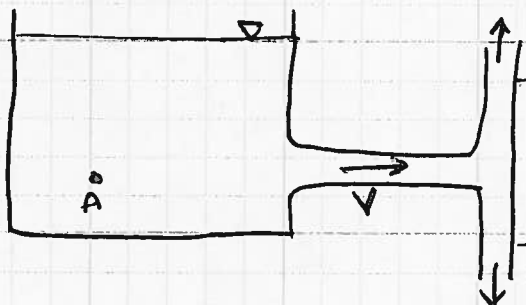


CE 3305 Engineering Fluid Mechanics
Exercise Set 15
Spring 2014

1. Problem 6.13, pg 239
2. Problem 6.64, pg 246
3. Problem 6.82, pg 248

6.13) A horizontal water jet at 70°F issues from a circular orifice in a large tank. The jet strikes a vertical plate that is normal to the axis of the jet. A force of 600 lbf is needed to hold the plate in place against the action of the jet. If the pressure in the tank is 25 psig at point A, what is the diameter of the jet just downstream of the orifice?

Sketch:



Known:

$$\begin{aligned} P_A &= 25 \text{ psig} \\ F_x &= 600 \text{ lbf} \\ T &= 70^\circ\text{F} \\ \rho &= 1.94 \text{ slugs/ft}^3 \\ \gamma &= 62.4 \text{ lbf/ft}^3 \end{aligned}$$

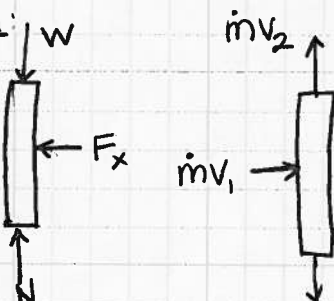
unknown:

$$D_{\text{jet}} = ?$$

Governing Equation

Bernoulli & momentum equation.

Solution:



From the inside of tank to nozzle exit Bernoulli's Eqn.

$$\frac{P_A}{\rho} = \frac{V_1^2}{2}$$

$$V_1 = \sqrt{\frac{2P_A}{\rho}} = \sqrt{\frac{2(25 \text{ lbf/in}^2)(144 \text{ in}^2/\text{ft}^2)}{62.4 \text{ lbf/ft}^3 \left(\frac{\text{slug}}{32.2 \text{ ft/s}^2} \right)}} = 60.9 \text{ ft/s}$$



6.13 continued)

$$\Sigma F_x = -\dot{m}V_{1x}$$

$$F_x = -(\dot{m}V_1) = \rho A V_1^2$$

$$A = \frac{F_x}{\rho V_1^2} = \frac{600 \text{ lbf}}{62.4 \text{ lbf/ft}^3 \times \text{slug/32.2 ft/s}^2 (60.9 \text{ ft/s})^2} = \frac{600 \text{ lbf}}{7187.2 \frac{\text{lbf} \cdot \text{ft}^2}{\text{ft}^4 \cdot \text{s}^2}}$$

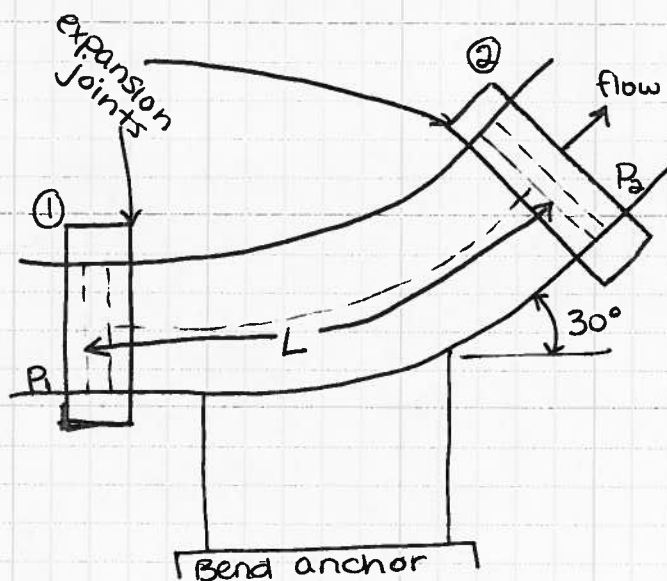
$$A = 0.083 \text{ ft}^2$$

$$d = \sqrt{\frac{4A}{\pi}} = \sqrt{\frac{4(0.083 \text{ ft}^2)}{\pi}} = 0.326 \text{ ft}$$

$$\boxed{A = 0.326 \text{ ft}}$$

6.64) This 30° vertical bend in a pipe with a 2ft diameter carries water ($\rho = 62.4 \text{ lbm/ft}^3$) at a rate of 31.4 cfs. If the pressure P_1 is 10 psi at the lower end of the bend, where the elevation is 100ft, and P_2 is 8.5 psi at the upper end, where the elevation is 103ft, what will be the vertical component of force that must be exerted by the "anchor" on the bend to hold it in position? The bend itself weighs 300lb and the length L is 4ft.

