdot(i)*(cp*(T3(i)-T2)+0.5*(V3(i)^2-V2(i)^2)); %unit in W

```



```

    Power1(i)=Power(i)/10^3; %unit in kW
    i=i+1;
end

```

```

figure (1)
plot(mdot',p_ratio','r')
xlabel('Mass flow [kg/s]')
ylabel('Pressure Ratio \pi')
%xlim([2 4.5])
grid on

```

```

figure (2)
plot(mdot',Power1','r')
xlabel('Mass flow [kg/s]')
ylabel('Power [kW]')
%xlim([3 4])
grid on

```

```

figure (3)
plot(mdot',eta','r')
xlabel('Mass flow [kg/s]')
ylabel('\eta')
%xlim([2 4.5])
grid on

```

```

figure (4)
plot(mdot',phi','r')
xlabel('Mass flow [kg/s]')
ylabel('\phi')
%xlim([3 4])
grid on

```

```

figure (5)
plot(mdot',ome','r')
xlabel('Mass flow [kg/s]')
ylabel('Rotation speed \omega')
%xlim([3 4])
grid on

```

```

figure (6)
plot(mdot',bet2_deg','r')
xlabel('Mass flow [kg/s]')
ylabel('\beta_2')
%xlim([3 4])
grid on

```

```

figure (7)
plot(mdot',alp3_deg','r')
xlabel('Mass flow [kg/s]')
ylabel('\alpha_3')
%xlim([3 4])
grid on

```

```

figure (8)
plot(mdot',V2','r*'); hold on
plot(mdot',W2','g'); hold off
xlabel('Mass flow [kg/s]')
ylabel('V_2,W_2(m/s)')
legend('V_2','W_2')
%xlim([3 4])

```

grid on

figure (9)

plot(mdot,V3,'r\*'); hold on

plot(mdot,W3,'g'); hold off

xlabel('Mass flow [kg/s]')

ylabel('V\_3,W\_3(m/s)')

legend('V\_3','W\_3')

%xlim([3 4])

grid on