2000

22-141 22-142 22-144

AMPAD.

"KINETIC ENERGY - ENERGY OF MOTION

ENERGY - ENERGY OF POSITION

ENERGY - ENERGY OF "COMPRESSION

ENERGY - THERMAL OSMOTIC THERMAL POTENTIAL

O CHEMICAL ENERGY - CHEMICAL-OSMOTICL PUTENMAL

· ELECTRICAL ENERGY - ELECTRO-OSMOTIC POTENTIAL

COUPLED-PROCESS THEORY

ENGINEERING PRIMARILY IN HYORAULIC CONCERNED WITH FIRST THREE ENERGY TYPES

	GRADIENT			
ASIDE: FLOW	HYDRAULIC	ELECTRIC POTENTIAL	TEMP.	CONCENTRATION
FLUID	DARLY; DARLY- WEISBACH	ELECTRO- OSMOSIS; CASAGRANOE	THERMAL OSMOSIS	CHEMICAL OSMOSIS
ELECTRICITY	Rovss	OHM	SEEBECK; THOMPSON	SEDIMENTATION LURREM
HEAT	THERMAL FILTRATION	PELNER	FOURIER	DUFOR
SOLUTES	ULTRA- FILTRATION	ELECTRO- PHORESIS	SORET	FICK

22-141 50 SHEETS 22-142 100 SHEETS 22-144 200 SHEETS

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ENERGY FLUX $IN = \int ep(V \cdot n) dA$ $e = \frac{dE}{dm}$ (ENERGY)

ENERGY FLUX OUT = $\int ep(V.n)dA$ $e = \hat{0} + \frac{1}{2}V^2 + g^2$

INTERNAL POTENTIAL ENTHALPY

"EQUATION OF STATE" - $\hat{U} = \hat{h} - \frac{P_{p}}{p}$

ENERGY IN C.V. = Sepd+

ENERGY CONSERVATION:

 $\frac{dQ}{dt} - \frac{dW}{dt} = \frac{2}{\partial t} \int e\rho dV + \int e\rho(V \cdot n) dA$ $\int cv. \quad c.s.$

HEAT
ADDED TO WORK DONE
SYSTEM BY SYSTEM

dw = dwsHAFT + dwpress + dwysious stress

WSHAFF: TURBINEIS) (+ WORK)
PUMP(S) (- WORK)

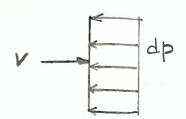
WPRESS : WORK DONE TO PUSH WATER AGAINST
PRESSURE

Wriscous & SHEAR WORK (USUALLY NEGLIGIBLE)

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WARESS !



COMBINE

$$\hat{Q} - \hat{w}_{s} - \hat{w}_{v} = \frac{d}{dt} \left(\hat{u}_{t} + \frac{1}{2} v^{2} + g_{z} \right) p dV$$

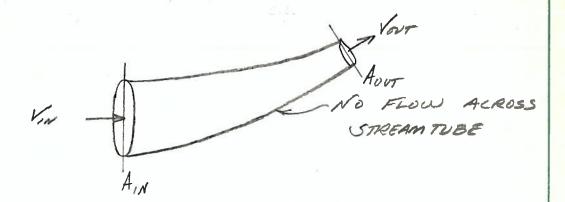
$$+ \int \left(\hat{h}_{t} + \frac{1}{2} v^{2} + g_{z} \right) \varphi(v \cdot n) dA$$

FOR STEADY FLOW THE VOLUME INTEGRAL VANISHES Q-Ws-Wr = S(h+ = V2+g=)p(V.n)dA

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ENERGY EQUATION: (STEADY FLOW) ALONG A STREAM TUBE



DIVIDE BY MASS FLUX: PQ - DISCHARGE

9 = & j s = ws ...

 $\hat{g} - i \hat{v}_s - i \hat{v}_v = h_{out}^2 + \frac{1}{2} v_{out}^2 + g \neq_{out}^2$ $\left(\hat{h}_{iN} + \frac{1}{2} v_{iN}^2 + g \neq_{in} \right)$

BREAK ENTHALPY & REARRANGE:

Unt p+ = Vin + g=in = Vour + Pour + I Vour + g Zour + ins + in - g

LET INCET HAVE SUBSCRIPT I, OUTLET HAVE SUBSCRIPT 2

 $\frac{p_1}{p} + \frac{1}{2}V_1^2 + g^2 = \frac{p_2}{p} + \frac{1}{2}V_2^2 + g^2 + \dot{w}_s + \dot{w}_v - \dot{g} + (\ddot{v}_2 - \ddot{v}_1)$

DIVIDE EX 9

VISCOUS SHEAR

 $\frac{p_1}{p_9} + \frac{V_1}{2g} + \frac{1}{2} = \frac{p_2}{p_9} + \frac{V_2^2}{2g} + \frac{1}{2} + h_5 + h_4 + (\tilde{U}_2 - \tilde{U}_1 - g)}{2}$

FRICTIONLESS EQUATION

PUMANG FLOW BERNOVILLI'S TERM

HEAT TRANSFER COMPONENT (FRICHON)

SUMMARY FOR STEADY PIPE FLOW

(1) CONTINUNITY: 4, V, = A2 V2 = Q

@ MOMENTUM: ZF=9Q(V,-V,)

3 ENERGY: \frac{p_1}{8} + \frac{V_1^2}{2g} + \frac{2}{2}, = \frac{p_2}{8} + \frac{V_2^2}{2g} + \frac{2}{2} + h_3 + h_4
\] FRICTION: HEAT TRANSFER

MOST PROBLEMS WE WILL SIMPLIFY ENERGY EQUATION BY ASSUMING 150-THERMAL PROLESSES

A, V, = A2 V2 = P

ZF=4Q(V2-V,)

E' + \frac{V_1^2}{2g} + \frac{2}{5}, \frac{1}{5}h_p = \frac{P^2}{5} + \frac{V_2^2}{2g} + \frac{7}{22} + h_T + h_F HEAD REMOVED BY FRICTION HEAD REMOVED

HEAD ADDED BY

BY TURBINE

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