Sketch:



known

$$D = 2 \text{ ft}$$

30° bend

$$\rho = 62.4 \text{ lbm/ft}^3$$

$$Q = 31.4 \text{ cfs}$$

$$P_1 = 10 \text{ psi} \quad z_1 = 100 \text{ ft}$$

$$P_2 = 8.5 \text{ psi} \quad z_2 = 103 \text{ ft}$$

$$W_{\text{bend}} = 300 \text{ lb}$$

$$L = 4 \text{ ft}$$

unknown:

$$F_{\text{anchor}} = ?$$

Governing Equation:

Momentum Equation

Solution:

$$\Sigma F_y = \rho Q (V_{2y} - V_{1y})$$

$$F_a - W_{\text{water}} - W_{\text{bend}} - P_2 A_2 \sin(30^\circ) = \rho Q (V \sin(30^\circ) - V \sin(0^\circ))$$

$$V = \frac{Q}{A} = \frac{31.4 \text{ cfs}}{\pi/4 (2 \text{ ft})^2} = 10.0 \text{ ft/s}$$



b.64 continued

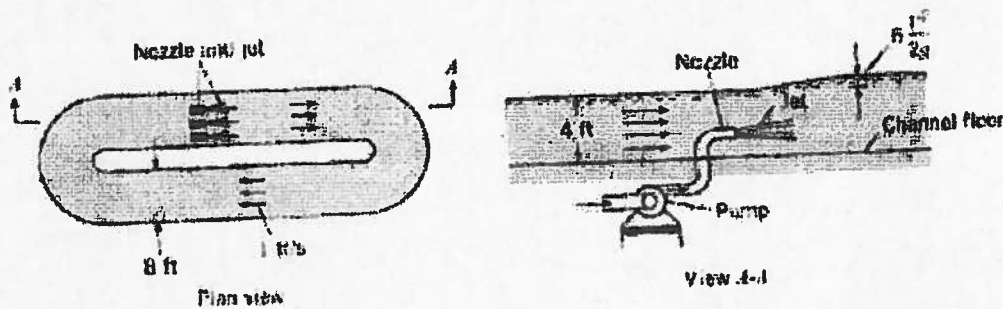
$$F_a = \frac{\pi}{4} (2\text{ft})^2 (4\text{ft}) (62.4 \text{ lbm/ft}^3) + 300 \text{ lb} +$$
$$\left(\frac{144 \text{ in}^2}{\text{ft}^2} \right) \frac{8.5 \text{ lb}}{\text{in}^2} \left(\frac{\pi}{4} (2\text{ft})^2 \right) \sin(30^\circ) + \frac{1.94 \text{ lbf}}{\text{ft}^4 \text{ s}^2} (31.4 \text{ cfs}) (10 \text{ ft/s} (0.5) - 0)$$
$$F_a = 784 \text{ lbf} + 300 \text{ lb} + 1922.1 \text{ lbf} + 304.6 \text{ lbf} = 3310.1 \text{ lbf}$$

$$F_a = 3310 \text{ lbf}$$

Name: _____

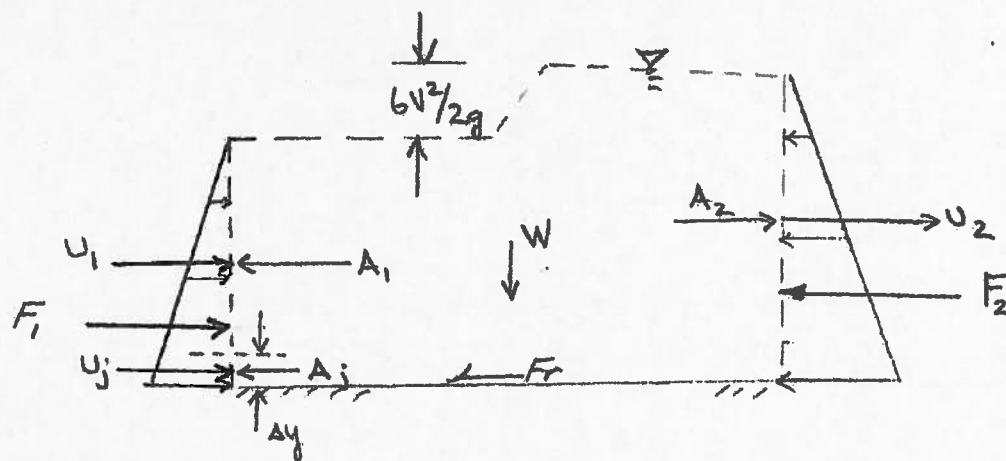
Problem 5 (Design Problem)

Jet pumps are sometimes used for special purposes such as pumping slurries or to circulate flow in basins where contact with mechanical impellers is not feasible, such as a fish-race in a hatchery. The figure below depicts the basic concept for this type of application. For the indicated fish-race, the jets would have to increase the water surface elevation downstream of the jets by an amount equal to $6V^2/2g$, where V is the average velocity in the basin (1 ft/sec in the drawing). *Design* a jet pump system (speed, nozzle diameter, and number of nozzles) to make such a re-circulating system work for a channel 8-feet wide and 4-feet deep. Your *design* should specify nominal diameters (i.e. nozzles made from pipes commonly available 1-in, 2-in, etc.)



Hints: This problem involves "analysis" to determine the required momentum added by the jet(s), and the total jet area and speed. The design should be based on this analysis with the understanding that the total jet area should be small as compared to the total flow area (otherwise the fish will get stuck!).

MIXING-ZONE



NEGLECT FRICTION ($F_f \sim 0$)

F_1 = PRESSURE FORCE APPROACH

F_2 = PRESSURE FORCE EXIT

U_1, A_1 = FREE STREAM SPEED & AREA

U_j, A_j = JET STREAM SPEED & AREA

U_2, A_2 = EXIT STREAM SPEED & AREA

MOMENTUM

$$\sum F_x = \frac{d}{dt} \int_{CV} \rho v_x dV + \int_{CS} \rho v_x (v \cdot dA)$$

$$F_1 - F_2 = -\rho U_j^2 U_j A_j - \rho U_1^2 U_1 A_1 + \rho U_2^2 U_2 A_2$$

$$A_1 = 8(y_1 - \Delta y)$$

$$A_2 = 8y_2$$

$$A_j = 8\Delta y$$

$$F_1 = \rho g \frac{y_1^2}{2} y_1 \cdot 8$$

$$F_2 = \rho g \frac{y_2^2}{2} y_2 \cdot 8$$

$$\therefore \cancel{\rho g} \left(\frac{y_1^2}{2} - \frac{y_2^2}{2} \right) = -\cancel{\rho U_j^2} 8\Delta y - \cancel{\rho U_1^2} 8(y_1 - \Delta y) + \cancel{\rho U_2^2} 8y_2$$

$$g \left(\frac{y_1^2 - y_2^2}{2} \right) = -U_j^2 \Delta y - U_1^2 (y_1 - \Delta y) + U_2^2 y_2$$

Note: y_2 is known!

$$0 = \frac{d}{dt} \int_{CV} \rho V d\tau + \sum_{CS} \rho(V \cdot \Delta A)$$

$$0 = U_2 A_2 - U_1 A_1 - U_j A_j$$

$$0 = U_2 y_2^2 - U_1 y_1^2 - U_j \Delta y$$

$$= U_2 y_2^2 - U_1 (y_1 - \Delta y)^2 - U_j \Delta y$$

$$\therefore U_2 y_2^2 = U_1 (y_1 - \Delta y)^2 - U_j \Delta y$$

$$U_2 = \frac{U_1 (y_1 - \Delta y)^2 - U_j \Delta y}{y_2^2}$$

Now ARRANGE ^{y₂} MOMENTUM IN TERMS U_j

$$U_j^2 \Delta y = -U_1^2 (y_1 - \Delta y) + U_2^2 y_2^2 - \frac{g}{2} (y_1^2 - y_2^2)$$

SUBSTITUTE U₂ FROM CONTINUITY

$$U_j^2 \Delta y = -U_1^2 (y_1 - \Delta y) + \left[\frac{U_1 (y_1 - \Delta y)^2 - U_j \Delta y}{y_2^2} \right]^2 y_2^2 - \frac{g}{2} [y_1^2 - y_2^2]$$

1. IMPLICIT EQUATION IN U_j Δy

SOLVE BY

① TRIAL & ERROR OR

② NEWTON'S METHOD

VERIFY WHAT'S KNOWN

$$U_1 = 1 \text{ ft/s (GIVEN)}$$

$$y_1 = 4 \text{ ft (GIVEN)}$$

$$y_2 = 4 \text{ ft} + \frac{6(1 \text{ ft/s})^2}{2(32.2 \text{ ft/s}^2)} = 4.0932 \text{ ft}$$

$$U_j = \text{UNKNOWN}$$

$$\Delta y = \text{UNKNOWN}$$

$$g = 32.2 \text{ ft/s}^2$$

$$U_2 = f(U_j, \Delta y)$$

RECALL Δy ≪ JET AREA.

JETS ARE SMALL! (IN SIZE)

$$U_j^2 \Delta y = \frac{-U_1^2 (y_1 - \Delta y)}{\Delta y} + \frac{U_1^2 (y_1 - \Delta y)^2}{y_2 \Delta y} - \frac{2 U_1 (y_1 - \Delta y) U_j \Delta y}{y_2 \Delta y} + \frac{U_j^2 \Delta y^2}{y_2 \Delta y} - \frac{g}{2} [y_1^2 - y_2^2] \frac{1}{\Delta y}$$

$$U_j^2 - \frac{U_j^2 \Delta y}{y_2} + \frac{2 U_1 (y_1 - \Delta y) U_j}{y_2} = \frac{-U_1^2 (y_1 - \Delta y)}{\Delta y} + \frac{U_1^2 (y_1 - \Delta y)^2}{y_2 \Delta y} - \frac{g}{2 \Delta y} [y_1^2 - y_2^2]$$

Now if we "pick" Δy ONLY UNKNOWN IS U_j \therefore SOLVABLE

SEE ATTACHED WORKSHEET

FOR Δy 'S FROM 0.1 TO 0.3

Δy	U_j	A_j
0.1	10.1 ft/s	0.8 ft ²
0.2	7.0 ft/s	1.6 ft ²
0.3	5.6 ft/s	2.4 ft ²

Now DETERMINE JET AREAS
IN 8 FOOT CHANNEL

$$A_j = \Delta y \cdot 8 \text{ ft}$$

FOR EACH A_j , DETERMINE NOZZLE SPECS

SEE SECOND WORKSHEET

# CIVE 3434 Exam#1, Problem #5 Jet Design			
# INPUT			
u1	1	Approach Speed	
y1	4	Approach Depth	
y2	4.0932	Exit Depth	
g	32.2	Gravitational Constant	
# DESIGN VARIABLE(S)			
delta_y	0.1	Jet Depth (Area)	
uj	10.13858	Jet Speed	
# COMPUTED VALUES			
y1-delta_y	3.9		
y1^2-y2^2	-0.75429		
y2*delta_y	0.40932		
u1^2	1		
uj^2	102.7905		
# COMPUTED VALUES			
Term 1	102.7905	Term 1	-39
Term 2	-2.51125	Term 2	37.15919
Term 3	19.32004	Term 3	121.4401
LHS	119.5993	RHS	119.5993
DIFF	9.65E-08		
# INPUT			
u1	1	Approach Speed	
y1	4	Approach Depth	
y2	4.0932	Exit Depth	
g	32.2	Gravitational Constant	
# DESIGN VARIABLE(S)			
delta_y	0.2	Jet Depth (Area)	
uj	6.988909	Jet Speed	
# COMPUTED VALUES			
y1-delta_y	3.8		
y1^2-y2^2	-0.75429		
y2*delta_y	0.81864		
u1^2	1		
uj^2	48.77498		
# COMPUTED VALUES			
Term 1	48.77498	Term 1	-19
Term 2	-2.38322	Term 2	17.63901
Term 3	12.98729	Term 3	80.72004
LHS	59.35905	RHS	59.35905
DIFF	-2.6E-07		
# INPUT			
u1	1	Approach Speed	
y1	4	Approach Depth	
y2	4.0932	Exit Depth	
g	32.2	Gravitational Constant	
# DESIGN VARIABLE(S)			
delta_y	0.3	Jet Depth (Area)	
uj	5.80887	Jet Speed	
# COMPUTED VALUES			
y1-delta_y	3.7		
y1^2-y2^2	-0.75429		
y2*delta_y	1.22796		
u1^2	1		
uj^2	31.46074		
# COMPUTED VALUES			
Term 1	31.46074	Term 1	-12.3333
Term 2	-2.30583	Term 2	11.14857
Term 3	10.14036	Term 3	48.48003
LHS	39.29527	RHS	39.29527
DIFF	-4.3E-07		

① SELECT THIS VALUE -

BY CHANGING THIS CELL

USE SOLVER TO MAKE THIS CELL = 0.0 ②

# CIVE 3434 Exam#					
# INPUT					
u1	1	Approach Speed			
y1	4	Approach Depth			
y2	4.0932	Exit Depth			
g	32.2	Gravitational Constant			
# DESIGN VARIABLES					
delta_y	0.1	Jet Depth (Area)			
uj	10.1385841236786	Jet Speed			
# COMPUTED VALUES					
y1-delta_y	=B4-B8				
y1^2-y2^2	=B4^2-B5^2				
y2-delta_y	=B8-B5				
u1^2	=B9^2				
uj^2	=B9^2				
# COMPUTED VALUES					
	Term_1	=B15		Term_1	=B14*B11/B8
	Term_2	=B15*B8/B5		Term_2	=B14*B11*B11/B13
	Term_3	=(2*B3*B11*B8)/B5		Term_3	=0.5*(B8*B12)/B8
	LHS	=C19+C20+C21		RHS	=F19+F20+F21
	DIFF	=C23-F23			
# INPUT					
u1	1	Approach Speed			
y1	4	Approach Depth			
y2	4.0932	Exit Depth			
g	32.2	Gravitational Constant			
# DESIGN VARIABLES					
delta_y	0.2	Jet Depth (Area)			
uj	6.98390894304089	Jet Speed			
# COMPUTED VALUES					
y1-delta_y	=B29-B33				
y1^2-y2^2	=B29^2-B30^2				
y2-delta_y	=B33-B30				
u1^2	=B28^2				
uj^2	=B34^2				
# COMPUTED VALUES					
	Term_1	=B40		Term_1	=B39*B36/B33
	Term_2	=B40*B33/B30		Term_2	=B39*B36*B38/B38
	Term_3	=(2*B28*B36*B34)/B30		Term_3	=0.5*(B31*B37)/B33
	LHS	=C44+C45+C46		RHS	=F44+F45+F46
	DIFF	=C48-F48			
# INPUT					
u1	1	Approach Speed			
y1	4	Approach Depth			
y2	4.0932	Exit Depth			
g	32.2	Gravitational Constant			
# DESIGN VARIABLES					
delta_y	0.8	Jet Depth (Area)			
uj	5.60898737282877	Jet Speed			
# COMPUTED VALUES					
y1-delta_y	=B54-B58				
y1^2-y2^2	=B54^2-B58^2				
y2-delta_y	=B58-B55				
u1^2	=B53^2				
uj^2	=B59^2				
# COMPUTED VALUES					
	Term_1	=B65		Term_1	=B64*B61/B58
	Term_2	=B65*B58/B55		Term_2	=B64*B61*B61/B63
	Term_3	=(2*B58*B61*B59)/B55		Term_3	=0.5*(B68*B62)/B58
	LHS	=C69+C70+C71		RHS	=F69+F70+F71
	DIFF	=C73-F73			

Nozzle_Design					
10 ft/sec design					
Diameter(in)	Area(ft^2)	Number	Specify	Total	Actual_Jet_Area
1	0.005454	146.7	147	0.80	
2	0.021817	36.7	37	0.81	
3	0.049087	16.3	17	0.83	
4	0.087266	9.2	10	0.87	
6	0.19635	4.1	5	0.98	
8	0.349066	2.3	3	1.05	
7 ft/sec design					
Diameter(in)	Area(ft^2)	Number		Total	Actual_Jet_Area
1	0.005454	293.4	293	1.60	
2	0.021817	73.3	73	1.59	
3	0.049087	32.6	34	1.67	
4	0.087266	18.3	19	1.66	
6	0.19635	8.1	9	1.77	
8	0.349066	4.6	5	1.75	
5.6 ft/sec design					
Diameter(in)	Area(ft^2)	Number		Total	Actual_Jet_Area
1	0.005454	440.0	441	2.41	
2	0.021817	110.0	111	2.42	
3	0.049087	48.9	49	2.41	
4	0.087266	27.5	28	2.44	
6	0.19635	12.2	13	2.55	
8	0.349066	6.9	7	2.44	
All these specifications will work but:					
Small diameters require a lot of nozzles, and these would be hard to maintain -- thus discard 1,2,3 in.					
8-in. would require a lot of head to generate required jet speeds					
Either 30 4-in nozzles or 15 6-in. would be good design. Using manifolds and valving					
one could select nozzle "banks" to produce desired fish race at variable flow speeds.					